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March 2015

### FDD8880

# N-Channel PowerTrench<sup>®</sup> MOSFET 30V, 58A, $9m\Omega$

#### **General Description**

This N-Channel MOSFET has been designed specifically to improve the overall efficiency of DC/DC converters using either synchronous or conventional switching PWM controllers. It has been optimized for low gate charge, low  $r_{\text{DS}(\text{ON})}$  and fast switching speed.

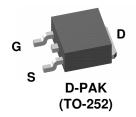
### **Applications**

DC/DC converters



#### **Features**

- $r_{DS(ON)} = 9m\Omega$ ,  $V_{GS} = 10V$ ,  $I_D = 35A$
- $r_{DS(ON)} = 12m\Omega$ ,  $V_{GS} = 4.5V$ ,  $I_D = 35A$
- High performance trench technology for extremely low  $r_{\mbox{\footnotesize{DS}}(\mbox{\footnotesize{ON}})}$
- · Low gate charge
- · High power and current handling capability
- RoHS Compliant





### **MOSFET Maximum Ratings** $T_C = 25$ °C unless otherwise noted

Symbol	Parameter	Ratings	Units
V <sub>DSS</sub>	Drain to Source Voltage	30	V
V <sub>GS</sub>	Gate to Source Voltage	±20	V
I <sub>D</sub>	Drain Current		
	Continuous ( $T_C = 25^{\circ}C$ , $V_{GS} = 10V$ ) (Note 1)	58	Α
	Continuous ( $T_C = 25^{\circ}C$ , $V_{GS} = 4.5V$ ) (Note 1)	51	Α
	Continuous ( $T_{amb} = 25^{\circ}C$ , $V_{GS} = 10V$ , with $R_{\theta JA} = 52^{\circ}C/W$ )	13	Α
	Pulsed	Figure 4	Α
E <sub>AS</sub>	Single Pulse Avalanche Energy (Note 2)	53	mJ
P <sub>D</sub>	Power dissipation	55	W
	Derate above 25°C	0.37	W/°C
T <sub>J</sub> , T <sub>STG</sub>	Operating and Storage Temperature	-55 to 175	°C

#### **Thermal Characteristics**

$R_{\theta JC}$	Thermal Resistance Junction to Case TO-252	2.73	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-252	100	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-252, 1in <sup>2</sup> copper pad area	52	°C/W

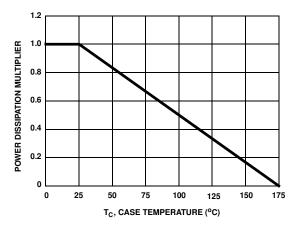
### **Package Marking and Ordering Information**

Device Marking	Device	Package	Reel Size	Tape Width	Quantity
FDD8880	FDD8880	TO-252AA	13"	16mm	2500 units

Symbol	Parameter	Test Conditions	Min	Тур	Max	Units
Off Chara	cteristics					
B <sub>VDSS</sub>	Drain to Source Breakdown Voltage	$I_D = 250 \mu A, V_{GS} = 0 V$	30	_	_	V
- 1000		V <sub>DS</sub> = 24V	-	-	1	-
I <sub>DSS</sub>	Zero Gate Voltage Drain Current	$V_{GS} = 0V$ $T_C = 150^{\circ}C$	-	-	250	μΑ
I <sub>GSS</sub>	Gate to Source Leakage Current	V <sub>GS</sub> = ±20V	-	-	±100	nA
On Chara	cteristics		•	•		
V <sub>GS(TH)</sub>	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}, I_{D} = 250 \mu A$	1.2	-	2.5	V
G3(111)		I <sub>D</sub> = 35A, V <sub>GS</sub> = 10V	-	0.007	0.009	
	Buria ta Carra Ca Baristana	I <sub>D</sub> = 35A, V <sub>GS</sub> = 4.5V	-	0.009	0.012	0
r <sub>DS(ON)</sub>	Drain to Source On Resistance	$I_D = 35A$ , $V_{GS} = 10V$ , $T_J = 175$ °C			0.015	$ \Omega$
Dvnamic	Characteristics	10				
C <sub>ISS</sub>	Input Capacitance		-	1260	-	рF
C <sub>OSS</sub>	Output Capacitance	$V_{DS} = 15V, V_{GS} = 0V,$	-	260	-	pF
C <sub>RSS</sub>	Reverse Transfer Capacitance	f = 1MHz	-	150	-	pF
R <sub>G</sub>	Gate Resistance	V <sub>GS</sub> = 0.5V, f = 1MHz	-	2.3	-	Ω
$Q_{g(TOT)}$	Total Gate Charge at 10V	V <sub>GS</sub> = 0V to 10V	-	23	31	nC
$Q_{g(5)}$	Total Gate Charge at 5V	$V_{GS} = 0V \text{ to } 5V$	-	13	17	nC
Q <sub>g(TH)</sub>	Threshold Gate Charge	$V_{DD} = 15V$	-	1.3	1.7	nC
Q <sub>gs</sub>	Gate to Source Gate Charge	$I_D = 35A$ $I_G = 1.0 \text{mA}$	-	3.8	-	nC
Q <sub>gs2</sub>	Gate Charge Threshold to Plateau	ig = 1.0mA	-	2.5	-	nC
Q <sub>gd</sub>	Gate to Drain "Miller" Charge		-	5.0	-	nC
	Characteristics (V <sub>GS</sub> = 10V)					
t <sub>ON</sub>	Turn-On Time		-	-	147	ns
t <sub>d(ON)</sub>	Turn-On Delay Time		-	8	-	ns
t <sub>r</sub>	Rise Time	V <sub>DD</sub> = 15V, I <sub>D</sub> = 35A	-	91	-	ns
t <sub>d(OFF)</sub>	Turn-Off Delay Time	$V_{GS} = 10V, R_{GS} = 10\Omega$	-	38	-	ns
t <sub>f</sub>	Fall Time		-	32	-	ns
t <sub>OFF</sub>	Turn-Off Time		-	-	108	ns
Drain-Sou	urce Diode Characteristics					
V <sub>SD</sub>	Source to Drain Diode Voltage	I <sub>SD</sub> = 35A	-	-	1.25	V
		I <sub>SD</sub> = 15A	-	-	1.0	V
t <sub>rr</sub>	Reverse Recovery Time	$I_{SD} = 35A$ , $dI_{SD}/dt = 100A/\mu s$	-	-	27	ns
Q <sub>RR</sub>	Reverse Recovered Charge	I <sub>SD</sub> = 35A, dI <sub>SD</sub> /dt = 100A/μs	-	-	14	nC

Notes:
 Package current limitation is 35A.
 Starting T<sub>J</sub> = 25°C, L = 0.14mH, I<sub>AS</sub> = 28A, V<sub>DD</sub> = 27V, V<sub>GS</sub> = 10V.





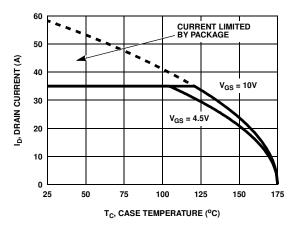


Figure 1. Normalized Power Dissipation vs Case Temperature

Figure 2. Maximum Continuous Drain Current vs Case Temperature

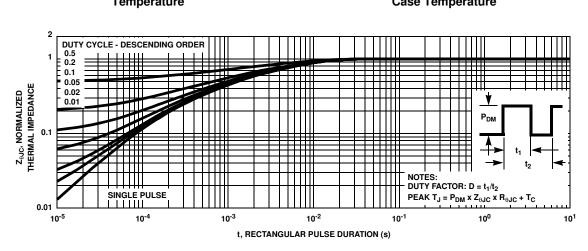


Figure 3. Normalized Maximum Transient Thermal Impedance

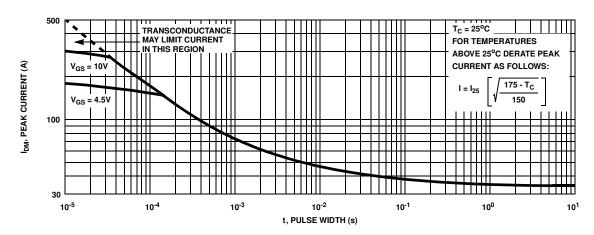
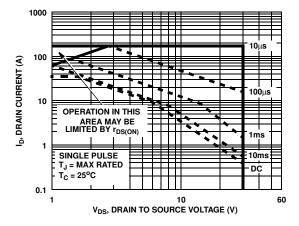


Figure 4. Peak Current Capability

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### Typical Characteristics $T_C = 25^{\circ}C$ unless otherwise noted



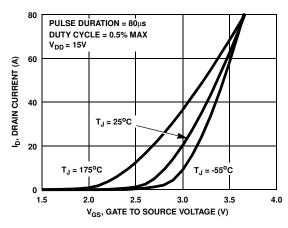
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Figure 5. Forward Bias Safe Operating Area

NOTE: Refer to Fairchild Application Notes AN7514 and AN7515

Figure 6. Unclamped Inductive Switching

Capability



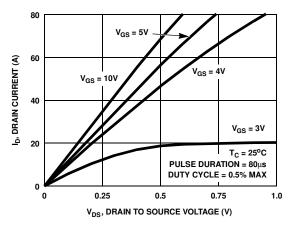
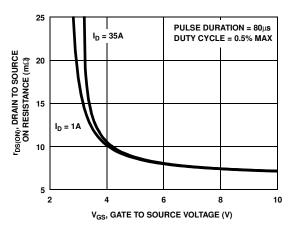


Figure 7. Transfer Characteristics

Figure 8. Saturation Characteristics



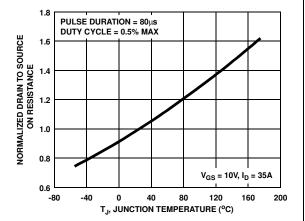


Figure 9. Drain to Source On Resistance vs Gate Voltage and Drain Current

Figure 10. Normalized Drain to Source On Resistance vs Junction Temperature

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### Typical Characteristics $T_C = 25^{\circ}C$ unless otherwise noted

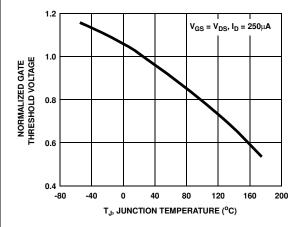


Figure 11. Normalized Gate Threshold Voltage vs
Junction Temperature

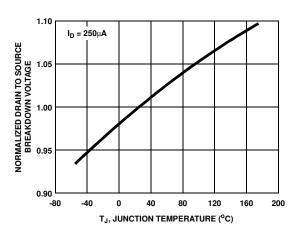


Figure 12. Normalized Drain to Source Breakdown Voltage vs Junction Temperature

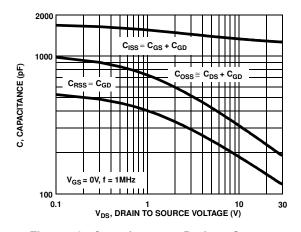


Figure 13. Capacitance vs Drain to Source Voltage

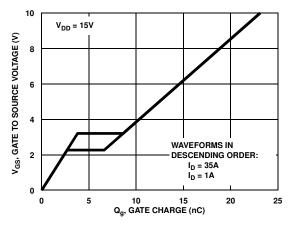


Figure 14. Gate Charge Waveforms for Constant Gate Current

### **Test Circuits and Waveforms**

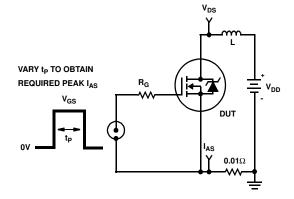


Figure 15. Unclamped Energy Test Circuit

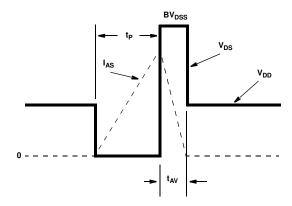


Figure 16. Unclamped Energy Waveforms

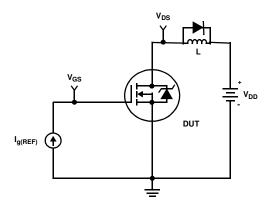


Figure 17. Gate Charge Test Circuit

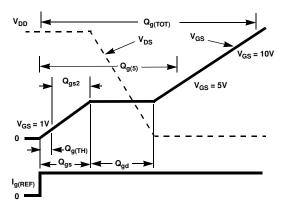


Figure 18. Gate Charge Waveforms

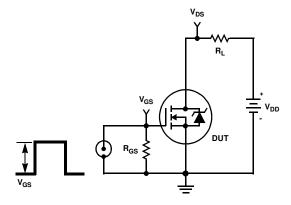


Figure 19. Switching Time Test Circuit

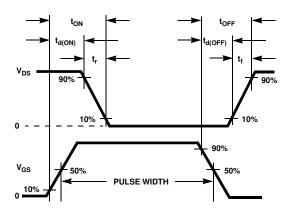


Figure 20. Switching Time Waveforms

### Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature,  $T_{JM}$ , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation,  $P_{DM}$ , in an application. Therefore the application's ambient temperature,  $T_A$  (°C), and thermal resistance  $R_{\theta JA}$  (°C/W) must be reviewed to ensure that  $T_{JM}$  is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}} \tag{EQ. 1}$$

In using surface mount devices such as the TO-252 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of  $P_{DM}$  is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- 2. The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the  $R_{\theta JA}$  for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeters square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\Theta JA} = 33.32 + \frac{23.84}{(0.268 + Area)}$$
 (EQ. 2)

Area in Inches Squared

$$R_{\theta JA} = 33.32 + \frac{154}{(1.73 + Area)}$$
 (EQ. 3)

Area in Centimeters Squared

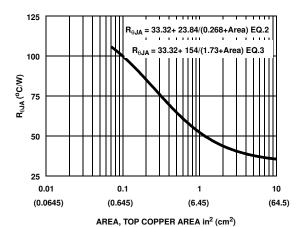
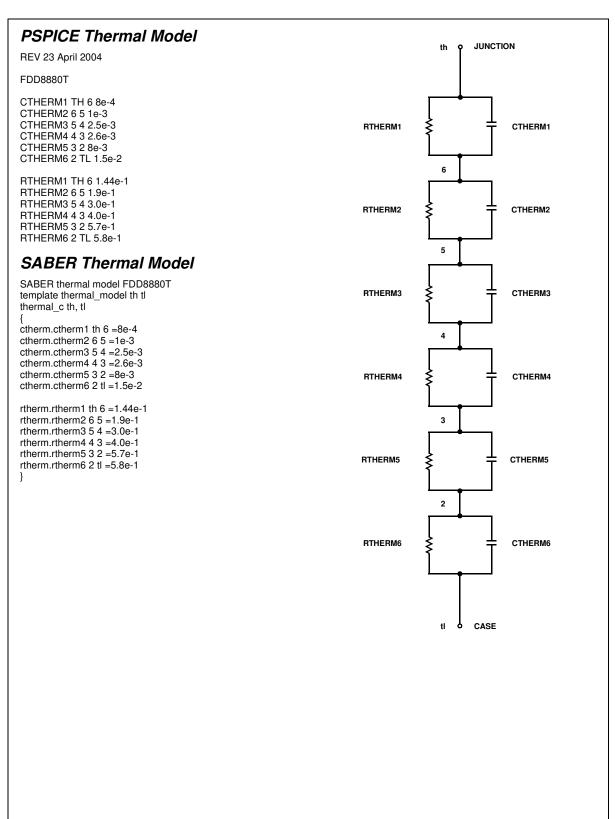


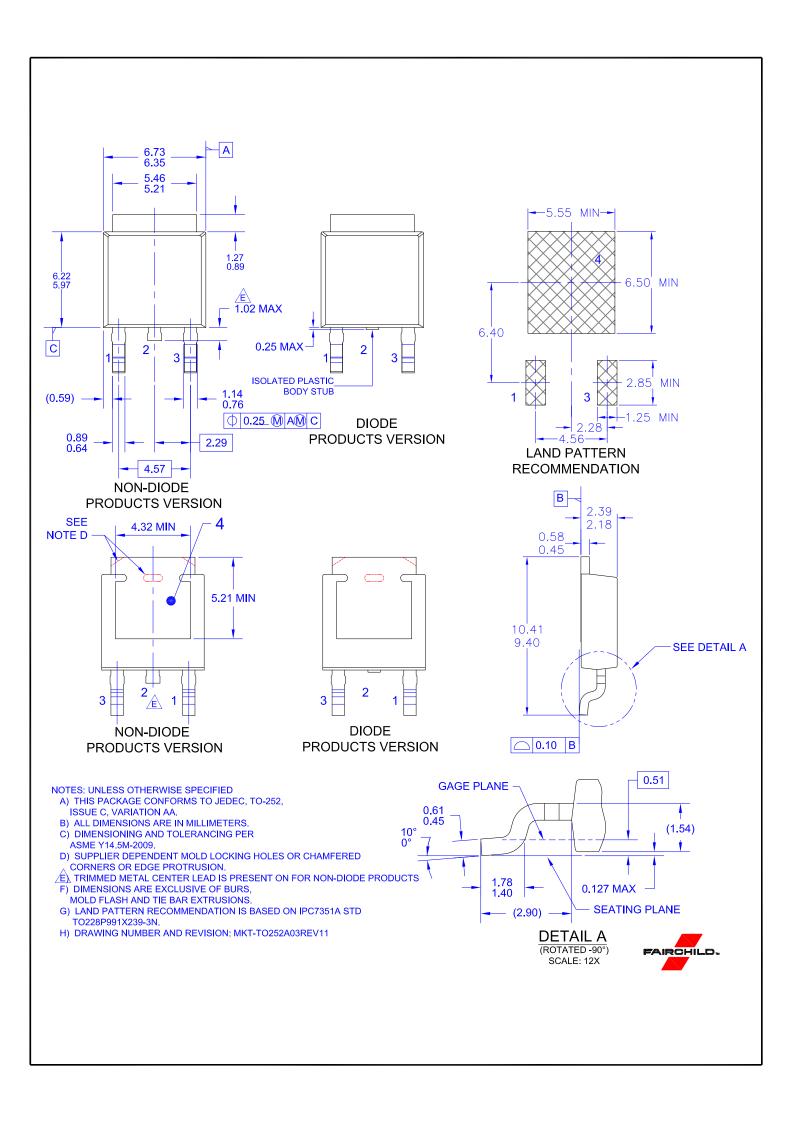
Figure 21. Thermal Resistance vs Mounting
Pad Area

#### **PSPICE Electrical Model** .SUBCKT FDD8880 2 1 3 ; rev April 2004 Ca 12 8 9.5e-10 Cb 15 14 9.5e-10 LDRAIN DPLCAP DRAIN Cin 6 8 1.15e-9 10 Dbody 7 5 DbodyMOD RLDRAIN RSLC1 Dbreak 5 11 DbreakMOD DBREAK T Dplcap 10 5 DplcapMOD FSI C 11 Ebreak 11 7 17 18 33.15 50 Eds 14 8 5 8 1 Egs 13 8 6 8 1 RDRAIN ■ DBODY **EBREAK ESG** Esa 6 10 6 8 1 **FVTHRES** Evthres 6 21 19 8 1 (19 8 Evtemp 20 6 18 22 1 MWFAK LGATE **EVTEMP** GATE **RGATE** \_\_\_\_ (18 22 **5** It 8 17 1 MMFD 9 20 MSTRO RI GATE Lgate 1 9 5.3e-9 LSOURCE CIN SOURCE Ldrain 2 5 1.0e-9 Lsource 3 7 1.7e-9 RSOURCE RLSOURCE RLgate 1 9 53 RBREAK RLďrain 2 5 10 13 8 14 13 18 RLsource 3 7 17 RVTEMP S1B Mmed 16 6 8 8 MmedMOD СВ 19 CA Mstro 16 6 8 8 MstroMOD IT 14 Mweak 16 21 8 8 MweakMOD VBAT EGS **EDS** Rbreak 17 18 RbreakMOD 1 8 Rdrain 50 16 RdrainMOD 3.2e-3 **RVTHRES** Rgate 9 20 2.2 RŠLC1 5 51 RSLCMOD 1e-6 RSLC2 5 50 1e3 Rsource 8 7 RsourceMOD 3.2e-3 Rvthres 22 8 RvthresMOD 1 Rvtemp 18 19 RvtempMOD 1 S1a 6 12 13 8 S1AMOD S1b 13 12 13 8 S1BMOD S2a 6 15 14 13 S2AMOD S2b 13 15 14 13 S2BMOD Vbat 22 19 DC 1 ESLC 51 50 VALUE={(V(5,51)/ABS(V(5,51)))\*(PWR(V(5,51)/(1e-6\*170),5))} .MODEL DbodyMOD D (IS=2E-12 IKF=10 N=1.01 RS=3.76e-3 TRS1=8e-4 TRS2=2e-7 + CJO=4.8e-10 M=0.55 TT=1e-17 XTI=2) .MODEL DbreakMOD D (RS=0.2 TRS1=1e-3 TRS2=-8.9e-6) .MODEL DplcapMOD D (CJO=5.5e-10 IS=1e-30 N=10 M=0.45) .MODEL MmedMOD NMOS (VTO=2.0 KP=10 IS=1e-30 N=10 TOX=1 L=1u W=1u RG=2.2) .MODEL MstroMOD NMOS (VTO=2.5 KP=170 IS=1e-30 N=10 TOX=1 L=1u W=1u) .MODEL MweakMOD NMOS (VTO=1.69 KP=0.05 IS=1e-30 N=10 TOX=1 L=1u W=1u RG=22 RS=0.1) .MODEL RbreakMOD RES (TC1=8.3e-4 TC2=-8e-7) .MODEL RdrainMOD RES (TC1=1.8e-3 TC2=8e-6) MODEL RSLCMOD RES (TC1=9e-4 TC2=1e-6) .MODEL RsourceMOD RES (TC1=5e-3 TC2=1e-6) .MODEL RvthresMOD RES (TC1=-1e-3 TC2=-8.2e-6) .MODEL RytempMOD RES (TC1=-2.6e-3 TC2=2e-7) .MODEL S1AMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-4 VOFF=-3.5) .MODEL S1BMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-3.5 VOFF=-4) .MODEL S2AMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-1.3 VOFF=-0.8) .MODEL S2BMOD VSWITCH (RON=1e-5 ROFF=0.1 VON=-0.8 VOFF=-1.3) **FNDS** Note: For further discussion of the PSPICE model, consult A New PSPICE Sub-Circuit for the Power MOSFET Featuring Global Temperature Options; IEEE Power Electronics Specialist Conference Records, 1991, written by William J. Hepp and C. Frank Wheatley.

#### SABER Electrical Model rev April 2004 template FDD8880 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=2e-12.ikf=10.nl=1.01.rs=3.76e-3.trs1=8e-4.trs2=2e-7.cjo=4.8e-10.m=0.55.tt=1e-17.xti=2) dp..model dbreakmod = (rs=0.2,trs1=1e-3,trs2=-8.9e-6) dp..model dplcapmod = (cjo=5.5e-10,isl=10e-30,nl=10,m=0.45) m..model mmedmod = $(type=_n, vto=2.0, kp=10, is=1e-30, tox=1)$ m..model mstrongmod = (type=\_n,vto=2.5,kp=170,is=1e-30, tox=1) m..model mweakmod = (type=\_n,vto=1.69,kp=0.05,is=1e-30, tox=1,rs=0.1) LDRAIN sw\_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-4,voff=-3.5) **DPLCAP** DRAIN sw\_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-3.5,voff=-4) 10 sw vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-1.3,voff=-0.8) RLDRAIN sw vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=-0.8,voff=-1.3) RSLC1 c.ca n12 n8 = 9.5e-10 51 RSLC2 € c.cb n15 n14 = 9.5e-10ISCI c.cin n6 n8 = 1.15e-9DBREAK 50 dp.dbody n7 n5 = model=dbodymod RDRAIN <u>6</u>8 dp.dbreak n5 n11 = model=dbreakmod FSG DBODY **FVTHRES** dp.dplcap n10 n5 = model=dplcapmod (<u>19</u>) **MWEAK** LGATE **EVTEMP** spe.ebreak n11 n7 n17 n18 = 33.15 <sub>GATE</sub> RGATE ММЕD 18 22 **EBREAK** spe.eds n14 n8 n5 n8 = 1 spe.egs n13 n8 n6 n8 = 1 **←**MSTRC RLGATE spe.esg n6 n10 n6 n8 = 1 LSOURCE spe.evthres n6 n21 n19 n8 = 1 CIN SOURCE 8 spe.evtemp n20 n6 n18 n22 = 1 RSOURCE RLSOURCE i.it n8 n17 = 1RBREAK I.lgate n1 n9 = 5.3e-9I.Idrain n2 n5 = 1.0e-9**₹RVTEMP** S1B oS2B I.Isource n3 n7 = 1.7e-919 CA IT (♠ 14 res.rlgate n1 n9 = 53 VBAT res.rldrain n2 n5 = 10 **EGS EDS** res.rlsource n3 n7 = 17 m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u **RVTHRES** m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u m.mweak n16 n21 n8 n8 = model=mweakmod. l=1u, w=1u res.rbreak n17 n18 = 1, tc1=8.3e-4,tc2=-8e-7 res.rdrain n50 n16 = 3.2e-3, tc1=1.8e-3,tc2=8e-6 res.rgate n9 n20 = 2.2res.rslc1 n5 n51 = 1e-6, tc1=9e-4,tc2=1e-6 res.rslc2 n5 n50 = 1e3res.rsource n8 n7 = 3.2e-3, tc1=5e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-1e-3,tc2=-8.2e-6 res.rvtemp n18 n19 = 1, tc1=-2.6e-3,tc2=2e-7 sw vcsp.s1a n6 n12 n13 n8 = model=s1amod sw\_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw\_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { |sc|: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))\*((abs(v(n5,n51)\*1e6/170))\*\*5))

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