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## 315/433MHz Receiver Evaluation Board Description

## Features

	Double superhet	architecture for	or high	degree	of image	rejection
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- ☐ FSK for digital data and FM reception for analog signal transmission
- ☐ FSK/FM demodulation with phase-coincidence demodulator
- ☐ Low current consumption in active mode and very low standby current
- ☐ Switchable LNA gain for improved dynamic range
- ☐ RSSI allows signal strength indication and ASK detection
- Surface mount package LQFP32

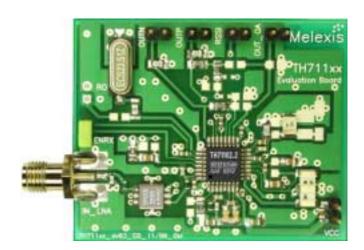
## Ordering Information Part No.

EVB71102-433-FSK EVB71102-433-ASK EVB71102-315-FSK EVB71102-315-ASK

## Application Examples

- General digital and analog 315 MHz or 433 MHz ISM band usage
- Low-power telemetry
- ☐ Alarm and security systems
- □ Remote Keyless Entry (RKE)
- ☐ Tire Pressure Monitoring System (TPMS)
- □ Garage door openers
- Home automation
- Pagers

## **Evaluation Board**



## General Description

The TH71102 FSK/FM/ASK double-conversion superheterodyne receiver IC is designed for applications in the European 433 MHz industrial-scientific-medical (ISM) band, according to the EN 300 220 telecommunications standard. It can also be used for any other system with carrier frequencies ranging from 300 MHz to 450 MHz (e.g. for applications in the US 315 MHz ISM band).



## 315/433MHz Receiver Evaluation Board Description

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## 315/433MHz Receiver **Evaluation Board Description**

## 1 Theory of Operation

### General 1.1

With the TH71102 receiver chip, various circuit configurations can be arranged in order to meet a number of different customer requirements. For FM/FSK reception the IF tank used in the phase coincidence demodulator can be constituted either by a ceramic resonator or an LC tank (optionally with a varactor diode to create an AFC circuit). In ASK configuration, the RSSI signal is feed to an ASK detector, which is constituted by the operational amplifier.

Demodulation	Type of receiver			
FM / FSK	narrow-band RX with ceramic demodulation tank			
FM / FSK	wide-band RX with LC demodulation tank			
ASK	RX with RSSI-based demodulation			

The superheterodyne configuration is double conversion where MIX1 and MIX2 are driven by the internal local oscillator signals LO1 and LO2, respectively. This allows a high degree of image rejection, achieved in conjunction with an RF front-end filter. Efficient RF front-end filtering is realized by using a SAW, ceramic or helix filter in front of the LNA and by adding an LC filter at the LNA output.

A single-conversion variant, called TH71101, is also available. Both Receiver ICs have the same die. At the TH71101 the second mixer MIX2 operates as an amplifier.

The TH71102 receiver IC consists of the following building blocks:

- PLL synthesizer (PLL SYNTH) for generation of the first and second local oscillator signals LO1 and LO2
- Parts of the PLL SYNTH are the high-frequency VCO1, the feedback dividers DIV 8 and DIV 2, a phase-frequency detector (PFD) with charge pump (CP) and a crystal-based reference oscillator (RO)
- Low-noise amplifier (LNA) for high-sensitivity RF signal reception
- First mixer (MIX1) for down-conversion of the RF signal to the first IF (IF1)
- Second mixer (MIX2) for down-conversion of the IF1 to the second IF (IF2)
- IF amplifier (IFA) to amplify and limit the IF2 signal and for RSSI generation
- Phase coincidence demodulator (DEMOD) with third mixer (MIX3) to demodulate the IF signal
- Operational amplifier (OA) for data slicing, filtering and ASK detection
- Bias circuitry for bandgap biasing and circuit shutdown

## Technical Data Overview

Input frequency range: 300 MHz to 450 MHz	Maximum input level: -10 dBm at ASK
Power supply range: 2.3 V to 5.5 V @ ASK	0 dBm at FSK
Temperature range: -40 °C to +85 °C	Image rejection: > 65 dB (e.g. with SAW
Standby current: 50 nA	front-end filter and at 10.7 MHz IF2)
Operating current: 6.5 mA at low gain mode	Spurious emission: < -70 dBm
8.2 mA at high gain mode	Input frequency acceptance: ±50 kHz
Sensitivity: -111 dBm 1) with 40 kHz IF filter BW	(with AFC option)
Sensitivity: -104 dBm <sup>2)</sup> with 150 kHz IF filter BW	RSSI range: 70 dB
Range of first IF1: 10 MHz to 80 MHz	Frequency deviation range: ±4 kHz to ±120 kHz
Range of second IF2: 400 kHz to 22 MHz	Maximum analog modulation frequency: 15 kHz
Maximum data rate: 80 kbit/s NRZ	,

1) at  $\pm$  8 kHz FSK deviation, BER =  $3\cdot10^{-3}$ , phase-coincidence demodulation and SAW front-end filter loss 2) at  $\pm$  50 kHz FSK deviation, BER =  $3\cdot10^{-3}$ , phase-coincidence demodulation and SAW front-end filter loss

For more detailed information, please refer to the latest TH71102 data sheet revision.

## 315/433MHz Receiver Evaluation Board Description

## 1.3 Block Diagram

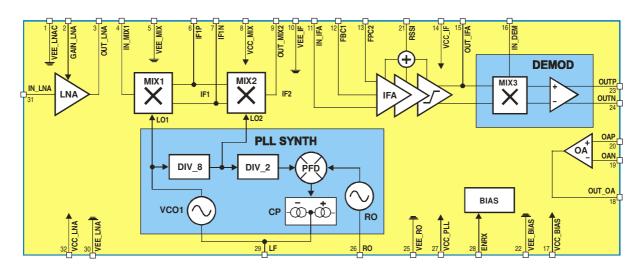


Fig. 1: TH71102 block diagram

## 1.4 Mode Configurations

ENRX	Mode	Description				
0	RX standby	RX disabled				
1	RX active	RX enable				

Note: ENRX are pulled down internally

## 1.5 LNA GAIN Control

V <sub>GAIN_LNA</sub>	Mode	Description			
< 0.8 V	HIGH GAIN	LNA set to high gain			
> 1.4 V	LOW GAIN	LNA set to low gain			

Note: hysteresis between gain modes to ensure stability

## 315/433MHz Receiver Evaluation Board Description

## 1.6 Frequency Planning

Frequency planning is straightforward for single-conversion applications because there is only one IF that might be chosen, and then the only possible choice is low-side or high-side injection of the LO signal (which is now the one and only LO signal in the receiver).

The receiver's double-conversion architecture requires careful frequency planning. Besides the desired RF input signal, there are a number of spurious signals that may cause an undesired response at the output. Among them are the image of the RF signal (that must be suppressed by the RF front-end filter), spurious signals injected to the first IF (IF1) and their images which could be mixed down to the same second IF (IF2) as the desired RF signal (they must be suppressed by the LC filter at IF1 and/or by low-crosstalk design).

By configuring the TH71102 for double conversion and using its internal PLL synthesizer with fixed feedback divider ratios of N1 = 8 (DIV\_8) and N2 = 2 (DIV\_2), four types of down-conversion are possible: low-side injection of LO1 and LO2 (**low-low**), LO1 low-side and LO2 high-side (**low-high**), LO1 high-side and LO2 low-side (**high-low**) or LO1 and LO2 high-side (**high-high**). The following table summarizes some equations that are useful to calculate the crystal reference frequency (REF), the first IF (IF1) and the VCO1 or first LO frequency (LO1), respectively, for a given RF and second IF (IF2).

Injection type	high-high	low-low	high-low	low-high
REF	(RF – IF2)/14	(RF – IF2)/18	(RF + IF2)/14	(RF + IF2)/18
LO1	16∙REF	16∙REF	16∙REF	16∙REF
IF1	LO1 – RF	RF – LO1	LO1 – RF	RF – LO1
LO2	2•REF	2•REF	2•REF	2•REF
IF2	LO2 – IF1	IF1 – LO2	IF1 – LO2	LO2 – IF1

## 1.6.1 Selected Frequency Plans

The following table depicts crystal, LO and image signals considering the examples of 315 MHz and 433.92 MHz RF reception at IF2 = 10.7 MHz.

Signal type	RF = 315 MHz	RF = 315 MHz	RF = 315 MHz	RF = 315.92 MHz	RF = 433.92 MHz	RF = 433.92 MHz	RF = 433.92 MHz	RF = 433.92 MHz
Injection type	high-high	low-low	high-low	low-high	high-high	low-low	high-low	low-high
REF / MHz	21.73571	16.90556	23.26429	18.09444	30.23000	23.51222	31.75857	24.70111
LO1 / MHz	347.77143	270.48889	372.22857	289.51111	483.68000	376.19556	508.13714	395.21778
IF1 / MHz	32.77143	44.51111	57.22857	25.48889	49.76000	57.72444	74.21714	38.70222
LO2 / MHz	43.47143	33.81111	46.52857	36.18889	60.46000	47.02444	63.51714	49.40222
RF image/MHz	380.54286	225.97778	429.45714	264.02222	533.44000	318.47112	582.35428	356.51556
IF1 image/MHz	54.17143	23.11111	35.82857	46.88889	71.16000	36.32444	52.81717	60.10222

The selection of the reference crystal frequency is based on some assumptions. As for example: the first IF and the image frequencies should not be in a radio band where strong interfering signals might occur (because they could represent parasitic receiving signals), the LO1 signal should be in the range of 300 MHz to 450 MHz (because this is the optimum frequency range of the VCO1). Furthermore the first IF should be as high as possible to achieve highest RF image rejection. The columns in bold depict the selected frequency plans to receive at 315 MHz and 433.92 MHz, respectively.

## 315/433MHz Receiver Evaluation Board Description

# 2 FSK Application Circuits

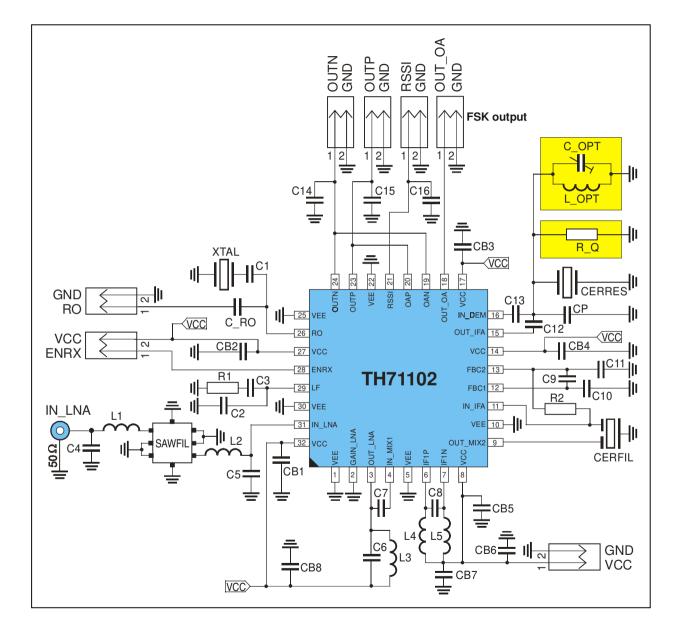


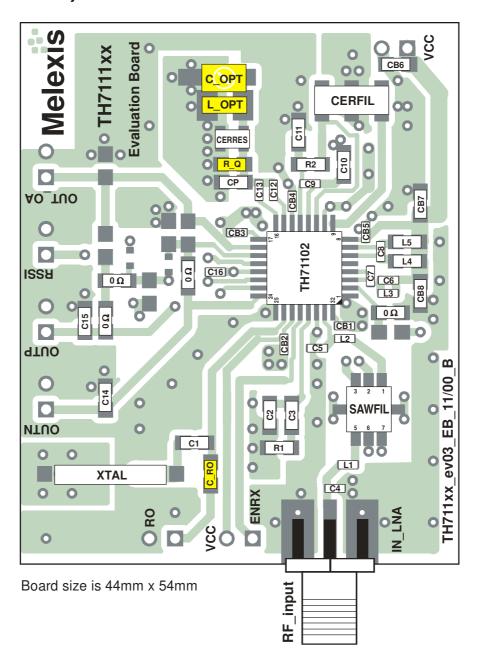
Fig. 2: Circuit diagram for FSK reception

EVB Description Feb./03



## 2.1 PCB Top View for FSK Reception

## Board layout data in Gerber format is available





## 315/433MHz Receiver Evaluation Board Description

## 2.2 Board Component Values for FSK (Fig. 2)

		Value	Value				
Part	Size	@ 315 MHz	@ 433.92 MHz	Tolerance	Description		
C1	0805	15 pF	15 pF	±10%	crystal series capacitor		
C2	0805	NIP	NIP	±10%	optional loop filter capacitor		
C3	0805	1 nF	1 nF	±10%	loop filter capacitor		
C4	0603	NIP	3.3 pF	±5%	capacitor to match to SAW filter input		
C5	0603	NIP	3.3 pF	±5%	capacitor to match to SAW filter output		
C6	0603	5.6 pF	4.7 pF	±5%	LNA output tank capacitor		
C7	0603	4.7 pF	2.2 pF	±5%	MIX1 input matching capacitor		
C8	0603	27 pF	27 pF	±5%	IF1 tank capacitor		
C9	0805	33 nF	33 nF	±10%	IFA feedback capacitor		
C10	0603	1 nF	1 nF	±10%	IFA feedback capacitor		
C11	0603	1 nF	1 nF	±10%	IFA feedback capacitor		
C12	0603	1.5 pF	1.5 pF	±5%	DEMOD phase-shift capacitor		
C13	0603	680 pF	680 pF	±10%	DEMOD coupling capacitor		
CP	0805	10 – 12 pF	10 – 12 pF	±5%	CERRES tuning capacitor		
C14	0805	10 – 47 pF	10 – 47 pF	±5%	demodulator output low-pass capacitor, depending on data rate		
C15	0805	10 – 47 pF	10 – 47 pF	±5%	demodulator output low-pass capacitor, depending on data rate		
C16	0603	1.5 nF	1.5 nF	±10%	RSSI output low-pass capacitor		
CB1 to CB5 CB7 to CB8	0603	330 pF	330 pF	±10%	blocking capacitor for VCC		
CB6	0805	33 nF	33 nF	±10%	blocking capacitor for VCC		
R1	0805	10 kΩ	10 kΩ	±10%	loop filter resistor		
R2	0805	390 Ω	390 Ω	±5%	CERFIL output matching resistor		
L1	0603	56 nH	33 nH	±5%	inductor to match SAW filter		
L2	0603	56 nH	33 nH	±5%	inductor to match SAW filter		
L3	0603	22 nH	15 nH	±5%	LNA output tank inductor		
L4	0805	100 nH	100 nH	±5%	IF1 tank inductor		
L5	0805	100 nH	100 nH	±5%	IF1 tank inductor		
L_OPT	1006	NIP	NIP	±5%	demodulator phase shift inductor, only required at FSK/FM with LC resonator		
C_OPT	3mm	NIP	NIP	±5%	demodulator phase shift capacitor, only required at FSK/FM with LC resonator		
R_Q	0805	NIP	NIP	±5%	optional lower-Q resistor, only required at FSK/FM with LC resonator		
C_RO	0805	330 pF	330 pF	±5%	optional capacitor to couple external RO signal		
XTAL	HC49 SMD	23.26429 MHz @ RF = 315 MHz	23.51222 MHz @ RF = 433.92 MHz	±25ppm calibr. ±30ppm temp.	$\begin{array}{l} \text{fundamental-mode crystal, } C_{load} = 10 \text{ pF} \\ \text{to 15pF, } C_{0, \text{ max}} = 7 \text{ pF, } R_{m, \text{ max}} = 50 \Omega \end{array}$		
SAWFIL	QCC8C		B3555	B <sub>3dB</sub> = 860 kHz	low-loss SAW filter from EPCOS		
			$(f_0 = 433.92 \text{ MHz})$	±100 kHz			
		B3551		$B_{3dB} = 900 \text{ kHz}$	<b>1</b>		
		$(f_0 = 315.00 \text{ MHz})$		±175 kHz			
CERFIL	Leaded	SFE10.7MFP	SFE10.7MFP	TBD	ceramic filter from Murata		
	type	@ B <sub>IF2</sub> = 40 kHz	@ B <sub>IF2</sub> = 40 kHz		_		
	SMD	SFECV10.7MJS-A	SFECV10.7MJS-A	±40 kHz			
	type	@ B <sub>IF2</sub> = 150 kHz	@ B <sub>IF2</sub> = 150 kHz				
CERRES	SMD type	CDACV10.7MG18-A Murata	CDACV10.7MG18-A Murata		ceramic demodulator tank, not required at FSK/FM with LC resonator		

NIP - not in place, may be used optionally

## **Evaluation Board Description** 315/433MHz Receiver

## ω ASK Application Circuits

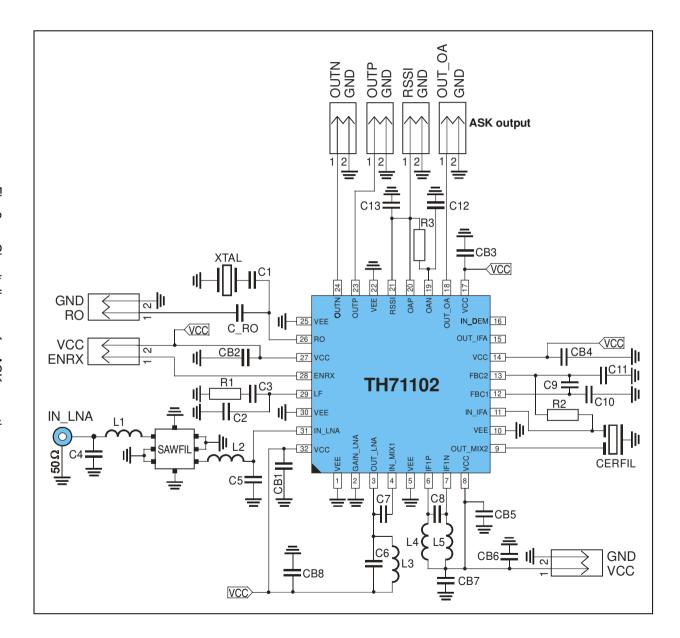
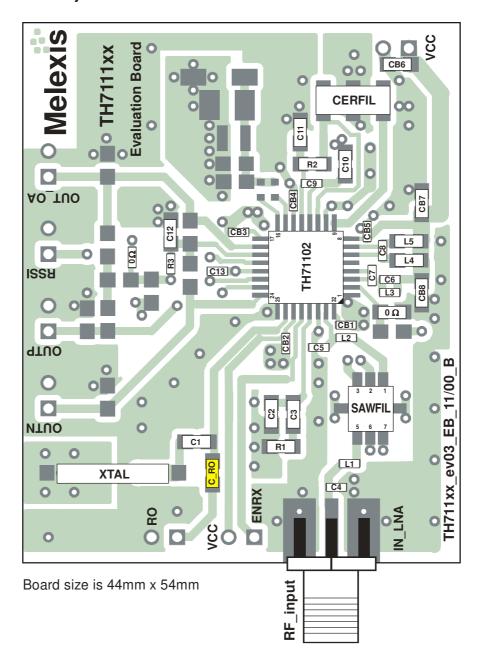


Fig. 3: Circuit diagram for ASK reception



## 3.1 PCB Top View for ASK Reception

## Board layout data in Gerber format is available



## 315/433MHz Receiver Evaluation Board Description

## 3.2 Board Component Values for ASK (Fig. 3)

Part	Size	Value @ 315 MHz	Value @ 433.92 MHz	Tolerance	Description
C1	0805	15 pF	15 pF	±10%	crystal series capacitor
C2	0805	NIP	NIP	±10%	optional loop filter capacitor
C3	0805	1 nF	1 nF	±10%	loop filter capacitor
C4	0603	NIP	3.3 pF	±5%	capacitor to match to SAW filter input
C5	0603	NIP	3.3 pF	±5%	capacitor to match to SAW filter output
C6	0603	5,6 pF	4.7 pF	±5%	LNA output tank capacitor
C7	0603	4.7 pF	2.2 pF	±5%	MIX1 input matching capacitor
C8	0603	27 pF	27 pF	±5%	IF1 tank capacitor
C9	0805	33 nF	33 nF	±10%	IFA feedback capacitor
C10	0603	1 nF	1 nF	±10%	IFA feedback capacitor
C11	0603	1 nF	1 nF	±10%	IFA feedback capacitor
C12	0805	1 nF to 100 nF	1 nF to 100 nF	±10%	ASK data slicer capacitor, depending on data rate
C13	0603	1.5 nF	1.5 nF	±10%	RSSI output low-pass capacitor
CB1 to CB5 CB7 to CB8	0603	330 pF	330 pF	±10%	blocking capacitor for VCC
CB6	0805	33 nF	33 nF	±10%	blocking capacitor for VCC
R1	0805	10 kΩ	10 kΩ	±10%	loop filter resistor
R2	0805	390 Ω	390 Ω	±5%	CERFIL output matching resistor
R3	0603	100 kΩ	100 kΩ	±5%	ASK data slicer resistor, depending on data rate
L1	0603	56 nH	33 nH	±5%	inductor to match SAW filter
L2	0603	56 nH	33 nH	±5%	inductor to match SAW filter
L3	0603	22 nH	15 nH	±5%	LNA output tank inductor
L4	0805	100 nH	100 nH	±5%	IF1 tank inductor
L5	0805	100 nH	100 nH	±5%	IF1 tank inductor
C_RO	0805	330 pF	330 pF	±5%	optional capacitor to couple external RO signal
XTAL	HC49	23.26429 MHz	23.51222 MHz @	±25ppm calibr.	fundamental-mode crystal, C <sub>load</sub> = 10 pF
	SMD	@ RF = 315 MHz	RF = 433.92 MHz	±30ppm temp.	to 15pF, $C_{0, max}$ = 7 pF, $R_{m, max}$ = 50 $\Omega$
SAWFIL	QCC8C		B3555	$B_{3dB} = 860 \text{ kHz}$	low-loss SAW filters from EPCOS
			$(f_0 = 433.92 \text{ MHz})$	±100 kHz	
		B3551 $(f_0 = 315.00 \text{ MHz})$		$B_{3dB} = 900 \text{ kHz}$ ±175 kHz	
CERFIL	Leaded	SFE10.7MFP	SFE10.7MFP	TBD	ceramic filters from Murata
	type	@ $B_{1F2} = 40 \text{ kHz}$	@ B <sub>IF2</sub> = 40 kHz		
	SMD	SFECV10.7MJS-A	SFECV10.7MJS-A	±40 kHz	]
	type	@ B <sub>IF2</sub> = 150 kHz	@ B <sub>IF2</sub> = 150 kHz		

NIP - not in place, may be used optionally



## 315/433MHz Receiver Evaluation Board Description

## 4 Package Dimensions

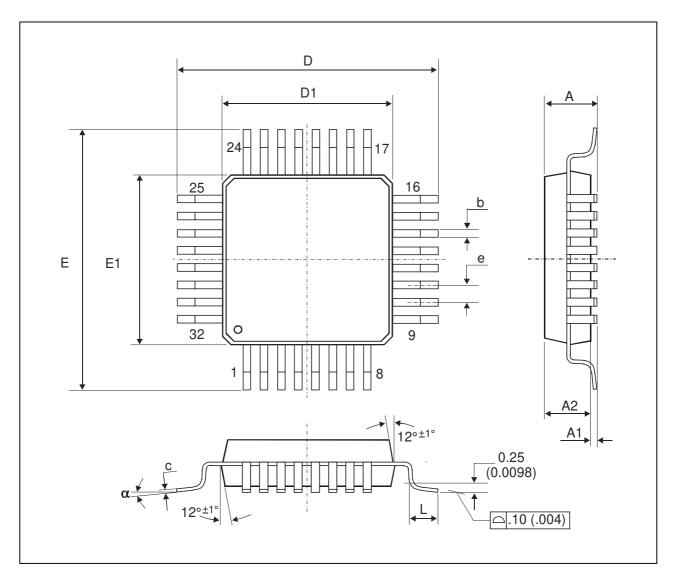


Fig. 4: LQFP32 (Low profile Quad Flat Package)

All Dimer	All Dimension in mm, coplanaríty < 0.1mm										
	E1, D1	E, D	Α	A1	A2	е	b	С	L	α	
min	7.00	0.00	1.40	0.05	1.35	0.0	0.30	0.09	0.45	0°	
max	7.00	9.00	1.60	0.15	1.45	0.8	0.45	0.20	0.75	7°	
All Dimer	All Dimension in inch, coplanaríty < 0.004"										
min	0.070	0.054	0.055	0.002	0.053	0.004	0.012	0.0035	0.018	0°	
max	0.276	0.276 0.354	0.063	0.006	0.057	0.031	0.018	0.0079	0.030	7°	



## 315/433MHz Receiver Evaluation Board Description

## 5 Reliability Information

Melexis devices are classified and qualified regarding suitability for infrared, vapor phase and wave soldering with usual (63/37 SnPb-) solder (melting point at 183degC). The following test methods are applied:

- IPC/JEDEC J-STD-020A (issue April 1999)
   Moisture/Reflow Sensitivity Classification For Nonhermetic Solid State Surface Mount Devices
- CECC00802 (issue 1994)
   Standard Method For The Specification of Surface Mounting Components (SMDs) of Assessed Quality
- MIL 883 Method 2003 / JEDEC-STD-22 Test Method B102 Solderability

For all soldering technologies deviating from above mentioned standard conditions (regarding peak temperature, temperature gradient, temperature profile etc) additional classification and qualification tests have to be agreed upon with Melexis.

The application of Wave Soldering for SMD's is allowed only after consulting Melexis regarding assurance of adhesive strength between device and board.

For more information on manufacturability/solderability see quality page at our website: <a href="http://www.melexis.com/">http://www.melexis.com/</a>

## 6 ESD Precautions

Electronic semiconductor products are sensitive to Electro Static Discharge (ESD). Always observe Electro Static Discharge control procedures whenever handling semiconductor products.



## 315/433MHz Receiver Evaluation Board Description

## 7 Disclaimer

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