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NANALOG
DEVICES

12-Bit Monitor and Control System with Multichannel ADC, DACs, Temperature Sensor, and Current Sense

Data Sheet **AD7294**

FEATURES

12-bit SAR ADC with 3 μs conversion time 4 uncommitted analog inputs Differential/single-ended VREF, 2 × VREF input ranges 2 high-side current sense inputs 5 V to 59.4 V operating range 0.5% max gain error ±200 mV input range 2 external diode temperature sensor inputs −55°C to +150°C measurement range ±2°C accuracy Series resistance cancellation 1 internal temperature sensor ±2°C accuracy Built-in monitoring features Minimum/maximum recorder for each channel Programmable alert thresholds Programmable hysteresis Four 12-bit monotonic 15 V DACs 5 V span, 0 V to 10 V offset 8 μs settling time 10 mA sink and source capability Power-on resets (POR) to 0 V Internal 2.5 V reference 2-wire fast mode I²C interface Temperature range: −40°C to +105°C Package type: 64-lead TQFP or 56-lead LFCSP

APPLICATIONS

Cellular base stations

GSM, EDGE, UMTS, CDMA, TD-SCDMA, W-CDMA, WiMAX Point-to-multipoint and other RF transmission systems 12 V, 24 V, 48 V automotive applications Industrial controls

GENERAL DESCRIPTION

The AD7294 contains all the functions required for generalpurpose monitoring and control of current, voltage, and temperature integrated into a single-chip solution. The device includes low voltage $(\pm 200 \text{ mV})$ analog input sense amplifiers for current monitoring across shunt resistors, temperature sense inputs, and four uncommitted analog input channels multiplexed into a SAR analog-to-digital converter (ADC) with a 3 μs conversion time. A high accuracy internal reference is provided to drive both the digital-to-analog converter (DAC) and ADC. Four 12-bit DACs provide the outputs for voltage control. The AD7294 also includes limit registers for alarm functions. The device is designed on Analog Devices, Inc., high voltage DMOS process for high voltage compliance, 59.4 V on the current sense inputs, and up to a 15 V DAC output voltage.

The AD7294 is a highly integrated solution that offers all the functionality necessary for precise control of the power amplifier in cellular base station applications. In these types of applications, the DACs provide 12-bit resolution to control the bias currents of the power transistors. Thermal diode-based temperature sensors are incorporated to compensate for temperature effects. The ADC monitors the high-side current and temperature. All this functionality is provided in a 64-lead TQFP or a 56-lead LFCSP operating over a temperature range of −40°C to +105°C.

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- PCN-PDN Information
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11/10—Rev. E to Rev. F

10/10—Rev. D to Rev. E

5/10—Rev. C to Rev. D

1/08—Revision 0: Initial Version

FUNCTIONAL BLOCK DIAGRAM

Figure 1.

SPECIFICATIONS

DAC SPECIFICATIONS

 $AV_{DD} = DV_{DD} = 4.5 V$ to 5.5 V, AGND = DGND = 0 V, internal 2.5 V reference; $V_{DRIVE} = 2.7 V$ to 5.5 V; T_A =-40°C to +105°C, unless otherwise noted. DAC OUTV+ AB and DAC OUTV+ CD = 4.5 V to 16.5 V, OFFSET IN x is floating, therefore, the DAC output span = 0 V to 5 V.

Table 1.

¹ This value indicates that the DAC output amplifiers can output voltages 15.5 mV below the DAC OUTV+ supply. If higher DAC OUTV+ supply voltages are used, the full-scale error of the DAC is typically 2 mV with no load.

² Samples are tested during initial release to ensure compliance; they are not subject to production testing.

ADC SPECIFICATIONS

 $AV_{DD} = DV_{DD} = 4.5 V$ to 5.5 V, $AGND = DGND = 0 V$, $V_{REF} = 2.5 V$ internal or external; $V_{DRIVE} = 2.7 V$ to 5.5 V; $V_{PP} = AV_{DD}$ to 59.4 V; T_A = -40° C to +105°C, unless otherwise noted.

¹ See the Terminology section for more details.

² Sampled during initial release to ensure compliance, not subject to production testing.
³ V_{IN+} or V_{IN−} must remain within GND/V_{DD}.
⁴ V_{IN−} = 0 V for specified performance. For full input range on V_{IN−}, se

GENERAL SPECIFICATIONS

 $AV_{DD} = DV_{DD} = 4.5 V$ to 5.5 V, AGND = DGND = 0 V, $V_{REF} = 2.5 V$ internal or external; $V_{DRIVE} = 2.7 V$ to 5.5 V; $V_{PP} = AV_{DD}$ to 59.4 V; DAC OUTV+ AB and DAC OUTV+ CD = 4.5 V to 16.5 V; OFFSET IN x is floating, therefore, DAC output span = 0 V to 5 V; T_A = -40° C to +105 $^{\circ}$ C, unless otherwise noted.

TIMING CHARACTERISTICS

I ²C Serial Interface

 $AV_{DD} = DV_{DD} = 4.5 V$ to 5.5 V, AGND = DGND = 0 V, $V_{REF} = 2.5 V$ internal or external; $V_{DRIVE} = 2.7 V$ to 5.5 V; $V_{PP} = AV_{DD}$ to 59.4 V; DAC OUTV+ AB and DAC OUTV+ CD = 4.5 V to 16.5 V; OFFSET IN x is floating, therefore, DAC output span = 0 V to 5 V; T_A = −40°C to +105°C, unless otherwise noted.

Table 4.

Parameter ¹	Limit at T _{MIN} , T _{MAX}	Unit	Description
f_{SCL}	400	kHz max	SCL clock frequency
t_1	2.5	us min	SCL cycle time
t ₂	0.6	μs min	t _{HIGH} , SCL high time
t_3	1.3	μs min	t_{low} , SCL low time
t ₄	0.6	µs min	t _{HD,STA} , start/repeated start condition hold time
t ₅	100	ns min	t_{SULSAT} , data setup time
t ₆	0.9	µs max	t _{HD,DAT} , data hold time
	0	us min	t _{HD,DAT} , data hold time
t ₇	0.6	us min	t _{su, STA} , setup time for repeated start
t_8	0.6	us min	t_{SUSTO} , stop condition setup time
t9	1.3	us min	t _{BUF} , bus free time between a stop and a start condition
t_{10}	300	ns max	t_{R} , rise time of SCL and SDA when receiving
	0	ns min	t_R , rise time of SCL and SDA when receiving (CMOS compatible)
t_{11}	300	ns max	t _F , fall time of SDA when transmitting
	0	ns min	t_F , fall time of SDA when receiving (CMOS compatible)
	300	ns max	t_F , fall time of SCL and SDA when receiving
	$20 + 0.1C_b^2$	ns min	t_F , fall time of SCL and SDA when transmitting
C_{b}	400	pF max	Capacitive load for each bus line

¹ See Figure 2.

 2 C_b is the total capacitance in pF of one bus line. t_R and t_F are measured between 0.3 DV_{DD} and 0.7 DV_{DD}.

Figure 2. I²C-Compatible Serial Interface Timing Diagram

Figure 3. Load Circuit for Digital Output

ABSOLUTE MAXIMUM RATINGS

 $T_A = 25$ °C, unless otherwise noted.¹

Table 5.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

To conform with IPC 2221 industrial standards, it is advisable to use conformal coating on the high voltage pins.

THERMAL RESISTANCE

Table 6. Thermal Resistance

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

¹ Transient currents of up to 100 mA do not cause SCR latch-up.

PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

Table 7. Pin Function Descriptions

¹ N/A means not applicable.

TYPICAL PERFORMANCE CHARACTERISTICS

Figure 6. Signal-to-Noise Ratio Single-Ended, VREF Range

Figure 7. Signal-to-Noise Ratio Single-Ended, $2 \times V_{REF}$ Range

Figure 8. Signal-to-Noise Ratio Differential, VREF Range

Figure 9. Signal-to-Noise Ratio Differential, $2 \times V_{REF}$ Range

Figure 11. ADC DNL Single-Ended, VREF Range

Figure 17. ADC DNL Differential, $2 \times V_{REF}$ Range

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Figure 24. Zoomed in Settling for a ¼ to ¾ Output Voltage Step

Figure 25. DAC Sinking Current at Input Code = $x000$, (Vout = 0 V)

Figure 26. DAC Sourcing Current at Input Code = $x000$, (V_{OUT} = 0 V)

Figure 27. DAC Output Voltage vs. Load Current, Input Code = x800

Figure 28. Response of the AD7294 to Thermal Shock Using 2N3906 (2N3906 Placed in a Stirred Oil Bath)

Figure 29. Response to Thermal Shock from Room Temperature into 50°C Stirred Oil (Both the AD7294 and the 2N3906 are Placed in a Stirred Oil Bath)

Figure 30. Temperature Error vs. Capacitor Between D+ and D−

Figure 31. Temperature Error vs. Series Resistance for 15 Typical Devices

on the AD7294

Figure 33. I_{SENSE} Power Supply Rejection Ratio vs. Supply Ripple Frequency Without V_{PP} Supply Decoupling Capacitors for a 500 mV Ripple

Figure 34. ISENSE Common-Mode Rejection Ratio vs. Ripple Frequency for a 400 mV Peak-To-Peak Ripple

TERMINOLOGY

DAC TERMINOLOGY

Relative Accuracy

For the DAC, relative accuracy or integral nonlinearity (INL) is a measure of the maximum deviation, in LSBs, from a straight line passing through the endpoints of the DAC transfer function.

Differential Nonlinearity

Differential nonlinearity (DNL) is the difference between the measured change and the ideal 1 LSB change between any two adjacent codes. A specified differential nonlinearity of ±1 LSB maximum ensures monotonicity. This DAC is guaranteed monotonic by design.

Zero Code Error

Zero code error is a measure of the output error when zero code (0x0000) is loaded to the DAC register. Ideally, the output should be 0 V. The zero code error is always positive in the AD7294 because the output of the DAC cannot go below 0 V. Zero code error is expressed in mV.

Full-Scale Error

Full-scale error is a measure of the output error when full-scale code (0xFFFF) is loaded to the DAC register. Ideally, the output should be V_{DD} – 1 LSB. Full-scale error is expressed in mV.

Gain Error

Gain error is a measure of the span error of the DAC. It is the deviation in slope of the DAC transfer characteristic from ideal, expressed as a percent of the full-scale range.

Total Unadjusted Error

Total unadjusted error (TUE) is a measure of the output error, taking all of the various errors into account.

Zero Code Error Drift

Zero code error drift is a measure of the change in zero code error with a change in temperature. It is expressed in μ V/°C.

Gain Error Drift

Gain error drift is a measure of the change in gain error with changes in temperature. It is expressed in (ppm of full-scale range)/°C.

ADC TERMINOLOGY

Signal-to-Noise and Distortion Ratio (SINAD)

The measured ratio of signal-to-noise and distortion at the output of the ADC. The signal is the rms amplitude of the fundamental. Noise is the sum of all nonfundamental signals up to half the sampling frequency $(f_s/2)$, excluding dc. The

ratio is dependent on the number of quantization levels in the digitization process; the more levels, the smaller the quantization noise. The theoretical signal-to-noise and distortion ratio for an ideal N-bit converter with a sine wave input is given by

Signal-to-(Noise + Distortion) = $(6.02 N + 1.76)$ dB

Thus, the SINAD is 74 dB for an ideal 12-bit converter.

Total Harmonic Distortion (THD)

The ratio of the rms sum of harmonics to the fundamental. For the AD7294, it is defined as

$$
THD(dB) = 20 \log \frac{\sqrt{V_2^2 + V_3^2 + V_4^2 + V_5^2 + V_6^2}}{V_1}
$$

where V_1 is the rms amplitude of the fundamental and V_2 , V_3 , V_4 , V_5 , and V_6 are the rms amplitudes of the second through sixth harmonics.

Peak Harmonic or Spurious Noise

The ratio of the rms value of the next largest component in the ADC output spectrum (up to $f_s/2$ and excluding dc) to the rms value of the fundamental. Typically, the value of this specification is determined by the largest harmonic in the spectrum, but for ADCs where the harmonics are buried in the noise floor, it is a noise peak.

Integral Nonlinearity

The maximum deviation from a straight line passing through the endpoints of the ADC transfer function. The endpoints are zero scale, a point 1 LSB below the first code transition, and full scale, a point 1 LSB above the last code transition.

Differential Nonlinearity

The difference between the measured and the ideal 1 LSB change between any two adjacent codes in the ADC.

Offset Error

The deviation of the first code transition (00…000) to $(00...001)$ from the ideal—that is, AGND + 1 LSB.

Offset Error Match

The difference in offset error between any two channels.

Gain Error

The deviation of the last code transition (111…110) to (111…111) from the ideal (that is, $REF_{IN}-1$ LSB) after the offset error has been adjusted out.

Gain Error Match

The difference in gain error between any two channels.

AD7294 Data Sheet

THEORY OF OPERATION **ADC OVERVIEW**

The AD7294 provides the user with a 9-channel multiplexer, an on-chip track-and-hold, and a successive approximation ADC based around a capacitive DAC. The analog input range for the device can be selected as a 0 V to V_{REF} input or a 2 \times V_{REF} input, configured with either single-ended or differential analog inputs. The AD7294 has an on-chip 2.5 V reference that can be disabled when an external reference is preferred. If the internal ADC reference is to be used elsewhere in a system, the output must first be buffered.

The various monitored and uncommitted input signals are multiplexed into the ADC. The AD7294 has four uncommitted analog input channels, $V_{\text{IN}}0$ to $V_{\text{IN}}3$. These four channels allow single-ended, differential, and pseudo differential mode measurements of various system signals.

ADC TRANSFER FUNCTIONS

The designed code transitions occur at successive integer LSB values (1 LSB, 2 LSB, and so on). In single-ended mode, the LSB size is $V_{REF}/4096$ when the 0 V to V_{REF} range is used and $2 \times V_{REF}/4096$ when the 0 V to $2 \times V_{REF}$ range is used. The ideal transfer characteristic for the ADC when outputting straight binary coding is shown in Figure 35.

In differential mode, the LSB size is $2 \times V_{REF}/4096$ when the 0 V to V_{REF} range is used, and $4 \times V_{REF}/4096$ when the 0 V to $2 \times V_{REF}$ range is used. The ideal transfer characteristic for the ADC when outputting twos complement coding is shown in Figure 36 (with the $2 \times V_{REF}$ range).

Figure 36. Differential Transfer Characteristic with V_{REF} \pm V_{REF} Input Range

For $V_{\text{IN}}0$ to $V_{\text{IN}}3$ in single-ended mode, the output code is straight binary, where

 $V_{IN} = 0$ V, $D_{OUT} = x000$, $V_{IN} = V_{REF} - 1$ LSB, and $D_{OUT} = xFFF$

In differential mode, the code is twos complement, where $V_{IN^+} - V_{IN^-} = 0$ V, and $D_{OUT} = x00$

$$
V_{IN+} - V_{IN-} = V_{REF} - 1
$$
 LSB, and
$$
D_{OUT} = x7FF
$$

 $V_{IN^+} - V_{IN^-} = -V_{REF}$, and $D_{OUT} = x800$

Channel 5 and Channel 6 (current sensor inputs) are twos complement, where

 $V_{IN^+} - V_{IN^-} = 0$ mV, and $D_{OUT} = x000$

 $V_{IN^+} - V_{IN^-} = V_{REF}/12.5 - 1$ LSB, $D_{OUT} = x7FF$

 $V_{IN^+} - V_{IN^-} = -V_{REF}/12.5$, $D_{OUT} = x800$

Channel 7 to Channel 9 (temperature sensor inputs) are twos complement with the LSB equal to 0.25°C, where

 $T_{IN} = 0$ °C, and $D_{OUT} = x000$ T_{IN} = +255.75°C, and D_{OUT} = x7FF $T_{IN} = -256$ °C, and $D_{OUT} = x800$

ANALOG INPUTS

The AD7294 has a total of four analog inputs. Depending on the configuration register setup, they can be configured as two single-ended inputs, two pseudo differential channels, or two fully differential channels. See the Register Setting section for further details.

Single-Ended Mode

The AD7294 can have four single-ended analog input channels. In applications where the signal source has high impedance, it is recommended to buffer the analog input before applying it to the ADC. The analog input range can be programmed to be either 0 V to V_{REF} or 0 V to 2 \times V_{REF}. In 2 \times V_{REF} mode, the input is effectively divided by 2 before the conversion takes place. Note that the voltage with respect to GND on the ADC analog input pins cannot exceed AV_{DD}.

If the analog input signal to be sampled is bipolar, the internal reference of the ADC can be used to externally bias up this signal so that it is correctly formatted for the ADC. Figure 37 shows a typical connection diagram when operating the ADC in single-ended mode.

Figure 37. Single-Ended Mode Connection Diagram

Differential Mode

The AD7294 can have two differential analog input pairs. Differential signals have some benefits over single-ended signals, including noise immunity based on the commonmode rejection of the device and improvements in distortion performance. Figure 38 defines the fully differential analog input of the AD7294.

The amplitude of the differential signal is the difference between the signals applied to V_{IN+} and V_{IN-} in each differential pair ($V_{IN+} - V_{IN-}$). The resulting converted data is stored in twos complement format in the result register. Simultaneously drive $V_{\text{IN}}0$ and $V_{\text{IN}}1$ by two signals, each of amplitude V_{REF} (or 2 \times VREF, depending on the range chosen), that are 180° out of phase. Assuming the 0∇ to V_{REF} range is selected, the amplitude of the differential signal is, therefore, -VREF to +VREF peak-topeak (2 \times V_{REF}), regardless of the common mode (V_{CM}).

The common mode is the average of the two signals

$$
(V_{IN+} + V_{IN-})/2
$$

The common mode is, therefore, the voltage on which the two inputs are centered.

This results in the span of each input being $V_{CM} \pm V_{REF}/2$. This voltage has to be set up externally, and its range varies with the reference value, V_{REF} . As the value of V_{REF} increases, the commonmode range decreases. When driving the inputs with an amplifier, the actual common-mode range is determined by the output voltage swing of the amplifier.

The common mode must be in this range to guarantee the functionality of the AD7294.

When a conversion takes place, the common mode is rejected, resulting in a virtually noise-free signal of amplitude -VREF to +VREF, corresponding to the digital output codes of −2048 to +2047 in twos complement format.

If the $2 \times V_{REF}$ range is used, the input signal amplitude extends from $-2 \times V_{REF}$ (V_{IN+} = 0 V, V_{IN−} = V_{REF}) to $+2 \times V_{REF}$ (V_{IN−} = 0 V, $V_{IN+} = V_{REF}$).

Driving Differential Inputs

The differential modes available on $V_{\text{IN}}0$ to $V_{\text{IN}}3$ in Table 13 require that V_{IN+} and V_{IN-} be driven simultaneously with two equal signals that are 180° out of phase. The common mode on which the analog input is centered must be set up externally. The common-mode range is determined by V_{REF} , the power supply, and the particular amplifier used to drive the analog inputs. Differential modes of operation with either an ac or dc input provide the best THD performance over a wide frequency range. Because not all applications have a signal preconditioned for differential operation, there is often a need to perform a singleended-to-differential conversion.

Using an Op Amp Pair

An op amp pair can be used to directly couple a differential signal to one of the analog input pairs of the AD7294. The circuit configurations illustrated in Figure 39 show how a dual op amp can be used to convert a single-ended bipolar signal into a differential unipolar input signal.

The voltage applied to Point A sets up the common-mode voltage. As shown in Figure 39, Point A connects to the reference, but any value in the common-mode range can be the input at Point A to set up the common mode. The AD8022 is a suitable dual op amp that can be used in this configuration to provide differential drive to the AD7294.

Care is required when choosing the op amp because the selection depends on the required power supply and system performance objectives. The driver circuits in Figure 39 are optimized for dc coupling applications requiring best distortion performance. The differential op amp driver circuit shown in Figure 39 is configured to convert and level shift a single-ended, ground referenced (bipolar) signal to a differential signal centered at the V_{REF} level of the ADC.

Figure 39. Dual Op Amp Circuit to Convert a Single-Ended Bipolar Signal into a Differential Unipolar Signal

Pseudo Differential Mode

The four uncommitted analog input channels can be configured as two pseudo differential pairs. Uncommitted input, $V_{\text{IN}}0$ and $\rm V_{\rm IN}$ are a pseudo differential pair, as are $\rm V_{\rm IN}$ and $\rm V_{\rm IN}$. In this mode, V_{IN+} is connected to the signal source, which can have a maximum amplitude of V_{REF} (or $2 \times V_{REF}$, depending on the range chosen) to make use of the full dynamic range of the device. A dc input is applied to V_{IN}−. The voltage applied to this input provides an offset from ground or a pseudo ground for the V_{IN+} input. Which channel is V_{IN+} is determined by the ADC channel allocation. The differential mode must be selected to operate in the pseudo differential mode. The resulting converted pseudo differential data is stored in twos complement format in the result register.

The governing equation for the pseudo differential mode, for $V_{IN}0$ is

$$
V_{OUT}=2(V_{IN+}-V_{IN-})-V_{REF_ADC}
$$

where V_{IN+} is the single-ended signal and V_{IN-} is a dc voltage.

The benefit of pseudo differential inputs is that they separate the analog input signal ground from the ADC ground, allowing dc common-mode voltages to be cancelled. The typical voltage range for V_{IN} – while in pseudo differential mode is shown in Figure 40; Figure 41 shows a connection diagram for pseudo differential mode.

Figure 41. Pseudo Differential Mode Connection Diagram

CURRENT SENSOR

05747-023

Two bidirectional high-side current sense amplifiers are provided that can accurately amplify differential current shunt voltages in the presence of high common-mode voltages from AV_{DD} up to 59.4 V. Each amplifier can accept a ± 200 mV differential input. Both current sense amplifiers have a fixed gain of 12.5 and utilize an internal 2.5 V reference.

An analog comparator is also provided with each amplifier for fault detection. The threshold is defined as

1.2 × Full-Scale Voltage Range

When this limit is reached, the output is latched onto a dedicated pin. This output remains high until the latch is cleared by writing to the appropriate register.

Figure 42. High-Side Current Sense

The AD7294 current sense comprises two main blocks: a differential and an instrumentation amplifier. A load current flowing through the external shunt resistor produces a voltage at the input terminals of the AD7294. Resistors R1 and R2 connect the input terminals to the differential amplifier (A1). A1 nulls the voltage appearing across its own input terminals by adjusting the current through R1 and R2 with Transistor Q1 and Transistor Q2. Common-mode feedback maintains the sum of these currents at approximately 50 μA. When the input signal to the AD7294 is zero, the currents in R1 and R2 are equal. When the differential signal is nonzero, the current increases through one of the resistors and decreases in the other. The current difference is proportional to the size and polarity of the input signal.

The differential currents through Q1 and Q2 are converted into a differential voltage by R3 and R4. A2 is configured as an instrumentation amplifier, buffering this voltage and providing additional

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gain. Therefore, for an input voltage of ± 200 mV at the pins, an output span of ±2.5 V is generated.

The current sensors on the AD7294 are designed to remove any flicker noise and offset present in the sensed signal. This is achieved by implementing a chopping technique that is transparent to the user. The VSENSE signal is first converted by the AD7294, the analog inputs to the amplifiers are then swapped, and the differential voltage is once again converted by the AD7294. The two conversion results enable the digital removal of any offset or noise. Switches on the amplifier inputs enable this chopping technique to be implemented. This process requires 6 μs in total to return a final result.

Choosing RSENSE

The resistor values used in conjunction with the current sense amplifiers on the AD7294 are determined by the specific application requirements in terms of voltage, current, and power. Small resistors minimize power dissipation, have low inductance to prevent any induced voltage spikes, and have good tolerance, which reduce current variations. The final values chosen are a compromise between low power dissipation and good accuracy. Low value resistors have less power dissipated in them, but higher value resistors may be required to utilize the full input range of the ADC, thus achieving maximum SNR performance.

When the sense current is known, the voltage range of the AD7294 current sensor (200 mV) is divided by the maximum sense current to yield a suitable shunt value. If the power dissipation in the shunt resistor is too large, the shunt resistor can be reduced, in which case, less of the ADC input range is used. Using less of the ADC input range results in conversion results, which are more susceptible to noise and offset errors because offset errors are fixed and are thus more significant when smaller input ranges are used.

RSENSE must be able to dissipate the I²R losses. If the power dissipation rating of the resistor is exceeded, its value may drift or the resistor may be damaged resulting in an open circuit. This can result in a differential voltage across the terminals of the AD7294 in excess of the absolute maximum ratings. Additional protection is afforded to the current sensors on the AD7294 by the recommended current limiting resistors, RF1 and RF2, as illustrated in Figure 43. The AD7294 can handle a maximum continuous current of 30 mA; thus, an RF2 of 1 k Ω provides adequate protection for the AD7294.

If I_{SENSE} has a large high frequency component, take care to choose a resistor with low inductance. Low inductance metal film resistors are best suited for these applications.

Current Sense Filtering

In some applications, it may be desirable to use external filtering to reduce the input bandwidth of the amplifier (see Figure 43). The −3 dB differential bandwidth of this filter is equal to

 $BW_{DM} = 1/(4\pi RC)$

Note that the maximum series resistance on the RS(+) and RS(−) inputs (as shown in Figure 42) is limited to a maximum of 1 kΩ due to back-to-back ESD protection diodes from $RS(+)$ and RS(−) to V_{PP}. Also, note that if RF1 and RF2 are in series with R1 and R2 (shown in Figure 42), it affects the gain of the amplifier. Any mismatch between RF1 and RF2 can introduce offset error.

Figure 43. Current Sense Filtering (RS_X Can Be Either RS1 or RS2)

For certain RF applications, the optimum value for RF1 and RF2 is 1 kΩ whereas CF1 can range from 1 μ F to 10 μ F. CF2 is a decoupling capacitor for the VPP supply. Its value is application dependent, but for initial evaluation, values in the range of 1 nF to 100 nF are recommended.

Kelvin Sense Resistor Connection

When using a low value sense resistor for high current measurement, the problem of parasitic series resistance can arise. The lead resistance can be a substantial fraction of the rated resistance, making the total resistance a function of lead length. Avoid this problem by using a Kelvin sense connection. This type of connection separates the current path through the resistor and the voltage drop across the resistor. Figure 44 shows the correct way to connect the sense resistor between the $RS(+)$ and RS(−) pins of the AD7294.

Figure 44. Kelvin Sense Connections (RSX Can Be Either RS1 or RS2)

ANALOG COMPARATOR LOOP

The AD7294 contains two setpoint comparators that are used for independent analog control. This circuitry enables users to quickly detect if the sensed voltage across the shunt has

increased about the preset ($V_{REF} \times 1.2$)/12.5. If this occurs, the ISENSE OVERRANGE pin is set to a high logic level enabling appropriate action to be taken to prevent any damage to the external circuitry.

The setpoint threshold level is fixed internally in the AD7294, and the current sense amplifier saturates above this level. The comparator also triggers if a voltage of less than AV_{DD} is applied to the RSENSE or V_{PP} pin.

TEMPERATURE SENSOR

The AD7294 contains one local and two remote temperature sensors. The temperature sensors continuously monitor the three temperature inputs and new readings are automatically available every 5 ms.

The on-chip, band gap temperature sensor measures the temperature of the system. Diodes are used in conjunction with the two remote temperature sensors to monitor the temperature of other critical board components.

Figure 45. Internal and Remote Temperature Sensors

The temperature sensor module on the AD7294 is based on the three current principle (see Figure 45), where three currents are passed through a diode and the forward voltage drop is measured at each diode, allowing the temperature to be calculated free of errors caused by series resistance.

Each input integrates, in turn, over a period of several hundred microseconds. This takes place continuously in the background, leaving the user free to perform conversions on the other channels. When integration is complete, a signal passes to the control logic to initiate a conversion automatically. If the ADC is in command mode, the temperature conversion is performed as soon as the next conversion is completed. In autocycle mode, the conversion is inserted into an appropriate place in the current sequence; see the Register Setting section for further details. If the ADC is idle, the conversion takes place immediately.

Three registers store the result of the last conversion on each temperature channel; these can be read at any time. In addition, in command mode, one or both of the two external channel registers can be read out as part of the output sequence.

Remote Sensing Diode

The AD7294 is designed to work with discrete transistors, 2N3904 and 2N3906. If an alternative transistor is used, the AD7294 operates as specified provided the following conditions are adhered to.

Ideality Factor

The ideality factor, n_f , of the transistor is a measure of the deviation of the thermal diode from ideal behavior. The AD7294 is trimmed for an n_f value of 1.008. Use the following equation to calculate the error introduced at a Temperature T ($^{\circ}$ C) when using a transistor whose n_f does not equal 1.008:

 $\Delta T = (n_f - 1.008) \times (273.15 \text{ K} + T)$

To factor this in, the user can write the ΔT value to the offset register. The AD7294 automatically adds it to, or subtracts it from, the temperature measurement.

Base Emitter Voltage

The AD7294 operates as specified provided that the baseemitter voltage is greater than 0.25 V at 8 μA at the highest operating temperature, and less than 0.95 V at 128 μA for the lowest operating temperature.

Base Resistance

The base resistance should be less than 100 Ω .

h_{FF} Variation

Use a transistor with small variation in h_{FE} (approximately 50 to 150). Small variation in h_{FE} indicates tight control of the V_{BE} characteristics.

For RF applications, the use of high Q capacitors functioning as a filter protects the integrity of the measurement. These capacitors, such as Johanson Technology 10 pF high Q capacitors: Reference Code 500R07S100JV4T, should be connected between the base and the emitter, as close to the external device as possible. However, large capacitances affect the accuracy of the temperature measurement; thus, the recommended maximum capacitor value is 100 pF. In most cases, a capacitor is not required; the selection of any capacitor is dependent on the noise frequency level.

Figure 46. Measuring Temperature Using an NPN Transistor

Figure 47. Measuring Temperature Using a PNP Transistor