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## High Performance Off-Line Controller ActiveSwitcher ${ }^{\text {TM }}$ IC Family

## FEATURES

- Lowest Total Cost Solution
- 0.15W Standby Power
- Emitter Drive Allows Safe NPN Transistor Flyback Use
- Hiccup Mode Short Circuit
- Current Mode Operation
- Over-Current Protection
- Under-voltage Protection with Auto-Restart
- Proprietary Scalable Output Driver
- Flexible Packaging Options (Including TO-92)
- 65kHz or 100kHz Switching Frequency
- Selectable 0.4A to 1.2A Current Limit


## APPLICATIONS

- Battery Chargers
- Power Adaptors
- Standby Power Supplies
- Appliances
- Universal Off-Line Power Supplies

Figure 1:
Simplified Application Circuit


ORDERING INFORMATION

| PART NUMBER | SWITCHING <br> FREQUENCY | CURRENT <br> LIMIT | JUNCTION <br> TEMPERATURE | PACKAGE | PINS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ACT30AHT | 65 kHz | 400 mA | $-40^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ | TO-92 | 3 |
| ACT30BHT | 65 kHz | 800 mA | $-40^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ | TO-92 | 3 |
| ACT30AYT | 65 kHz | 400 mA | $-40^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ | SOT23-B | 3 |

## PIN CONFIGURATION



## PIN DESCRIPTIONS

| PIN |  | DAME | DESCRIPTION |
| :---: | :---: | :---: | :--- |
| TO-92 | SOT23-B |  |  |
| 1 | 1 | VDD | Power Supply Pin. Connect to optocoupler's emitter. Internally limited to 5.5V max. <br> Bypass to GND with a proper compensation network. |
| 2 | 3 | GND | Ground. |
| 3 | 2 | DRV | Driver Output (TO-92 Only). Connect to emitter of the high voltage NPN or <br> MOSFET. For ACT30A/C, DRV pin is internally connected to DRV1. For ACT30B/D. <br> DRV pin is internally connected to both DRV1 and DRV2. |

## ABSOLUTE MAXIMUM RATINGS ${ }^{\circledR}$

| PARAMETER | VALUE | UNIT |
| :--- | :---: | :---: |
| VDD, FREQ to GND | -0.3 to 6 | V |
| VDD Current | 20 | mA |
| DRV, DRV1, DRV2 to GND | -0.3 to 18 | V |
| Continuous DRV, DRV1, DRV2 Current | Internally limited | A |
| Maximum Power Dissipation | TO-92 | 0.6 |
|  | W |  |
|  |  | 0.39 |
| Operating Junction Temperature | -40 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature | -55 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec) | 300 | ${ }^{\circ} \mathrm{C}$ |

(1): Do not exceed these limits to prevent damage to the device. Exposure to absolute maximum rating conditions for long periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

( $\mathrm{V}_{\text {VDD }}=4 \mathrm{~V}, \mathrm{~T}_{J}=25^{\circ} \mathrm{C}$, unless otherwise specified.)

| PARAMETER | SYMBOL | TEST CONDITIONS |  | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {VDD }}$ Start Voltage | $\mathrm{V}_{\text {Start }}$ | Rising edge |  | 4.75 | 5 | 5.25 | V |
| DRV1 Start Voltage | $\mathrm{V}_{\text {DRVSt }}$ | DRV1 must be higher than this voltage to start up. | ACT30A |  | 8.6 | 10.5 | V |
|  |  |  | ACT30B |  | 9.6 | 11.5 |  |
| DRV1 Short-Circuit Detect Threshold | $\mathrm{V}_{\text {SCDRV }}$ |  |  | 6.35 | 6.8 | 7.25 | V |
| $\mathrm{V}_{\text {VDD }}$ Under-Voltage Threshold | $\mathrm{V}_{\text {UV }}$ | Falling edge |  | 3.17 | 3.35 | 3.63 | V |
| $\mathrm{V}_{\text {VDD }}$ Clamp Voltage |  | 10 mA |  | 5.15 | 5.45 | 5.95 | V |
| Startup Supply Current | $\mathrm{I}_{\text {DDST }}$ | $\mathrm{V}_{\mathrm{VDD}}=4 \mathrm{~V}$ before $\mathrm{V}_{\mathrm{UV}}$ |  |  | 0.23 | 0.45 | mA |
| Supply Current | $\mathrm{I}_{\mathrm{DD}}$ |  |  |  | 0.7 | 1 | mA |
| Switching Frequency | $\mathrm{f}_{\text {sw }}$ | ACT30A/B or FREQ $=0$ |  | 50 | 65 | 80 | kHz |
| Maximum Duty Cycle | $\mathrm{D}_{\text {MAX }}$ | ACT30A, $\mathrm{V}_{\text {VDD }}=4 \mathrm{~V}$ |  | 67 | 75 | 83 | \% |
|  |  | ACT30B, $\mathrm{V}_{\text {VDD }}=4 \mathrm{~V}$ |  | 60 |  |  |  |
| Minimum Duty Cycle | $\mathrm{D}_{\text {MIN }}$ | $\mathrm{V}_{\mathrm{VDD}}=4.6 \mathrm{~V}$ |  | 3.5 |  |  | \% |
| Effective Current Limit | $\mathrm{I}_{\text {LIM }}$ | $\mathrm{V}_{\mathrm{VDD}}=\mathrm{V}_{\mathrm{UV}}+0.1 \mathrm{~V}$ | ACT30A | 340 | 400 | 480 | mA |
|  |  |  | ACT30B with DRV1 = DRV2 | 680 | 800 | 920 |  |
| $\mathrm{V}_{\text {VDD }}$ to DRV1 Current Coefficient | $\mathrm{G}_{\text {GAIN }}$ |  |  |  | -0.29 |  | A/V |
| VDD Dynamic Impedance | RVDD |  |  |  | 9 |  | k $\Omega$ |
| DRV1 or DRV2 Driver OnResistance | R ${ }_{\text {DRV1, }}$ $\mathrm{R}_{\mathrm{DRV} 2}$ | $\mathrm{I}_{\mathrm{DRV} 1}=\mathrm{I}_{\mathrm{DRV} 2}=0.05 \mathrm{~A}$ |  |  | 3.6 |  | $\Omega$ |
| DRV1 Rise Time |  | 1 nF load, $15 \Omega$ pull-up |  |  | 30 |  | ns |
| DRV1 Fall Time |  | 1 nF load, $15 \Omega$ pull-up |  |  | 20 |  | ns |
| DRV1 and DRV2 Switch Off Current |  | Driver off, $\mathrm{V}_{\mathrm{DRV} 1}=\mathrm{V}_{\mathrm{DRV} 2}=10 \mathrm{~V}$ |  |  | 12 | 30 | $\mu \mathrm{A}$ |

## FUNCTIONAL BLOCK DIAGRAM


(1): FREQ terminal wire-bonded to VDD in ACT30C/D (TO-92)
(2): DRV2 terminal wire-bonded to DRV1 in ACT30B/D (TO-92)

## FUNCTIONAL DESCRIPTION

As seen in the Functional Block Diagram, the main components include switching control logic, two onchip medium-voltage power-MOSFETs with parallel current sensor, driver, oscillator and ramp generator, current limit VC generator, error comparator, hiccup control, bias and under voltagelockout, and regulator circuitry.

As seen in the Functional Block Diagram, the design has six internal terminals. $V_{\text {VDD }}$ is the power supply terminal. DRV1 and DRV2 are linear driver outputs that can drive the emitter of an external high voltage NPN transistor or N-channel MOSFET. This emitter-drive method takes advantage of the high $\mathrm{V}_{\mathrm{CBO}}$ of the transistor, allowing a low cost transistor such as '13003 ( $\mathrm{V}_{\text {сво }}=700 \mathrm{~V}$ ) or '13002 $\left(\mathrm{V}_{\text {CBO }}=600 \mathrm{~V}\right.$ ) to be used for a wide AC input range. The slew-rate limited driver coupled with the turn-off characteristics of an external NPN transitor result in lower EMI.

The driver peak current is designed to have a negative voltage coefficient with respect to supply voltage $\mathrm{V}_{\text {VDD }}$, so that lower supply voltage automatically results in higher DRV1 peak current. This way, the optocoupler can control $\mathrm{V}_{\mathrm{VDD}}$ directly to affect driver current.

## Startup Sequence

Figure 1 shows a Simplified Application Circuit for the ACT30. Initially, the small current through resistor R1 charges up the capacitor C1, and the BJT acts as a follower to bring up the DRV1 voltage. An internal regulator generates a $\mathrm{V}_{\mathrm{VDD}}$ voltage equal to $\mathrm{V}_{\mathrm{DRV} 1}-3.6 \mathrm{~V}$ for $\mathrm{ACT} 30 \mathrm{~A}\left(\mathrm{~V}_{\mathrm{DRV} 1}-\right.$ 4.6 V for ACT 30 B ) but limits it to 5.5 V max. As $\mathrm{V}_{\mathrm{Vdd}}$ crosses 5 V , the regulator sourcing function stops and $\mathrm{V}_{\text {VDD }}$ begins to drop due to its current consumption. As $\mathrm{V}_{\text {VDD }}$ voltage decreases below 4.75 V , the IC starts to operate with increasing driver current. When the output voltage reaches regulation point, the optocoupler feedback circuit stops $\mathrm{V}_{\mathrm{VDD}}$ from decreasing further. The switching action also allows the auxiliary windings to take over in supplying the C1 capacitor. Figure 2 shows a typical startup sequence for the ACT30.

To limit the auxiliary voltage, use a 12 V zener diode for ACT30A or a 13V zener diode for ACT30B (D1 diode in Figure 1).

Even though up to $2 \mathrm{M} \Omega$ startup resistor (R1) can be used due to the very low startup current, the actual R1 value should be chosen as a compromise between standby power and startup time delay.

Figure 2:

## Startup Waveforms



## Normal Operation

In normal operation, the feedback signal from the secondary side is transmitted through the optocoupler as a current signal into $V_{\text {VDD }}$ pin, which has dynamic impedance of $9 \mathrm{k} \Omega$. The resulting $\mathrm{V}_{\text {VDD }}$ voltage affects the switching of the IC. As seen in the Functional Block Diagram, the Current Limit VC Generator uses the $\mathrm{V}_{\mathrm{VDD}}$ voltage difference with 4.75 V to generate a proportional offset at the negative input of the Error Comparator.
The drivers turn on at the beginning of each switching cycle. The current sense resistor current, which is a fraction of the transformer primary current, increases with time as the primary current increases. When the voltage across this current sense resistor plus the oscillator ramp signal equals Error Comparator's negative input voltage, the drivers turn off. Thus, the peak DRV1 current has a negative voltage coefficient of $-0.29 \mathrm{~A} / \mathrm{V}$ and can be calculated from the following:
$I_{\text {DRV1PEAK }}=0.29 \mathrm{~A} / \mathrm{V} \times\left(4.75 \mathrm{~V}-V_{V D D}\right)$
for $\mathrm{V}_{\mathrm{VDD}}<4.75 \mathrm{~V}$ and duty cycle $<50 \%$.
When the output voltage is lower than regulation, the current into $\mathrm{V}_{\text {VDD }}$ pin is zero and $\mathrm{V}_{\text {VDD }}$ voltage decreases. At $\mathrm{V}_{V D D}=\mathrm{V}_{\mathrm{UV}}=3.35 \mathrm{~V}$, the peak DRV1 current has maximum value of 400 mA .

## Current Limit Adjustment

The IC's proprietary driver arrangement allows the current limit to be easily adjusted between 400 mA and 1.2A. To understand this, the drivers have to be utilized as linear resistive devices with typically
$3.6 \Omega$ (rather than as digital output switches). The current limit can then be calculated through linear combination as shown in Figure 3. For TO-92 package, the ACT30A are preprogrammed to 400 mA current limit and the ACT30B are preprogrammed to 800 mA current limit, for SOT23B package, the ACT30A are preprogrammed to 400 mA current limit.

Figure 3:
Driver Output Configurations


## Pulse Modulation

The PFWM Switching Control Logic block operates in different modes depending on the output load current level. At light load, the $\mathrm{V}_{\text {vDD }}$ voltage is around 4.75 V . The energy delivered by each switching cycle (with minimum on time of 500 ns ) to the output causes $\mathrm{V}_{\text {VDD }}$ to increase slightly above 4.75 V . The FPWM Switching Control Logic block is able to detect this condition and prevents the IC from switching until $V_{V D D}$ is below 4.75 V again. This results in a pulse-modulation action with fixed pulse width and varying frequency, and low power consumption because the switching frequency is reduced. Typical system standby power consumption is 0.15 W .

## Short Circuit Hiccup

When the output is short circuited, the ACT30 enters hiccup mode operation. In this condition, the auxiliary supply voltage collapses. An on-chip detector compares DRV1 voltage during the offtime of each cycle to 6.8 V . If DRV1 voltage is below 6.8 V , the IC will not start the next cycle, causing both the auxiliary supply voltage and $\mathrm{V}_{\text {vDD }}$ to reduce further. The circuit enters startup mode when $\mathrm{V}_{\mathrm{VDD}}$ drops below 3.35 V . This hiccup behavior continues until the short circuit is removed. In this behavior, the effective duty cycle is very low resulting in very low short circuit current.

To make sure that the IC enters hiccup mode easily, the transformer should be constructed so that there is close coupling between secondary and auxiliary, so that the auxiliary voltage is low when the output is short-circuited. This can be achieved with the primary/auxiliary/secondary sequencing from the bobbin.

## APPLICATIONS INFORMATION

## External Power Transistor

The ACT30 allows a low-cost high voltage power NPN transistor such as '13003 or '13002 to be used safely in a flyback configuration. The required collector voltage rating for $\mathrm{V}_{\mathrm{AC}}=265 \mathrm{~V}$ with full output load is at least 600 V to 700 V . As seen in Figure 4, the breakdown voltage of an NPN is significantly improved when it is driven at its emitter. Thus, the ACT30 and '13002 or '13003 combination meet the necessary breakdown safety requirement even though RCC circuits using '13002 or '13003 do not. Table 1 lists the breakdown voltage of some transistors appropriate for use with the ACT30.

Table 1:

## Recommended Power Transistor List

| DEVICE | $\mathbf{V}_{\text {CBO }}$ | $\mathbf{V}_{\text {CEO }}$ | $\mathbf{I}_{\mathbf{C}}$ | $\mathbf{h}_{\text {FEMIN }}$ | PACKAGE |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MJE13002 | 600 V | 300 V | 1.5 A | 8 | TO-126 |
| MJE13003, <br> KSE13003 | 700 V | 400 V | 1.5 A | 8 | TO-126 |
| STX13003 | 700 V | 400 V | 1 A | 8 | TO-92 |

Figure 4:
NPN Reverse Bias Safe Operation Area


The power dissipated in the NPN transistor is equal to the collector current times the collector-emitter voltage. As a result, the transistor must always be in saturation when turned on to prevent excessive power dissipation. Select an NPN transistor with sufficiently high current gain ( $\mathrm{h}_{\text {FEMIN }}>8$ ) and a base drive resistor ( R 2 in Figure 1) low enough to ensure that the transistor easily saturates.

Figure 5:

## A 3.75W Charger Using ACT30A in Combination with TL431



## Application Example

The application circuit in Figure 5 provides a $5 \mathrm{~V} / 0.75 \mathrm{~A}$ constant voltage/constant current output. The performance of this circuit is summarized in Table 2.

Table 2:
System Performance of Circuit in Figure 5

|  | 110 VAC | 220 VAC |
| :---: | :---: | :---: |
| Standby Power | 0.09 W | 0.15 W |
| Current Limit | 0.75 A | 0.75 A |
| Full Load Efficiency | $65 \%$ | $67 \%$ |

## Layout Considerations

The following should be observed when doing layout for the ACT30:

1) Use a "star point" connection at the GND pin of ACT30 for the VDD bypass components (C5 and C6 in Figure 5), the input filter capacitor (C2 in Figure 5) and other ground connections on the primary side.
2) Keep the loop across the input filter capacitor, the transformer primary windings, and the high voltage transistor, and the ACT30 as small as possible.
3) Keep ACT30 pins and the high voltage transistor pins as short as possible.
4) Keep the loop across the secondary windings, the output diode, and the output capacitors as small as possible.
5) Allow enough copper area under the high voltage transistor, output diode, and current shunt resistor for heat sink.

## PACKAGE OUTLINE

## TO-92 PACKAGE OUTLINE AND DIMENSIONS (AMMO TAPE PACKING)



| SYMBOL | DIMENSION IN <br> MILIMETERS |  | DIMENSION IN <br> INCHES |  |
| :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX |
| A | 3.300 | 3.700 | 0.130 | 0.146 |
| A1 | 1.100 | 1.400 | 0.043 | 0.055 |
| b | 0.380 | 0.550 | 0.015 | 0.022 |
| c | 0.360 | 0.510 | 0.014 | 0.020 |
| D | 4.400 | 4.700 | 0.173 | 0.185 |
| D1 | 3.430 |  | 0.135 |  |
| E | 4.300 | 4.700 | 0.169 | 0.185 |
| e | 1.270 TYP | 0.050 TYP |  |  |
| e1 | 2.440 | 2.640 | 0.096 | 0.104 |
| D |  |  |  |  |
| h | 0.000 | 0.380 | 0.000 | 0.015 |


| SYMBOL | DIMENSION IN <br> MILIMETERS |  | DIMENSION IN <br> INCHES |  |
| :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX |
| $\Delta \mathrm{k}$ | -1.000 | 1.000 | -0.039 | 0.039 |
| F1, F2 | 2.200 | 2.800 | 0.087 | 0.110 |
| H | 19.00 | 21.00 | 0.748 | 0.827 |
| H0 | 15.50 | 16.50 | 0.610 | 0.650 |
| L1 | 2.500 |  | 0.098 |  |
| P | 12.40 | 13.00 | 0.488 | 0.512 |
| $\Delta \mathrm{P}$ | -1.000 | 1.000 | -0.039 | 0.039 |
| P0 | 12.50 | 12.90 | 0.492 | 0.508 |
| P1 | 3.550 | 4.150 | 0.140 | 0.163 |
| P2 | 6.050 | 6.650 | 0.238 | 0.262 |
| Q1 | 3.800 | 4.200 | 0.150 | 0.165 |
| t1 | 0.350 | 0.450 | 0.014 | 0.018 |
| t2 | 0.150 | 0.250 | 0.006 | 0.010 |
| W | 17.50 | 19.00 | 0.689 | 0.748 |
| W0 | 5.500 | 6.500 | 0.217 | 0.256 |
| W1 | 8.500 | 9.500 | 0.335 | 0.374 |
| W2 |  | 1.000 |  | 0.039 |

## SOT23-B PACKAGE OUTLINE AND DIMENSIONS



| SYMBOL | DIMENSION IN <br> MILLIMETERS |  | DIMENSION IN <br> INCHES |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX |  |  |
| A | 1.900 | 1.150 | 0.035 | 0.045 |  |  |
| A1 | 0.000 | 0.100 | 0.000 | 0.004 |  |  |
| A2 | 0.900 | 1.050 | 0.035 | 0.041 |  |  |
| b | 0.300 | 0.500 | 0.012 | 0.020 |  |  |
| c | 0.080 | 0.150 | 0.003 | 0.006 |  |  |
| D | 2.800 | 3.000 | 0.110 | 0.118 |  |  |
| E | 1.200 | 1.400 | 0.047 | 0.055 |  |  |
| E1 | 2.250 | 2.550 | 0.089 | 0.100 |  |  |
| e | 0.950 TYP |  | 0.037 TYP |  |  |  |
| e1 | 1.800 | 2.000 | 0.071 |  |  |  |
| L | 0.550 |  | REF | 0.022 |  | REF |
| L1 | 0.300 |  | 0.500 | 0.012 |  | 0.020 |
| $\theta$ | $0^{\circ}$ |  | $8^{\circ}$ | $0^{\circ}$ |  | $8^{\circ}$ |

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