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## Contact us

Tel: +86-755-8981 8866 Fax: +86-755-8427 6832
Email \& Skype: info@chipsmall.com Web: www.chipsmall.com Address: A1208, Overseas Decoration Building, \#122 Zhenhua RD., Futian, Shenzhen, China

# Full Function Synchronous Buck Power Block 

Integrated Power Semiconductors, Control IC \& Passives

## Features

- 3.3 V to 12 V input voltage ${ }^{(1)}$
- 20A maximum load capability, with no derating up to $T_{P C B}=90^{\circ} \mathrm{C}$
- 5 bit DAC settable, 0.925 V to 2 V output voltage range (2)
- Configurable down to $3.3 \mathrm{Vin} \&$ up to 3.3 Vout with simple external circuit (3)
- 200 kHz or 300 kHz nominal switching frequency
- Optimized for very low power losses
- Over \& undervoltage protection
- Adjustable lossless current limit
- Internal features minimize layout sensitivity *
- Very small outline $14 \mathrm{~mm} \times 14 \mathrm{~mm} \times 3 \mathrm{~mm}$

iP1001 Power Block


## Description

The iP1001 is a fully optimized solution for high current synchronous buck applications requiring up to 20A. The iP1001 is optimized for single-phase applications, and includes a full function fast transient response PWM control, with an optimized power semiconductor chip-set and associated passives, achieving benchmark power density. Very few external components are required, including output inductor, input \& output capacitors. Further range of operation to 3.3 Vin can be achieved with the addition of a simple external boost circuit, and operation up to 3.3 Vout can be achieved with a simple external voltage divider.
iPOWIR technology offers designers an innovative board space-saving solution for applications requiring high power densities. iPOWIR technology eases design for applications where component integration offers benefits in performance and functionality. iPOWIR technology solutions are also optimized internally for layout, heat transfer and component selection.


* Although, all of the difficult PCB layout and bypassing issues have been addressed with the internal design of the iPOWIR block, proper layout techniques should be applied for the design of the power supply board. There are no concerns about unwanted shutdowns common to switching power supplies, if operated as specified. The iPOWIR block will function normally, but not optimally without any additional input decoupling capacitors. Input decoupling capacitors should be added at Vin pin for stable and reliable long term operation. No additional bypassing is required on the Vdd pin. See layout guidelines in datasheet for more detailed information.


## Absolute Maximum Ratings

| Parameter | Symbol | Min | Typ | Max | Units | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ to PGND |  | -0.3 | - | 16.0 | V |  |
| $\mathrm{V}_{\mathrm{DD}}$ to PGND |  | -0.3 | - | 6.0 |  |  |
| $\mathrm{V}_{\mathrm{FS}}$ |  | -0.3 | - | $\mathrm{V}_{\mathrm{DD}}+0.3$ |  |  |
| $\mathrm{V}_{\mathrm{F}}$ |  | -0.3 | - | $\mathrm{V}_{\mathrm{DD}}+0.3$ |  |  |
| D0-D4 |  | -0.3 | - | $\mathrm{V}_{\mathrm{DD}}+0.3$ |  |  |
| PGOOD to PGND |  | -0.3 | - | 6.0 |  |  |
| ENABLE to PGND |  | -0.3 | - | 6.0 |  |  |
| ILIM |  | -0.3 | - | $\mathrm{V}_{\mathrm{DD}}+0.3$ |  |  |
| FREQ |  | -0.3 | - | $\mathrm{V}_{\mathrm{DD}}+0.3$ |  |  |
| Output RMS Current |  | - | - | 20 | A |  |
| Block Temperature | $\mathrm{T}_{\text {BLK }}$ | -40 | - | 125 | ${ }^{\circ} \mathrm{C}$ |  |

Recommended Operating Conditions

| Parameter | Symbol | Min | Typ | Max | Units | Conditions |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| Supply Voltage | $\mathrm{V}_{\mathrm{DD}}$ | 4.5 | - | 5.5 | V |  |
| Input Voltage Range (1) | $\mathrm{V}_{\mathbb{I N}}$ | 3.3 | - | 12 |  | With $4.5 \mathrm{~V}<\mathrm{V}_{\mathrm{DD}}<5.5 \mathrm{~V}$ |
| Output RMS Current from $\mathrm{V}_{\mathrm{SW}}(4)$ | Iout $_{\mathrm{VSW}}$ | - | - | 20 | A |  |
| Output Voltage Range ${ }^{(2)}$ | $\mathrm{V}_{\text {OUT }}$ | 0.925 | - | 2.0 | V | DAC Setting <br> see VID code, Table1. |

Electrical Specifications @ $\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V} \& \mathrm{~T}_{\mathrm{PCB}} 0^{\circ} \mathrm{C}-90^{\circ} \mathrm{C}$ (Unless otherwise specified)

| Parameter | Symbol | Min | Typ | Max | Units | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power Loss | $\mathrm{P}_{\text {Loss }}$ | - | 3.1 | 3.9 | W | $300 \mathrm{kHz}, 12 \mathrm{~V}_{\mathrm{IN}}, 1.3 \mathrm{Vout}, 20 \mathrm{~A}$ |
| Over Current Shutdown |  | - | 25 | - | A | $\begin{aligned} & \mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=1.3 \mathrm{~V}, \\ & \text { FREQ }=300 \mathrm{KHz}, \mathrm{R}_{\text {LIM }}=340 \mathrm{k} \end{aligned}$ |
| Soft Start Time |  | - | 1.8 | - | ms |  |
| Output Voltage Accuracy |  | -2 | - | 2 | \% | All DAC codes $T_{\text {BLK }}=-40^{\circ} \mathrm{C} \text { to } 125^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\text {F }}$ Input Resistance |  | - | 181 | - | $\mathrm{k} \Omega$ |  |
| Frequency | FREQ | - | 200 | - | kHz | freq pin connected to $V_{\text {DD }}$ |
|  |  | - | 300 | - |  | freq pin floating |
| $\mathrm{V}_{\mathrm{DD}}$ Undervoltage Lockout |  | - | 4.2 | - | V | 200 mV hysteresis |
| Output Undervoltage Shutdown Threshold |  | - | 0.8 | - | V |  |
| Output Undervoltage Protection Blanking Time |  | - | 20 | - | ms | ENABLE going high on start-up |
| Output Overvoltage Shutdown Threshold at $\mathrm{V}_{\mathrm{F}}$ |  | - | 2.25 | - | V | See OVP note in Design Guidelines |
| PGOOD Trip Threshold | PGOOD | - | $\mathrm{V}_{\mathrm{DAC}}-5 \%$ | - | V | At $\mathrm{V}_{\mathrm{F}}$ |
| PGOOD Leakage Current |  | - | 1 | - | $\mu \mathrm{A}$ | PGOOD output high <br> Forced to 5.5 V |
| PGOOD Output Low Voltage |  | - | - | 0.4 | V | $\mathrm{I}_{\text {sink }}=1 \mathrm{~mA}$ |
| Logic Input High Voltage |  | 2.4 | - | - | V | DO-D4, Enable |
| Logic Input Low Voltage |  | - | - | 0.8 | V | D0-D4, Enable |

International

Electrical Specifications (continued)

| Parameter | Symbol | Min | Typ | Max | Units | Conditions |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| $\mathrm{V}_{\mathrm{DD}}$ Operating Current | $\mathrm{I}_{\mathrm{VDD}}$ | - | 25 | - | mA | Enable High, 300 kHz |
| $\mathrm{V}_{\mathrm{DD}}$ Quiescent Current | $\mathrm{I}_{\mathrm{QVDD}}$ | - | 600 | - | $\mu \mathrm{A}$ | Shutdown mode |
| $\mathrm{V}_{\mathrm{IN}}$ Quiescent Current | $\mathrm{I}_{\mathrm{QVIN}}$ | - | - | 1 | mA | Enable Low, VIN = 12V |
| ILIM to SGND Internal Resistance |  | - | 300 | - | $\mathrm{k} \Omega$ | Measured ILIM pin to SGND |

## Notes :

(1) For Vin less than 4.5 V requires external $5 \mathrm{~V}_{\mathrm{DD}}$ supply.
(2) Can be modified to operate up to $3.3 \mathrm{~V}_{\text {out }}$, outside of DAC settable range. See Design Guidelines on how to set output voltage greater than 2 V .
(3) See design guidelines.
(4) See Fig. 5 for Recommended Operating Area


Fig 1. Power Loss vs Current


Fig 2. Safe Operating Area (SOA) vs $T_{P C B}$

## Adjusting the Power Loss and SOA curves for different operating conditions

To make adjustments to the power loss curves in Fig. 1, multiply the normalized value obtained from the curves in Figs. 3, or 4 by the value indicated on the power loss curve in Fig. 1. If multiple adjustments are required, multiply all of the normalized values together, then multiply that product by the value indicated on the power loss curve in Fig. 1. The resulting product is the final power loss based on all factors.

To make adjustments to the SOA curve in Fig. 2, determine the maximum allowed PCB temperature in Fig. 2 at the required operating current. Then, add the correction temperature from the normalized curves in Figs. 3 or 4 to find the final maximum allowable PCB temperature. When multiple adjustments are required, add all of the temperatures together, then add the sum to the PCB temperature indicated on the SOA graph to determine the final maximum allowable PCB temperature based on all factors.

Note: If input voltage $<5$ Vin nominal operation is required then first see Fig. 5 for maximum current capability limit.
Operating Conditions for the examples below:
$\begin{array}{ll}\text { Output Current }=20 \mathrm{~A} & \text { Input Voltage }=7 \mathrm{~V} \\ \text { Output Voltage }=2.5 \mathrm{~V} & \end{array}$

## Adjusting for Maximum Power Loss:

(Fig. 1) Maximum power loss $=5 \mathrm{~W}$
(Fig. 3) Normalized power loss for output voltage $\approx 1.14$
(Fig. 4) Normalized power loss for input voltage $\approx 0.89$
Adjusted Power Loss $=5 \mathrm{~W} \times 0.89 \times 1.14 \approx 5.07 \mathrm{~W}$

## Adjusting for SOA Temperature:

(Fig. 2) SOA PCB Temperature $=90^{\circ} \mathrm{C}$
(Fig. 3) Normalized SOA PCB Temperature for output voltage $\approx-4.5^{\circ} \mathrm{C}$
(Fig. 4) Normalized SOA PCB Temperature for input voltage $\approx 4^{\circ} \mathrm{C}$
Adjusted SOA PCB Temperature $=90^{\circ} \mathrm{C}+4^{\circ} \mathrm{C}-4.5^{\circ} \mathrm{C} \approx \underline{89.5{ }^{\circ} \mathrm{C}}$


Fig 3. Normalized Power Loss vs $\mathrm{V}_{\text {out }}$


Fig 5. Recommended Operating Area

| D4 | D3 | D2 | D1 | D0 | $\begin{gathered} \text { OUTPUT } \\ \text { VOLTAGE(V) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 0 | 2.00 |
| 0 | 0 | 0 | 0 | 1 | 1.95 |
| 0 | 0 | 0 | 1 | 0 | 1.90 |
| 0 | 0 | 0 | 1 | 1 | 1.85 |
| 0 | 0 | 1 | 0 | 0 | 1.80 |
| 0 | 0 | 1 | 0 | 1 | 1.75 |
| 0 | 0 | 1 | 1 | 0 | 1.70 |
| 0 | 0 | 1 | 1 | 1 | 1.65 |
| 0 | 1 | 0 | 0 | 0 | 1.60 |
| 0 | 1 | 0 | 0 | 1 | 1.55 |
| 0 | 1 | 0 | 1 | 0 | 1.50 |
| 0 | 1 | 0 | 1 | 1 | 1.45 |
| 0 | 1 | 1 | 0 | 0 | 1.40 |
| 0 | 1 | 1 | 0 | 1 | 1.35 |
| 0 | 1 | 1 | 1 | 0 | 1.30 |
| 0 | 1 | 1 | 1 | 1 | Shutdown* |
| 1 | 0 | 0 | 0 | 0 | 1.275 |
| 1 | 0 | 0 | 0 | 1 | 1.250 |
| 1 | 0 | 0 | 1 | 0 | 1.225 |
| 1 | 0 | 0 | 1 | 1 | 1.200 |
| 1 | 0 | 1 | 0 | 0 | 1.175 |
| 1 | 0 | 1 | 0 | 1 | 1.150 |
| 1 | 0 | 1 | 1 | 0 | 1.125 |
| 1 | 0 | 1 | 1 | 1 | 1.100 |
| 1 | 1 | 0 | 0 | 0 | 1.075 |
| 1 | 1 | 0 | 0 | 1 | 1.050 |
| 1 | 1 | 0 | 1 | 0 | 1.025 |
| 1 | 1 | 0 | 1 | 1 | 1.000 |
| 1 | 1 | 1 | 0 | 0 | 0.975 |
| 1 | 1 | 1 | 0 | 1 | 0.950 |
| 1 | 1 | 1 | 1 | 0 | 0.925 |
| 1 | 1 | 1 | 1 | 1 | Shutdown* |

* Shutdown : Upon receipt of the shutdown code (per VID code table above), both FETs are turned OFF and the output is discharged as the undervoltage protection is activated.

Table 1. VID Code Table (2)


Fig 6. Overcurrent adjustment settings using $R_{\text {LIM }}$

| Pin Name | Ball Designator | Pin Description |
| :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | $\begin{aligned} & \text { A9-A12, B9-B12, C9- } \\ & \text { C14, D9-D14, E9-E16, } \\ & \text { F9-F16, G9-G16 } \end{aligned}$ | Input voltage connection node. |
| NC | A1, A6-A7, A13-A15, В1, В6-B7, B13-B16, C3, C6-C7, C15-C16, D3-D4, D6, D15-D 16 E3-E6, F1-F5, G1-G5, H1-H5, J1-J2, J6-J8, K6-K 8, L6-L8, M6-M8, N4-N5, N7-N8, P4-P5, P7-P8, R6-R8, S6-S8 | No electrical connection. |
| $\mathrm{V}_{\text {sw }}$ | $\begin{aligned} & \text { H9-H14, J11-J14, K11- } \\ & \text { K14, L11-L14, N11- } \\ & \text { N14, M11-M14, P11- } \\ & \text { P14, R11-R14, S11-S14 } \end{aligned}$ | Output inductor connection node. |
| PGND | H15-H16, J15-J16, K9- <br> K10, K15-K16, L9- <br> L10, L15-L16, M9- <br> M10, M15-M16, N9- <br> N10, N15-N16, P9-P10, <br> P15-P16, R9-R10, R15- <br> R16, S9-S10, S15-S16 | Power ground. |
| $\mathrm{V}_{\text {DD }}$ | R4-R5, S4-S5 | Control Power connection node |
| SGND | A $2-\mathrm{A} 3, \mathrm{~B} 2-\mathrm{B} 3$ | Signal ground. |
| GNDS | E1 | Remote Ground Sense Pin. Connect to PGND for $\mathrm{V}_{\text {OUT }}>2 \mathrm{~V}$ |
| ENABLE | R3, S3 | Commands output ON or OFF. Active floating (internally pulled high). When logic low, the synchronous MOSFET is turned ON. |
| NC | R2, S2 | No electrical connection, internally pulled high, must leave floating. |
| PGOOD | R1, S 1 | Internally pulled-up to $\mathrm{V}_{\mathrm{DD}}$. |
| $\mathrm{V}_{\mathrm{F}}$ | C1-C2 | Output voltage feedback local sense. |
| $\mathrm{V}_{\mathrm{FS}}$ | D 1-D2 | Output voltage remote sense feedback signal. For greater than $2 \mathrm{~V}_{\text {OUT }}$, disconnect from remote load and connect to $\mathrm{V}_{\mathrm{F}}$. |
| D0 | P1-P2 | VID code setting D/A inputs. Internally pulled high. |
| D 1 | N1-N2 |  |
| D2 | M 1-M2 |  |
| D3 | L1-L2 |  |
| D4 | K 1-K2 |  |
| ILIM | A5, B5, C5 | Current limit threshold setting pin. See ILIM curve for external resistor values. |
| FREQ | A4, B4 | Switching frequency selector pin. Floating selects 300 kHz , tied to $\mathrm{V}_{\mathrm{DD}}$ selects 200 kHz . |

Table 2. Pin Description


Fig 7. Power loss test circuit

International


Fig 8. Recommended PCB Footprint (Top View)

## iP1001 User's Design Guidelines

The iP1001 is a 20A power block that consists of optimized power semiconductors, PWM control and its associated passive components. It is based on a synchronous buck topology and offers an optimized solution where space, efficiency and noise caused by stray parasitics are of concern. The iP1001 components are integrated in a ball grid array (BGA) package where the electrical and thermal conduction is accomplished through solder balls.

## FUNCTIONALDESCRIPTION

## $V_{\text {IN }}$

The standard iP1001 operating input voltage range is 5 V to 12 V . The input voltage can also be easily configured to run at voltages down to 3.3 V .

## FREQ

The PWM control is pseudo current mode. The ESR of the output filter capacitor is used for current sensing and the output voltage ripple developed across the ESR provides the PWM ramp signal.
iP1001 offers two switching frequency settings, 200 kHz and 300 kHz . At a given setting the switching frequency will remain relatively constant independent of load current.
$\mathrm{V}_{\mathrm{DD}}$ (+5V bias)
An external 5 V bias supply is required to operate the iP1001. In applications where input voltages are lower than 4.5 V , and where 5 V is not available, a special boost circuit is required to supply $\mathrm{V}_{\mathrm{DD}}$ with 5 V (as shown in the reference design).

## Soft Start, $\mathrm{V}_{\mathrm{DD}}$ UndervoItage Lockout

When $\mathrm{V}_{\mathrm{DD}}$ rises above 4.2 V a soft start is initiated by ramping the maximum allowable current limit. The ramp time is typically 1.8 ms . An external capacitor can be added across the current limit resistor from ILIM to PGND to provide up to 5 ms ramp time. Select the capacitor according to the $10 \mathrm{nf} / \mathrm{ms}$ rule.

PGOOD
The PGOOD comparator constantly monitors $\mathrm{V}_{\mathrm{F}}$ for undervoltage. A $5 \%$ drop in output voltage can cause PGOOD to go low. PGOOD pin is internally pulledup to $\mathrm{V}_{\mathrm{DD}}$ through a $100 \mathrm{~K}, 5 \%$ resistor. If it is desired to use the PGOOD signal to enable another stage using iP1001, then it is recommended to filter and buffer PGOOD to prevent transients appearing at the output from pulling PGOOD low.

## OVP (Output Overvoltage Protection)

If the overvoltage trip 2.25 V threshold is reached, the OVP is triggered, the circuit is shutdown and the bottom FET is latched on discharging the output filter capacitor. Pulling ENABLE low resets the latch. The overvoltage trip threshold is scaled accordingly, if output voltages greater than 2 V are set through voltage dividers.

## UVP (Output Undervoltage Protection)

The Output Undervoltage Protection trip threshold is fixed at 0.8 V . If ENABLE is pulled up and $V_{F}$ is below 0.8 V for a duration of $10-20 \mathrm{~ms}$, the PWM will be in a latched state, with the bottom FET latched on, and will not restart until ENABLE is recycled.

## DAC Converter (D0-D4)

The output voltage is programmed through a 5 -bit DAC (see the VID code in table 1). The output voltage can be programmed from 0.925 V to 2 V . To eliminate external resistors, the DAC pins are internally pulled up. To set for output voltages above 2 V , the DAC must be set to 2 V and a resistor divider, $R 3 \& R 4$ (see Fig 10.), is used. The values of the resistors are selected using equation 1.

Equation 1: $\quad$ Vout $=V_{F} \times(1+R 3 / R 4)$
where $V_{F}$ is equal to the DAC setting
and R 4 is recommended to be $\sim 1 \mathrm{k} \Omega$

| ENABLE | Bottom <br> FET | Mode | Comments |
| :---: | :---: | :---: | :--- |
| Low | ON | Shutdown |  |
| High | OFF | Shutdown | DAC code $=$ X1111, Both FETs <br> are turned OFF. |
| High | Switching | PWM (Running) | Fault latch set by OVP or UVP. <br> This mode will sustain until $V_{\text {DD }}$ <br> is cycled or ENABLE is reset. |
| High | ON | Fault |  |

Table 3 - iP1001 Operating Truth Table

DESIGNPROCEDURE

## Inductor Selection

The inductor is selected according to the following expression.

$$
\begin{aligned}
& \mathrm{L}=\mathrm{V}_{\text {OUT }} \times(1-\mathrm{D}) /\left(\mathrm{fsw} \times \Delta \mathrm{I}_{\mathrm{L}}\right) \\
& \text { where, } \mathrm{D}=\mathrm{V}_{\text {oUT }} / \mathrm{V}_{\text {IN }} \\
& \mathrm{V}_{\text {ouT }} \text { is the output voltage in Volts, } \\
& \text { fsw is the switching frequency in } \mathrm{kHz}, \\
& \Delta \mathrm{I}_{\mathrm{L}} \text { is the output inductor ripple current. }
\end{aligned}
$$

The inductor value should be selected from $0.8 \mu \mathrm{H}$ to $2.0 \mu \mathrm{H}$ range.

## Output Capacitor Selection

Use tantalum or POSCAP type capacitors for iP1001. Selection of the output capacitors depends on several factors.

- Low effective ESR for ripple and load transient requirements.
- Stability.

To support the load transients and to stay within a specified voltage dip $\Delta V$ due to the transients, ESR selection should satisfy the following equation:

$$
\mathrm{R}_{\mathrm{ESR}} \leq \Delta \mathrm{V} / \Delta \mathrm{I}
$$

where, $\Delta l$ is the transient load step
If output voltage ripple is required to be maintained at specified levels then, the following expression should be used to select the output capacitors.

$$
\mathrm{R}_{\mathrm{ESR}} \leq \mathrm{V}_{\mathrm{p}-\mathrm{p}} / \Delta \mathrm{I}_{\mathrm{L}}
$$

where, $V_{p-p}$ is the peak to peak output voltage ripple.
The value of the output capacitor ESR zero frequency also determines stability. The value of the ESR zero frequency is calculated by the expression:

$$
R_{\text {ESR }}=1 /\left(2 \pi \times f_{E S R} \times C_{\text {OUT }}\right)
$$

A $470 \mu \mathrm{~F}$ POSCAP capacitor has a maximum $35 \mathrm{~m} \Omega$ of ESR which provides 9.7 kHz zero frequency.
The ESR zero frequency must be set below 12 kHz . This value is calculated assuming the capacitor datasheet maximum ESR value.

Example:
To determine the amount of capacitance to meet a 30 mVp -p output ripple, with 4A inductor current ripple requirement.

The calculated ESR will be $=30 \mathrm{mV} / 4 \mathrm{~A}=$ $7.5 \mathrm{~m} \Omega$. This will require $5 \times 470 \mathrm{uF}$ POSCAP capacitors. The total ESR will result in a 9.7 kHz zero frequency.

## For stable operation:

- Set the resonant frequency fo of the output inductor and capacitor between 2 kHz and 4 kHz . The resonant frequency is calculated using the following expression:

$$
\mathrm{f}_{\mathrm{o}}=1 /(2 \pi \times(\sqrt{\mathrm{LC}}))
$$

- Select the output inductor value between $0.8 \mu \mathrm{H}$ to $2.0 \mu \mathrm{H}$ and the output capacitance between $1880 \mu \mathrm{~F}(4 \mathrm{x} 470 \mu \mathrm{~F}$ ) and $5600 \mu \mathrm{~F}(12 \mathrm{x} 470 \mu \mathrm{~F}$ )
- Set the minimum output ripple voltage to be greater than $0.5 \%$ of the output voltage. Select the capacitor by ESR and by voltage rating rather than capacitance.


## External Input Capacitor Selection

The switching currents impose RMS current requirements on the input capacitors. The following expression allows the selection of the input capacitors, based on the input RMS current:

$$
I_{\text {RMS }}=I_{\text {LOAD }} \times(\sqrt{ } D \times(1-D))
$$

where, $\mathrm{D}=\mathrm{V}_{\text {OUT }} / V_{\text {IN }}$

## Application Issues

## Setting $\mathrm{V}_{\text {out }}$ above 2V

In certain applications where the output voltage is required to be set higher than the maximum DAC code setting of 2 V , it is possible to use an external resistive voltage divider which, for accuracy, needs to have $1 \%$ or better tolerance. The switching frequency should be set at 200 kHz by connecting the FREQ pin to $\mathrm{V}_{\mathrm{DD}}$. Also, the output voltage should never be set higher than 3.3 V with a $\mathrm{V}_{\text {IN }}$ minimum of 5 V , or 2.5 V with a $\mathrm{V}_{1 \mathbb{N}}$ minimum of 3.3 V . The DAC code should be set to 2 V and the following equation used to select the resistors:

$$
V_{\text {OUT }}=V_{F} \times(1+R 3 / R 4)
$$

See the reference design for reference designators.
Note that the impedance at $\mathrm{V}_{\mathrm{F}}$ is $180 \mathrm{~K} \Omega \pm 35 \%$. It is recommended that R 3 be calculated assuming a value of $1 \mathrm{k} \Omega$ for R 4 . Connect $\mathrm{V}_{\mathrm{Fs}}$ to $\mathrm{V}_{\mathrm{F}}$ and GNDS to PGND.

Duty Cycle $\mathrm{D}=\mathrm{V}_{\text {OUT }} / \mathrm{V}_{\text {IN }}>50 \%$
For duty cycles $>50 \%$ the switching frequency should be set at 200 kHz . 300 kHz switching frequency can be selected if the output is less than 2 V and the duty cycle is $<50 \%$.
For duty cycles $>50 \%$, add external compensation ramp from the Vsw terminal of the iP1001 device as shown in the reference design through R9 resistor and C21 capacitor (Fig 10a.). For optimum performance maintain a RC time constant of approximately $5 \mu \mathrm{~s}$.

## Layout Guidelines

For stable and noise free operation of the whole power system it is recommended that the designer uses to the following guidelines.

1. Follow the layout scheme presented in Fig.9. Make sure that the output inductor L1 is placed as close to the iP1001 as possible to prevent noise propagation that can be caused by switching of power at the switching node $V_{S W}$, to sensitive circuits.
2. Provide a mid-layer solid ground with connections to the top layer through vias. The two PGND pads of the iP1001 also need to be connected to the same ground plane through vias.
3. Do not connect SGND pins of the iP1001 to PGND.
4. To increase power supply noise immunity, place input and output capacitors close to one another, as shown in the layout diagram. This will provide short high current paths that are essential at the ground terminals.
5. Although there is a certain degree of $\mathrm{V}_{\mathrm{IN}}$ bypassing inside the iP1001, the external input decoupling capacitors should be as close to the device as possible.
6. In situations where the load is located at an appreciable distance from the iP1001 block, it is recommended that at least one or two capacitors be placed close to the iP1001 to derive the $\mathrm{V}_{\mathrm{F}}$ signal.
7. The $\mathrm{V}_{\mathrm{F}}$ connection to the output capacitors should be as short as possible and should be routed as far away from noise generating traces as possible.
8. $\mathrm{V}_{\mathrm{FS}}$ \& GNDS pins need to be connected at the load for remote sensing. If remote sensing is not used connect $V_{F S}$ to $V_{F}$ and GNDS to PGND.
9. Refer to IR application note AN-1029 to determine what size vias and what copper weight and thickness to use when designing the PCB.


Fig 9. iP1001 suggested layout

## iP1001 Reference Design

The schematics in Fig.10a \& 10b and complete Bill of Materials in Table 4 are provided as a reference design to enable a preliminary evaluation of iP 1001. They represent a simple method of applying the iP1001 solution in a synchronous buck topology.
Fig. 10a shows the implementation for $<5 \mathrm{~V}_{\text {IN }}$ nominal applications, and Fig. 10b shows the implementation for $5 \mathrm{~V}_{\text {IN }}-12 \mathrm{~V}_{\text {IN }}$ nominal applications.

The connection pins are provided through the solder balls on the bottom layer of the package. A total power supply solution is presented with the addition of inductor L1 and the output capacitors C11-C14. Input capacitors C1-C10 are for bypassing in the $5 \mathrm{~V}_{\text {IN }}-12 \mathrm{~V}_{\text {IN }}$ application, but only C1-C3 are required for $<5 \mathrm{~V}_{\text {IN }}$ applications (refer to the BOM for values). Switches 1-5 of SW1 are used to program the output voltage. Refer to the VID table provided in this datasheet for the code that corresponds to the desired output voltage. Resistors R2 \& R4 need to be removed for operation at standard VID levels ( $0.925 \mathrm{~V}-2.0 \mathrm{~V}$, leave R3 $=0 \Omega$ ). Switch 8 of SW1 enables the output when floating (internally pulled high). The $5 \mathrm{~V} \mathrm{~V}_{\mathrm{DD}}$ power terminal and input power terminals are provided as separate inputs. They can be connected together if the application requires only 5 V nominal input voltage.

The reference design also offers a higher output voltage option for greater than 2.0 V , up to 3.3 V . For output voltages above 2V, the DAC setting must be set to 2 V , and then select resistors R3 \& R4 per Equation 1 on page 10 for the desired output voltage. Remove R5 and connect $V_{F}$ to $V_{F S}$ through R2, where R2 $=0 \Omega$. In this case, GNDS should be referenced to PGND. Tighter regulation can be achieved by using resistors with less than $1 \%$ tolerance. For Vin $<5 \mathrm{~V}$ and Vout $>2 \mathrm{~V}$, the frequency select pin (FREQ) must be set to 200 kHz (connected to $\mathrm{V}_{\text {DD }}$ ).

For applications with $\mathrm{V}_{\text {IN }}<5 \mathrm{~V}$ and where there is no auxiliary 5 V available, connections JP2 and JP3 must be provided in order to enable the boost circuit. This will provide $5 \mathrm{~V} \mathrm{~V}_{\mathrm{DD}}$ necessary for the iP1001 internal logic to function. The boost circuit will convert 3.3 V input voltage to 5 V , to power the $V_{\text {DD }}$, and will provide enough power to supply the internal logic for up to five iP1001 power blocks.


Fig 10a. - Reference Design Schematic For $<4.5 \mathrm{~V}_{\text {IN }}$


Fig 10b. - Reference Design Schematic For $5 \mathrm{~V}_{\mathrm{IN}}-12 \mathrm{~V}_{\mathrm{IN}}$ Nominal

IRDCiP1001-A (For operation $<4.5 \mathrm{~V}_{\text {iv }}$ )

| Designator | Value | Part Type | Footprint | Mfr. | Mfr. P/N |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1, C3, C5 | 100uF | Capacitor, 6.3V, 20\%, X5R | 1812 | TDK | C4532X5R0J107MT |
| C2, C4, C6, C7, C8, C9, C10, C15 |  | Not Installed | - | - |  |
| C11, C12, C13, C14 | 470uF | Capacitor, 6.3V, 20\%, Tantalum | 7343 | Sanyo | 6TPB470M |
| C16, C19 | 0.100uF | Capacitor, 50V, 10\%, X7R | 1206 | Novacap | 1206B104K500N |
| C17, C18 | 10.0uF | Capacitor, 16V, 10\%, X5R | 1210 | TDK | C3225X5R1C106KT |
| C20 | 1.00uF | Capacitor, 10V, 10\%, X7R | 0805 | MuRata | GRM40X7R105K010 |
| C21 | 47.0pF | Capacitor, 50V, 5\%, C0G | 1206 | MuRata | GRM42-6C0G470J050A |
| D1 | 40 V | Schottky Diode, 40V, 2.1A | D-64 | International Rectifier | 10MQ040N |
| JP1, JP2, JP3 | - | Test Point | - | Samtec | TSW-102-07-LS |
| JP1-1, JP2-1, JP3-1 | - | Shunt | - | Samtec | SNT-100-BKT |
| L1 | 1.06 uH | Inductor, 16A, 20\%, Ferrite | SMT | Panasonic | ETQP6F1R1BFA |
| L2 | 22 uH | Inductor, 0.68A, 20\%, Ferrite | SMT | Sumida | CR43-220 |
| R1 | $0 \Omega$ | Resistor, $0 \Omega$ Jumper | 2716 | Isotek Corp | SMT-R000 |
| R2 | - | For <2Vout, Not installed For $>2$ Vout, Resistor, $0 \Omega$ Jumper | SMT | - | - |
| R3 | - | For <2Vout, Resistor, $0 \Omega$ Jumper For $>2$ Vout see formula for value | SMT | - | - |
| R4 | - | For <2Vout, Not installed For $>2$ Vout recommend $1 \mathrm{k} \Omega$ see formula for detail | SMT | - | - |
| R5 | - | For <2Vout, Resistor, 0 $\Omega$ Jumper For >2Vout, Not installed | 1206 | Panasonic | ERJ-8GEY0R00 |
| R6 | $0 \Omega$ | Resistor, $0 \Omega$ Jumper | 1206 |  | - |
| R7 | 340k | Resistor, 340k $\Omega$, 1\% $340 \mathrm{k} \Omega$ sets for 20A limit. See ILIM formula for other values | 1206 | ROHM | MCR18EZHF3403 |
| R8 | 100k $\Omega$ | Resistor, 100k』, $5 \%$ | 1206 | ROHM | MCR18EZHJ104 |
| R9 | 91k | Resistor, 91k ${ }^{\text {, } 5 \%}$ | 1206 | ROHM | MCR18EZHJ913 |
| SW1 |  | 8 -position DIP switch | SMT | C\&K Components | SD08H0SK |
| TP1, TP3 | - | Not Installed | - | - | - |
| TP2, TP4, TP5 | - | Test Point | - | Keystone | 1502-2 |
| U1 | - | Power Block | SSBGA $14 \mathrm{~mm} \times 14 \mathrm{~mm}$ | International Rectifier | iP1001 |
| U2 | - | IC, Step-Up DC-DC Converter, 0.5A | 8uMAX | Maxim | MAX1675EUA |

IRDCiP1001-B (For operation $5 \mathrm{~V}_{\text {is }}$ to $12 \mathrm{~V}_{\text {iN }}$ )

| Designator | Value | Part Type | Footprint | Mfr. | Mfr. P/N |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C1 C2 C3 C4 C5 C6 C7 C8 C9 C10 | 10.0uF | Capacitor, 25V, 10\%, X5R | 1812 | MuRata | GRM43-2X5R106K25A |
| C11 C12 C13 C14 | 470uF | Capacitor, 6.3V, 20\%, Tantalum | 7343 | Sanyo | 6TPB470M |
| C16 | 0.100uF | Capacitor, 50V, 10\%, X7R | 1206 | Novacap | 1206B104K500N |
| C15, C17, C18, C19, C20, C21 | - | Not Installed | - | - | - |
| D1 | 40V | Schottky Diode, 40V, 2.1A | D-64 | International Rectifier | 10MQ040N |
| JP1, JP2, JP3 | - | Not Installed | - | - | - |
| JP1-1, JP2-1, JP3-1 | - | Not Installed | - | - | - |
| L1 | 1.06uH | Inductor, 16A, 20\%, Ferrite | SMT | Panasonic | ETQP6F1R1BFA |
| L2 | - | Not Installed | - | - | - |
| R1 | $0 \Omega$ | Resistor, $0 \Omega$ Jumper | 2716 | Isotek Corp | SMT-R000 |
| R2 | - | For <2Vout, Not installed For $>2$ Vout, Resistor, $0 \Omega$ Jumper | SMT | - | - |
| R3 | - | For <2Vout, Resistor, $0 \Omega$ Jumper For $>2$ Vout see formula for value | SMT | - | - |
| R4 | - | $\begin{gathered} \text { For }<2 \text { Vout, Not installed } \\ \text { For }>2 \text { Vout recommend } 1 \mathrm{k} \Omega \\ \text { see formula for detail } \\ \hline \end{gathered}$ | SMT | - | - |
| R5 | - | For <2Vout, Resistor, $0 \Omega$ Jumper For $>2$ Vout, Not installed | 1206 | Panasonic | ERJ-8GEY0R00 |
| R6 | $0 \Omega$ | Resistor, $0 \Omega$ Jumper | 1206 | - | - |
| R7 | 340 k ת | Resistor, $340 \mathrm{k} \Omega$, 1\% $340 \mathrm{k} \Omega$ sets for 20A limit. <br> See ILIM formula for other values | 1206 | ROHM | MCR18EZHF3403 |
| R8, R9 | - | Not Installed | - | - | - |
| SW1 | - | 8 -position DIP switch | SMT | C\&K Components | SD08H0SK |
| TP1 TP2 TP4 TP5 | - | Test Point | - | Keystone | 1502-2 |
| TP3 | - | Not Installed | - | - | - |
| U1 | - | Power Block | $\begin{gathered} \text { SSBGA } \\ 14 \mathrm{~mm} \times 14 \mathrm{~mm} \end{gathered}$ | International Rectifier | iP1001 |
| U2 | - | Not Installed | - | - | - |

Table 4 - Reference Design Bill of Materials


## Mechanical Drawing

Refer to the following application notes for detailed guidelines and suggestions when implementing iPOWIR Technology products:

AN-1028: Recommended Design, Integration and Rework Guidelines for International Rectifier's iPOWIR Technology BGA Packages
This paper discusses the assembly considerations that need to be taken when mounting iPOWIR BGA's on printed circuit boards. This includes soldering, pick and place, reflow, inspection, cleaning and reworking recommendations.

## AN-1029: Optimizing a PCB Layout for an iPOWIR Technology Design

This paper describes how to optimize the PCB layout design for both thermal and electrical performance. This includes placement, routing, and via interconnect suggestions.

AN-1030: Applying iPOWIR Products in Your Thermal Environment
This paper explains how to use the Power Loss and SOA curves in the data sheet to validate if the operating conditions and thermal environment are within the Safe Operating Area of the iPOWIR product.


NOTES:

1. OUTLINE CONFORMS TO EIA-481 \& EIA-541.



NOTES:

1. CONTROLING DIMENSION: MILIMETER.
2. ALL DIMENSIONS ARE SHOWN IN MILLIMETERS (INCHES).
3. OUTLINE CONFORMS TO EIA-481 \& EIA-541.

## Tape \& Reel Information

Data and specifications subject to change without notice. This product has been designed and qualified for the industrial market. Qualification Standards can be found on IR's Web site.
IR WORLD HEADQUARTERS: 233 Kansas St., El Segundo, California 90245, USA Tel: (310) 252-7105
TAC Fax: (310) 252-7903
Visit us at www.irf.com for sales contact information.03/02

