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EVALUATION KIT AVAILABLE

# Remote Antenna, Current-Sense and LDO/Switches



## General Description

The MAX16946/MAX16947 high-voltage, high-side, current-sense LDO/switches feature internal current limiting to prevent system damage due to fault conditions. The MAX16946 provides a fixed regulated 8.5V output voltage or an adjustable 3.3V to 15V output voltage. The MAX16946 can also be configured as a switch, while the MAX16947 is only available as a switch. The input voltage range for both devices extends from 4.5V to 18V (45V tolerant), making the devices ideal for providing phantom power to remote radio-frequency low-noise amplifiers (LNAs) in automotive applications.

The devices monitor the load current and provide an analog output voltage proportional to the sensed load current. Accurate internal current limit protects the input supply against both overload and short-circuit conditions. Two open-drain fault indicator outputs indicate to the microprocessor when a short circuit, an open-load condition, or a short-to-battery condition exists. An overtemperature shutdown is also indicated by means of the current-sense amplifier's output voltage.

A fault-blanking feature allows the devices to ignore momentary faults such as those caused by the charging of capacitive loads during hot-swapping, preventing false alarms to the system. The devices feature short-to-battery protection to latch off the internal LDO/pass switch during a short-to-battery event. During a thermal overload, the devices reduce power dissipation by going into thermal shutdown. They include an active-low, high-voltage-compatible shutdown input to place them in low-power shutdown mode.

The MAX16946 is available in thermally enhanced, 16-pin TQFN-EP and QSOP-EP packages. The MAX16947 is available in a 16-pin QSOP package. Both devices operate over the -40°C to +105°C temperature range.

## Ordering Information

| PART | PIN-PACKAGE | OUTPUT |
|---|---|---|
| **MAX16946**GEE/V+** | 16 QSOP-EP* | Switch or LDO |
| MAX16946GTE/V+ | 16 TQFN-EP* | Switch or LDO |
| **MAX16947**GEE/V+** | 16 QSOP | Switch |

***Note:*** *All devices are specified over the -40°C to +105°C operating temperature range.*

*/V Denotes an automotive qualified part.*

*+Denotes a lead(Pb)-free/RoHS-compliant package.*

**EP = Exposed pad.*

***Future product—contact factory for availability.*

## Features

- ♦ Switch Phantom Power-On/Off Under µC Control
- ♦ Precision Adjustable Current Limit
  - 300mA (max), $T_A$ = +105°C
  - 500mA (max), $T_A$ = +85°C (MAX16946 in SW Mode Only)
- ♦ Regulated Output Voltage (MAX16946)—8.5V Fixed or Adjustable Between 3.3V and 15V
- ♦ Current Measurement Analog Voltage Output
- ♦ Detect Open-Load and Short-Circuit Conditions
- ♦ Provide Open-Drain Fault Signals ($\overline{SC}$ and $\overline{OL}$)
- ♦ Overcurrent Blanking During Startup
- ♦ Thermal Shutdown
- ♦ AEC-Q100 Qualified
- ♦ -40°C to +105°C Operating Temperature Range

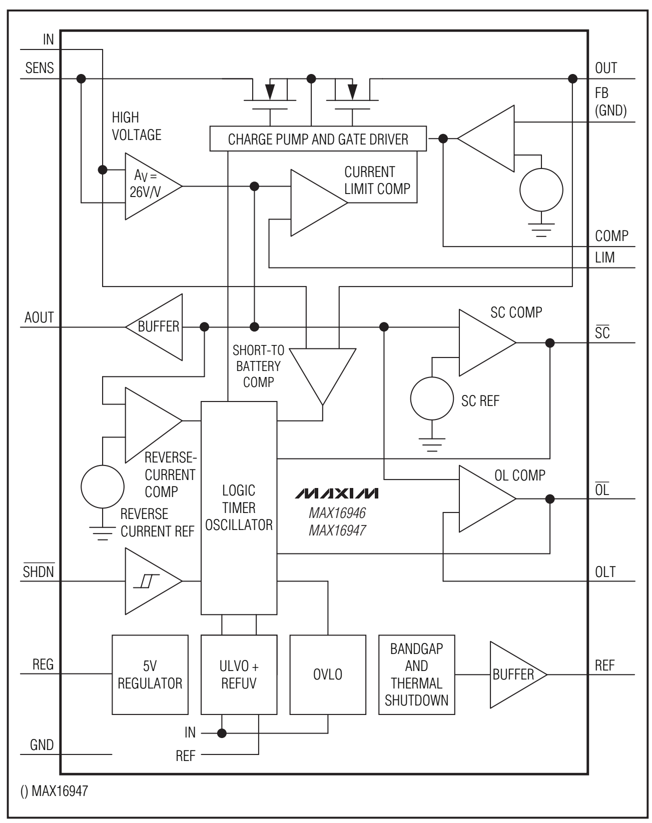
## Applications

Remote LNA Phantom Power

Automotive Safety and Infotainment

Automotive Remote Module Power

## Functional Diagram






***For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.***

# Remote Antenna, Current-Sense and LDO/Switches

## ABSOLUTE MAXIMUM RATINGS

$\overline{SC}$, $\overline{OL}$, REG to GND ....-0.3V to +6.0V
OLT, LIM, FB, AOUT, REF,
COMP to GND ....-0.3V to ($V_{REG}$ + 0.3V)
IN, SENS, $\overline{SHDN}$ to GND ....-0.3V to +28V
IN, SENS, $\overline{SHDN}$ to GND (< 1s)....-0.3V to +45V
OUT to GND ....-0.3V to +20V
IN to SENS....-0.3V to +0.3V
Continuous Power Dissipation ($T_A$ = +70°C)
QSOP (derate 9.5mW/°C above +70°C) ....761mW
QSOP-EP (derate 22.7mW/°C above +70°C)....1818mW
TQFN-EP (derate 25mW/°C above +70°C)....2000mW

Junction-to-Ambient Thermal Resistance ($\theta_{JA}$) (Note 1)
QSOP ....105°C/W
QSOP-EP....44°C/W
TQFN-EP ....40°C/W
Junction-to-Case Thermal Resistance ($\theta_{JC}$) (Note 1)
QSOP ....37°C/W
QSOP-EP....6°C/W
TQFN-EP ....6°C/W
Operating Temperature Range.... -40°C to +105°C
Junction Temperature .... -40°C to +150°C
Storage Temperature Range.... -65°C to +150°C
Lead Temperature (soldering, 10s) ....+300°C
Soldering Temperature (reflow) ....+260°C

**Note 1:** Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a four-layer board. For detailed information on package thermal considerations, refer to **www.maxim-ic.com/thermal-tutorial**.

*Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.*

## ELECTRICAL CHARACTERISTICS

($V_{IN}$ = 12V, $V_{GND}$ = 0V, $T_A$ = -40°C to +105°C, unless otherwise noted. Typical values are at $T_A$ = $T_J$ = +25°C.)

| PARAMETER | SYMBOL | CONDITIONS | | MIN | TYP | MAX | UNITS |
|---|---|---|---|---|---|---|---|
| **POWER SWITCH/LDO** | | | | | | | |
| IN Operating Supply Range | $V_{IN}$ | Full performance | | 4.5 | | 18 | V |
| | | Output switched off (Note 2) | | | | 28 | V |
| | | Output switched off for < 1s (Note 2) | | | | 45 | V |
| IN Supply Current | $I_{CC}$ | $V_{\overline{SHDN}}$ > 2.4V, $T_A$ = +25°C | | | 2.1 | 2.6 | mA |
| IN Shutdown Supply Current | $I_{SD}$ | $V_{\overline{SHDN}}$ = $V_{GND}$, $T_A$ = +25°C, $V_{IN}$ = 12V | | | | 7 | µA |
| Undervoltage Lockout (Rising) | $V_{UVLO}$ | Falling $V_{IN}$ | | | 3.5 | | V |
| | | Rising $V_{IN}$ | | | 3.9 | | |
| | | Hysteresis | | | 0.4 | | |
| Internal Switch Voltage Drop | $V_{SW}$ | Measured between SENS and OUT while sourcing 100mA, FB grounded, SW operation, $T_A$ = +25°C, 4.5V < $V_{IN}$ < 18V | | | | 0.20 | V |
| | | Measured between SENS and OUT while sourcing 100mA, FB grounded, SW operation, $T_A$ = +105°C, 4.5V < $V_{IN}$ < 18V (Note 2) | | | 0.2 | 0.25 | V |
| Internal Voltage Regulator | $V_{REG}$ | $I_{REG}$ = 0mA, $T_A$ = +25°C | | | 5 | | V |
| Feedback Voltage | $V_{FB}$ | MAX16946 only, LDO mode with FB connected to external resistive divider | $I_{OUT}$ = 5mA to 150mA, 4.5V ≤ $V_{IN}$ ≤ 18V | 0.97 | 1 | 1.03 | V |
| | | | $I_{OUT}$ = 2mA to 200mA, 4.5V < $V_{IN}$ ≤ 18V | 0.95 | 1 | 1.05 | V |

## ELECTRICAL CHARACTERISTICS (continued)

($V_{IN}$ = 12V, $V_{GND}$ = 0V, $T_A$ = -40°C to +105°C, unless otherwise noted. Typical values are at $T_A$ = $T_J$ = +25°C.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
|---|---|---|---|---|---|---|
| Feedback Input Bias Current | $I_{FB}$ | $V_{FB}$ = 1.0V, LDO mode, $T_A$ = +25°C | -0.5 | | +0.5 | µA |
| | | $V_{FB}$ = 1.0V, LDO mode, $T_A$ = +105°C | | 0 | | |
| Fixed 8.5V to LDO Mode Feedback Threshold | $V_{FB\_TH}$ | Switching to LDO mode from fixed 8.5V | 3.3 | | 4.2 | V |
| Adjustable Output Voltage Range | $V_{OUT}$ | LDO mode with external resistive divider, $V_{IN}$ > $V_{OUT}$ + $V_{DROPOUT}$ (Note 3) | 3.3 | | 15 | V |
| FB Load Regulation | | $V_{IN}$ - $V_{OUT}$ ≥ 2V, $I_{OUT}$ = 5mA to 100mA, LDO mode | | -2 | | % |
| FB Line Regulation | | $V_{IN}$ - $V_{OUT}$ ≥ 2V, $I_{OUT}$ = 6mA, LDO mode | | 20 | | mV/V |
| Fixed 8.5V Output Voltage | $V_{OUT\_8.5V}$ | $I_{OUT}$ = 5mA, LDO mode with internal resistive divider, 9V ≤ $V_{IN}$ ≤ 18V | 8.33 | 8.5 | 8.67 | V |
| Power-Supply Rejection Ratio | PSRR | $V_{IN}$ - $V_{OUT}$ ≥ 2V, f = 100Hz, LDO mode | | 50 | | dB |
| Startup Response Time | $t_{ST}$ | $\overline{SHDN}$ rising to switch/LDO on, time needed to charge $C_{COMP}$ = 0.1µF | | 10 | | ms |
| OUT Pulldown Resistor Value | $R_{OUT\_OFF}$ | $V_{\overline{SHDN}}$ = $V_{GND}$, $T_A$ = +25°C | | | 250 | kΩ |
| COMP Power-Down Resistor Value | $R_{COMP\_OFF}$ | $V_{\overline{SHDN}}$ = $V_{GND}$, $T_A$ = +25°C | | | 120 | kΩ |
| **CURRENT-SENSE AMPLIFIER** | | | | | | |
| AOUT Gain | $A_V$ | $V_{AOUT}$/($V_{IN}$ - $V_{SENS}$), measured with $V_{IN}$ - $V_{SENS}$ = 20mV and 100mV, 4.5V < $V_{IN}$ < 18V | 25.35 | 26 | 26.65 | V/V |
| Current-Sense Amplifier Input Voltage Range | $V_{INR}$ | Drop across the shunt resistor, normal operation | 0 | | 125 | mV |
| AOUT Zero-Current Output Voltage | $V_{AOUT\_ZS}$ | ($V_{IN}$ - $V_{SENS}$) = 0V, 4.5V < $V_{IN}$ < 18V | 0.368 | 0.4 | 0.432 | V |
| Maximum AOUT Voltage | $V_{AOUT\_FS}$ | ($V_{IN}$ - $V_{SENS}$) = 125mV, if $V_{LIM}$ = $V_{REF}$ then $V_{AOUT(MAX)}$ = 3V | | 3.65 | | V |
| AOUT Drive Capability | $I_{AOUT}$ | ($V_{IN}$ - $V_{SENS}$) = 30mV | 1.0 | | | mA |
| AOUT Leakage Current | $I_{AOUT\_LEAK}$ | $V_{\overline{SHDN}}$ = $V_{GND}$, $T_A$ = +25°C | 2 | | | µA |
| SENS Leakage Current | $I_{SENS\_LEAK}$ | $V_{\overline{SHDN}}$ = $V_{GND}$, $T_A$ = +25°C | | | 2 | µA |
| **REFERENCE** | | | | | | |
| REF Output Voltage | $V_{REF}$ | 4.5V < $V_{IN}$ < 18V | 2.94 | 3 | 3.06 | V |
| REF Undervoltage | $V_{REF\_UV}$ | $V_{REF}$ falling | 2.18 | | 2.72 | V |
| REF Output Current | $I_{REF}$ | | 100 | | | µA |
| REF Leakage Current | $I_{REF\_LEAK}$ | $V_{\overline{SHDN}}$ = $V_{GND}$, $T_A$ = +25°C | | | 2 | µA |
| **FAILURE DETECTION COMPARATORS** | | | | | | |
| Open-Load Comparator Input Common-Mode Range | $V_{OLT\_CMR}$ | (Note 2) | 0.4 | | 1.7 | V |
| Open-Load Comparator Offset Voltage | $V_{OLT\_OS}$ | $V_{OLT}$ = 1.05V | -40 | 0 | +40 | mV |

## ELECTRICAL CHARACTERISTICS (continued)

($V_{IN}$ = 12V, $V_{GND}$ = 0V, $T_A$ = -40°C to +105°C, unless otherwise noted. Typical values are at $T_A$ = $T_J$ = +25°C.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
|---|---|---|---|---|---|---|
| OLT Input Bias Current | $I_{OLT}$ | $V_{OLT}$ = 1.05V, $T_A$ = +25°C | -0.5 | | +0.5 | µA |
| | | $V_{OLT}$ = 1.05V, $T_A$ = +105°C | | 0 | | |
| Initial Open-Load Blanking Time | $t_{OL}$ | A switched open load is blanked for $t_{OL}$ | 100 | | | ms |
| Open-Load Glitch Immunity | $t_{OL\_GLITCH}$ | $I_{OUT}$ < $I_{OL}$ | 10 | | 100 | µs |
| Current-Limit Comparator Input Common-Mode Range | $V_{LIM\_CMR}$ | If $V_{LIM}$ is derived from REF then maximum voltage at LIM is 3V (Note 2) | 1.7 | | 3.65 | V |
| Current-Limit Comparator Input Offset Voltage | $V_{LIM\_OS}$ | $V_{LIM}$ = 2.675V | -80 | 0 | +80 | mV |
| LIM Input Bias Current | $I_{LIM\_BIAS}$ | $V_{LIM}$ = 2.675V, $T_A$ = +25°C | -0.5 | | +0.5 | µA |
| | | $V_{LIM}$ = 2.675V, $T_A$ = +105°C | | 0 | | |
| Short-Circuit AOUT Voltage Threshold | $V_{SC}$ | Rising $V_{AOUT}$ at which the $\overline{SC}$ output asserts low, hysteresis of 40mV, 4.5V < $V_{IN}$ < 18V | 1.65 | 1.7 | 1.75 | V |
| Short-Circuit Current Blanking Time | $t_{BLANK}$ | $I_{OUT}$ > $I_{SC}$ | 100 | | | ms |
| Delay Time Before Retry After Short-Circuit Current Turn-Off | $t_{RETRY}$ | $I_{OUT}$ > $I_{SC}$ | 1100 | | | ms |
| IN Overvoltage Lockout Threshold | $V_{OVLO}$ | $V_{IN}$ rising, hysteresis = 0.5V (typ) | 19 | 21 | 23 | V |
| Short-to-BAT Threshold in Off-State | $V_{OUT\_BAT}$ | Short to battery detected when $V_{IN}$ - $V_{OUT}$ < $V_{OUT\_BAT}$ | 0 | 250 | 500 | mV |
| Reverse-Current Detection Level | $V_{REV}$ | Power switch on (SW or LDO mode), $V_{REV}$ = $V_{IN}$ - $V_{SENS}$, $V_{REV}$ = -9.6mV produces $V_{AOUT}$ = 150mV, $V_{REV}$ = -5.7mV produces $V_{AOUT}$ = 250mV | -9.6 | | -5.7 | mV |
| Reverse-Current Shutdown Time | $t_{SD\_REV}$ | Delay to shut down switch or LDO after $V_{REV}$ exceeds -7.7mV (typ), $T_A$ = +25°C | | | 5 | µs |
| Feedback Voltage Out of Range | $V_{FB\_ERR}$ | LDO mode | 1.12 | | 1.28 | V |
| Reverse-Current Blanking Time for Short-Circuit Events | $t_{REV\_BLANK}$ | Switching on and off into a temporary load (short-circuit events) | | 16 | | ms |
| **OVERTEMPERATURE PROTECTION** | | | | | | |
| Thermal Shutdown Threshold | $T_{SHDN}$ | | | +170 | | °C |
| Thermal Shutdown Hysteresis | $T_{HYST}$ | | | 15 | | °C |
| **LOGIC** | | | | | | |
| $\overline{SC}$, $\overline{OL}$ Output-Voltage Low | $V_{OL}$ | Sinking current = 1mA | | | 0.4 | V |
| $\overline{SC}$, $\overline{OL}$ Open-Drain Leakage Current | $I_{\overline{SC}\_LEAK}$, $I_{\overline{OL}\_LEAK}$ | $\overline{SC}$, $\overline{OL}$ not asserted, $V_{\overline{SC}}$ = $V_{\overline{OL}}$ = 5V, $T_A$ = +25°C | | | 1 | µA |

## ELECTRICAL CHARACTERISTICS (continued)

($V_{IN}$ = 12V, $V_{GND}$ = 0V, $T_A$ = -40°C to +105°C, unless otherwise noted. Typical values are at $T_A$ = $T_J$ = +25°C.)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
|---|---|---|---|---|---|---|
| $\overline{SHDN}$ Input-Voltage High | $V_{\overline{SHDN}\_HI}$ | | 2.7 | | | V |
| $\overline{SHDN}$ Input-Voltage Low | $V_{\overline{SHDN}\_LO}$ | | | | 0.8 | V |
| $\overline{SHDN}$ Input Current | $I_{\overline{SHDN}}$ | $V_{\overline{SHDN}}$ > 6V | | 5 | | µA |
| $\overline{SHDN}$ Off-Time | $t_{\overline{SHDN}\_OFF}$ | | 150 | 256 | 420 | µs |

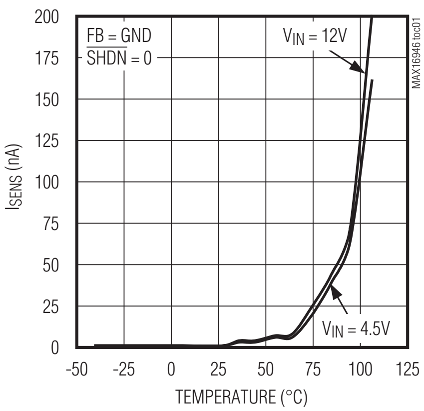
**Note 2:** Guaranteed by design and not production tested.

**Note 3:** $V_{DROPOUT}$ is voltage from $V_{IN}$ to $V_{OUT}$ and includes drop across the sense resistor and internal power FET. Additionally, $V_{OUT} + V_{DROPOUT} < V_{OVLO(MIN)}$ = 19V.

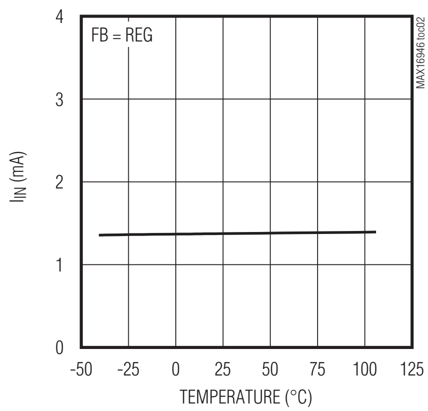
## *Typical Operating Characteristics*

($V_{IN}$ = 14V, $R_{SENSE}$ = 0.5Ω, $T_A$ = +25°C, unless otherwise noted.)

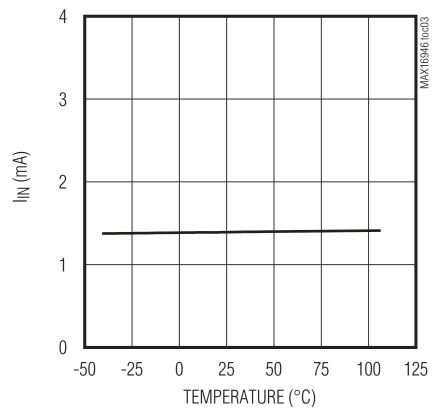
**SENSE LEAKAGE CURRENT vs. TEMPERATURE**



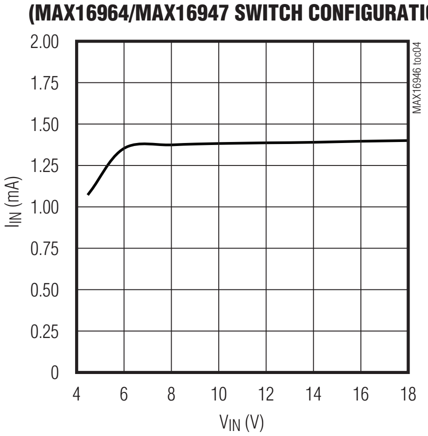

**OPERATING SUPPLY CURRENT vs. TEMPERATURE (MAX16946 8.5V LDO CONFIGURATION)**



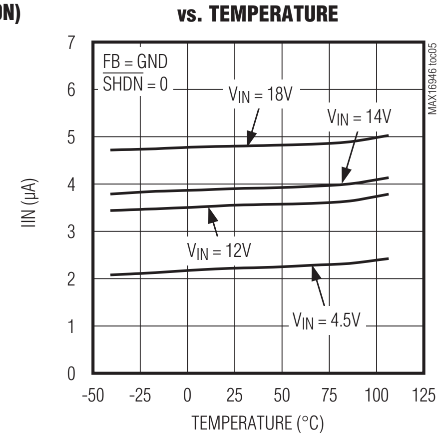

**OPERATING SUPPLY CURRENT vs. TEMPERATURE (MAX16946/MAX16947 SWITCH CONFIGURATION)**



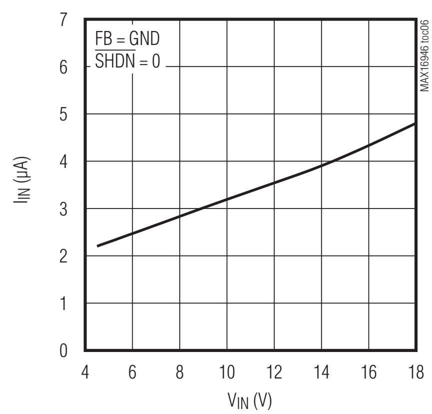

**OPERATING SUPPLY CURRENT vs. SUPPLY VOLTAGE (MAX16964/MAX16947 SWITCH CONFIGURATION)**




**SHUTDOWN SUPPLY CURRENT vs. TEMPERATURE**




**SHUTDOWN SUPPLY CURRENT vs. SUPPLY VOLTAGE**

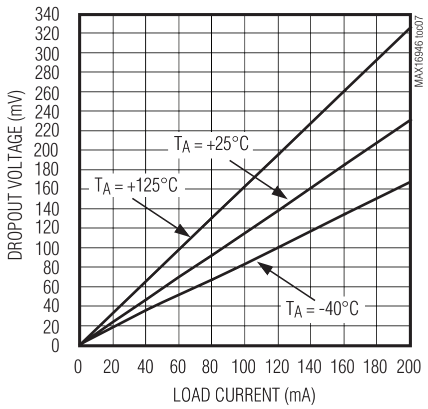


# Remote Antenna, Current-Sense and LDO/Switches

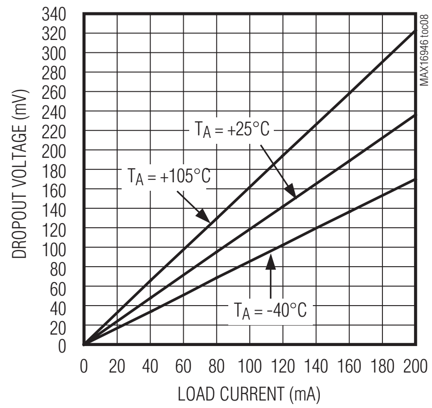
## Typical Operating Characteristics (continued)

($V_{IN}$ = 14V, $R_{SENSE}$ = 0.5Ω, $T_A$ = +25°C, unless otherwise noted.)

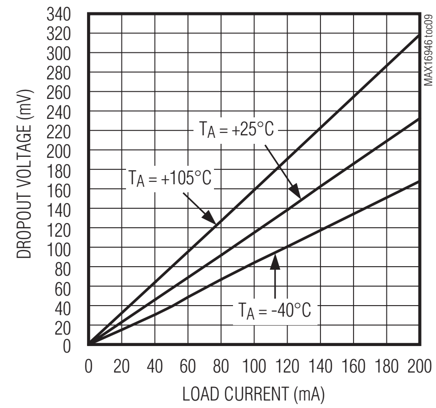
**DROPOUT VOLTAGE vs. LOAD CURRENT (SWITCHED OUTPUT)**



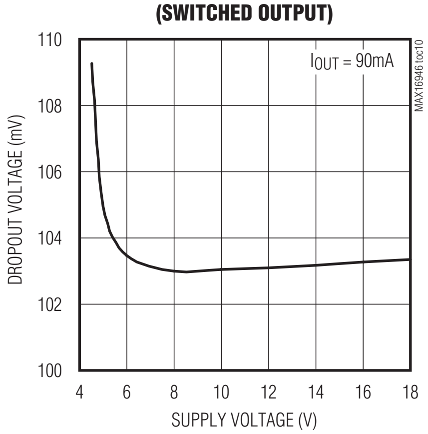

**DROPOUT VOLTAGE vs. LOAD CURRENT (OUTPUT = 5V)**



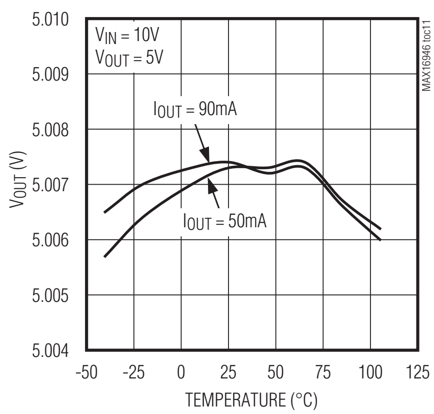

**DROPOUT VOLTAGE vs. LOAD CURRENT (OUTPUT = 8.5V)**



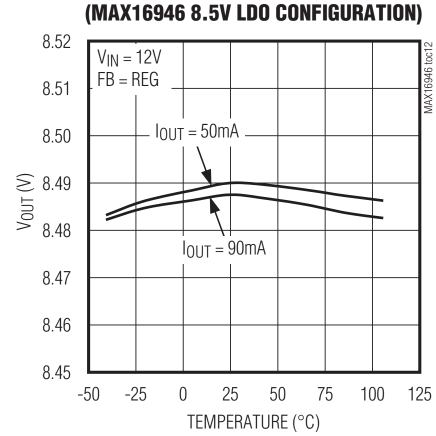

**DROPOUT VOLTAGE vs. SUPPLY VOLTAGE (SWITCHED OUTPUT)**



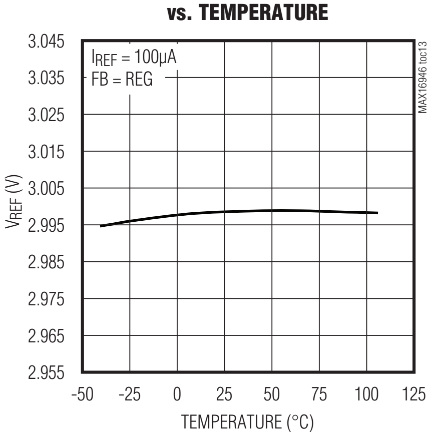

**OUTPUT VOLTAGE vs. TEMPERATURE**



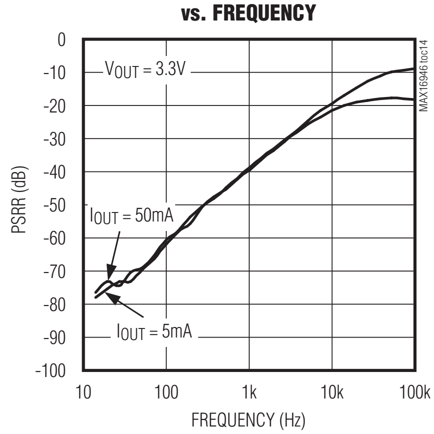

**OUTPUT VOLTAGE vs. TEMPERATURE (MAX16946 8.5V LDO CONFIGURATION)**



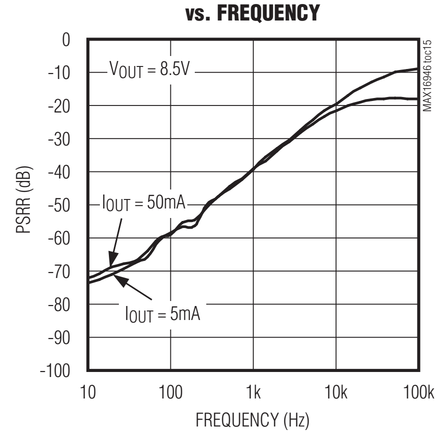

**REF OUTPUT VOLTAGE vs. TEMPERATURE**




**POWER-SUPPLY REJECTION RATIO vs. FREQUENCY**



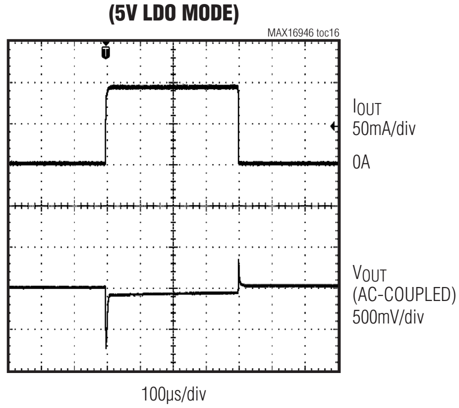

**POWER-SUPPLY REJECTION RATIO vs. FREQUENCY**



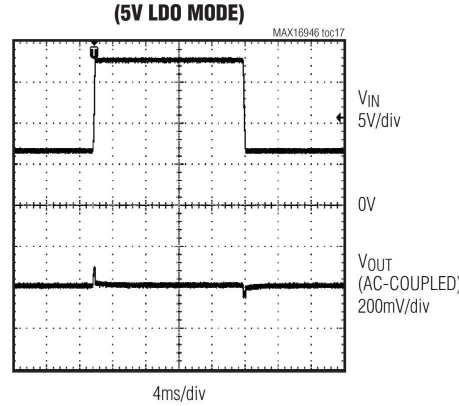
## Typical Operating Characteristics (continued)

($V_{IN}$ = 14V, $R_{SENSE}$ = 0.5Ω, $T_A$ = +25°C, unless otherwise noted.)

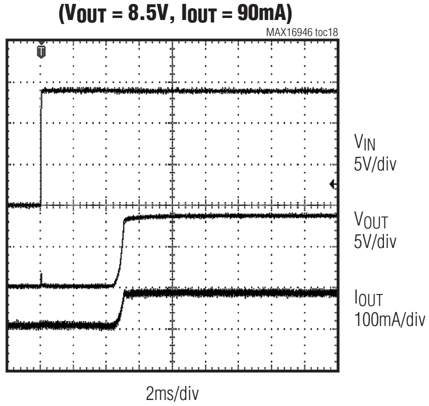
**LOAD TRANSIENT RESPONSE (5V LDO MODE)**



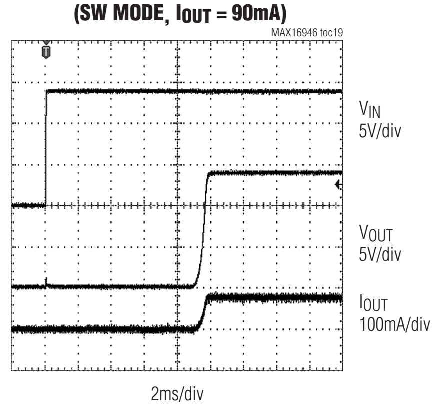

**LINE TRANSIENT RESPONSE (5V LDO MODE)**



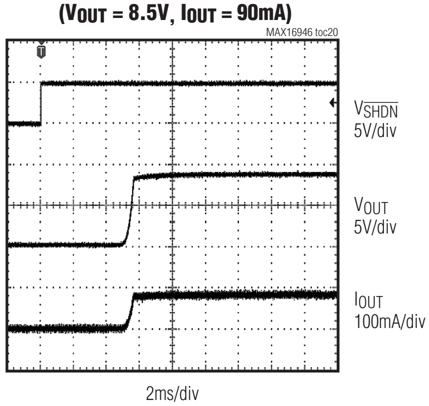

**POWER-UP WAVEFORMS ($V_{OUT}$ = 8.5V, $I_{OUT}$ = 90mA)**



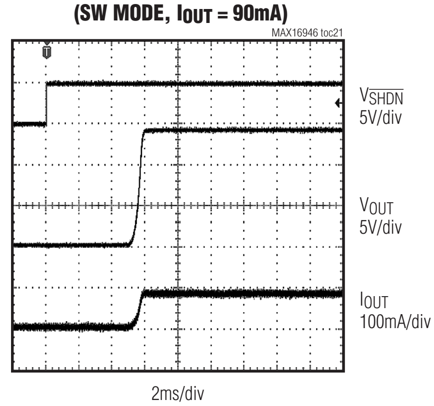

**POWER-UP WAVEFORMS (SW MODE, $I_{OUT}$ = 90mA)**




**STARTUP WAVEFORMS ($V_{OUT}$ = 8.5V, $I_{OUT}$ = 90mA)**




**STARTUP WAVEFORMS (SW MODE, $I_{OUT}$ = 90mA)**

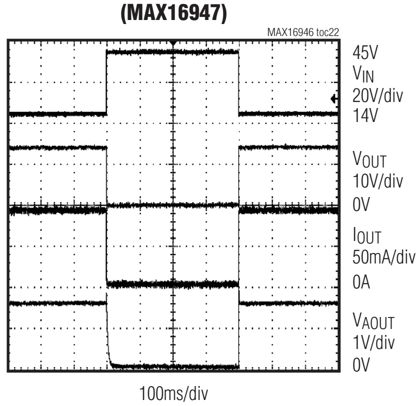


# Remote Antenna, Current-Sense and LDO/Switches

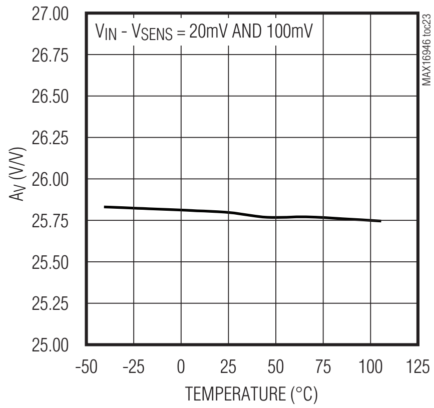
## Typical Operating Characteristics (continued)

($V_{IN}$ = 14V, $R_{SENSE}$ = 0.5Ω, $T_A$ = +25°C, unless otherwise noted.)

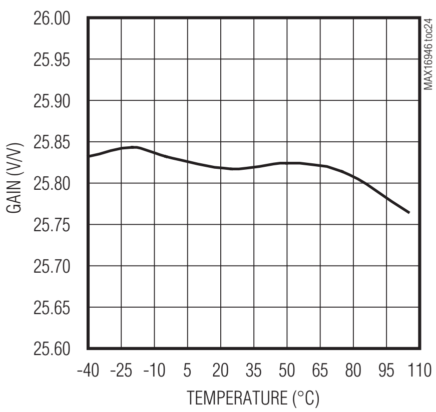
**HIGH-VOLTAGE LINE TRANSIENT RESPONSE (MAX16947)**



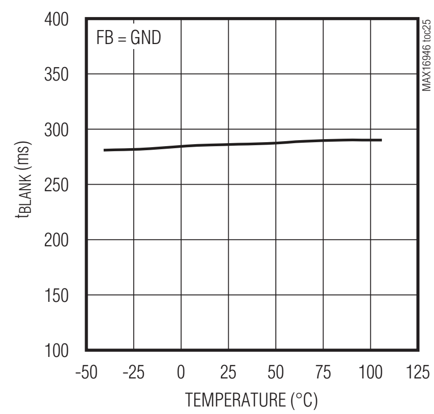

**AOUT GAIN vs. TEMPERATURE**



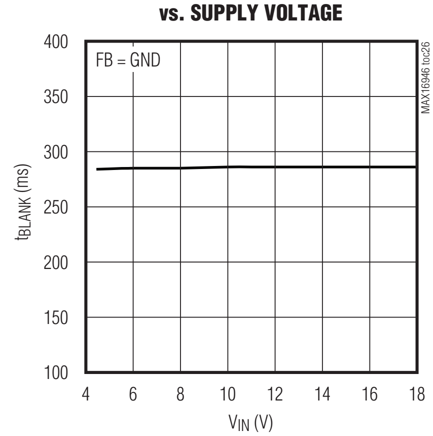

**CURRENT-SENSE AMPLIFIER GAIN vs. TEMPERATURE**



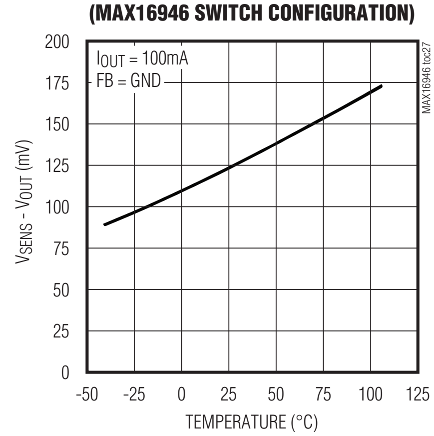

**OVERCURRENT BLANKING TIME vs. TEMPERATURE**




**OVERCURRENT BLANKING TIME vs. SUPPLY VOLTAGE**

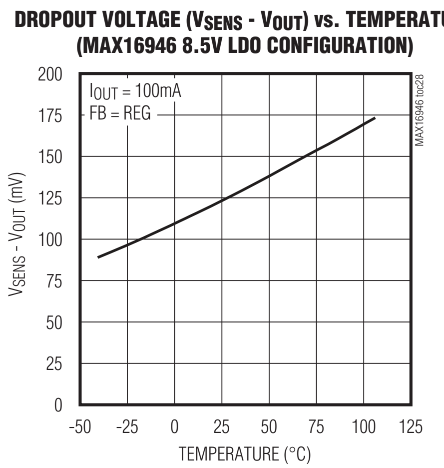


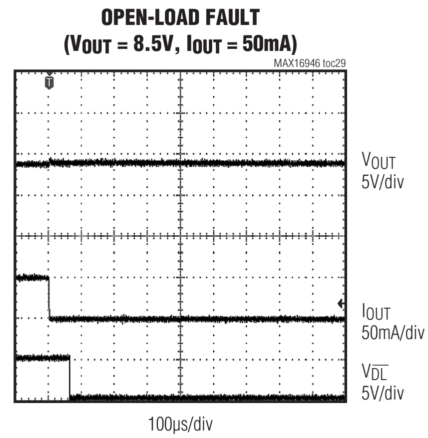

**DROPOUT VOLTAGE ($V_{SENS}$ - $V_{OUT}$) vs. TEMPERATURE (MAX16946 SWITCH CONFIGURATION)**

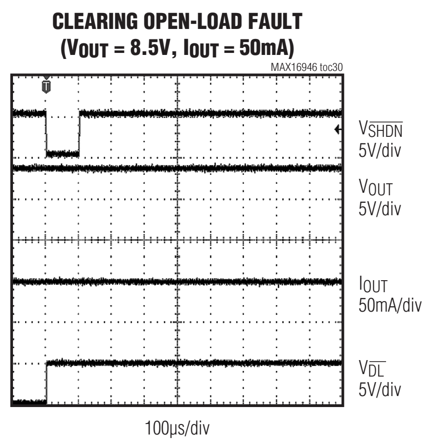


## Typical Operating Characteristics (continued)

($V_{IN}$ = 14V, $R_{SENSE}$ = 0.5Ω, $T_A$ = +25°C, unless otherwise noted.)

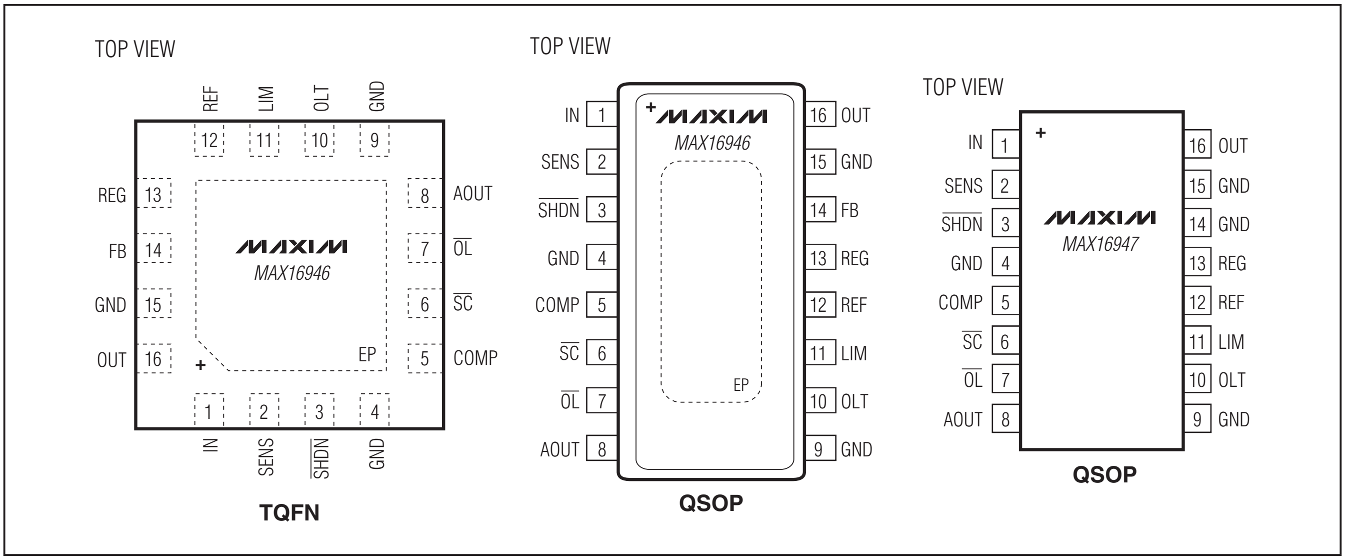


# Remote Antenna, Current-Sense and LDO/Switches

## Pin Configurations




## Pin Description

| PIN | | NAME | FUNCTION |
|---|---|---|---|
| MAX16946 | MAX16947 | | |
| 1 | 1 | IN | Input Voltage. Bypass IN to GND with a low-ESR ceramic capacitor with a minimum value of 0.1µF. |
| 2 | 2 | SENS | Current-Sense Amplifier Input. Connect the sense resistor between SENS and IN. |
| 3 | 3 | $\overline{SHDN}$ | Active-Low Shutdown Input. Drive $\overline{SHDN}$ low for more than 360µs to turn off the device. Pulsing $\overline{SHDN}$ low for less than $t_{SHDN\_OFF}$ clears the $\overline{OL}$ output. $\overline{SHDN}$ is high-voltage compatible and is connected to IN for normal operation. |
| 4, 9, 15 | 4, 9, 14, 15 | GND | Ground |
| 5 | 5 | COMP | LDO Compensation. Connect a 0.1µF ceramic capacitor between COMP and GND to compensate the LDO. |
| 6 | 6 | $\overline{SC}$ | Open-Drain Short-Circuit Indicator Output. $\overline{SC}$ goes low when the load current is greater than the set short-circuit current threshold or when there is a short-to-battery fault. Connect $\overline{SC}$ to a 10kΩ pullup resistor. See Table 1. |
| 7 | 7 | $\overline{OL}$ | Open-Drain Open-Load Indicator Output. $\overline{OL}$ goes low when the load current is lower than the set open-load current threshold or when there is a short-to-battery fault. Connect $\overline{OL}$ to a 10kΩ pullup resistor. See Table 1. |
| 8 | 8 | AOUT | Current Monitor Voltage Output. AOUT can be used to measure the load current by means of an external ADC. AOUT has a current drive capability of 1mA. Bypass AOUT to GND with a 15nF ceramic capacitor. See Table 1. |
| 10 | 10 | OLT | Open-Load Current Threshold Setting Input. A resistive divider between REF, OLT, and GND sets the open-load current threshold. |
| 11 | 11 | LIM | Current-Limit Setting input. Connect a resistive divider from REF, LIM, and GND to set the current limit of the switch or LDO. Alternatively, externally drive LIM (not to exceed 3.65V) to set the current limit. |

## Pin Description (continued)

| PIN | | NAME | FUNCTION |
|---|---|---|---|
| MAX16946 | MAX16947 | | |
| 12 | 12 | REF | +3V Nominal Reference Output. REF has a current drive capability of 100µA. |
| 13 | 13 | REG | Internal Regulator +5V Output. REG powers all internal blocks. Do no use REG to supply power to external circuitry. Bypass REG to GND with a 1µF capacitor. |
| 14 | — | FB | Feedback Input (MAX16946 Only). Connect FB to GND to configure the MAX16946 as a switch. Connect FB to REG for an LDO with a fixed 8.5V output. Connect to the center tap of an external resistive divider connected between OUT and GND to adjust the output voltage of the LDO. |
| 16 | — | OUT | Switch or LDO Output (MAX16946 Only). OUT is either a switch or LDO output depending on the connection of FB. |
| — | 16 | OUT | Switch Output |
| — | — | EP | Exposed Pad (MAX16946 Only). Connect EP to the ground plane for optimal heat dissipation. Do not use EP as the only electrical ground connection. |

## Detailed Description

The MAX16946/MAX16947 high-voltage, high-side, current-sense LDO/switches feature internal current limiting to prevent system damage due to fault conditions. The MAX16946 provides a regulated 8.5V output voltage fixed or adjustable from 3.3V to 15V. The MAX16946 can also be configured as a switch, while the MAX16947 is only available as a switch. The input voltage range for both devices extends from 4.5V to 18V (45V tolerant), making the devices ideal for providing phantom power to remote radio-frequency low-noise amplifiers (LNAs) in automotive applications.

The devices monitor the load current and provide an analog output voltage proportional to the sensed load current. Accurate internal current-limit protects the input supply against both overload and short-circuit conditions. Two open-drain fault indicator outputs indicate to the microprocessor when a short circuit, an open-load condition, or a short-to-battery condition exists. An overtemperature shutdown is also indicated by means of the current-sense amplifier's output voltage.

A fault-blanking feature allows the devices to ignore momentary faults such as those caused by the charging of capacitive loads during hot-swapping, preventing false alarms to the system. The devices feature short-to-battery protection to latch off the internal LDO/pass switch during a short-to-battery event and thermal overload. They include an active-low, high-voltage-compatible shutdown input to place them in low-power shutdown mode.

### Current-Sense Amplifier

The integrated current-sense amplifier employs a differential amplifier that amplifies the voltage between IN and SENS. A sense resistor, $R_{SENSE}$, is connected across IN and SENS. Typical sense resistor values range between 0.25Ω and 2Ω. When the load current passes through the sense resistor, a voltage drop develops across it. The current-sense amplifier amplifies this voltage.

The current-sense amplifier features an internally fixed gain of $A_V$ = 26V/V (typ). The following equations show the relationship between the current-sense amplifier output voltage ($V_{AOUT}$) and load current:

$$(V_{IN} - V_{SENS})(V) = I_{LOAD}(A) \times R_{SENSE}(\Omega)$$

$$V_{AOUT}(V) = A_V(V/V) \times (V_{IN} - V_{SENS})\ (V) + 0.4V$$

If LIM is connected to REF, the maximum output voltage of AOUT is $V_{AOUT\_FS}$ = 3V. If LIM is externally driven to 3.65V, the maximum output voltage of AOUT extends to $V_{AOUT\_FS}$ = 3.65V. The maximum AOUT voltage is always equal to $V_{LIM}$, the voltage at LIM.

AOUT is the output of an internal buffer with 1mA current drive capability. Bypass AOUT to ground with a 15nF ceramic capacitor.

# Remote Antenna, Current-Sense and LDO/Switches

### Load Protection

The devices monitor the load current through an external sense resistor and perform the following actions:

- If the monitored current is lower than the set open-load current, the devices signal that there is an open-load (see the *Open Load* section).
- If the monitored current is greater than the set short-circuit current ($I_{SC}$), the devices enter the short-circuit mode (see the *Short Circuit and Current Limit* section).

The devices also perform a short-to-battery detection before the internal switch turns on. During normal operation, reverse-current detection protects the devices from short-to-battery events (see the *Short-to-Battery and Reverse-Current Detection* section).

In addition, thermal shutdown protects the devices from overheating (see the *Thermal Shutdown* section).

Two open-drain fault indicator outputs ($\overline{OL}$ and $\overline{SC}$) and the AOUT voltage indicate the devices' status (Table 1).

### Open Load

If the load current drops below the open-load current threshold, the $\overline{OL}$ output latches low. An open-load condition does not turn off the internal switch. To unlatch the $\overline{OL}$ output, pulse $\overline{SHDN}$ low for less than $t_{\overline{SHDN\_OFF}}$ (150µs min). Keeping $\overline{SHDN}$ low for longer than $t_{\overline{SHDN\_OFF}}$ shuts down the device.

The open-load current threshold is adjustable. Connect a resistive divider between REF, the open-load current threshold adjustment input (OLT), and GND to set the open-load current threshold (see the *Open-Load Current Threshold Selection* section).

### Short Circuit and Current Limit

If the load current exceeds the set short-circuit current threshold ($I_{SC}$), the $t_{BLANK}$ timer begins counting. During this period, the load current is limited to the current limit set by the voltage at LIM. If the overcurrent condition persists beyond $t_{BLANK}$, $\overline{SC}$ asserts low and the internal switch turns off. The timer resets if the overcurrent condition disappears before the blanking time ($t_{BLANK}$) has elapsed.

If the switch is turned off at the end of $t_{BLANK}$, a retry timer ($t_{RETRY}$) starts immediately after the blanking time has elapsed, and during that time the switch stays off. At the end of $t_{RETRY}$, the switch turns on again while $\overline{SC}$ stays low. If the fault still exists, the cycle repeats. If the fault has been removed, the switch stays on and $\overline{SC}$ goes high after the blanking time $t_{BLANK}$. During retry when the switch is off, the current through the switch is zero. Blanking time and retry time have fixed values of 100ms (min) and 1100ms (min), respectively.

Figures 1–4 show the response of the devices to the presence and removal of overcurrent conditions.

The current-limit threshold is adjustable. Connect a resistive divider between REF, the current-limit setting input (LIM), and GND to set the current-limit threshold. Alternatively, externally drive LIM (not to exceed 3.65V) to set the current-limit threshold (see the *Current-Limit Threshold Selection* section).

The short-circuit current threshold depends on the value of the sense resistor and is calculated as follows:

$$I_{SC} = \frac{1.3V}{R_{SENSE} \times A_V}$$

where $A_V$ is the gain of the internal current-sense amplifier and is equal to 26V/V and $R_{SENSE}$ is the sense resistor value.

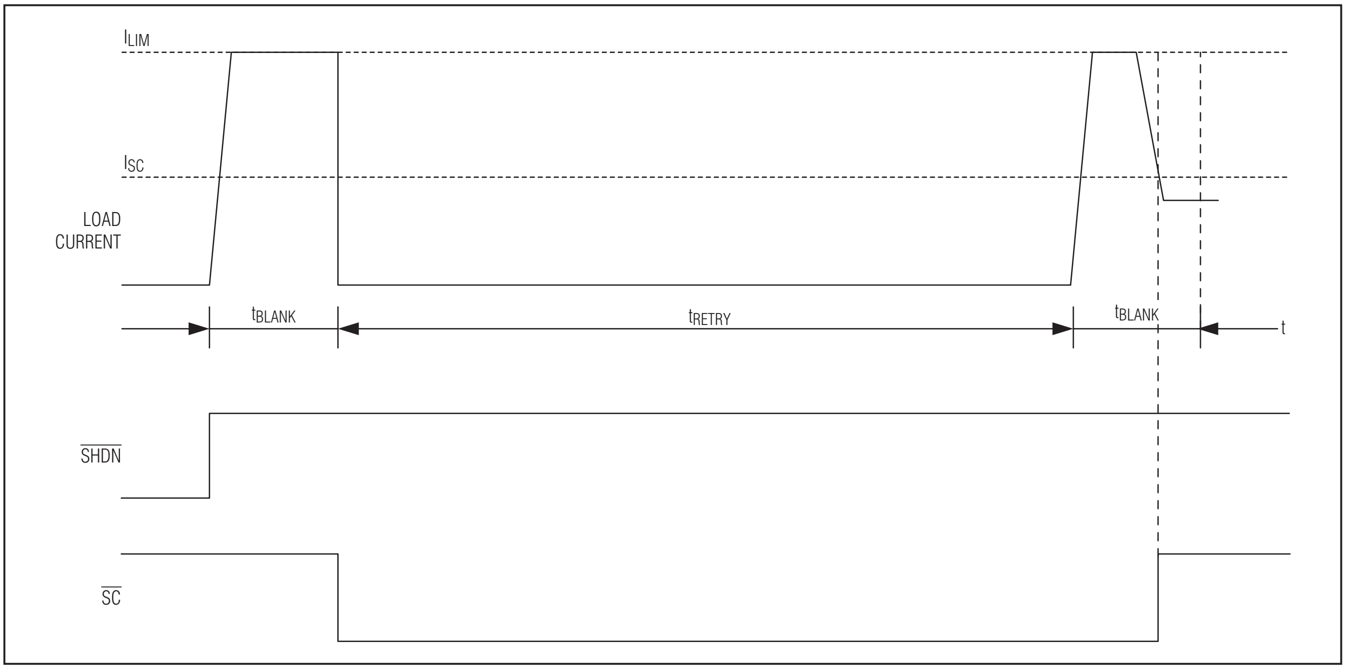



*Figure 1. Turn-On into Temporary Short Circuit*

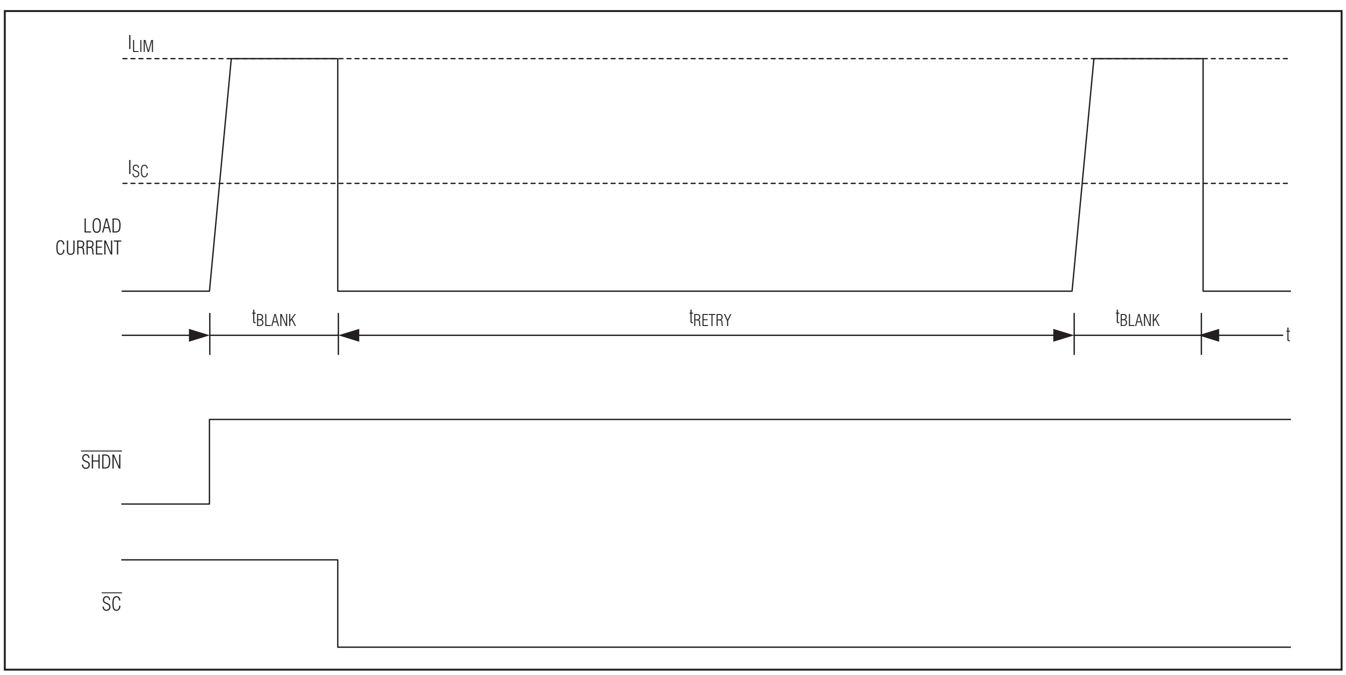



*Figure 2. Turn-On into Hard Short Circuit*

# Remote Antenna, Current-Sense and LDO/Switches

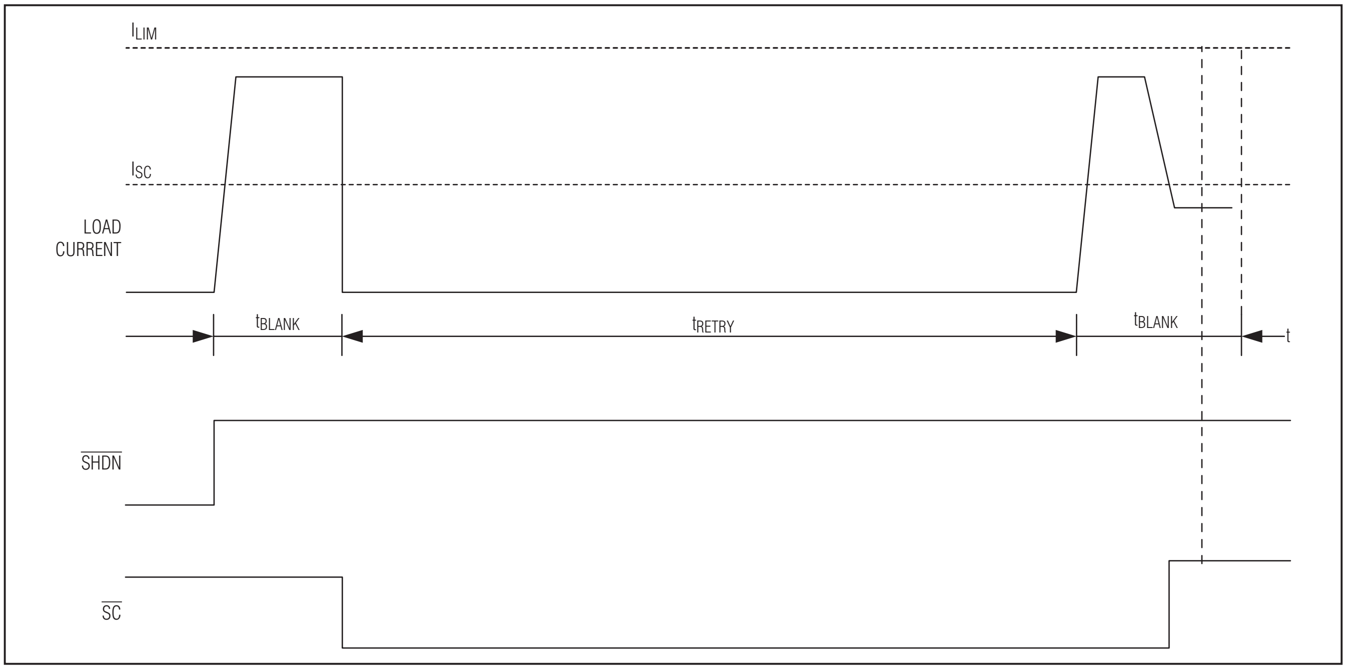



*Figure 3. Turn-On into Temporary Heavy Load*

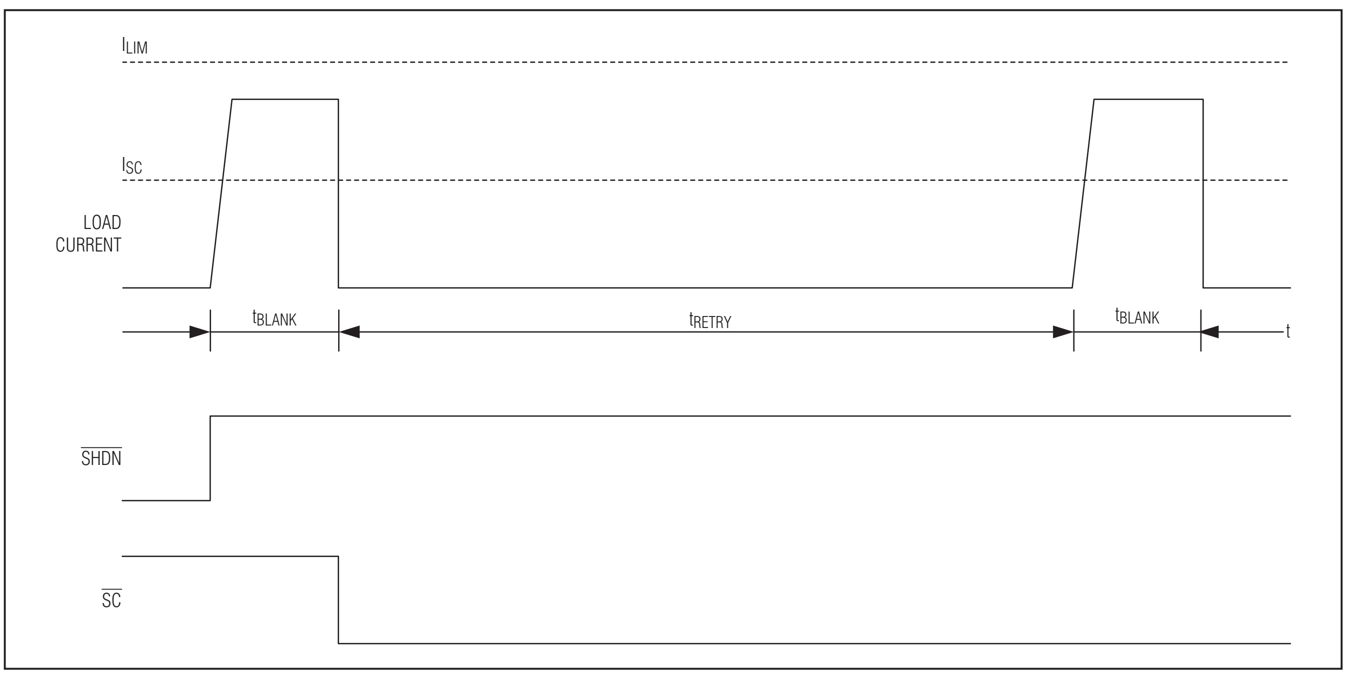



*Figure 4. Turn-On into Heavy Load*

### Short-to-Battery and Reverse-Current Detection

It is possible for OUT to be shorted to the battery due to a fault in the system. The devices detect this failure by comparing the OUT voltage and the IN voltage before the switch turns on. Every time the switch turns on, such as at the end of the retry time, or once the thermal shutdown condition disappears, the short-to-battery detection is performed. At this point, if the device detects the short-to-battery fault, the switch stays off and both $\overline{SC}$ and $\overline{OL}$ assert low (Table 1).

Series inductance and the output capacitor can produce ringing during a short-circuit condition, resulting in an output voltage that temporarily exceeds the input voltage. Blanking is implemented during and immediately after a short-circuit event to prevent false triggering of the reverse-current detection. The reverse-current blanking time ($t_{REV\_BLANK}$) is 16ms (typ). If the reverse current produces a $V_{SENSE}$ ($V_{IN}$ - $V_{SENSE}$) less than -7.7mV (typ) for a duration greater than the blanking time, the device latches off the switch and both $\overline{SC}$ and $\overline{OL}$ assert low.

### Thermal Shutdown

Thermal-shutdown circuitry protects the devices from overheating. The switch turns off immediately when the junction temperature exceeds +170°C (typ) (Table 1). The switch turns on again after the device temperature drops by approximately +15°C (typ). Thermal shutdown is indicated by 0V on AOUT.

### Undervoltage and Overvoltage Lockout

The devices include undervoltage lockout circuitry (UVLO) to prevent erroneous switch operation when the input voltage goes below 3.5V (typ) during startup and brownout conditions. Input voltages of less than 3.5V inhibit operation of the device by turning off the internal charge pump and the switch.

These devices also feature an overvoltage lockout (OVLO) threshold of 21V (typ). When $V_{IN}$ is greater than $V_{OVLO}$, the device immediately turns off the switch and the internal charge pump.

### Shutdown ($\overline{SHDN}$)

The devices feature an active-low shutdown input ($\overline{SHDN}$) to place them into a low-power shutdown mode. The devices turn off and consume a 7μA maximum (at $V_{IN}$ = 12V) of shutdown current when $\overline{SHDN}$ is driven low for greater than 360μs. Driving $\overline{SHDN}$ high initiates a device turn-on with short-to-battery detection. Pulsing $\overline{SHDN}$ low for less than $t_{\overline{SHDN\_OFF}}$ clears the $\overline{OL}$ output.

### Internal Reference (REF)

The devices feature a 3V bandgap reference output, stable over supply voltage and temperature. The reference has a current drive capability of 100μA. Use resistive dividers connected to REF to set the open-load current threshold and the current-limit threshold. Do not use REF to drive external circuitry.

### Internal +5V Linear Regulator (REG)

The devices feature an internal regulator that regulates the input voltage to +5V to power all internal circuitry. Bypass the regulator output (REG) to GND with a 1μF ceramic capacitor. Do not use this regulator to power external circuitry.

## Table 1. MAX16946/MAX16947 Status Truth Table

| $\overline{SC}$ | $\overline{OL}$ | $V_{AOUT}$ (V) | DEVICE STATUS | ACTION TAKEN |
|---|---|---|---|---|
| 1 | 1 | ($I_{LOAD}$ x $R_{SENSE}$) x 26 + 0.4 | Normal operation | None |
| 0 | 1 | ($I_{LOAD}$ x $R_{SENSE}$) x 26 + 0.4 | Short circuit | Autoretry |
| 1 | 0 | ($I_{LOAD}$ x $R_{SENSE}$) x 26 + 0.4 | Open load | $\overline{OL}$ latched low |
| 0 | 0 | 0.4 after switching off | Reverse current (on-state) | Switch/LDO latched off |
| | | | OUT short-to-battery (off-state), $V_{OUT}$ too high ( LDO mode) | Switch/LDO turned off as long as condition persists |
| 1 | 1 | 0 | Thermal shutdown, $V_{IN}$ overvoltage, $V_{IN}$ undervoltage | Switch/LDO and AOUT turns off as long as condition persists |
| | | | REF undervoltage | Switch/LDO, AOUT, and REF turned off as long as condition persists |

# Remote Antenna, Current-Sense and LDO/Switches

## Applications Information

### Choosing the Sense Resistor

Ideally, the maximum load current develops the full-scale sense voltage across the current-sense resistor. The current-sense amplifier output voltage is given by:

$$V_{AOUT} = A_V \times (V_{IN} - V_{SENS}) + 0.4V$$

where $V_{AOUT}$ is the output voltage of the current-sense amplifier, and $A_V$ is the gain of the current-sense amplifier of 26V/V (typ).

Calculate the maximum value for $R_{SENSE}$, so that the amplified differential voltage across IN and SENS does not exceed the short-circuit AOUT voltage threshold of $V_{SC}$ = 1.7V (typ), which is defined in the *Electrical Characteristics* table:

$$R_{SENSE} = \frac{V_{SC} - 0.4V}{I_{LOAD(FULL\_SCALE)} \times A_V}$$

Typical sense resistor values range between 0.25Ω and 2Ω.

During normal operation, when the load current is less than the short-circuit current threshold, the maximum AOUT voltage is equal to $V_{SC}$. When a short circuit to ground is present and the device goes into autoretry, the maximum AOUT voltage extends to $V_{LIM}$, the voltage at LIM.

Keep inductance low if $I_{SENSE}$ has a large high-frequency component. Wire-wound resistors have the highest inductance, while metal film is somewhat better. Low-inductance, metal-film resistors are also available. Instead of being spiral wrapped around a core, as in metal-film or wire-wound resistors, they are a straight band of metal and are available in values under 1Ω.

Because of the high current that flows through $R_{SENSE}$, eliminate parasitic trace resistance from causing errors in the sense voltage.

### Open-Load Current Threshold Selection

A resistive divider between REF, OLT, and GND sets the open-load current threshold. See Figure 5.

Use the following formula to set the desired open-load current threshold:

$$R_2 = \frac{R_1}{\left(\frac{V_{REF}}{R_{SENSE} \times I_{OL} \times A_V + 0.4V} - 1\right)}$$

where $I_{OL}$ is the desired open-load current threshold, $A_V$ is the current-sense amplifier gain (26V/V typical), and $V_{REF}$ is the reference voltage (3V typ). Size $R_1$ and $R_2$ large enough so that the equivalent resistance of the resistive dividers used to set the open-load and current-limit thresholds does not exceed the REF output 100µA drive capability.

For example, to set the open-load current threshold at 10mA, using a 0.5Ω sense resistor, use the following method to calculate the value of $R_1$ and $R_2$:

$$R_2 = \frac{R_1}{\left(\frac{3V}{0.5\Omega \times 0.01A \times 26V/V + 0.4V} - 1\right)}$$

Choose $R_1$ = 470kΩ and calculate $R_2$ as 100kΩ.

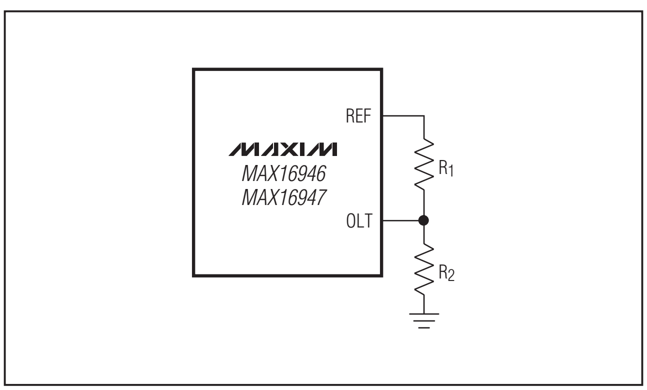



*Figure 5. Open-Load Current Threshold Selection*

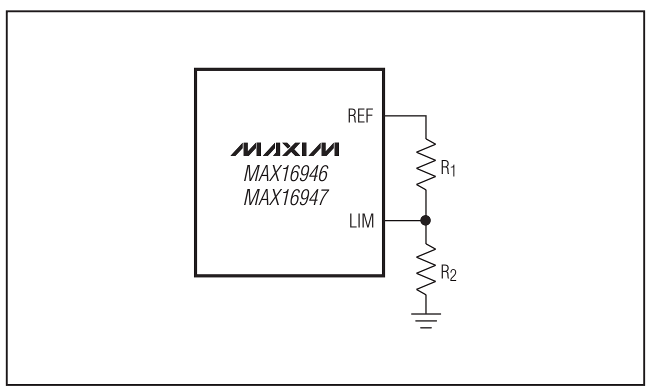



*Figure 6. Current-Limit Threshold Selection*

### Current-Limit Threshold Selection

A resistive divider between REF, LIM, and GND sets the current-limit threshold. See Figure 6.

Use the following formula to set the desired current-limit threshold:

$$R_2 = \frac{R_1}{\left(\frac{V_{REF}}{R_{SENSE} \times I_{CL} \times A_V + 0.4V} - 1\right)}$$

where $I_{CL}$ is the desired current-limit threshold, $A_V$ is the current-sense amplifier gain (26V/V typ), and $V_{REF}$ is the reference voltage (3V typ). Size $R_1$ and $R_2$ large enough so that the equivalent resistance of the resistive dividers used to set the open-load and current-limit thresholds does not exceed the REF output 100µA drive capability.

For example, to set the current-limit threshold at 120mA, using a 0.5Ω sense resistor, use the following method to calculate the value of $R_1$ and $R_2$:

$$R_2 = \frac{R_1}{\left(\frac{3V}{0.5\Omega \times 0.120A \times 26V/V + 0.4V} - 1\right)}$$

Choose $R_1$ = 83kΩ and calculate $R_2$ as 156kΩ.

### Using an External Reference

Use an external reference with resistive dividers as an alternative means of setting the current-limit and open-load current thresholds. The equations shown in the *Open-Load Current Threshold Selection* and *Current-Limit Threshold Selection* sections are still applicable when using an external reference. In those equations, set $V_{REF}$ equal to the voltage of the external reference.

When using the devices' 3V reference, the maximum voltage at LIM is $V_{LIM}$ = 3V and is obtained by connecting LIM to REF. When using an external reference, set the voltage at LIM to no greater than $V_{LIM(MAX)}$ = 3.65V.

### Fixed/Adjustable Output Voltage

The MAX16946 is configurable to provide a fixed 8.5V output or as an adjustable LDO with an output between 3.3V and 15V. Connect a resistive divider between OUT, FB, and GND to set the output to the desired voltage, as shown in Figure 7. Connect FB to REG to configure the MAX16946 as an 8.5V LDO, as shown in Figure 8. FB is regulated to 1.0V with ±3% accuracy for a load current between 5mA and 150mA. The accuracy falls to ±5% for a load current between 2mA and 200mA. Select a value for $R_1$ and calculate $R_2$ as follows:

$$R_2 = \frac{R_1}{\left(\frac{V_{OUT}}{V_{FB}} - 1\right)}$$

Select $R_1$ so that the maximum input bias current at FB is negligible compared to the total current going through $R_1$.

### Compensation Capacitor

Compensate the LDO regulator by bypassing COMP to GND with a 0.1µF ceramic capacitor.

### Input Capacitor

Connect a low-leakage ceramic capacitor from IN to GND to limit the input-voltage drop during momentary output short-circuit conditions and to protect the device against transients due to inductance in the IN line. For example, use at least a 0.1µF ceramic capacitor if the input inductance (including any stray inductance) is estimated to be 20µH. Larger capacitor values reduce the voltage undershoot and voltage overshoot in case of reverse current at the input.

### Output Capacitor

In an analogous fashion to the input capacitor, an output capacitor protects the device against transients due to any series inductance in the output. Under no conditions should the voltage on OUT go below -0.3V as specified in the *Absolute Maximum Ratings* section. A Schottky diode is required to clamp transients that go below ground. For example, with a 2.2mH series inductance, to avoid excessive ringing at the output, bypass OUT to GND with not more than 0.1µF capacitance. Additionally, bypassing OUT to GND with a 2.2µF ceramic capacitor in series with a 10Ω resistor reduces ringing caused by load current transients through a maximum 2.2mH series inductance.

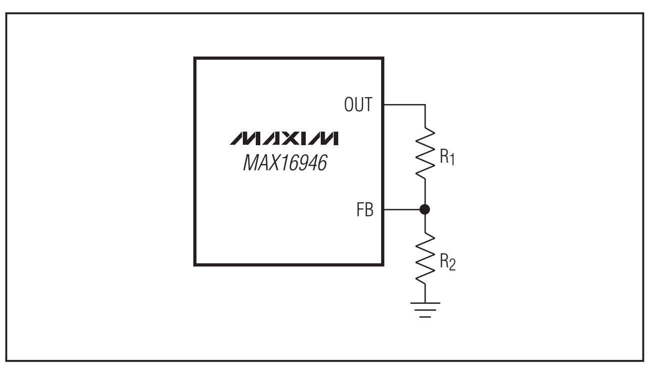



*Figure 7. Adjustable Output-Voltage Selection*

# Remote Antenna, Current-Sense and LDO/Switches

### Layout and Thermal Dissipation

To optimize the switch response time to output short-circuit condition, it is very important to keep all traces as short as possible to reduce the effect of undesirable parasitic inductance. Place input and output capacitors as close as possible to the device (no more than 5mm). IN and OUT must be connected with wide short traces to the power bus. During normal operation in switch mode, the power dissipation is small and the package temperature change is minimal. In LDO mode, the power dissipation is given by:

$$(V_{IN} - V_{OUT}) \times I_{LOAD} + V_{IN} \times I_{IN}$$

If the output is continuously shorted to ground at the maximum supply voltage, the devices are protected because the total power dissipated during the short is scaled down by the duty cycle imposed by the protection:

$$P_{(MAX)} = \frac{V_{VIN(MAX)} \times I_{OUT(MAX)} \times t_{BLANK}}{t_{RETRY} + t_{BLANK}}$$

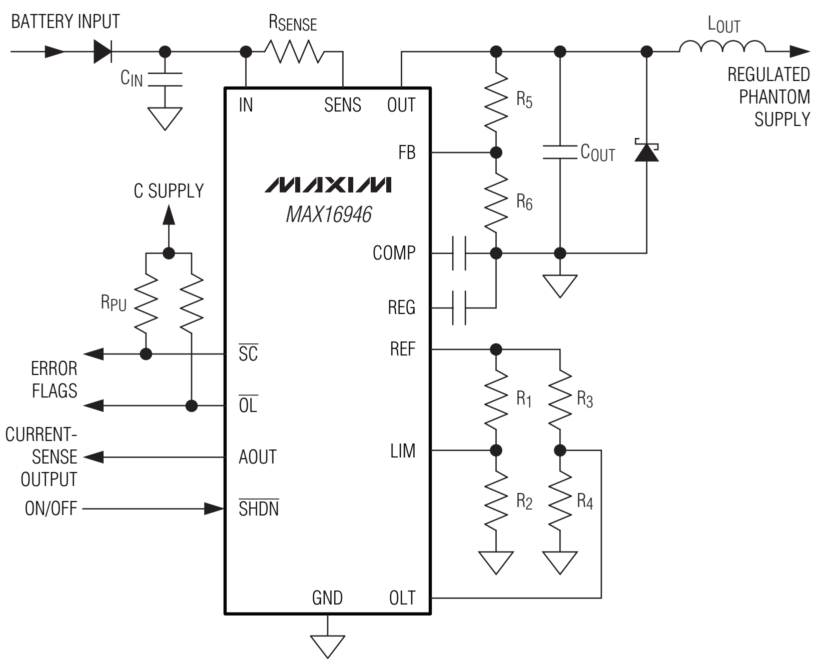



*Figure 8. LDO with Adjustable Output Voltage (3.3V to 15V)*

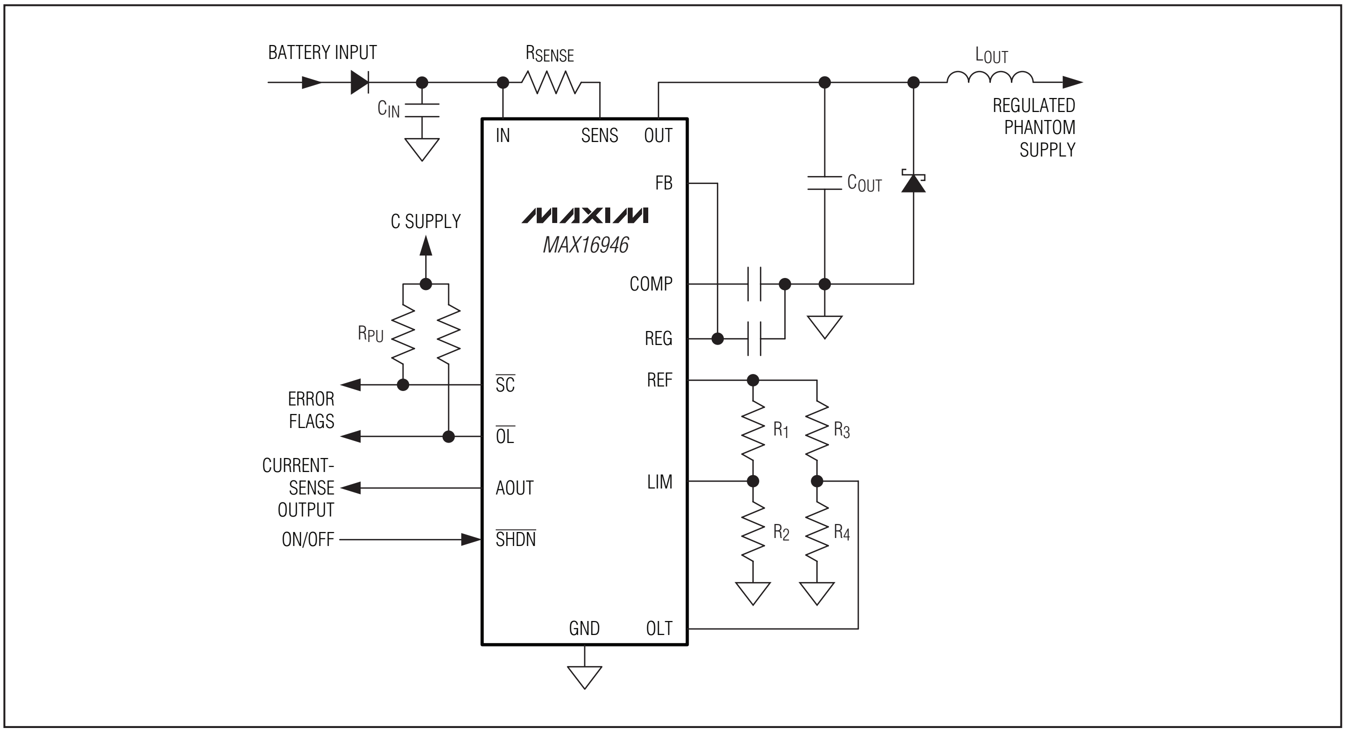



*Figure 9. LDO with Fixed 8.5V Output*

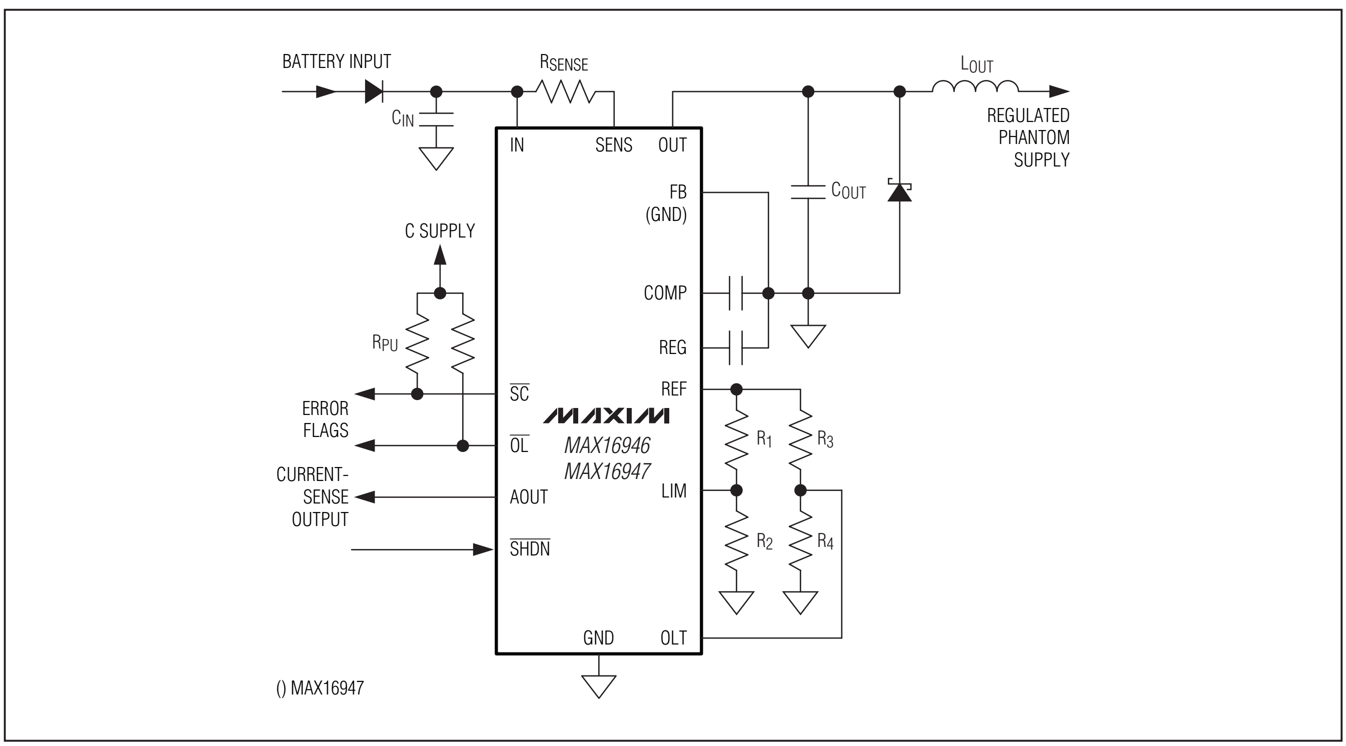



*Figure 10. Input Switched to Output*

# Remote Antenna, Current-Sense and LDO/Switches

## Chip Information

PROCESS: BiCMOS

## Package Information

For the latest package outline information and land patterns, go to **www.maxim-ic.com/packages**. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

| PACKAGE TYPE | PACKAGE CODE | OUTLINE NO. | LAND PATTERN NO. |
|---|---|---|---|
| 16 QSOP | E16+5 | **21-0055** | **90-0167** |
| 16 QSOP-EP | E16E+10 | **21-0112** | **90-0239** |
| 16 TDFN-EP | T1644+4 | **21-0139** | **90-0070** |

## Revision History

| REVISION NUMBER | REVISION DATE | DESCRIPTION | PAGES CHANGED |
|---|---|---|---|
| 0 | 9/10 | Initial release | — |