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# Dual and Quad 50MHz, 800V/µs Op Amps

#### **FEATURES**

- 50MHz Gain Bandwidth
- 800V/µs Slew Rate
- 5mA Maximum Supply Current per Amplifier
- Unity-Gain Stable
- C-Load<sup>™</sup> Op Amp Drives All Capacitive Loads
- 9nV/√Hz Input Noise Voltage
- 1mV Maximum Input Offset Voltage
- 1µA Maximum Input Bias Current
- 250nA Maximum Input Offset Current
- ±13V Minimum Output Swing into 500Ω
- ±3.2V Minimum Output Swing into 150Ω
- 4.5V/mV Minimum DC Gain, R<sub>1</sub>=1k
- 60ns Settling Time to 0.1%, 10V Step
- 0.2% Differential Gain,  $A_{V}=2$ ,  $R_{I}=150\Omega$
- 0.3° Differential Phase,  $A_V=2$ ,  $R_I=150\Omega$
- Specified at ±2.5V, ±5V, and ±15V

## **APPLICATIONS**

- Wideband Amplifiers
- Buffers
- Active Filters
- Video and RF Amplification
- Cable Drivers
- Data Acquisition Systems

### DESCRIPTION

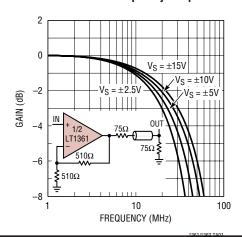
The LT1361/LT1362 are dual and quad low power high speed operational amplifiers with outstanding AC and DC performance. The amplifiers feature much lower supply current and higher slew rate than devices with comparable bandwidth. The circuit topology is a voltage feedback amplifier with matched high impedance inputs and the slewing performance of a current feedback amplifier. The high slew rate and single stage design provide excellent settling characteristics which make the circuit an ideal choice for data acquisition systems. Each output drives a  $500\Omega$  load to  $\pm 13 \text{V}$  with  $\pm 15 \text{V}$  supplies and a  $150\Omega$  load to  $\pm 3.2 \text{V}$  on  $\pm 5 \text{V}$  supplies. The amplifiers are stable with any capacitive load making them useful in buffer or cable driving applications.

The LT1361/LT1362 are members of a family of fast, high performance amplifiers using this unique topology and employing Linear Technology Corporation's advanced bipolar complementary processing. For a single amplifier version of the LT1361/LT1362 see the LT1360 data sheet. For higher bandwidth devices with higher supply currents see the LT1363 through LT1365 data sheets. For lower supply current amplifiers see the LT1354 to LT1359 data sheets. Singles, duals, and quads of each amplifier are available.

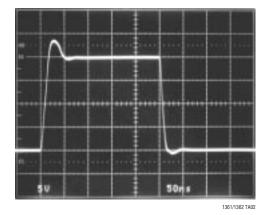
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## TYPICAL APPLICATION

Cable Driver Frequency Response



 $A_V = -1$  Large-Signal Response

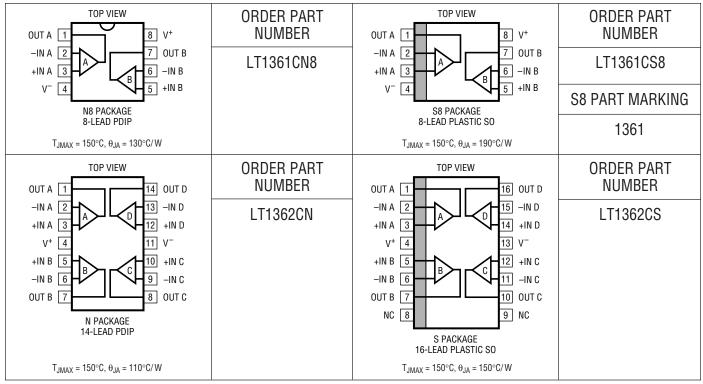


## **ABSOLUTE MAXIMUM RATINGS** (Note 1)

Total Supply Voltage (V <sup>+</sup> to V <sup>-</sup> )	36V
Differential Input Voltage	
(Transient Only) (Note 2)	±10V
Input Voltage	±V <sub>S</sub>
Output Short-Circuit Duration (Note 3)	

Operating Temperature Range (Note 8) ...-40°C to 85°C Specified Temperature Range (Note 9) ...-40°C to 85°C Maximum Junction Temperature (See Below)

## PACKAGE/ORDER INFORMATION



Consult factory for Industrial and Military grade parts.

## **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	(Note 4)	±15V		0.3	1.0	mV
			±5V		0.3	1.0	mV
			±2.5V		0.4	1.2	mV
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V		80	250	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V		0.3	1.0	μА
e <sub>n</sub>	Input Noise Voltage	f = 10kHz	±2.5V to ±15V		9		nV/√Hz
in	Input Noise Current	f = 10kHz	±2.5V to ±15V		0.9		pA/√Hz
R <sub>IN</sub>	Input Resistance	$V_{CM} = \pm 12V$	±15V	20	50		MΩ
	Input Resistance	Differential	±15V		5		MΩ
C <sub>IN</sub>	Input Capacitance		±15V		3		pF



# **ELECTRICAL CHARACTERISTICS** $T_A = 25^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted.

Input Voltage Range	SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	MIN TYP	MAX	UNITS
Input Voltage Range		Input Voltage Range +					
Input Voltage Range							
150				±2.5V	0.5 1.1		
CMRR   Common Mode Rejection Ratio   V <sub>CM</sub> = ±12V		Input Voltage Range –					
CMBR         Common Mode Rejection Ratio         V <sub>CM</sub> = ±12V V <sub>CM</sub> = ±25V							
No.		<u> </u>				-0.5	
PSRR	CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$				
PSRR   Power Supply Rejection Ratio   V <sub>S</sub> = ±2.5V to ±15V   93   105   dB							
Ayol.   Large-Signal Voltage Gain   Voltage Gain   Voltage 10V, RL = 500Ω   ±15V   3.0   6.5   VimV   Voltage 210V, RL = 500Ω   ±15V   3.0   6.5   VimV   Voltage 22.5V, RL = 150Ω   ±5V   3.0   6.4   VimV   Voltage 22.5V, RL = 150Ω   ±5V   1.5   4.2   VimV   Voltage 22.5V, RL = 150Ω   ±5V   1.5   4.2   VimV   Voltage 22.5V, RL = 150Ω   ±2.5V   2.5   5.2   VimV   Voltage 22.5V, RL = 150Ω   ±2.5V   1.3   5.1   3.9   ±4V   RL = 500Ω. Vim = ±40mV   ±15V   3.1   3.0   3.6   ±4V   RL = 500Ω. Vim = ±40mV   ±15V   3.2   3.8   ±4V   RL = 500Ω. Vim = ±40mV   ±5V   3.2   3.8   ±4V   RL = 500Ω. Vim = ±40mV   ±5V   3.2   3.8   ±4V   Vim = ±3.2V   ±5V   2.6   3.4   mA   MA   MA   MA   MA   MA   MA   MA	PSRR	Power Supply Rejection Ratio					
Voint = ±10V, Ri_ = 500Ω		1177		+15V			
Vout = ±2.5V, Ri_ = 500Ω	AVUL	Large orginal voltage dam					
Vout							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							V/mV
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			$V_{OUT} = \pm 1V$ , $R_L = 500\Omega$	±2.5V	2.5 5.2		V/mV
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$V_{OUT}$	Output Swing					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Output Current	- "				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	IOUT	Output Current					
Sign   Sign   Rate   A <sub>V</sub> = -2, (Note 5)	Isc	Short-Circuit Current		-			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	Slew Rate		±15V	600 800		V/us
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			, , , , , , , , , , , , , , , , , , , ,				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Full Power Bandwidth	10V Peak, (Note 6)				MHz
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			3V Peak, (Note 6)	±5V	18.6		MHz
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	GBW	Gain Bandwidth	f = 200kHz				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{ c c c c c c } \hline & Overshoot & A_V = 1, 0.1V & \pm 15V & 35 & \% \\ \hline & Propagation Delay & 50\% \ V_{IN} \ to \ 50\% \ V_{OUT}, 0.1V & \pm 15V & 5.2 & ns \\ \hline & & & & & & & & & & & & & \\ \hline & & & &$	$t_r$ , $t_f$	Rise Time, Fall Time	A <sub>V</sub> = 1, 10%-90%, 0.1V				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		Overally and	0.40				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Uversnoot	$A_V = 1, 0.1V$				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		Dropagation Daloy	500/ V +o 500/ V 0.1V				
$ \begin{array}{ c c c c c c } \hline t_S & Settling Time & 10V Step, 0.1\%, A_V = -1 & \pm 15V & 60 & ns \\ 10V Step, 0.01\%, A_V = -1 & \pm 15V & 90 & ns \\ 5V Step, 0.1\%, A_V = -1 & \pm 5V & 65 & ns \\ \hline \\ Differential Gain & f = 3.58MHz, A_V = 2, R_L = 150\Omega & \pm 15V & 0.20 & \% \\ & \pm 5V & 0.20 & \% & 0.20 & \% \\ & f = 3.58MHz, A_V = 2, R_L = 1k & \pm 15V & 0.04 & \% \\ & \pm 5V & 0.02 & \% & 0.02 & \% \\ \hline \\ Differential Phase & f = 3.58MHz, A_V = 2, R_L = 150\Omega & \pm 15V & 0.40 & Deg \\ & \pm 5V & 0.30 & Deg \\ & \pm 5V & 0.30 & Deg \\ & \pm 5V & 0.26 & Deg \\ \hline \\ R_0 & Output Resistance & A_V = 1, f = 1MHz & \pm 15V & 1.4 & \Omega \\ \hline \\ Channel Separation & V_{OUT} = \pm 10V, R_L = 500\Omega & \pm 15V & 100 & 113 & dB \\ \hline \\ I_S & Supply Current & Each Amplifier & \pm 15V & 4.0 & 5.0 & mA \\ \hline \end{array} $		FTOPAGALIOH Delay	30 % VIN 10 30 % VOUT, 0.1V				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	te	Settling Time	10V Step. 0.1%. A <sub>V</sub> = −1				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			5V Step, 0.1%, $A_V = -1$	±5V	65		ns
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Differential Gain	$f = 3.58MHz, A_V = 2, R_L = 150\Omega$	±15V			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			$f = 3.58MHz, A_V = 2, R_L = 1k$				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		B.W I.B.	( 0.50141				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Differential Phase	$T = 3.58 \text{MHz}, A_V = 2, R_L = 150 \Omega$				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			f = 3.58MHz Δυ = 2 Rι = 1k				_
R <sub>0</sub> Output Resistance $A_V = 1$ , $f = 1MHz$ ±15V1.4ΩChannel Separation $V_{OUT} = \pm 10V$ , $R_L = 500Ω$ ±15V100113dBI <sub>S</sub> Supply CurrentEach Amplifier±15V4.05.0mA			1 - 0.56W112, 7\forall - 2, 1\forall - 1\forall				
Channel Separation $V_{OUT} = \pm 10V$ , $R_L = 500Ω$ $\pm 15V$ 100     113     dB $I_S$ Supply Current     Each Amplifier $\pm 15V$ 4.0     5.0     mA	$\overline{R_0}$	Output Resistance	A <sub>V</sub> = 1, f = 1MHz				
Is Supply Current Each Amplifier ±15V 4.0 5.0 mA		<u>'</u>					
	Is	· · · · · · · · · · · · · · · · · · ·			4.0	5.0	
	J						



## **ELECTRICAL CHARACTERISTICS**

The • denotes the specifications which apply over the temperature range

 $0^{\circ}C \leq T_{A} \leq 70^{\circ}C,~V_{CM}$  = 0V unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>		MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	(Note 4)	±15V ±5V ±2.5V	•			1.5 1.5 1.7	mV mV mV
	Input V <sub>OS</sub> Drift	(Note 7)	±2.5V to ±15V	•		9	12	μV/°C
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V	•			350	nA
I <sub>B</sub>	Input Bias Current		±2.5V to ±15V	•			1.5	μΑ
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$ $V_{CM} = \pm 2.5V$ $V_{CM} = \pm 0.5V$	±15V ±5V ±2.5V	•	84 77 66			dB dB dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		•	91			dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$V_{OUT} = \pm 12V, R_L = 1k$ $V_{OUT} = \pm 10V, R_L = 500\Omega$ $V_{OUT} = \pm 2.5V, R_L = 500\Omega$ $V_{OUT} = \pm 2.5V, R_L = 150\Omega$ $V_{OUT} = \pm 1V, R_L = 500\Omega$	±15V ±15V ±5V ±5V ±2.5V	•	3.6 2.4 2.4 1.0 2.0			V/mV V/mV V/mV V/mV V/mV
V <sub>OUT</sub>	Output Swing	$\begin{array}{l} R_L = 1k,  V_{IN} = \pm 40mV \\ R_L = 500\Omega,  V_{IN} = \pm 40mV \\ R_L = 500\Omega,  V_{IN} = \pm 40mV \\ R_L = 150\Omega,  V_{IN} = \pm 40mV \\ R_L = 500\Omega,  V_{IN} = \pm 40mV \end{array}$	±15V ±15V ±5V ±5V ±2.5V	•	13.4 12.8 3.4 3.1 1.2			±V ±V ±V ±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 12.8V$ $V_{OUT} = \pm 3.1V$	±15V ±5V	•	25 20			mA mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	•	32			mA
SR	Slew Rate	$A_V = -2$ , (Note 5)	±15V ±5V	•	475 185			V/μs V/μs
GBW	Gain Bandwidth	f = 200kHz	±15V ±5V	•	31 22			MHz MHz
	Channel Separation	$V_{OUT} = \pm 10V, R_L = 500\Omega$	±15V	•	98			dB
I <sub>S</sub>	Supply Current	Each Amplifier Each Amplifier	±15V ±5V	•			5.8 5.6	mA mA

## The ullet denotes the specifications which apply over the temperature range $-40^{\circ}C \leq T_A \leq 85^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted. (Note 9)

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>		MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	(Note 4)	±15V ±5V ±2.5V	•			2.0 2.0 2.2	mV mV mV
	Input V <sub>OS</sub> Drift	(Note 7)	±2.5V to ±15V	•		9	12	μV/°C
I <sub>OS</sub>	Input Offset Current		±2.5V to ±15V	•			400	nA
$I_B$	Input Bias Current		±2.5V to ±15V	•			1.8	μΑ
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 12V$ $V_{CM} = \pm 2.5V$ $V_{CM} = \pm 0.5V$	±15V ±5V ±2.5V	•	84 77 66			dB dB dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.5 V \text{ to } \pm 15 V$		•	90			dB
A <sub>VOL</sub>	Large-Signal Voltage Gain	$\begin{array}{c} V_{OUT} = \pm 12V, \; R_L = 1k \\ V_{OUT} = \pm 10V, \; R_L = 500\Omega \\ V_{OUT} = \pm 2.5V, \; R_L = 500\Omega \\ V_{OUT} = \pm 2.5V, \; R_L = 150\Omega \\ V_{OUT} = \pm 1V, \; R_L = 500\Omega \end{array}$	±15V ±15V ±5V ±5V ±2.5V	•	2.5 1.5 1.5 0.6 1.3			V/mV V/mV V/mV V/mV V/mV

# **ELECTRICAL CHARACTERISTICS** The $\bullet$ denotes the specifications which apply over the temperature range $-40^{\circ}C \le T_A \le 85^{\circ}C$ , $V_{CM} = 0V$ unless otherwise noted. (Note 9)

SYMBOL	PARAMETER	CONDITIONS	V <sub>SUPPLY</sub>	M	IN TYP	MAX	UNITS
V <sub>OUT</sub>	Output Swing	$R_L = 1k, V_{IN} = \pm 40mV$	±15V	13	.4		±V
		$R_L = 500\Omega$ , $V_{IN} = \pm 40$ mV	±15V	12	.0		±V
		$R_L = 500\Omega, V_{IN} = \pm 40 \text{mV}$	±5V	3	.4		±V
		$R_L = 150\Omega$ , $V_{IN} = \pm 40$ mV	±5V	3	.0		±V
		$R_L = 500\Omega, V_{IN} = \pm 40 \text{mV}$	±2.5V	1	.2		±V
I <sub>OUT</sub>	Output Current	$V_{OUT} = \pm 12.0V$	±15V	2	4		mA
		$V_{OUT} = \pm 3.0 V$	±5V	2	0		mA
I <sub>SC</sub>	Short-Circuit Current	$V_{OUT} = 0V$ , $V_{IN} = \pm 3V$	±15V	3	0		mA
SR	Slew Rate	$A_V = -2$ , (Note 5)	±15V	45	50		V/µs
			±5V	17	75		V/µs
GBW	Gain Bandwidth	f = 200kHz	±15V	3	0		MHz
			±5V	2	0		MHz
	Channel Separation	$V_{OUT} = \pm 10V$ , $R_L = 500\Omega$	±15V	9	8		dB
Is	Supply Current	Each Amplifier	±15V			6.0	mA
		Each Amplifier	±5V			5.8	mA

**Note 1:** Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

**Note 2:** Differential inputs of  $\pm 10$ V are appropriate for transient operation only, such as during slewing. Large, sustained differential inputs will cause excessive power dissipation and may damage the part. See Input Considerations in the Applications Information section of this data sheet for more details.

**Note 3:** A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted indefinitely.

Note 4: Input offset voltage is pulse tested and is exclusive of warm-up drift.

**Note 5:** Slew rate is measured between  $\pm 10V$  on the output with  $\pm 6V$  input for  $\pm 15V$  supplies and  $\pm 1V$  on the output with  $\pm 1.75V$  input for  $\pm 5V$  supplies.

**Note 6:** Full power bandwidth is calculated from the slew rate measurement: FPBW =  $SR/2\pi V_P$ .

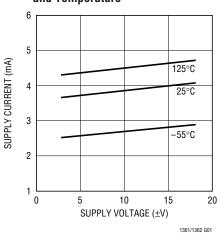
Note 7: This parameter is not 100% tested.

**Note 8:** The LT1361C/LT1362C are guaranteed functional over the operating temperature range of  $-40^{\circ}$ C to  $85^{\circ}$ C.

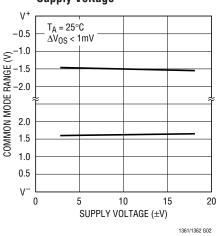
**Note 9:** The LT1361C/LT1362C are guaranteed to meet specified performance from 0°C to 70°C. The LT1361C/LT1362C are designed, characterized and expected to meet specified performance from  $-40^{\circ}\text{C}$  to 85°C, but are not tested or QA sampled at these temperatures. For guaranteed l-grade parts, consult the factory.

## TYPICAL PERFORMANCE CHARACTERISTICS

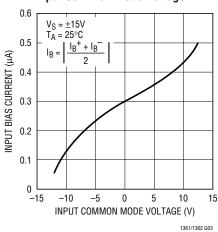




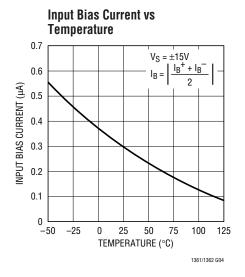
#### Input Common Mode Range vs Supply Voltage

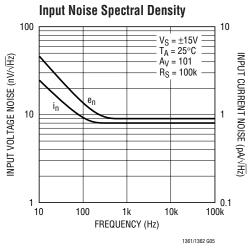


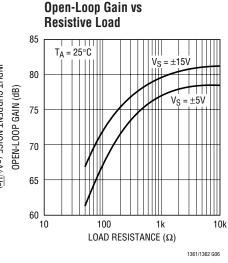
#### Input Bias Current vs Input Common Mode Voltage

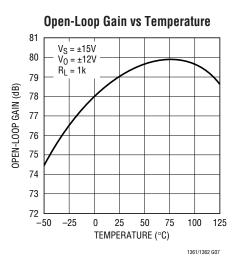


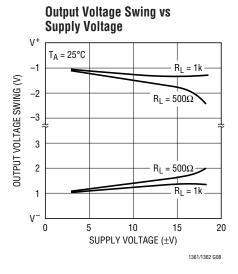


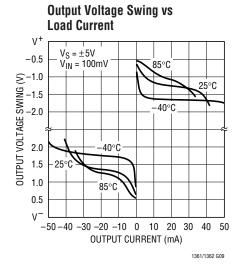


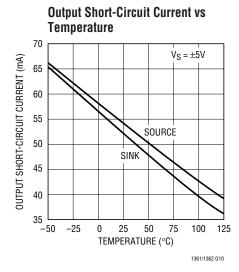


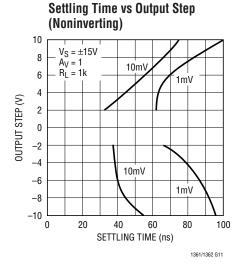


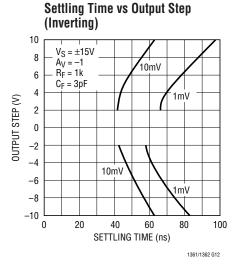


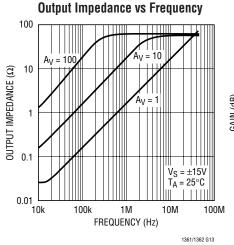


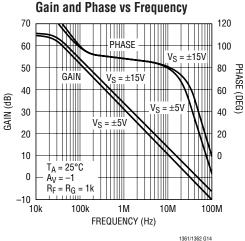


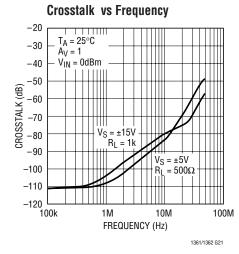




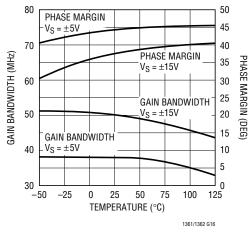




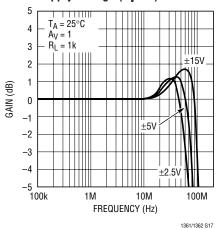




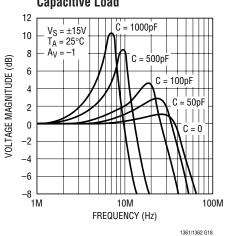
#### Gain Bandwidth and Phase Margin vs Temperature



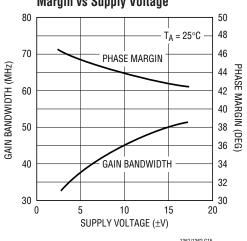




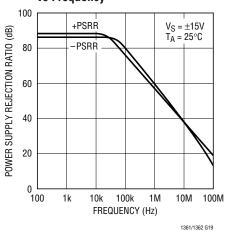
Frequency Response vs Capacitive Load



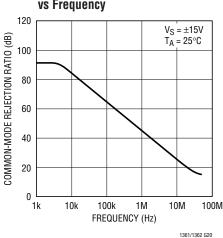
#### Gain Bandwidth and Phase Margin vs Supply Voltage



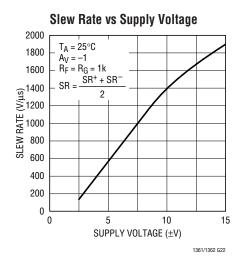
# Power Supply Rejection Ratio vs Frequency

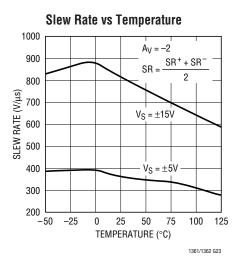


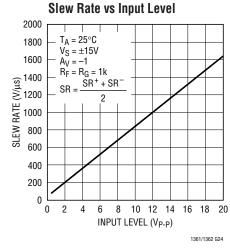
# Common Mode Rejection Ratio vs Frequency

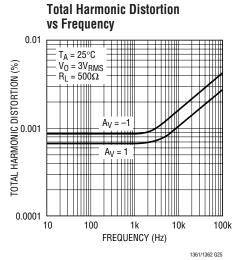


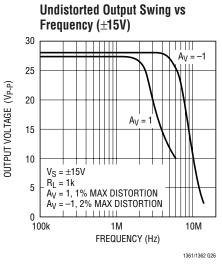


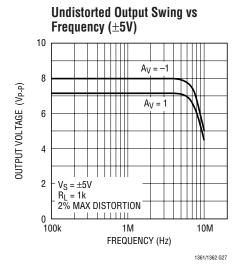


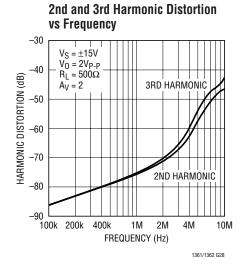


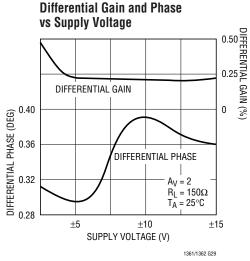


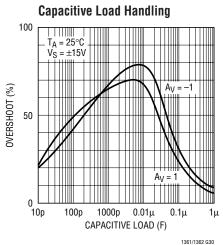




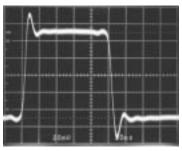






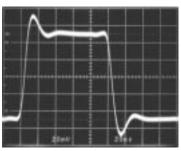


Small-Signal Transient  $(A_V = 1)$ 



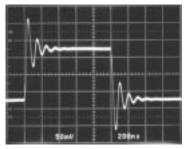
1361/1362 TA31

Small-Signal Transient  $(A_V = -1)$ 



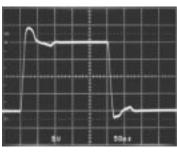
1361/1362 TA32

Small-Signal Transient  $(A_V = -1, C_L = 500pF)$ 



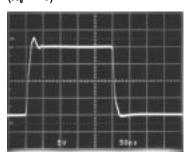
1001/1000 TA00

Large-Signal Transient  $(A_V = 1)$ 



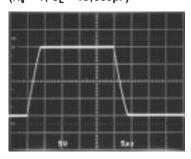
1361/1362 TA34

Large-Signal Transient  $(A_V = -1)$ 



1361/1362 TA35

Large-Signal Transient  $(A_V = 1, C_L = 10,000pF)$ 



1361/1362 TA36

## APPLICATIONS INFORMATION

#### **Layout and Passive Components**

The LT1361/LT1362 amplifiers are easy to use and tolerant of less than ideal layouts. For maximum performance (for example, fast 0.01% settling) use a ground plane, short lead lengths, and RF-quality bypass capacitors (0.01 $\mu$ F to 0.1 $\mu$ F). For high drive current applications use low ESR bypass capacitors (1 $\mu$ F to 10 $\mu$ F tantalum). The parallel combination of the feedback resistor and gain setting resistor on the inverting input combine with the input capacitance to form a pole which can cause peaking or oscillations. If feedback resistors greater than  $5k\Omega$  are used, a parallel capacitor of value

$$C_F > R_G \times C_{IN}/R_F$$

should be used to cancel the input pole and optimize dynamic performance. For unity-gain applications where a large feedback resistor is used,  $C_F$  should be greater than or equal to  $C_{\mathsf{IN}}$ .

#### **Input Considerations**

Each of the LT1361/LT1362 inputs is the base of an NPN and a PNP transistor whose base currents are of opposite polarity and provide first-order bias current cancellation. Because of variation in the matching of NPN and PNP beta, the polarity of the input bias current can be positive or negative. The offset current does not depend on NPN/PNP beta matching and is well controlled. The use of balanced source resistance at each input is recommended for applications where DC accuracy must be maximized.

The inputs can withstand transient differential input voltages up to 10V without damage and need no clamping or source resistance for protection. Differential inputs, however, generate large supply currents (tens of mA) as required for high slew rates. If the device is used with sustained differential inputs, the average supply current will increase, excessive power dissipation will result and the part may be damaged. The part should not be used as a comparator, peak detector or other open-loop applica-

#### APPLICATIONS INFORMATION

tion with large, sustained differential inputs. Under normal, closed-loop operation, an increase of power dissipation is only noticeable in applications with large slewing outputs and is proportional to the magnitude of the differential input voltage and the percent of the time that the inputs are apart. Measure the average supply current for the application in order to calculate the power dissipation.

#### **Capacitive Loading**

The LT1361/LT1362 are stable with any capacitive load. This is accomplished by sensing the load induced output pole and adding compensation at the amplifier gain node. As the capacitive load increases, both the bandwidth and phase margin decrease so there will be peaking in the frequency domain and in the transient response as shown in the typical performance curves. The photo of the small signal response with 500pF load shows 60% peaking. The large signal response shows the output slew rate being limited to  $5V/\mu s$  by the short-circuit current. Coaxial cable can be driven directly, but for best pulse fidelity a resistor of value equal to the characteristic impedance of the cable (i.e.,  $75\Omega$ ) should be placed in series with the output. The other end of the cable should be terminated with the same value resistor to ground.

#### **Circuit Operation**

The LT1361/LT1362 circuit topology is a true voltage feedback amplifier that has the slewing behavior of a current feedback amplifier. The operation of the circuit can be understood by referring to the simplified schematic. The inputs are buffered by complementary NPN and PNP emitter followers which drive a  $500\Omega$  resistor. The input voltage appears across the resistor generating currents which are mirrored into the high impedance node. Complementary followers form an output stage which buffers the gain node from the load. The bandwidth is set by the input resistor and the capacitance on the high impedance node. The slew rate is determined by the current available to charge the gain node capacitance. This current is the differential input voltage divided by R1, so the slew rate is proportional to the input. Highest slew rates are therefore seen in the lowest gain configurations. For example, a 10V output step in a gain of 10 has only a 1V input step,

whereas the same output step in unity gain has a 10 times greater input step. The curve of Slew Rate vs Input Level illustrates this relationship. The LT1361/LT1362 are tested for slew rate in a gain of -2 so higher slew rates can be expected in gains of 1 and -1, and lower slew rates in higher gain configurations.

The RC network across the output stage is bootstrapped when the amplifier is driving a light or moderate load and has no effect under normal operation. When driving a capacitive load (or a low value resistive load) the network is incompletely bootstrapped and adds to the compensation at the high impedance node. The added capacitance slows down the amplifier which improves the phase margin by moving the unity-gain frequency away from the pole formed by the output impedance and the capacitive load. The zero created by the RC combination adds phase to ensure that even for very large load capacitances, the total phase lag can never exceed 180 degrees (zero phase margin) and the amplifier remains stable.

#### **Power Dissipation**

The LT1361/LT1362 combine high speed and large output drive in small packages. Because of the wide supply voltage range, it is possible to exceed the maximum junction temperature under certain conditions. Maximum junction temperature  $(T_J)$  is calculated from the ambient temperature  $(T_A)$  and power dissipation  $(P_D)$  as follows:

 $\begin{array}{ll} LT1361CN8: \ T_J = T_A + (P_D \times 130^{\circ} C/W) \\ LT1361CS8: \ T_J = T_A + (P_D \times 190^{\circ} C/W) \\ LT1362CN: \ T_J = T_A + (P_D \times 110^{\circ} C/W) \\ LT1362CS: \ T_J = T_A + (P_D \times 150^{\circ} C/W) \end{array}$ 

Worst case power dissipation occurs at the maximum supply current and when the output voltage is at 1/2 of either supply voltage (or the maximum swing if less than 1/2 supply voltage). For each amplifier  $P_{DMAX}$  is:

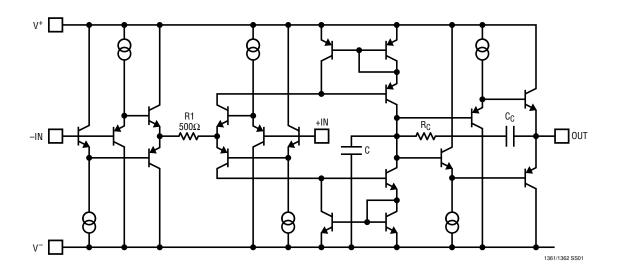
$$P_{DMAX} = (V^+ - V^-)(I_{SMAX}) + (V^+/2)^2/R_L$$

Example: LT1362 in S16 at 70°C,  $V_S$  =  $\pm 5V$ ,  $R_L$  =  $100\Omega$ 

$$P_{DMAX} = (10V)(5.6mA) + (2.5V)^2/100\Omega = 119mW$$

 $T_{JMAX} = 70^{\circ}C + (4 \times 119 \text{mW})(150^{\circ}C/W) = 141^{\circ}C$ 

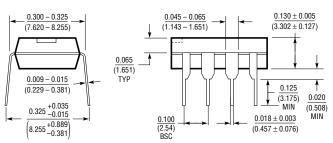
## SIMPLIFIED SCHEMATIC

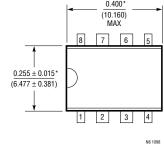


## PACKAGE DESCRIPTION

Dimension in inches (millimeters) unless otherwise noted.

#### N8 Package 8-Lead PDIP (Narrow 0.300) (LTC DWG # 05-08-1510)

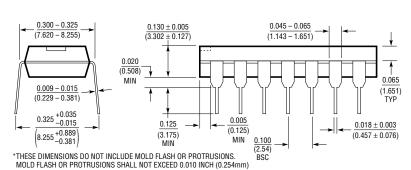


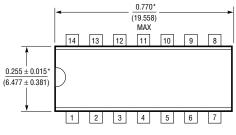


\*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm)

#### N Package 14-Lead PDIP (Narrow 0.300)

(LTC DWG # 05-08-1510)



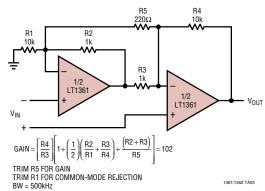


N14 1098

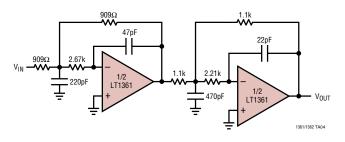


### TYPICAL APPLICATIONS

#### Two Op Amp Instrumentation Amplifier



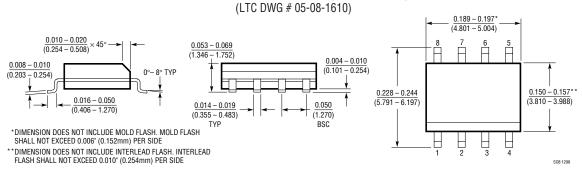
#### 1MHz, 4th Order Butterworth Filter



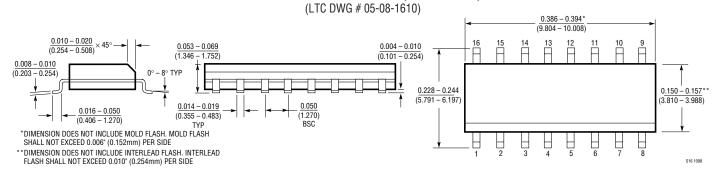
## PACKAGE DESCRIPTION

Dimension in inches (millimeters) unless otherwise noted.

#### S8 Package 8-Lead Plastic Small Outline (Narrow 0.150)



#### S Package 16-Lead Plastic Small Outline (Narrow 0.150)



## RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1360	50MHz, 800V/μs Op Amp	Single Version of LT1361/LT1362
LT1364/LT1365	Dual and Quad 70MHz, 1000V/µs Op Amps	Faster Version of LT1361/LT1362, V <sub>OS</sub> = 1.5mV, I <sub>S</sub> = 6.3mA/Amplifier
LT1358/LT1359	Dual and Quad 25MHz, 600Vµs Op Amps	Lower Power Version of LT1361/LT1362, V <sub>OS</sub> = 0.6mV, I <sub>S</sub> = 2mA/Amplifier
LT1813	Dual 100MHz, 700V/µs Op Amps	Low Voltage, Low Power LT1361, I <sub>S</sub> = 3mA/Amplifier