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# White LED Driver for large LCD panel 

## BD9422EFV

## -General Description

BD9422EFV is a high efficiency driver for white LEDs and designed for large LCD panel. This IC is built-in high current drive and high responsibility type 6ch LED drivers and 1ch boost DCDC converter. BD9422EFV has some protect function against fault conditions, such as the over-voltage protection (OVP), LED OPEN and SHORT protection, the over current limit protection of DCDC (OCP). Therefore BD9422EFV is available for the fail-safe design over a wide range output voltage.

## - Key Specification

■ Operating power supply voltage range: 9.0 V to 35.0 V

- Oscillator frequency:
$500 \mathrm{kHz}(\mathrm{RT}=30 \mathrm{k} \Omega)$
- Operating Current: 9mA (typ.)
- Operating temperature range:
$-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$


## - Applications

TV, Computer Display, Notebook, LCD Backlighting

## - Typical Application Circuit

## -Features

- 6ch Constant LED drivers, available 400mA drive per 1ch.
- Constant current accuracy $\pm 1.8 \%$ (IC only)
- Each 6ch external PWM inputs can control independent dimming.
- Current analog (linear) dimming by VREF
- 1ch boost controller with current mode (external FET)
- Several protection functions
DCDC part
: OCP/OVP/UVLO/TSD

LED driver part :OPEN,SHORT detection

- SHORT detection voltage is set by LSP terminal. Error detection output FAIL terminal inside (normal=Open, error=Drain)
- Master/Slave mode inside


## -Package

HTSSOP-B40 Pin Pitch:


Figure 2. HTSSOP-B40

Figure 1. Typical Application Circuit

$\bullet$ Operating Ratings $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$

| Parameter | Symbol | Range | Unit |
| :--- | :---: | :---: | :---: |
| Power supply voltage | VCC | 9 to 35 | V |
| DC/DC oscillation frequency | FCT | 100 to $1250 * 5$ | kHz |
| VREF input voltage | VREF | 0.2 to 2.5 | V |
| LSP terminal input voltage | VLSP | 0.8 to 3 | V |
| FB terminal output voltage | VFB | 0 to 3.3 | V |
| M_DET terminal output voltage | VM_DET | 0 to REG9V | V |

The operating conditions written above are constants of the IC unit. Be careful enough when setting the constant in the actual set.
-External Components Recommended Range

| Item | Symbol | Setting Range | Unit |
| :--- | :---: | :---: | :---: |
| VCC terminal connection capacitance | CVCC | 1.0 to 10 | $\mu \mathrm{~F}$ |
| Soft-start set capacitance | SS | 0.001 to 1.0 | $\mu \mathrm{~F}$ |
| Timer latch set capacitance | CP | 0.001 to 2.7 | $\mu \mathrm{~F}$ |
| Operating frequency set resistance | RT | 12 to 150 | $\mathrm{k} \Omega$ |
| REG9V terminal connection capacitance | CREG9V | 2.2 to 10 | $\mu \mathrm{~F}$ |

The values described above are constants for a single IC. Adequate attention must be paid to setting of a constant for an actual set of parts

## -Pin Configuration

-Physical Dimension Tape and Marking Diagram


Figure 4. HTSSOP-B40
－1．1 Electrical Characteristics 1（Unless otherwise specified， $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{VCC}=24 \mathrm{~V}$ ）

| Parameter | Symbol | Limit |  |  | Unit | Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min． | Typ． | Max． |  |  |
| 【Whole device】 |  |  |  |  |  |  |
| Operating circuit current | ICC | － | 9 | 16 | mA | $\begin{aligned} & \text { STB=3V,LED1-6=ON, } \\ & \mathrm{RT}=30 \mathrm{k} \Omega \end{aligned}$ |
| Stand－by circuit current | ISTB | － | 12 | 20 | $\mu \mathrm{A}$ | $\mathrm{STB}=0 \mathrm{~V}$ |
| 【REG9V block】 |  |  |  |  |  |  |
| REG9V output voltage | REG9V | 8.9 | 9.0 | 9.1 | V | $10=0 \mathrm{~mA}$ |
| Maximum REG9V output current | IREG9V | 20 | － | － | mA |  |
| 【Switching block】 |  |  |  |  |  |  |
| N terminal source resistance | RONH | － | 2.5 | 3.5 | $\Omega$ | $10 \mathrm{~N}=-10 \mathrm{~mA}$ |
| $N$ terminal sink resistance | RONL | － | 3.0 | 4.2 | $\Omega$ | $1 \mathrm{ON}=10 \mathrm{~mA}$ |
| 【Over current protection（OCP）block】 |  |  |  |  |  |  |
| Over current protection voltage | VOCP | 0.40 | 0.45 | 0.50 | V | VCS＝SWEEP UP |
| 【Soft－start block】 |  |  |  |  |  |  |
| SS terminal source current | ISS | －1．4 | －1．0 | －0．6 | $\mu \mathrm{A}$ |  |
| SS terminal release voltage | VSS | 2.9 | 3.0 | 3.1 | V | SS＝SWEEP UP |
| 【Error amplifier block】 |  |  |  |  |  |  |
| LED control voltage | VLED | 0.66 | 0.7 | 0.74 | V | LED＿LV＝0．7V |
| FB sink current | IFBSINK | 55 | 100 | 155 | $\mu \mathrm{A}$ | LED＝2．0V，VFB＝1．0V |
| FB source current（Master） | IFBSOURCEM | －155 | －100 | －55 | $\mu \mathrm{A}$ | LED $=0 \mathrm{~V}, \mathrm{VFB}=1.0 \mathrm{~V}, \mathrm{CS}=0 \mathrm{~V}$ |
| FB source current（Slave） | IFBSWRCKS | －310 | －200 | －110 | $\mu \mathrm{A}$ | LED $=0 \mathrm{~V}, \mathrm{VFB}=1.0 \mathrm{~V}, \mathrm{CS}=5 \mathrm{~V}$ |
| LED＿LV terminal input current | ILED＿LV | －2 | 0 | 2 | uA | VLED＿LV＝3V |
| 【CT oscillator block】 |  |  |  |  |  |  |
| Oscillation frequency | FCT | 440 | 500 | 560 | kHz | $\mathrm{RT}=30 \mathrm{k} \Omega$ |
| MAX DUTY | DMAX | 83 | 89 | 96 | \％ |  |
| 【Over voltage protection（OVP）block】 |  |  |  |  |  |  |
| OVP detection voltage | VOVP | 2.34 | 2.43 | 2.52 | V | VOVP＝SWEEP UP |
| OVP hysteresis voltage | VOVPHYS | 10 | 50 | 100 | mV | VOVP＝SWEEP DOWN |
| OVP feedback voltage | FBOVP | 0.93 | 1.05 | 1.17 | V | $\begin{aligned} & \text { PMW1-6=0V,SS=2.8V, } \\ & \text { VLED_LV=0.7V } \end{aligned}$ |
| 【Short current protection（SCP）block】 |  |  |  |  |  |  |
| Short circuit protection voltage | VSCP | 0.12 | 0.20 | 0.28 | V | VOVP＝SWEEP DOWN |
| 【M＿LED block】 |  |  |  |  |  |  |
| Diode forward voltage | VFLED | 1120 | 1340 | 1560 | mV | VLED $=0 \mathrm{~V}$ |
| Forward voltage offset each ch | VFOFFSET | － | － | 20 | mV | VLED $=0 \mathrm{~V}$ |
| REG9V pull up resistance | RM＿DET | 60 | 100 | 140 | k $\Omega$ |  |

－1．2 Electrical Characteristics 2（Unless otherwise specified， $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{VCC}=24 \mathrm{~V}$ ）

| Parameter | Symbol | Limit |  |  | Unit | Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min． | Typ． | Max． |  |  |
| 【UVLO block】 |  |  |  |  |  |  |
| Operation power source voltage（VCC） | VUVLO＿VCC | 7.0 | 7.5 | 8.0 | V | VCC＝SWEEP UP |
| Hysteresis voltage（VCC） | VUHYS＿VCC | 150 | 300 | 600 | mV | VCC＝SWEEP DOWN |
| UVLO Release voltage | VUVLO＿U | 2.40 | 2.50 | 2.60 | V | VUVLO＝SWEEP UP |
| UVLO detection voltage | VUVLOD＿U | 2.15 | 2.30 | 2.45 | V | VUVLO＝SWEEP DOWN |
| UVLO terminal input resistance | RUVLO | 395 | 610 | 825 | k $\Omega$ | VUVLO $=3 \mathrm{~V}$ |
| 【Filter block】 |  |  |  |  |  |  |
| CP detection voltage | VCP | 1.9 | 2.0 | 2.1 | V | CP＝SWEEP UP |
| CP source current | ICP | －1．2 | －1．0 | －0．8 | $\mu \mathrm{A}$ | $\mathrm{VCP}=0 \mathrm{~V}$ |
| 【LED driver block】 |  |  |  |  |  |  |
| S terminal voltage | VSLED | 196 | 200 | 204 | mV | V REF $=1.0 \mathrm{~V}$ |
|  |  | 294.6 | 300 | 305.4 | mV | $\mathrm{VREF}=1.5 \mathrm{~V}$ |
|  |  | 392.8 | 400 | 407.2 | mV | $\mathrm{VREF}=2.0 \mathrm{~V}$ |
|  |  | 491 | 500 | 509 | mV | $\mathrm{VREF}=2.5 \mathrm{~V}$ |
| LED current rise time | ILEDtr | － | 400 | 760 | ns | $\mathrm{VREF}=0.3 \mathrm{~V}, \mathrm{RS}=2 \Omega$ |
| LED current fall time | ILEDtf | － | 100 | 280 | ns | $\mathrm{VREF}=0.3 \mathrm{~V}, \mathrm{RS}=2 \Omega$ |
| OPEN detection voltage | VOPEN | 0.12 | 0.20 | 0.28 | V | VLED＝SWEEP DOWN |
| SHORT detection voltage | VSHORT | 5.7 | 6.0 | 6.3 | V | $\begin{aligned} & \text { VLED=SWEEPUP, } \\ & \text { VLSP=1.2V } \\ & \hline \end{aligned}$ |
| SHORT MASK voltage | VSHTMASK | 2.85 | 3.0 | 3.15 | V |  |
| VREF terminal input current | IVREF | －2 | 0 | 2 | $\mu \mathrm{A}$ | $V \mathrm{VREF}=3 \mathrm{~V}$ |
| LSP terminal input current | ILSP | －2 | 0 | 2 | $\mu \mathrm{A}$ | VLSP＝3V |
| 【STB block】 |  |  |  |  |  |  |
| STB terminal HIGH voltage | STBH | 2.0 | － | VCC | V |  |
| STB terminal LOW voltage | STBL | －0．3 | － | 0.8 | V |  |
| STB terminal Pull Down resistance | RSTB | 0.5 | 1.0 | 1.5 | $\mathrm{M} \Omega$ | STB $=3 \mathrm{~V}$ |
| 【PWM IN block】 |  |  |  |  |  |  |
| PWM terminal HIGH voltage | PWMH | 2.0 | － | 20 | V |  |
| PWM terminal LOW voltage | PWML | －0．3 | － | 0.8 | V |  |
| PWM terminal Pull Down resistance | RPWM | 200 | 300 | 400 | $\mathrm{k} \Omega$ | PWM $=3 \mathrm{~V}$ |
| 【FAIL＿MODE，FAIL＿RST，SUMPWM block】 |  |  |  |  |  |  |
| Input terminal High voltage | VINH | 2.0 | － | 20 | V |  |
| Input terminal Low voltage | VINL | －0．3 | － | 0.8 | V |  |
| Input terminal Pull Down resistance | RVIN | 60 | 100 | 140 | $\mathrm{k} \Omega$ | $\mathrm{VIN}=3 \mathrm{~V}$ |
| 【FAIL block（OPEN DRAIN）】 |  |  |  |  |  |  |
| FAIL LOW output voltage | VOL | 0.25 | 0.5 | 1.0 | V | $1 \mathrm{OL}=1 \mathrm{~mA}$ |

-1.3 Pin Descriptions

| No | Pin name | In/Out | Function | rating [V] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | VCC | IN | Power source terminal | -0.3 to 36 |
| 2 | FAIL | OUT | Abnormality detection output terminal (OPEN DRAIN) | -0.3 to 36 |
| 3 | REG9V | OUT | 9 V regulator output terminal | -0.3 to 13 |
| 4 | N.C. | - | Non connection terminal | - |
| 5 | N | OUT | DC/DC switching output terminal | -0.3 to 13 |
| 6 | PGND | IN | Power GND terminal | - |
| 7 | CS | IN | DC/DC FET output current detection terminal | -0.3 to 7 |
| 8 | OVP | IN | Overvoltage protection detection terminal | -0.3 to 7 |
| 9 | M_DET | OUT | LED Diode OR output terminal | -0.3 to 13 |
| 10 | SUMPWM | IN/OUT | PWM signal enable/disable detection terminal | -0.3 to 7 |
| 11 | LED1 | OUT | LED output 1 | -0.3 to 60 |
| 12 | LED2 | OUT | LED output 2 | -0.3 to 60 |
| 13 | LED3 | OUT | LED output 3 | -0.3 to 60 |
| 14 | LED4 | OUT | LED output 4 | -0.3 to 60 |
| 15 | LED5 | OUT | LED output 5 | -0.3 to 60 |
| 16 | LED6 | OUT | LED output 6 | -0.3 to 60 |
| 17 | STB | IN | Standby control terminal | -0.3 to 36 |
| 18 | PWM1 | IN | PWM dimming input signal terminal for LED 1 | -0.3 to 22 |
| 19 | PWM2 | IN | PWM dimming input signal terminal for LED 2 | -0.3 to 22 |
| 20 | PWM3 | IN | PWM dimming input signal terminal for LED 3 | -0.3 to 22 |
| 21 | PWM4 | IN | PWM dimming input signal terminal for LED 4 | -0.3 to 22 |
| 22 | PWM5 | IN | PWM dimming input signal terminal for LED 5 | -0.3 to 22 |
| 23 | PWM6 | IN | PWM dimming input signal terminal for LED 6 | -0.3 to 22 |
| 24 | FAIL_RST | IN | FAIL output reset terminal | -0.3 to 22 |
| 25 | S6 | IN | Connecting terminal for LED 6 constant current setting resistor | -0.3 to 7 |
| 26 | S5 | IN | Connecting terminal for LED 5 constant current setting resistor | -0.3 to 7 |
| 27 | S4 | IN | Connecting terminal for LED 4 constant current setting resistor | -0.3 to 7 |
| 28 | S3 | IN | Connecting terminal for LED 3 constant current setting resistor | -0.3 to 7 |
| 29 | S2 | IN | Connecting terminal for LED 2 constant current setting resistor | -0.3 to 7 |
| 30 | S1 | IN | Connecting terminal for LED 1 constant current setting resistor | -0.3 to 7 |
| 31 | CP | OUT | Connecting terminal for non-reaction time setting capacitor | -0.3 to 7 |
| 32 | SS | OUT | Connecting terminal for soft-start time setting capacitor | -0.3 to 7 |
| 33 | FB | OUT | Error amplifier output terminal | -0.3 to 7 |
| 34 | RT | OUT | Connecting terminal for DC/DC frequency setting resistor | -0.3 to 7 |
| 35 | VREF | IN | Analog dimming DC voltage input terminal | -0.3 to 7 |
| 36 | LED_LV | IN | LED control voltage set terminal | -0.3 to 7 |
| 37 | LSP | IN | LED SHORT detection voltage setting terminal | -0.3 to 7 |
| 38 | FAIL_MODE | IN | FAIL function change terminal | -0.3 to 7 |
| 39 | UVLO | IN | Low voltage malfunction prevention detection terminal | -0.3 to 10.5 |
| 40 | AGND | IN | GND terminal for analog part | - |

-1.4.1 I/O equivalence circuit
(

Figure 5. I/O equivalence circuit

## -1.5Typical Performance Curves (reference data)



Figure 6. Circuit current


Figure 8. FB v.s. Duty Cycle


Figure 10. PWM terminal threshold voltage


Figure 7. Stand-by circuit current


Figure 9. VREF v.s. Sx


Figure 11. Block Diagram

## -3.1 Pin Configuration

## 1 pin. VCC

Power supply terminal of IC. The input range is 9 to 35 V .
The operation starts over $\mathrm{VCC}=7.5 \mathrm{~V}$ (typ.) and the system stops under $\mathrm{VCC}=7.2 \mathrm{~V}$ (typ.).

## 2 pin. FAIL

FAIL signal output terminal (NMOS open-drain). NMOS is OPEN at the normal operation so FAIL pin is Hi-Z. NMOS becomes ON state ( 500 ohm typ.) at the abnormal detection. It is possible to select the FAlL type from latch type (FAIL_MODE=L) or one shot pulse (FAIL_MODE=H).Please refer to the detail explanation<38pin. FAIL_MODE terminal>

## 3 pin. REG9V

REG9V is a 9 V output pin used delivering 20 mA at
maximum for switching power supply of $N$ terminal.
Use at a current higher than 20 mA may affect the reference voltage within IC, which may result in malfunction. It will also cause heating of IC itself. Therefore it is recommended to set the load as small as possible.
The characteristic of VCC line regulation at REG9V is shown as figure. VCC must be used in more than 10.5 V for stable 9 V output.
Install an oscillation prevention ceramic capacitor ( 2.2 to $10 \mu \mathrm{~F}$ ) nearest to VREG between VREG-AGND terminals.


4 pin. N.C
Figure 12.
Non connect pin. Please set it the open state or deal with connecting the GND.

## 5 pin. $N$

Gate driving output pin of external NMOS of DC/DC converter with 0 to 9 V (REG9V) swing. Output resistance of High side is 2.5 ohm(typ.), Low side is 3.0 ohm(typ.) in ON state. The oscillation frequency is set by a resistance connected to RT pin. For details, see the explanation of <34pin. RT terminal>.

## 6pin. PGND

Power GND terminal of output terminal, N driver:

## 7pin. CS

Inductor current detection resistor connecting terminal of DC/DC current mode: it transforms the current flowing through the inductor into voltage by sense resistor R $\mathrm{R}_{\mathrm{CS}}$ connected to CS terminal, and this voltage is compared with that set in the error amplifier by current detection comparator to control DC/DC output voltage. RCS also performs over current protection (OCP) and stops switching action when the voltage of CS terminal is 0.45 V (typ.) or higher (Pulse by Pulse).

## 8 pin. OVP

OVP terminal is the detection terminal of overvoltage protection (OVP) and short circuit protection (SCP) for DC/DC output voltage. Depending on the setting of the FAIL_MODE terminal, FAIL and CP terminal behave differently when an abnormality is detected. For details, see the table for each protection operation is described in $\bullet 3.2$ and $\bullet 3.3$. During the soft start (SS), there is a function which returns the OVP voltage to error amplifier to boost DC/DC output voltage at all Low PWM (OVPFB function). After completion of SS, this function is disabled.

## 9 pin. M_DET

The Di OR output terminal of LED 1 to 6 . The output is the voltage which is added a diode forward voltage(two diode stack) to the lowest voltage among 6 LED terminals.

## 10pin. SUMPWM

This is a judging terminal if high signal is input to PWM terminal or not. Using in Master/slave mode, one SUMPWM terminal is connected to another. And if any PWM signal becomes high between master and slave, the SUMPWM terminal becomes high, too. For details, please refer to •3.4 Connecting operation of Master/ slave.

## 11 to 16pin. LED1 to LED6

LED constant current driver output terminal. Setting of LED current value is adjustable by setting the VREF voltage and connecting a resistor to $S$ terminal. For details, see the explanation of $<25$ to 30 pin. $S 1$ to S6, 35pin. VREF $>$.
The PWM dimming frequency of LED current driver and upper/lower limit of the duty need to be set in a manner that necessary linearity of PWM dimming characteristics can be secured referring to the following figures:

Start/Stop time of constant current driver (PWM pulse response)
Start-up time depends on the VREF value; the response becomes quick, so that voltage is high.
In the way of reference, the current response upon application of current rise rate and pulse PWM1us (current pulse) to describe the dependence of VREF. It needs to be adequately verified with an actual device because the response rate may vary with application conditions.


Figure 13.


Figure 14.

17pin. STB
ON/OFF setting terminal for IC, which can be used perform a reset at shutdown.

* The voltage of STB input in the sequence of VCC $\rightarrow$ STB.
* Voltage input in STB terminal switches the state of IC (IC ON/OFF). Using the terminal between the 2 states ( 0.8 to 2.0 V ) needs to be avoided.


## 18 to 23pin. PWM1 to PWM6

ON/OFF terminal of LED driver: it inputs PWM dimming signal directly to PWM terminal and change of DUTY enables dimming. High/Low level of PWM terminal is shown as follows:

| State | PWM voltage |
| :--- | :--- |
| LED ON | PWM $=2.0$ to 20 V |
| LED OFF | PWM $=-0.3$ to 0.8 V |

## 24pin.FAIL_RST

Reset terminal of the protection circuit and FAIL terminal:
Return the latch stopped protection block by setting the FAIL_RST to High. During High state, operation is masked by the latch system protection.

## 25 to 30pin. S1 to S6, 35pin. VREF

$S$ terminal is a connecting terminal for LED constant current setting resistor, output current ILED is in an inverse relationship to the resistance value.
VREF terminal is a terminal for analog dimming; output current ILED is in a proportional relationship to the voltage value to be input.
VREF terminal is assumed that it is set by dividing the resistance with a high degree of accuracy, VREF terminal inside the IC is in open state (High Impedance). It is necessary to input voltage to divide the resistance from the output of REG9V or use external power source. Using the terminal in open state needs to be avoided.
The relationship among output current ILED, VREF input voltage, and RS resistance has the following equation:

$$
I_{L E D}=\frac{V R E F[\mathrm{~V}]}{\mathrm{RS}[\Omega]} \times 0.2[\mathrm{~A}]
$$

The voltage of $S$ terminal is following equation:

$$
\mathrm{VS}=0.2 \times V R E F[V]
$$



VREF=1.2V, RS=2 [ $\Omega$ ] ILED $=120[\mathrm{~mA}]$

Figure 15.

[^0]* For the adjustment of LED current with analog dimming by VREF, note that the output voltage of the DC/DC converter largely changes accompanied by LED VF changes if the VREF voltage is changed rapidly. In particularly, when the VREF voltages become high to low, it makes the LED terminal voltage seem higher transiently, which may influence application such as activation of the LED short circuit protection. It needs to be adequately verified with an actual device when analog dimming is used.


## 31pin. CP

Terminal which sets the time from detection of abnormality until shutdown (Timer latch). When the LED short protection, LED open protection or SCP is detected, it perform s constant current charge of 1.0 uA (typ.) to external capacitor. When the CP terminal voltage reaches 2.0 V (typ.), the IC is latched and FAIL terminal operates (at FAIL_MODE = L).

## 32pin. SS

Terminal which sets soft-start time of DC/DC converter: it performs constant current charge of 1.0 uA to the external capacitor connected with SS terminal, which enables soft-start of DC/DC converter.
Since the LED protection function (OPEN/SHORT detection) works when the SS terminal voltage reaches 3.0 V (typ.) or higher, it must be set to bring stability to conditions such as DC/DC output voltage and LED constant current drive operation, etc. before the voltage of 3.0 V is detected.

## 33pin. FB

Output terminal of the error amplifier of DC/DC converter which controls current mode:
The voltage of LED terminal which is the highest VF voltage among 6 LED strings and the voltage of LED_LV terminal become input of the error amplifier. The DC/DC output voltage is kept constant to control the duty of the output N terminal by adjusting the FB voltage.
The voltage of other LED terminals is, as a result, higher by the variation of Vf. Phase compensation setting is separately described in •3.7 How to set phase compensation.

A resistor and a capacitor need to be connected in series nearest to the terminal between FB and AGND.
The state in which all PWM signals are in LOW state brings high Impedance, keeping FB voltage. This action removes the time of charge to the specified voltage, which results in speed-up in DC/DC conversion.

## 34pin. RT

RT sets charge/discharge current determining frequency inside IC.
Only a resistor connected to RT determines the drive frequency inside IC, the relationship has the following equation: FCT is 500 kHz at $\mathrm{RT}=30 \mathrm{kohm}$.


Figure 16.


Figure 17.

36pin. LED_LV
LED_LV terminal sets the reference voltage error amplifier. LED_LV terminal is assumed that it is set by dividing the resistance with a high degree of accuracy, LED_LV terminal inside the IC is in open state (High Impedance). It is necessary to input voltage to divide the resistance from the output of REG9V or use external power source. Using the terminal in open state needs to be avoided.
According to output current, lowering LED_LV voltage can reduce the loss and heat generation inside IC. However, it is necessary to ensure the voltage between drain and source of FET inside IC, so LED_LV voltage has restriction on the following equation.

## VLED_LV $\geqq$ (LED-S terminal voltage) $\mathbf{+} 0.2 \times V R E F[V]$

For example, at ILED $=100 \mathrm{~mA}$ setting by $\mathrm{VREF}=1 \mathrm{~V}$, from figure the voltage between LED and S terminal is required 0.27 V at $\mathrm{Tj}=85^{\circ} \mathrm{C}$, so LED_LV voltage must be at least a minimum 0.47 V .

Note: Rises in VLED_LV voltage and LED current accelerate heat generation of IC. Adequate consideration needs to be taken to thermal design in use.
Note: LED_LV voltage is not allowed setting below 0.3 V .
Note: LED current by raising LED_LV voltage can flow to MAX 400mA, use with care in the dissipation of the package.

## 37pin. LSP

Terminal which sets LED SHORT detection voltage: The input impedance of LSP pin is High Impedance, because it is assumed that the input of LSP terminal is set by dividing the resistance with a high degree of accuracy.
The LSP terminal is assumed that it is set by dividing the resistance with a high degree of accuracy, LSP terminal inside the IC is in open state (High Impedance). It is necessary to input voltage to divide the resistance from the output of REG9V or use external power source. Using the terminal in open state needs to be avoided. Set LSP voltage in the range of 0.8 V to 3.0 V .

$$
L E D_{\text {SHORT }}=5 \times V L S P \quad[V]
$$

LED SHORT $^{\text {:LSP }}$ detection Voltage, VLSP:LSP terminal voltage
The conditions there are restrictions on short LED detection. For details, see the explanation of section •3.5.2 Setting the LED short detect voltage (LSP pin).

## 38pin. FAIL_MODE

Output mode of FAIL can be change by FAIL_MODE terminal. When FAIL_MODE is in Low state, the output of FAIL terminal is the latch mode. FAIL terminal is latched after the CP charge time from detection of abnormal state. When FAIL_MODE is in High
 state, the output of FAIL terminal is one-shot-pulse mode. At detected abnormality, firstly FAIL is in Low state (Drain state). FAIL returns to High state (Open state) if abnormality is cleared after CP charge time, In this mode, there is no latch stop for protection operation in IC. Monitoring the FAIL with the Microcomputer, decide to stop working IC.
For FAIL MODE $=\mathrm{H}$ when the detection sequence, see the explanation of section $\bullet$ 3.8.3 Protective operation sequence at FAIL MODE=H. On application to change modes is prohibited.

## 39pin. UVLO

UVLO terminal of the power of step-up DC/DC converter: at 2.5 V (typ.) or higher, IC starts step-up operation and stops at 2.3 V or lower (typ.). (It is not shutdown of IC.) UVLO can be used to perform a reset after latch stop of the protections.

The power of step-up DC/DC converter needs to be set detection level by dividing the resistance. If any problem on the application causes noise on UVLO terminal which results in unstable operation of DC/DC converter, a capacitance of approximately 1000 pF needs to be connected between UVLO and AGND terminals.

## 40pin. AGND

Analog GND for IC

## -3.2 Protection Operation at FAIL Latch output (FAILMODE=L)

-3.2.1 List of the Threshold Function terminal(typ. condition)
Please decide the resistance divider of the various protection detection using the following table.

| Protection name | Detection <br> Pin name | Detection condition | PWM | Release condition | Protection type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LED Open | LEDx | $\begin{gathered} \text { LEDx }<0.2 \mathrm{~V}(4 \mathrm{clk}) \\ \mathrm{SS}>3 \mathrm{~V} \end{gathered}$ | High | LEDx $>0.2 \mathrm{~V}$ (*1) | Stop the CH latch after the CP charge is completed. |
| LED short | LEDx | $\begin{gathered} \text { LEDx }>5 \times \mathrm{VLSP}(4 \mathrm{clk}) \\ \mathrm{SS}>3 \mathrm{~V} \end{gathered}$ | High | LEDx < 5xVLSP(3clk) | Stop the CH latch after the CP charge is completed. |
| UVLO | UVLO | UVLO < 2.3V | - | UVLO > 2.5 V | Stop the system |
| OVP | OVP | OVP > 2.43 V | - | OVP < 2.4V | Stop the N output |
| SCP | OVP | OVP < 0.2V | - | OVP > 0.2V | Stop the N output. Stop the system after the CP charge is completed. |
| OCP | CS | CS $>0.45 \mathrm{~V}$ | - | CS < 0.45V | Stop the N output under the detection. (Pulse by Pulse) |

It is possible to reset with the FAIL_RST terminal to release the latch stop.
(*1) The release condition of OPEN protection is depend on its release timing.

| No. | The timing of release of LEDx voltage (LEDx <br> $0.2 \mathrm{~V})$ | The release condition |
| :--- | :--- | :--- |
| 1 | LED pin voltage is released during PWM=H. | LED pin voltage is normal range during 3clk(3 positive edge) |
| 2 | LED pin voltage is released during PWM=L. | As PWM=L, LED pin voltage do not exceed Short <br> protection voltage (VLSP) during more than 3clk. or <br> PWM positive edge is input when LED pin voltage do not <br> exceed VLSP for more than 3clk. |

- 3.2.2 List of Protection function

| Protection function | Action when protection function is detected |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | DC/DC converter | LED driver | Soft-start | FAIL terminal |
| STB | Stop | Stop | Discharge | OPEN |
| LED Open | Normal operation <br> (Stop when all LED <br> CH stop) | Stop after CP charge <br> (Latch operation) | Normal operation | DRAIN after the CP <br> charge is completed. <br> (Latch operation) |
| LED short | Normal operation <br> *1 | Stop after CP charge <br> (Latch operation) | Normal operation | DRAIN after the CP <br> charge is completed. <br> (Latch operation) |
| UVLO | Stop | Stop | Discharge | GND |
| OVP | Stop N output | Normal operation | Normal operation | OPEN |
| SCP | Stop N output | Stop after CP charge <br> (Latch operation) | Discharge after latch | DRAIN after the CP <br> charge is completed. <br> (Latch operation) |
| OCP | Stop the N output <br> (Pulse by Pulse) | Normal operation | Normal operation | OPEN |

[^1]
## -3.3 Protection operation when the FAIL one shot outputs(FAILMODE=H)

-3.3.1 List of the threshold function terminal (typ. condition)
Please decide the resistance divider of the various protection detection using the following table.

| Protection <br> name | Detection <br> Pin name | Detection <br> condition |  | PWM | Release condition |
| :---: | :---: | :---: | :---: | :---: | :---: |$\quad$ Protection type

-3.3.2 List of the protection function

| Protection <br> function | Action when protection function is detected |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | DC/DC converter | LED driver | Soft-start | FAIL terminal |
| STB | Stop | Stop | Discharge | OPEN |
| LED Open | Normal operation <br> (Stop when the all CH <br> stop) | Normal operation | Normal operation | DRAIN under <br> the detection |
| LED short | Normal operation | Normal operation | Normal operation | DRAIN under <br> the detection |
| UVLO | Stop | Stop | Discharge | DRAIN |
| OVP | Stop the N output | Normal operation | Normal operation | DRAIN |
| SCP | Stop the N output | Normal operation | Normal operation | DRAIN |
| OCP | Stop the $N$ output <br> (Pulse by Pulse) | Normal operation | Normal operation | OPEN |

## -3.4 Connecting operation of Master/ slave



Recognized master mode and even one of slave's PWM on

Add pull-up resistance

Recognized master mode and all PWM off in Master and Slave

Cut FB output

Recognized slave mode and all PWM off in Slave

> Cut FB output

Figure 19.

Connecting plural BD9422EFVs makes it a Master/slave, a DCDC in Master construct a system to drive LED driver. Here, explanation of Master/slave operation in connecting 2 ICs.

## [MSDET] Convertor for recognizing Master/slave

Detect the voltage of CS terminal to judge master or slave of itself. The CS terminal of slave is OPEN when the Master/slave mode is used. The CS terminal is high due to being supplied constant current from IC inside. The CS terminal of Master is connected a resistance for DCDC switching current detection and swing 0 V to 0.45 V on operating. Convertor can detect the differences of the voltage, which is a Master/slave recognizing signal.
[SUMPWMDET] Converter for all PWM signal detection
SUMPWM terminal is connected a switch that is ON when the PWM signal is high and a pull down resistance 100k』. SUMPWM terminal becomes high more than one PWM signals are high.
When the SUMPWM terminal is connected between master and slave, it can judge if more than one signals of the entire PWM signal in master/slave becomes high.

The operation of error amplifier part is decided by the signal of MSDET and SUMPWM
1.Error amplifier output part Diode/non diode

If the IC recognizes slave mode, the diode is connected to error amplifier output and cut the supply of sink side of error amplifier.
2.Error amplifier output part Pull up resistance/ non pull up resistance

If the IC recognizes master mode and the PWM of slave become ON more than one, the pull up resistance is connected.
3. Error amplifier output FB output cut

In master recognizing, if all the PWM signals are OFF error amplifier output is cut.
In slave recognizing, if all the PWM signals of slave side are OFF error amplifier output is cut.
These are collected, the table below.


## -3.5 Setting of the external components. (typ. condition)

## -3.5.1 Setting the LED current (VREF and Sx pin)

First, VREF pin voltage is determined. When performing Analog dimming, be careful of VREF pin input range ( 0.2 to 2.5 V ) and decide typical voltage.
In BD9422EFV, LED constant current is controlled by Sx terminal voltage as a reference point. Sx terminal is controlled to become one fifth of the voltage of VREF terminal voltage. In the case of $\mathrm{VREF}=1 \mathrm{~V}$, it is set to $\mathrm{Sx}=0.2 \mathrm{~V}$.
Therefore, when the resistance to Sx terminal versus GND is set to "RS", the relationship between RS, VREF and ILED is as follows

$$
R_{S}[o h m]=\frac{V_{V R E F}[V]}{I_{L E D}[A] \times 5}
$$

## -3.5.2 Setting the LED short detect voltage (LSP pin)

The voltage of LED short detection can be arbitrarily set up with LSP pin voltage.
LSP pin cannot be used by OPEN because of High Impedance. Please be sure to applied voltage from the exterior. About LED short detection voltage, if "VLEDshort" and LSP pin voltage are set to "VLSP", it is as follows.

$$
V_{L S P}[V]=\frac{V L E D_{\text {short }}[V]}{5}
$$



Since the setting range of a LSP pin is set to 0.8 V to 3.0 V , VLEDshort can be set up in 4 V to 15 V .

## -Equation of setting LSP detect Voltage

When the detection voltage VLSP of LSP is set up by resistance division of R1 and R2 using REG9V, it becomes like the following formula.

$$
V L E D_{\text {short }}=\left(R E G 9 V \times \frac{R 2}{R 1+R 2}\right) \times 5 \quad[V]
$$

*Also including the variation in IC, please also take the part variation in a set into consideration for an actual constant setup, and inquire enough to it.

## -3.5.3 Timer latch time(CP pin)

When various abnormalities are detected, the source current of 1.0 uA is first flowed from CP pin.
BD9422EFV don't stop by latch, unless abnormal state is continues and CP pin voltage reaches continues 2 V .
With the capacity linked to CP pin, the unresponded time from detection to a latch stop. The relationship between the unresponded time "Tcp" and CP pin connection capacitor "Ccp" is as follows.

$$
\mathrm{C}_{\mathrm{CP}}[\mathrm{~F}]=\frac{\mathrm{T}_{\mathrm{CP}}[\mathrm{~S}] \times 1.0 \times 10^{-6}[\mathrm{~A}]}{2.0[\mathrm{~V}]}
$$

## -3.5.4 Setting the soft-start time (SS pin)

The starting time of a DCDC output is dependent on SS pin connection capacity.
Moreover, although SS pin is charged by source current of 1uA, IC does not perform LED protection as under DCDC starting state until SS pin voltage arrive to 3.0 V .
(The soft starting time set up here should be the mask time of a under [ starting ], and please keep in mind that it differs from time until a DCDC output is stabilized.)
Time until a DCDC output is stabilized is greatly dependent on a ratio of step-up or load.
The relationship between soft starting time "TSS" and SS pin connection capacity "CSS" is as follows.

$$
\mathrm{C}_{\mathrm{ss}}[\mathrm{~F}]=\frac{\mathrm{T}_{\mathrm{ss}}[\mathrm{~S}] \times 1.0 \times 10^{-6}[\mathrm{~A}]}{3.0[\mathrm{~V}]}
$$

## -3.5.5 DCDC operation frequency (RT pin)

The oscillation frequency of the DCDC output is decided by RT resistance.
BD9422EFV is designed to become a $500-\mathrm{kHz}$ setup at the time of 30 kohm .
RT resistance and frequency have a relation of an inverse proportion, and become settled as the following formula.

$$
R_{R T}=\frac{1.5 \times 10^{10}}{f_{S W}}[\Omega]
$$

$$
f_{s w}=\mathrm{DCDC} \text { convertor oscillation frequency [Hz] }
$$

Please connect RT resistance close as much as possible from RT pin and an AGND pin.

## -3.5.6 Maximum DCDC output voltage(Vout ,Max)

The DCDC output maximum voltage is restricted by Max Duty of $N$ output.
Moreover, the voltage needed in order that Vf may modulate by LED current also with the same number of LEDs.
Vf becomes high, so that there is generally much current.
When you have grasped the variation factor of everythings, such as variation in a DCDC input voltage range, the variation and temperature characteristics of LED load, and external parts, please carry out a margin setup.

## -3.5.7 Setting the OVP

In BD9422EFV, when over voltage in VOUT line is detected, the instant stop of the $N$ pin output is carried out, and voltage rise operation is stopped. But the latch stop by CP charge is not performed. If VOUT drops by naturally discharge, it is less than the hysteresis voltage of OVP detection and the oscillation condition is fulfilled, N output will be resumed again.

## -Equation of setting OVP detect

$$
\begin{equation*}
V O V P=2.43 \times \frac{R 1+R 2}{R 2} \tag{V}
\end{equation*}
$$

N pin output is suspended at the time of SCP detection, it stops step-up operation, and the latch protection by CP timer.

## -Equation of setting SCP detect

$$
V S C P=0.2 \times \frac{R 1+R 2}{R 2} \quad[V]
$$



Figure21.

Moreover, there is an OVPFB function which returns OVP voltage and controls error amplifier so that output voltage may be raised, even when there is no PWM signal during a soft start.

## -The VOUT setting formula by OVPFB in Soft Start

$$
\begin{equation*}
V O U T=\left(\frac{3}{2} \frac{R 1+R 2}{R 2}+\frac{R 1}{400}\right) \times V_{L E D_{-} L V} \tag{V}
\end{equation*}
$$

## -3.5.8 FAIL Logic

FAIL signal output pin (OPEN DRAIN); when an abnormality is detected, NMOS is brought into GND Level. The rating of this pin is 36 V .

| State | FAIL output |
| :---: | :---: |
| In normal state, In STB | OPEN |
| In completion of an abnormality, when the | GND Level |
| UVLO is detected(after CP latch) | (500ohm typ.) |

## -3.5.9 How to set the UVLO

UVLO pin detect the power supply voltage: Vin for step-up DC/DC converters. Operation starts operation on more than 2.5 V (typ.) and Operation stops on less than 2.3 V (typ.) .
Since internal impedance exists in UVLO pin, cautions are needed for selection of resistance for resistance division.
A Vin voltage level to make it detecting becomes settled like the following formula by resistance division of R1 and R2 (unit: $k \Omega$ ).
-Equation of setting UVLO release

$$
\operatorname{Vin}_{D E T}=2.5 \times\left\{\frac{R 1+R 2}{R 2}+\left(\frac{1}{1400 k+125 k}+\frac{1}{530 k+480 k}\right) \times R 1\right\} \quad[V
$$

Equation of setting UVLO lock


Figure 22.

$$
\begin{equation*}
\operatorname{Vin}_{\text {lock }}=2.3 \times\left\{\frac{R 1+R 2}{R 2}+\left(\frac{1}{1400 k+125 k}+\frac{1}{530 k+480 k+87 k}\right) \times R 1\right\} \tag{V}
\end{equation*}
$$

*Also including the variation in IC, please also take the part variation in a set into consideration for an actual constant setup, and inquire enough to it.

## -3.5.10 Setting of the LED_LV voltage (LED_LV pin)

LED_LV pin is in the OPEN (High Impedance) state.
Please be sure to use an external seal of approval, carrying out by inputting REG9V output by resistance division. It cannot use in the state of OPEN.

## -Equation of Setting LED_LV voltage

When LED_LV voltage is set up by resistance division of R1 and R2 using REG9V, it becomes like the following formula.

$$
V_{L E D_{-} L V}=R E G 9 V \times \frac{R 2}{R 1+R 2}[V]
$$

*Also including the variation in IC, please also take the part variation in a set into consideration for an actual constant setup, and inquire enough to it.

## -3.6 Selecting of DCDC part

Selecting inductor L

Figure 23.
The value of inductor has a great influence on input ripple current. As
解 frequency becomes high, the ripple current of an inductor $\triangle \mathrm{IL}$ becomes low.
$\Delta I L=\frac{\left(V_{\text {OUT }}-V_{I N}\right) \times V_{I N}}{L \times V_{\text {OUT }} \times f_{S W}}[A]$
When the efficiency is expressed by Equation (2), input peak current will be given by Equation (3).
$\eta=\frac{V_{\text {OUT }} \times I_{\text {OUT }}}{V_{I N} \times I_{I N}}$
$I L_{\text {MAX }}=I_{I N}+\frac{\Delta I L}{2}=\frac{V_{\text {OUT }} \times I_{\text {OUT }}}{V_{I N} \times \eta}+\frac{\Delta I L}{2}$
Here,
L : reactance value $[\mathrm{H}] \quad \mathrm{V}_{\text {out: }} \mathrm{DC} / \mathrm{DC}$ output voltage $[\mathrm{V}]$
$\mathrm{V}_{\text {IN: }}$ input voltage [V]
Lout: output load current (total of LED current) [A]
$\mathrm{I}_{\mathrm{IN}:}$ input current $[\mathrm{A}] \quad \mathrm{F}_{\mathrm{Sw}}$ : oscillation frequency $[\mathrm{Hz}]$
Generally, $\triangle \mathrm{IL}$ is set at around 30 to $50 \%$ of output load current.

Figure 24.

* Current exceeding the rated current value of inductor flown through the coil causes magnetic saturation, resulting in decrease in efficiency. Inductor needs to be selected to have such adequate margin that peak current does not exceed the rated current value of the inductor.
* To reduce inductor loss and improve efficiency, inductor with low resistance components (DCR, ACR) needs to be selected.

Selecting output capacitor Cout


Figure 25.

Output capacitor needs to be selected in consideration of equivalent series resistance required to even the stable area of output voltage or ripple voltage. Be aware that set LED current may not be flown due to decrease in LED terminal voltage if output ripple voltage is high.
Output ripple voltage $\Delta \mathrm{V}_{\text {OUt }}$ is determined by Equation (4):
$\Delta V_{\text {OUT }}=I L M A X \times R_{E S R}+\frac{1}{C_{\text {OUT }}} \times \frac{I_{\text {OUT }}}{\eta} \times \frac{1}{f_{S W}}[V]$
$\mathrm{R}_{\mathrm{ESR}}$ : equivalent series resistance of Cout

* Rating of capacitor needs to be selected to have adequate margin against output voltage.
* To use an electrolytic capacitor, adequate margin against allowable current is also necessary. Be aware that current larger than set value flows transitionally in case that LED is provided with PWM dimming especially.


## Selecting switching MOSFET

Though there is no problem if the absolute maximum rating is the rated current of $L$ or (withstand voltage of $\mathrm{C}_{\text {out }}+$ rectifying diode) VF or higher, one with small gate capacitance (injected charge) needs to be selected to achieve high-speed switching.

* One with over current protection setting or higher is recommended.
* Selection of one with small ON resistance results in high efficiency.

Selecting rectifying diode
A schottky barrier diode which has current ability higher than the rated current of $L$, reverse voltage larger than withstand voltage of Cout, and low forward voltage VF especially needs to be selected.

Selecting MOSFET for load switch and its soft-start
As a normal step-up DC/DC converter does not have a switch on the path from $\mathrm{V}_{\text {In }}$ to $\mathrm{V}_{\text {out, }}$, output voltage is generated even though IC is OFF. To keep output voltage at 0 V until IC works, PMOSFET for load switch needs to be inserted between $\mathrm{V}_{\mathbb{I N}}$ and the inductor. FAIL terminal needs to be used to drive the load switch. PMOSFET for the load switch of which gate-source withstand voltage and drain-source withstand voltage are both higher than $\mathrm{V}_{\text {IN }}$ needs to be selected.
To provide soft-start for the load switch, a capacitor must be inserted among gates and sources.

## -3.7 How to set phase compensation

DC/DC converter application controlling current mode has each one pole (phase lag) $f_{p}$ due to CR filter composed of output capacitor and output resistance (= LED current) and ZERO (phase lead) $\mathrm{fz}_{z}$ by output capacitor and ESR of the capacitor. Moreover, step-up DC/DC converter has RHP ZERO f phase lag $\left(-90^{\circ}\right)$ as pole does, cross-over frequency $f_{c}$ needs to be set at RHP ZERO or lower.


Figure 26. Output part


Figure 27. Error Amplifier
i. Determine Pole $f_{p}$ and RHPZERO $f_{Z R H P}$ of DC/DC converter:

$$
f_{p}=\frac{I_{\text {LED }}}{2 \pi \times V_{\text {OUT }} \times C_{\text {OUT }}}[H z] \quad f_{\text {ZRHP }}=\frac{V_{\text {OUT }} \times(1-D)^{2}}{2 \pi \times L \times I_{\text {LED }}}[H z]
$$

Here, , $I_{L E D}==$ sum of LED current, $\quad D=\frac{V_{\text {OUT }}-V_{I N}}{V_{\text {OUT }}}$
ii. Determine Phase compensation to be inserted into error amplifier (with $f_{c}$ set at $1 / 5$ of $f_{\text {ZRHP }}$ )

$$
R_{F B 1}=\frac{f_{R H Z P} \times R_{C S} \times I_{L E D}}{5 \times f_{p} \times g m \times V_{O U T} \times(1-D)}[\Omega] \quad C_{F B 1}=\frac{1}{2 \pi \times R_{F B 1} \times f_{p}}[F]
$$

Here,

$$
g m=1.036 \times 10^{-3}[S]
$$

iii. Determine ZERO to compensate ESR ( $\mathrm{R}_{\text {ESR }}$ ) of $\mathrm{C}_{\text {OUT }}$ (electrolytic capacitor)

$$
C_{F B 2}=\frac{R_{E S R} \times C_{O U T}}{R_{F B 1}}[F]
$$

* When a ceramic capacitor (with $\mathrm{R}_{\text {ESR }}$ of the order of millimeters) is used to $\mathrm{C}_{\text {Out }}$, too, operation is stabilized by insertion of $R_{\text {ESR }}$ and $C_{F B 2}$.

Though increase in $\mathrm{R}_{\mathrm{FB} 1}$ and decrease in $\mathrm{C}_{\text {FB1 }}$ are necessary to improve transient response, it needs to be adequately verified with an actual device in consideration of variation between external parts since phase margin is decreased.
-3.8 Timing chart -3.8.1 Normal operation sequence

-ILED* current is independent controlled by each PWM* pin.
-FAIL pin is pulled up.

Figure 28.
-3.8.2 Protective operation state transition table at FAIL_MODE=L
(Open detection)

| before CP charge |  | $\rightarrow$ | CP charge |  | $\rightarrow$ | $\mathrm{CP}=2 \mathrm{~V}$ arrival |  | end of state |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PWM | Error state |  | PWM | Error state |  | PWM | Error state |  |
| L(no pulse) or pulse less than 4 cnt . | don't care | discharge | - | - |  | - | - | normal state |
| pulse over 4cnt. | Not detect | discharge | - | - |  | - | - | normal state |
|  | detect | start charge | L(no pulse) | Not detect | discharge | - | - | normal state |
|  |  |  |  | detect | charge | L(no pulse) | Not detect | normal state |
|  |  |  |  |  |  |  | detect | CH latch FAIL latch |
|  |  |  |  |  |  | H(input pulse) | Not detect | normal state |
|  |  |  |  |  |  |  | detect | CH latch FAIL latch |
|  |  |  | H(input pulse) | Not detect | discharge | - | - | normal state |
|  |  |  |  | detect | charge | L(no pulse) | Not detect | normal state |
|  |  |  |  |  |  |  | detect | CH latch FAIL latch |
|  |  |  |  |  |  | H(input pulse) | Not detect | normal state |
|  |  |  |  |  |  |  | detect | CH latch FAIL latch |

(Short detection)

| before CP charge |  | $\rightarrow$ | CP charge |  | $\rightarrow$ | $\mathrm{CP}=2 \mathrm{~V}$ arrival |  | end of state |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PWM | Error state |  | PWM | Error state |  | PWM | Error state |  |
| L(no pulse) or puse less than 4cnt. | don't care | discharge | - | - |  | - | - | normal state |
| pulse over 4cnt. | detect | discharge | - | - |  | - | - | normal state |
|  |  | start charge | L(no pulse) | don't care | charge | L(no pulse) | don't care | CH latch FAIL latch |
|  |  |  |  |  |  | H(input pulse) | Not deetect | normal state |
|  |  |  |  |  |  |  | detect | CH latch FAIL latch |
|  |  |  | H(input pulse) | Not detect | discharge | - | - | normal state |
|  |  |  |  | detect | charge | L(no pulse) | don't care | CH latch FAIL latch |
|  |  |  |  |  |  | H(input pulse) | Not deetect | normal state |
|  |  |  |  |  |  |  | detect | CH latch FAIL latch |

With "the pulse of less than 4 cnt ", it is defined as the pulse width from (100n)sec to (Hi time of less than 4 cnt of DCDC frequency). In the pulse below (100n)sec, since delay from a PWM pin input to internal logic exists, it becomes unfixed.

- 3.8.3 Protective operation sequence at FAIL_MODE=H


## - Basic sequence



Figure 29.

## - Actual sequence



Figure 30.

The above chart is sample of SHORT detection, but the chart of OPEN detection is also same structure.

## -3.8.4 About LED SHORT detection

LED SHORT detection don't work by individual ch. The followings are needed for detection.

- Detection channel is PWM=H and LED terminal voltage is over LED SHORT detection threshold voltage.
- Except for detection ch, any 1 ch is $\mathrm{PWM}=\mathrm{H}$ and LED terminal voltage is under 3 V .
- The above-mentioned 2 states continue over 4clk of DCDC oscillation frequency.

Detection sequence is the followings.(omit 4clk mask)


Figure 31.

## -Operational Notes

1.) This product is produced with strict quality control, but might be destroyed if used beyond its absolute maximum ratings including the range of applied voltage or operation temperature. Failure status such as short-circuit mode or open mode can not be estimated. If a special mode beyond the absolute maximum ratings is estimated, physical safety countermeasures like fuse needs to be provided.
2.) Connecting the power line to IC in reverse polarity (from that recommended) may cause damage to IC. For protection against damage caused by connection in reverse polarity, countermeasures, installation of a diode between external power source and IC power terminal, for example, needs to be taken.
3.) When this product is installed on a printed circuit board, attention needs to be paid to the orientation and position of IC. Wrong installation may cause damage to IC. Short circuit caused by problems like foreign particles entering between outputs or between an output and power GND also may cause damage.
4.) Since the back electromotive force of external coil causes regenerated current to return, countermeasures like installation of a capacitor between power source and GND as the path for regenerated current needs to be taken. The capacitance value must be determined after it is adequately verified that there is no problem in properties such that the capacity of electrolytic capacitor goes down at low temperatures. Thermal design needs to allow adequate margin in consideration of allowable loss (Pd) in actual operation state.
5.) The GND pin needs to be at the lowest potential in any operation state.
6.) Thermal design needs to be done with adequate margin in consideration of allowable loss (Pd) in actual operation state.
7.) Use in a strong magnetic field may cause malfunction.
8.) Output Tr needs to not exceed the absolute maximum rating and ASO while using this IC. As CMOS IC and IC which has several power sources may undergo instant flow of rush current at turn-on, attention needs to be paid to the capacitance of power source coupling, power source, and the width and run length of GND wire pattern.
9.) This IC includes temperature protection circuit (TSD circuit). Temperature protection circuit (TSD circuit) strictly aims blockage of IC from thermal runaway, not protection or assurance of IC. Therefore use assuming continuous use and operation after this circuit is worked needs to not be done.
10.) As connection of a capacitor with a pin with low impedance at inspection of a set board may cause stress to IC, discharge needs to be performed every one process. Before a jig is connected to check a process, the power needs to be turned off absolutely. Before the jig is removed, as well, the power needs to be turned off.
11.) This IC is a monolithic IC which has $P+$ isolation for separation of elements and $P$ board between elements. A P-N junction is formed in this $P$ layer and $N$ layer of elements, composing various parasitic elements. For example, a resistance and transistor are connected to a terminal as shown in the figure,

- When GND>(Terminal A) in the resistance and when GND>(Terminal B) in the transistor (NPN), P-N junction operates as a parasitic diode.
- When GND>(Terminal B) in the transistor (NPN), parasitic NPN transistor operates in N layer of other elements nearby the parasitic diode described before.
Parasitic elements are formed by the relation of potential inevitably in the structure of IC. Operation of parasitic elements can cause mutual interference among circuits, malfunction as well as damage. Therefore such use as will cause operation of parasitic elements like application of voltage on the input terminal lower than GND ( P board) need to not be done.

(Pin B)




Figure 32. Example of Simple Structure of Monolithic IC

Status of this document
The Japanese version of this document is formal specification. A customer may use this translation version only for a reference to help reading the formal version.
If there are any differences in translation version of this document formal version takes priority.


## -Marking Diagram

HTSSOP-B40 (TOP VIEW)


## -Physical Dimension Tape and Reel Information

HTSSOP-B40



[^0]:    *Attention: Rises LED current accelerate heat generation of IC. Adequate consideration needs to be taken to thermal design in use.

[^1]:    (*1) Short protection doesn't hang when becoming remainder 1ch. DCDC output falls as LED short.

