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Tel: +86-755-8981 8866 Fax: +86-755-8427 6832 Email & Skype: info@chipsmall.com Web: www.chipsmall.com Address: A1208, Overseas Decoration Building, #122 Zhenhua RD., Futian, Shenzhen, China



### **\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_General Description**

The MAX1664 integrates power-supply and backplane drive circuitry for active-matrix thin-film-transistor (TFT) liquid crystal displays. Included are a single-output, pulsewidth-modulation boost converter (0.25Ω switch), a dual-output (positive and negative) gate-driver supply using one inductor, an LCD backplane driver, and a simple phase-locked loop to synchronize all three outputs.

High switching frequency (1MHz nominal) and phaselocked operation allow the use of small, minimumheight external components while maintaining low output noise. A  $+2.8V$  to  $+5.5V$  input voltage range allows operation with any logic supply. Output voltages are adjustable to  $+5.5V$  (DC-DC 1) and to  $+28V$  and -10V (DC-DC 2). The negative output voltage can be adjusted to -20V with additional components. Also included are a logic-level shutdown and a "Ready" output (RDY) that signals when all three outputs are in regulation.

The boost-converter operating frequency can be set at 16, 24, or 32 times the backplane clock. This flexibility allows a high DC-DC converter frequency to be used with LCD backplane clock rates ranging from 20kHz to 72kHz. The MAX1664 is supplied in a 1.1mm-high TSSOP package.

**\_Applications**

LCD Modules LCD Panels



### **MAXIM**

**\_ Maxim Integrated Products 1**

**\_Features**

- ♦ **Integrates All Active Circuitry for Three DC-DC Converters**
- ♦ **Ultra-Small External Components (ceramic capacitors, 2µH to 5µH inductors)**
- ♦ **DC-DC Converters Phase-Locked to Backplane Frequency for Lowest Noise**
- ♦ **Low Operating Voltage (down to +2.8V)**
- ♦ **Adjustable Output Voltage from VIN to +5.5V**
- ♦ **Load Currents Up to 500mA**
- ♦ **Adjustable TFT Gate Driver Output: Positive, VIN to +28V Negative, 0 to -10V (-20V with added components)**
- ♦ **Includes 0.35**Ω **Backplane Driver**
- ♦ **1µA Shutdown Current**
- ♦ **Power-Ready Output Signal**

### **\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_Ordering Information**



### **Typical Operating Circuit**



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### **ABSOLUTE MAXIMUM RATINGS**





Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

### **ELECTRICAL CHARACTERISTICS**

 $(V_{IN} = V_{INP} = 3.3V, \overline{SHDN} = IN, V_{BPVDD} = 4V, V_{BPVSS} = -1V, PGND1 = PGND2 = FPLL = GND, f_{BPCLK} = 30kHz, T_A = 0°C to +70°C,$ unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .)



### **ELECTRICAL CHARACTERISTICS (continued)**

 $(V_{IN} = V_{INP} = 3.3V, \overline{SHDN} = IN, V_{BPVDD} = 4V, V_{BPVSS} = -1V, PGND1 = PGND2 = FPLL = GND, f_{BPCLK} = 30kHz, T_A = 0°C to +70°C,$ unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .)



**Note 1:** DC-DC 1 operates at one-half of the V<sub>CO</sub> frequency (f<sub>C</sub> / 2).

$$
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$$

**MAX1664 MAX1664**



**MAX1664**

### **Typical Operating Characteristics (continued)**

 $_{0.001}^{\circ}$ 

M

100

150

50

0.001 0.01 0.1 1

CLOAD FROM BPDRV TO GI

FALL TIME

LOAD CAPACITANCE (µF)

( $f_{\text{BPCLK}}$  = 22.5kHz, FPLL = GND, L1 = 3.3µH, L2 = 4.7µH,  $T_A$  = +25°C, unless otherwise noted.)

0

**MAXIM** 

LX1

BPDRV P-CHANNEL

0 20 30 10 40 50 60 70 80 90

LX2P

BPDRV N-CHANNEL

TEMPERATURE (°C)

400 200

800 600





**\_ 5**



*IVI AXI IVI* 

### **\_Pin Description**



**MAX1664**



Figure 1. Functional Diagram

### **\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_Detailed Description**

The MAX1664 combines power supply and backplane drive circuitry for active matrix thin-film-transistor (TFT) liquid crystal displays (LCD) into one IC. Included are a pulse-width-modulation (PWM) boost converter, a dualoutput (positive and negative) converter using one inductor, an LCD backplane driver, and a phaselocked loop (PLL) to synchronize all three outputs to the backplane clock.

A high switching frequency (1MHz nominal) and phaselocked operation allow the use of small, minimumheight external components while maintaining low output noise. Output voltages are adjustable to +5.5V (DC-DC 1) and to +28V and -10V (DC-DC 2). The negative output voltage can be set to as low as -20V with additional components.

The frequency ratio between the DC-DC 1 converter and the backplane clock can be set to 16, 24, or 32. This flexibility allows high DC-DC converter frequencies

to be used with LCD backplane clock rates ranging from 20kHz to 72kHz.

#### **Start-Up**

At start-up, both converters remain disabled until VREF reaches 90% of its nominal value. VOUT1 is activated first. Once VOUT1 is regulated, VOUT2- is enabled. VOUT2+ is held at 0 until VOUT2- is within 90% of its regulation target. All three outputs power up in a similar order when power is applied or when coming out of shutdown. See the Out-of-Shutdown Sequence photo in the Typical Operating Characteristics section.

#### **DC-DC 1 Boost Converter**

DC-DC 1 uses a current-mode boost PWM architecture to produce a positive regulated voltage, adjustable from 3V to 5.5V (but not less than  $V_{IN}$ ). This converter uses an internal N-channel MOSFET with a maximum on-resistance of 0.5Ω. Cycle-by-cycle peak current limiting protects the switch under fault conditions. Upon start-up, DC-DC 1 is the first converter to be enabled.



### **Table 1. Switching Frequency Options**

\*See Figure 2

Fixed-frequency, current-mode operation ensures that the switching noise exists only at the operating frequency and its harmonics. The switching frequency is phase locked to the backplane clock input. Table 1 illustrates the possible switching-frequency options.

#### **DC-DC 2 Dual Outputs**

DC-DC 2 uses a synchronized, fixed on-time PFM architecture to provide the positive and negative output voltages that allow the driver ICs to turn the TFT gates on and off. When pulses occur, they are synchronized to DC-DC 1, thereby minimizing converter interactions and subharmonic interference.

The DC-DC 2 inductor current is always discontinuous, enabling the dual outputs to be regulated independently. This allows one output to be at 100% load while the other is at no load.

#### **DC-DC 2 Operation**

In normal operation, DC-DC 2 alternates between charging the negative and positive outputs (Figure 1). During the first half-cycle of the PFM clock period, both the N-channel and P-channel MOSFETs turn on, applying the input supply across inductor L2. This causes the inductor current to ramp up at a rate proportional to VINP. During the second half-cycle, the P-channel MOSFET turns off and the inductor transfers its energy into the negative output filter capacitor.

Assuming that the energy transfer is completed during this second half-cycle and the inductor current ramps down to zero, the process is repeated for the positive output during the next clock cycle. During the first half of the second clock cycle, both the N-channel and Pchannel MOSFETs turn on again. The current in the inductor again rises at the same rate. During the second half of the second clock cycle, the N-channel MOSFET is turned off and this time the inductor energy transfers to the positive output filter capacitor.

During conditions of heavy loads, DC-DC 2 will continue to operate in this manner, alternately delivering pulses to the negative and positive outputs. For lighter loads, the controller may skip one or more cycles of either polarity, thereby keeping the outputs in regulation. See Table 1 for the relationship between the maximum DC-DC 2 pulse frequency and the backplane clock frequency.

**Outputs with Low Step-Up or Inversion Ratios** For DC-DC 2 output voltage setpoints, which require minimum step-up or inversion ratios (for example,  $V_{\text{OUT+}}$  < 6V or  $V_{\text{OUT-}}$  > -3V, when  $V_{\text{INP}}$  = 5V), more than one half-cycle may be required to transfer the inductor energy to the appropriate output filter capacitor. In such cases, subsequent conversion cycles are delayed, as necessary, by one or more PFM clock cycles to preserve discontinuous mode operation.

#### **Backplane Driver**

The MAX1664 provides a low-impedance backplane driver, as shown in Figure 1, that level-translates the BPCLK signal from a logic level to BPV<sub>DD</sub>/BPV<sub>SS</sub> levels. The backplane driver consists of an N-channel/P-channel complementary pair of high-current MOSFETs. These devices drive BPDRV to either BPV<sub>DD</sub> or BPV<sub>SS</sub> when BPCLK goes either high or low, respectively. The switches have a maximum on-resistance of  $0.7\Omega$  with a typical propagation delay of 50ns. Power for the backplane driver can be taken from the output of DC-DC 1,  $V_{\text{OUT1}}$ , as shown in the Typical Operating Circuit.

#### **Phase-Locked Loop**

The MAX1664 contains an on-board PLL to synchronize the PWM and PFM converter clocks to the backplane clock (Figure 2). This will minimize noise and interference. The PLL is a frequency-multiplying type, generating a nominal 1MHz clock signal for DC-DC 1 and a nominal 500kHz clock for DC-DC 2. Three input frequency ranges, spanning 20kHz to 72kHz, permit synchronization over a broad range of backplane clock input frequencies while maintaining optimal conversion frequencies (Table 1).

**MAX1664**



Figure 2. Internal PLL Operation within the MAX1664

The heart of the PLL is the VCO, which is trimmed to a nominal frequency of 1.92MHz for a control voltage (at the PLLC pin) of 1.250V. This high-frequency internal clock is divided digitally with a division ratio selected by pin-strapping FPLL to GND, REF, or IN. This divided clock is compared to the backplane clock by an internal phase comparator (rising-edge triggered). The phase detector in turn adjusts the VCO control voltage until the two frequencies (and phases) match. This feedback loop is compensated at the PLLC pin.

In some applications, the backplane clock may be halted for several cycles between screen scans or may not be immediately applied on power-up. The PLL contains a proprietary phase-detector architecture that minimizes frequency error during clock dropouts of more than two cycles and re-establishes lock immediately when the clock resumes.

#### **Ready Indicator (RDY)**

The RDY pin has an open-drain output and indicates when all three outputs are in regulation. The open-drain output becomes high impedance when all three converter outputs are within 10% of their regulation setpoints.

### **Design Procedure and \_\_\_\_\_\_\_\_\_\_\_\_\_\_Component Selection**

#### **Output Voltage Selection**

The three output voltages as well as the DC bias for the backplane clock are adjustable on the MAX1664, as shown in Figure 3. Set each output using two standard 1% resistors to form a voltage divider between the selected output and its respective feedback pin. Use the following equations to calculate the resistances.



Figure 3. Output Voltage Selection

**DC-DC 1 Output**

For V<sub>OUT1</sub> = 5V, typical values are R2 = 100kΩ and R1 = 301kΩ. To set V<sub>OUT1</sub> to another voltage, choose R2 = 100k $\Omega$  and CFB1 = 50pF, and calculate R1 as follows:

$$
R1 = R2 \left( \frac{V_{\text{OUT1}}}{V_{\text{FB1}}} - 1 \right)
$$

#### **DC-DC 2 Positive Output**

For VOUT2+ = 15V, typical values are R8 =  $49.9k\Omega$  and  $R7 = 549k\Omega$ . To set VOUT2+ to another voltage, choose  $R8 = 49.9k\Omega$  and calculate R7 as follows:

$$
R7 = R8 \left( \frac{V_{\text{OUT2+}}}{V_{\text{FB2+}}} - 1 \right)
$$

#### **DC-DC 2 Negative Output**

For the negative output voltage, the FB2- threshold voltage is 0. For  $V_{\text{OUT2-}} = -5V$ , typical values are R5 = 49.9kΩ and R6 = 200kΩ. To set  $V_{\text{OUT2+}}$  to another voltage, choose R5 =  $49.9k\Omega$  and calculate R6 as follows:

$$
\text{R6} = \text{R5} \left| \frac{\text{V}_{\text{OUT2-}}}{\text{V}_{\text{REF}}}\right|
$$

#### **DC Bias for the Backplane Driver**

For  $V_{DCBIAS}$  =  $V_{BPVDD}/2$ , typical values are R3 = R4 = 100kΩ. To set the DC bias to a different value, choose R4 and calculate R3 as follows:

$$
R3 = R4 \left( \frac{V_{BPVDD} - V_{BPVSS}}{V_{DCBIAS} - V_{BPVSS}} - 1 \right)
$$

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$$



Figure 4. Detailed Typical Operating Circuit

#### **Inductor Selection**

The optimum inductor value for L1 is 3.3µH, as shown in Figure 4. Inductors with less than 300mΩ DC series resistance are recommended to achieve the highest efficiency. Using a larger value for L1 (e.g., 4.7µH) increases the output current capability of DC-DC 1 (by reducing the peak ripple current) at the expense of size and the additional output filter capacitance needed for loop stability.

For DC-DC 2, at large input voltages (i.e., 5V) and low switching frequencies (i.e., ≤400kHz), the value of L2 should be increased (e.g., 6.8µH or 10µH) to limit the peak current. In some cases it may be necessary to reduce the value of L2 to increase the output current capability of DC-DC 2 (Table 2). The relationship between input voltage, output voltage, switching frequency, inductor value, and maximum load current for DC-DC 2 is complex and nonlinear. This relationship is summarized in Table 2. The L2 equation is as follows:

$$
L2 > \frac{V_{INP} - \left[R_{ON(LX2P)} + R_{ON(LX2N)} + R_{L2}\right] \frac{(I_{PEAK})}{2}}{I_{PEAK} \times 2 \left(f_{DC-DC-1}\right)}
$$

where:

Internal MOSFET on-resistance:  $R_{ON(LX2P)} = R_{ON(LX2N)} = 0.9\Omega$  typical External inductor DC resistance:  $R_{L2} = 0.3\Omega$  typical Inductor peak current: IPEAK = 700mA (750mA absolute maximum)

Due to the MAX1664's high switching frequency, inductors with a high-frequency core material such as ferrite are recommended. Powdered iron compounds are not recommended due to their higher core losses. Typical small-size, low-profile inductors include the ILS-3825 (Dale Electronics-Vishay) and the CLQ61B (Sumida). These inductors are primarily used for DC-DC converters with low height requirements. See Table 3 for more information on manufacturers who provide low-profile inductors.

**MAX1664**

**MAX1664** 

# **MAX1664 (kHz) (V) (V) (V)**

### **Table 2. Typical DC-DC 2 Operation**

**INDUCTOR PEAK CURRENT\* (mA) fDC-DC 2(MAX) (kHz) IOUT2-(MAX) (mA) IOUT2+(MAX) (mA) L2 (µH) fBPCLK VIN VOUT2- VOUT2+** +20 | -10 | 5.0 | 30.0 | 4.7 | 10 | 15 | 480 | 500 +20 | -10 | 5.0 | 25.0 | 4.7 | 10 | 18 | 400 | 550 +20 | -10 | 5.0 | 22.5 | 4.7 | 11 | 20 | 360 | 640 +20 | -10 | 4.5 | 30.0 | 2.7 | 10 | 17 | 480 | 679 +20 | -10 | 4.5 | 30.0 | 4.7 | 8 | 12 | 480 | 450 +20 | -10 | 4.5 | 25.0 | 4.7 | 8 | 14 | 400 | 500 +20 | -10 | 4.5 | 22.5 | 4.7 | 9 | 16 | 360 | 580 +20 | -10 | 3.3 | 30.0 | 4.7 | 4 | 8 | 480 | 496 +20 | -10 | 3.3 | 30.0 | 4.7 | 4 | 5 | 480 | 340 +20 | -10 | 3.3 | 25.0 | 2.7 | 6 | 10 | 400 | 583 +20 | -10 | 3.3 | 25.0 | 4.7 | 4 | 7 | 400 | 370 +20 | -10 | 3.3 | 22.5 | 2.7 | 6 | 12 | 360 | 643 +20 | -10 | 3.3 | 22.5 | 4.7 | 4 | 8 | 360 | 425 +20 | -10 | 3.0 | 30.0 | 2.7 | 3 | 6 | 480 | 451 +20 | -10 | 3.0 | 30.0 | 4.7 | 3 | 4 | 480 | 300 +20 | -10 | 3.0 | 25.0 | 2.7 | 4 | 8 | 400 | 530 +20 | -10 | 3.0 | 25.0 | 4.7 | 2 | 5 | 400 | 340 +20 | -10 | 3.0 | 22.5 | 2.7 | 5 | 10 | 360 | 585 +20 | -10 | 3.0 | 22.5 | 4.7 | 3 | 6 | 360 | 385 +15 | -5 | 5.0 | 22.5 | 4.7 | 20 | 43 | 360 | 600 +15 | -5 | 4.5 | 22.5 | 4.7 | 15 | 35 | 360 | 550 +15 | -5 | 3.3 | 22.5 | 2.7 | 10 | 27 | 360 | 643 +15 | -5 | 3.3 | 22.5 | 4.7 | 7 | 19 | 360 | 425 +15 | -5 | 3.0 | 22.5 | 2.7 | 8 | 23 | 360 | 585 +15 | -5 | 3.0 | 22.5 | 4.7 | 6 | 15 | 360 | 375

\*Note: Absolute maximum peak current at LX2P and LX2N is 750mA.

#### **Diode Selection**

The MAX1664's high switching frequency requires fast diodes. Schottky diodes such as the MBR0520L and MBR0540L (Motorola) are recommended because they have the necessary power ratings in a low-height SOD-123 package. Also recommended is the MBRM5817 which is 1.1mm high. Use a Schottky diode with a forward current rating greater than:

$$
I_F > \frac{I_{OUT} V_{OUT}}{0.9 V_{IN}}
$$

For the positive output of DC-DC 2, use a Schottky diode with a voltage rating that exceeds  $V_{\text{OUT2}+}$ . For the negative output, use a Schottky diode with a rating

that exceeds  $V_{IN}$  +  $V_{OUT2}$ . See Table 3 for more information on Schottky diode manufacturers.

#### **Filter Capacitor Selection**

An output filter capacitor's ESR and size can greatly influence a switching converter's output ripple, as shown in the following equation.

$$
V_{RIPPLE(PK-PK)} \cong I_{PEAK} \times R_{ESR} + I_{OUT}\left(\frac{t_{ON}}{C_{OUT}}\right)
$$
  
DC-DC 1  $t_{ON} = \frac{1}{f_{DC-DC 1}} \left(\frac{V_{OUT1} + V_F - V_{IN}}{V_{OUT1} + V_F}\right)$   
DC-DC 2  $t_{ON} = \frac{1}{2 f_{DC-DC 1}}$ 

Ceramic capacitors are recommended because they have low ESR and the lowest profile. Typical ceramic capacitors are the C3225X5R series from TDK and JMK325 series from Taiyo Yuden. See Table 3 for more information on the manufacturers who provide surfacemount ceramic capacitors.

#### **PLL Compensation**

In most applications, the recommended compensation component values shown in Figure 4 will give optimal system performance. If no backplane clock is used, connect PLLC to REF.



#### **Table 3. Component Manufacturers**

### **\_\_\_\_\_\_\_\_\_\_\_\_\_Applications Information**

#### **Increasing VOUT Above 5.5V**

For VOUT1 output voltages above 5.5V, connect the supplemental charge pump circuit shown in Figure 5. The connection shown supplies a 10V 150mA output, but other voltages from  $2 \times V_{IN}$  to 10V can be set by selecting the appropriate values for R1 and R2 (see DC-DC 1 Output section). C2–C4 are shown as parallel combinations of 3.3µF ceramic capacitors so that a 1.1mm height restriction can be met. If height is not restricted, then larger values can be used instead of parallel capacitor combinations.

**3.3V to -20V Charge-Pump Configuration**  For applications requiring negative voltages down to -20V, an inverting charge-pump block can be added to the VOUT2- output (Figure 6). Typical values for CF and

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Figure 5. Charge Pump Configuration to Increase VOUT1 Above 5.5V.

COUT are 0.47µF to 1µF and 4.7µF to 10µF, respectively. As a general rule, COUT should be ten times greater than CF. This circuit operates as follows:

- 1) During the first PFM cycle, the voltage at V1 is charged by inductor L2 to some fraction of its final steady-state voltage, in the normal manner described in the Detailed Description.
- 2) During the first half of subsequent PFM cycles, pin LX2P is pulled to VINP, and capacitor CF is charged to (VINP +  $|V_1|$  - V<sub>D</sub>), where V<sub>D</sub> is a diode forward voltage.
- 3) During subsequent second half-cycles when LX2P flies negatively below  $V1$ , capacitor  $C_F$  transfers some of its energy to output capacitor COUT, which then is charged to a negative voltage of approximately (VINP + 2 x  $|V_1|$  - 2x V<sub>D</sub>).
- 4) This process continues until VOUT reaches the desired voltage, as determined by the ratio of the FB2- feedback resistors.
- 5) During steady-state (in-regulation) operation, the magnitude of the voltage at LX2P is equal to  $(N_{\text{OUT}})/2 - V_{\text{NP}}/2 + V_{\text{D}})$ , which must be limited to less than 10V.

#### **Supply Connections and Layout**

The MAX1664 performs both precision analog and high-power switching functions. Carefully plan supply connections, bypassing, and layout. Bypass IN and INP with a 33Ω isolation resistor (R9, Figure 4) between them. In addition, sufficient low-ESR bypassing must be provided on the INP bus to ensure stability of DC-DC 1.

A solid ground plane under the power components, with a separate ground plane under the analog nodes, is highly recommended. These ground planes should be connected at a single, quiet point. Analog reference and feedback signals should be referred to and routed over the analog ground plane. Figure 7 shows a typical layout using separate ground planes.



Figure 6. VOUT2- Voltage-Doubler Charge Pump





Figure 7a. MAX1664 Component Placement Guide Figure 7b. MAX1664 PC Board Layout—Component Side

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Figure 7c. MAX1664 PC Board Layout—Solder Side

### **\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_Chip Information**

TRANSISTOR COUNT: 838

**MAX1664**



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**16 \_Maxim Integrated Products, 120 San Gabriel Drive, Sunnyvale, CA 94086 408-737-7600**

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