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# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## General Description

The MAX17021/MAX17082/MAX17482 are 2/1-phase-interleaved Quick-PWM™ step-down VID power-supply controllers for notebook CPUs. True out-of-phase operation reduces input ripple current requirements and output-voltage ripple, while easing component selection and layout difficulties. The Quick-PWM control provides instantaneous response to fast load-current steps. Active voltage positioning reduces power dissipation and bulk output capacitance requirements and allows ideal positioning compensation for tantalum, polymer, or ceramic bulk output capacitors.

A slew-rate controller allows controlled transitions between VID codes, controlled soft-start and shutdown, and controlled exit from suspend. A thermistor-based temperature sensor provides a programmable thermal-fault output (VRHOT). A current monitor output (IMON) provides an analog current output proportional to the power consumed by the CPU (MAX17082/MAX17482 only). Output under-voltage, overvoltage (MAX17021/MAX17082 only), and thermal protection shut the controller down when any of these faults are detected. A voltage-regulator power-OK (PWRGD) output indicates the output is in regulation. Additionally, the MAX17021/MAX17082/MAX17482 feature true differential current sense and a phase-good (PHASEGD) output that indicates a phase imbalance fault condition.

The MAX17021 supports the IMVP-6+ specification while the MAX17082/MAX17482 support the IMVP-6.5 requirements. The MAX17021/MAX17082/MAX17482 are available in a 5mm x 5mm, 40-pin TQFN package.

## Applications

IMVP-6+/IMVP-6.5 Core Supply  
Multiphase CPU Core Supply  
Voltage-Positioned, Step-Down Converters  
Notebook/Desktop Computers  
Blade Servers

## Ordering Information

PART	TEMP RANGE	PIN-PACKAGE
MAX17021GTL+	-40°C to +105°C	40 TQFN-EP*
MAX17082GTL+	-40°C to +105°C	40 TQFN-EP*
MAX17482GTL+	-40°C to +105°C	40 TQFN-EP*

+Denotes a lead-free (Pb)/RoHS-compliant package.

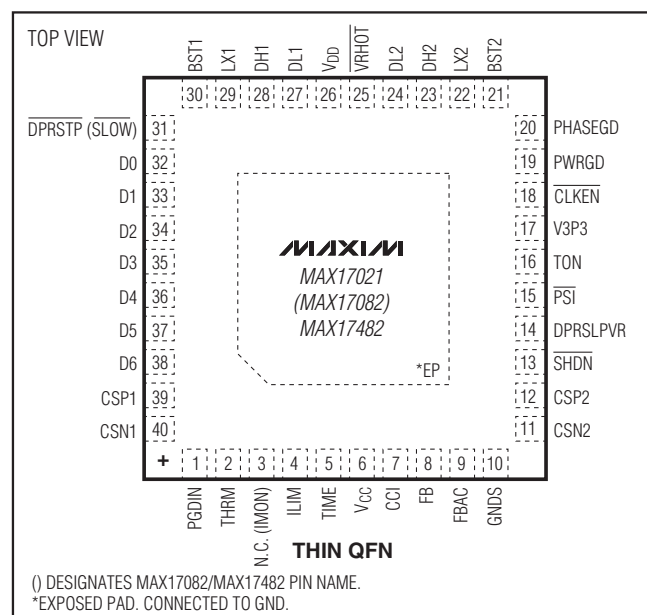
\*EP = Exposed pad.

Quick-PWM is a trademark of Maxim Integrated Products, Inc.

## Features

- ◆ Single-/Dual-Phase, Quick-PWM Controllers
- ◆ MAX17021 IMVP-6+ (Montevina)
- ◆ MAX17082/MAX17482 IMVP-6.5 (Calpella)
- ◆  $\pm 0.5\%$   $V_{OUT}$  Accuracy Over Line, Load, and Temperature
- ◆ 7-Bit 0 to 1.50V VID Control
- ◆ Dynamic Phase Selection Optimizes Active/Sleep Efficiency
- ◆ Transient Phase Overlap Reduces Output Capacitance
- ◆ Integrated Boost Switches
- ◆ Active Voltage Positioning with Adjustable Gain
- ◆ Programmable 200kHz to 800kHz Switching Frequency
- ◆ Accurate Current Balance and Current Limit
- ◆ Adjustable Slew-Rate Control
- ◆ Power-Good, Clock Enable, and Thermal-Fault Outputs
- ◆ Phase Current Imbalance Fault Output
- ◆ Drives Large Synchronous Rectifier MOSFETs
- ◆ 4V to 26V Battery Input-Voltage Range
- ◆ Undervoltage and Thermal-Fault Protection
- ◆ Overvoltage Protection (MAX17021/MAX17082)
- ◆ Soft-Startup and Soft-Shutdown

## Pin Configuration



MAX17021/MAX17082/MAX17482

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## ABSOLUTE MAXIMUM RATINGS

V <sub>CC</sub> , V <sub>DD</sub> , V3P3 to GND	-0.3V to +6V
D0–D6 to GND	-0.3V to +6V
PGDIN, DPRSLPVR, $\overline{\text{PSI}}$ to GND	-0.3V to +6V
DPRSTP (MAX17021) to GND	-0.3V to +6V
SLOW (MAX17082/MAX17482) to GND	-0.3V to +6V
CSP1, CSP2, CSN1, CSN2 to GND	-0.3V to +6V
THRM, ILIM, PHASEGD to GND	-0.3V to +6V
PWRGD, $\overline{\text{VRHOT}}$ to GND	-0.3V to +6V
CLKEN to GND	-0.3V to V3P3 + 0.3V
FB, FBAC to GND	-0.3V to V <sub>CC</sub> + 0.3V
TIME, CCI to GND	-0.3V to V <sub>CC</sub> + 0.3V
IMON to GND (MAX17021/MAX17082)	-0.3V to V <sub>CC</sub> + 0.3V
GNDS to GND	-0.3V to +0.3V
SHDN to GND (Note 1)	-0.3V to +16V
TON to GND	-0.3V to +30V

DL1, DL2 to GND	-0.3V to V <sub>DD</sub> + 0.3V
BST1, BST2 to GND	-0.3V to +36V
BST1, BST2 to V <sub>DD</sub>	-0.3V to +30V
LX1 to BST1	-6V to +0.3V
LX2 to BST2	-6V to +0.3V
DH1 to LX1	(-0.3V to V <sub>BST1</sub> ) + 0.3V
DH2 to LX2	(-0.3V to V <sub>BST2</sub> ) + 0.3V
Continuous Power Dissipation	
40-Pin 5mm x 5mm TQFN Up to +70°C	1778mW
(derate above +70°C)	22.2mW/°C
Operating Temperature Range	-40°C to +105°C
Junction Temperature	+150°C
Storage Temperature Range	-65°C to +165°C
Lead Temperature (soldering, 10s)	+300°C

**Note 1:**  $\overline{\text{SHDN}}$  might be forced to 12V for the purpose of debugging prototype boards using the no-fault test mode, which disables fault protection and overlapping operation.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

(Circuit of Figure 1, V<sub>IN</sub> = 10V, V<sub>CC</sub> = V<sub>DD</sub> = V $\overline{\text{SHDN}}$  = V<sub>PGDIN</sub> = V $\overline{\text{PSI}}$  = V<sub>ILIM</sub> = 5V, V3P3 = 3.3V, DPRSLPVR = GNDS = GND, V<sub>CSP1</sub> = V<sub>CSN1</sub> = V<sub>CSP2</sub> = V<sub>CSN2</sub> = 1.0000V, FB = FBAC, R<sub>FBAC</sub> = 3.57k $\Omega$  from FBAC to CSN1, D6–D0 = [0101000]; MAX17082/MAX17482: V $\overline{\text{SLOW}}$  = 5V; MAX17021: DPRSTP = GND; T<sub>A</sub> = 0°C to +85°C, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C.)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS		
<b>PWM CONTROLLER</b>								
Input-Voltage Range		V <sub>CC</sub> , V <sub>DD</sub>	4.5		5.5	V		
		V3P3	3.0		3.6			
DC Output-Voltage Accuracy	V <sub>OUT</sub>	Measured at FB with respect to GNDS; includes load-regulation error (Note 2)	DAC codes from 0.8125V to 1.5000V	-0.5		+0.5	%	
			DAC codes from 0.3750V to 0.8000V	-7		+7		mV
			DAC codes from 0 to 0.3625V	-20		+20		
Boot Voltage	V <sub>BOOT</sub>	MAX17021 IMVP-6+	1.194	1.200	1.206	V		
		MAX17082/MAX17482 IMVP-6.5	1.094	1.100	1.106			
Line Regulation Error		V <sub>CC</sub> = 4.5V to 5.5V, V <sub>IN</sub> = 4.5V to 26V		0.1		%		
FB Input Bias Current		T <sub>A</sub> = +25°C	-0.1		+0.1	$\mu$ A		
GNDS Input Range			-200		+200	mV		
GNDS Gain	A <sub>GNDS</sub>	$\Delta V_{\text{OUT}}/\Delta V_{\text{GNDS}}$	0.97	1.00	1.03	V/V		
GNDS Input Bias Current	I <sub>GNDS</sub>	T <sub>A</sub> = +25°C	-0.5		+0.5	$\mu$ A		
TIME Regulation Voltage	V <sub>TIME</sub>	R <sub>TIME</sub> = 71.5k $\Omega$	1.985	2.000	2.015	V		

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MAX17021/MAX17082/MAX17482

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = \overline{V_{SHDN}} = V_{PGDIN} = \overline{V_{PSI}} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $\overline{V_{SLOW}} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = 0^\circ C$  to  $+85^\circ C$ , unless otherwise noted. Typical values are at  $T_A = +25^\circ C$ .)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS	
TIME Slew-Rate Accuracy		$R_{TIME} = 71.5k\Omega$ (12.5mV/ $\mu s$ nominal)	-10		+10	%	
		$R_{TIME} = 35.7k\Omega$ (25mV/ $\mu s$ nominal) to 178k $\Omega$ (5mV/ $\mu s$ nominal)	-15		+15		
		Soft-start and soft-shutdown: $R_{TIME} = 35.7k\Omega$ (3.125mV/ $\mu s$ nominal) to 178k $\Omega$ (0.625mV/ $\mu s$ nominal)	-25		+25		
		Slow: IMVP-6.5 (MAX17082/MAX17482): $\overline{V_{SLOW}} = 0V$ , 1/2 of nominal slew rate, $R_{TIME} = 71.5k\Omega$ (6.25mV/ $\mu s$ nominal); IMVP-6+ (MAX17021): $\overline{V_{DPRSTP}} = V_{DPRSLPVR} = 5V$ , 1/4 of nominal slew rate, $R_{TIME} = 71.5k\Omega$ (3.125mV/ $\mu s$ nominal)	-15		+15		
		Slow: IMVP-6.5 (MAX17082/MAX17482): $\overline{V_{SLOW}} = 0V$ , 1/2 of nominal slew rate, $R_{TIME} = 35.7k\Omega$ (12.5mV/ $\mu s$ nominal) to 178k $\Omega$ (2.5mV/ $\mu s$ nominal); IMVP-6+ (MAX17021): $\overline{V_{DPRSTP}} = V_{DPRSLPVR} = 5V$ 1/4 of nominal slew rate, $R_{TIME} = 35.7k\Omega$ (6.25mV/ $\mu s$ nominal) to 178k $\Omega$ (1.25mV/ $\mu s$ nominal)	-15		+15		
On-Time	$t_{ON}$	Measured at $DH_-$ (Note 3)	$R_{TON} = 96.75k\Omega$ (600kHz per phase), 167ns nominal	-15		+15	%
			$R_{TON} = 200k\Omega$ (300kHz per phase), 333ns nominal	-10		+10	
			$R_{TON} = 303.25k\Omega$ (200kHz per phase), 500ns nominal	-15		+15	
Minimum Off-Time	$t_{OFF(MIN)}$	Measured at $DH_-$ (Note 3)		300	350	ns	
TON Shutdown Input Current	$I_{RTON,SDN}$	$\overline{SHDN} = GND$ , $V_{IN} = 26V$ , $V_{CC} = V_{DD} = 0V$ or 5V, $T_A = +25^\circ C$		0.01	0.1	$\mu A$	
<b>BIAS CURRENTS</b>							
Quiescent Supply Current ( $V_{CC}$ )	$I_{CC}$	Measured at $V_{CC}$ , $V_{DPRSLPVR} = 5V$ , FB forced above the regulation point		2.5	5	mA	
Quiescent Supply Current ( $V_{DD}$ )	$I_{DD}$	Measured at $V_{DD}$ , $V_{DPRSLPVR} = 0V$ , FB forced above the regulation point, $T_A = +25^\circ C$		0.02	1	$\mu A$	

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = V_{SHDN} = V_{PGDIN} = V_{PSI} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from  $FBAC$  to  $CSN1$ ,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $V_{SLOW} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = 0^\circ C$  to  $+85^\circ C$ , unless otherwise noted. Typical values are at  $T_A = +25^\circ C$ .)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS	
Quiescent Supply Current (V3P3)	$I_{3P3}$	Measured at V3P3, FB forced within the $\overline{CLKEN}$ power-good window		2	4	$\mu A$	
Shutdown Supply Current ( $V_{CC}$ )	$I_{CC,SDN}$	Measured at $V_{CC}$ , $\overline{SHDN} = GND$ , $T_A = +25^\circ C$		0.01	1	$\mu A$	
Shutdown Supply Current ( $V_{DD}$ )	$I_{DD,SDN}$	Measured at $V_{DD}$ , $\overline{SHDN} = GND$ , $T_A = +25^\circ C$		0.01	1	$\mu A$	
Shutdown Supply Current (V3P3)	$I_{3P3,SDN}$	Measured at V3P3, $\overline{SHDN} = GND$ , $T_A = +25^\circ C$		0.01	1	$\mu A$	
<b>FAULT PROTECTION</b>							
Output Overvoltage-Protection Threshold (MAX17021/MAX17082 Only)	VOVP	Skip mode after output reaches the regulation voltage or PWM mode; measured at FB with respect to the voltage target set by the VID code; see Table 4.	250	300	350	mV	
		Soft-start, soft-shutdown, skip mode, and output have not reached the regulation voltage; measured at FB	IMVP-6.5 (MAX17082)	1.45	1.50	1.55	V
			IMVP-6+ (MAX17021)	1.75	1.80	1.85	
		Minimum OVP threshold; measured at FB	0.8				
Output Overvoltage-Propagation Delay (MAX17021/MAX17082 Only)	$t_{OVP}$	FB forced 25mV above trip threshold		10		$\mu s$	
Output Undervoltage-Protection Threshold	$V_{UVP}$	Measured at FB with respect to the voltage target set by the VID code; see Table 4	-450	-400	-350	mV	
Output Undervoltage-Propagation Delay	$t_{UVP}$	FB forced 25mV below trip threshold		10		$\mu s$	
$\overline{CLKEN}$ Startup Delay and Boot Time Period	$t_{BOOT}$	Measured from the time when FB reaches the boot target voltage (Note 2)	20	60	100	$\mu s$	
PWRGD Startup Delay		Measured at startup from the time when $\overline{CLKEN}$ goes low	3	6.5	10	ms	
$\overline{CLKEN}$ and PWRGD Threshold		Measured at FB with respect to the voltage target set by the VID code; see Table 4, 20mV hysteresis (typ)	Lower threshold, falling edge (undervoltage)	-350	-300	-250	mV
			Upper threshold, rising edge (overvoltage)	+150	+200	+250	
$\overline{CLKEN}$ and PWRGD Delay		FB forced 25mV outside the PWRGD trip thresholds		10		$\mu s$	
PHASEGD Delay		$V_{(CCI,FB)}$ forced 25mV outside trip thresholds		10		$\mu s$	

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MAX17021/MAX17082/MAX17482

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = \overline{V_{SHDN}} = V_{PGDIN} = \overline{V_{PSI}} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $\overline{V_{SLOW}} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = 0^\circ C$  to  $+85^\circ C$ , unless otherwise noted. Typical values are at  $T_A = +25^\circ C$ .)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS	
CLKEN, PWRGD, and PHASEGD Transition Blanking Time (VID Transitions)	$t_{BLANK}$	Measured from the time when FB reaches the target voltage (Note 2)		20		$\mu s$	
PHASEGD Transition Blanking Time (Phase 2 Enable Transitions)		Number of DH2 pulses for which PHASEGD is blanked after phase 2 is enabled		32		Pulses	
$\overline{CLKEN}$ Output Low Voltage		Low state, $I_{SINK} = 3mA$			0.4	V	
$\overline{CLKEN}$ Output High Voltage		High state, $I_{SOURCE} = 3mA$	V3P3 - 0.4			V	
PWRGD, PHASEGD Output Low Voltage		Low state, $I_{SINK} = 3mA$			0.4	V	
PWRGD, PHASEGD Leakage Current		High-impedance state, PWRGD, PHASEGD forced to 5V, $T_A = +25^\circ C$			1	$\mu A$	
CSN1 Pulldown Resistance in Shutdown		$\overline{SHDN} = 0$ , measured after soft-shutdown completed ( $DL_- = low$ )		10		$\Omega$	
VCC Undervoltage Lockout (UVLO) Threshold	$V_{UVLO(VCC)}$	Rising edge, 65mV typical hysteresis, controller disabled below this level	4.05	4.27	4.48	V	
<b>THERMAL PROTECTION</b>							
$\overline{VRHOT}$ Trip Threshold		Measured at THRM as a percentage of VCC, falling edge, typical hysteresis = 75mV	29	30	31	%	
$\overline{VRHOT}$ Delay	$t_{VRHOT}$	THRM forced 25mV below the $\overline{VRHOT}$ trip threshold, falling edge		10		$\mu s$	
$\overline{VRHOT}$ Output On-Resistance	$R_{ON(\overline{VRHOT})}$	Low state		2	10	$\Omega$	
$\overline{VRHOT}$ Leakage Current		High-impedance state, $\overline{VRHOT}$ forced to 5V, $T_A = +25^\circ C$			1	$\mu A$	
THRM Input Leakage	$I_{THRM}$	$V_{THRM} = 0$ to 5V, $T_A = +25^\circ C$	-0.1		+0.1	$\mu A$	
Thermal-Shutdown Threshold	$T_{SHDN}$	Typical hysteresis = 15°C		160		°C	
<b>VALLEY CURRENT LIMIT, DROOP, AND CURRENT BALANCE</b>							
Current-Limit Threshold Voltage (Positive)	$V_{LIMIT}$	$V_{CSP\_} - V_{CSN\_}$	$V_{TIME} - V_{LIM} = 100mV$	7	10	13	mV
			$V_{TIME} - V_{LIM} = 500mV$	45	50	55	
			$ILIM = V_{CC}$	20	22.5	25	
Current-Limit Threshold Voltage (Negative) Accuracy	$V_{LIMIT(NEG)}$	$V_{CSP\_} - V_{CSN\_}$ , nominally -125% of $V_{LIMIT}$	-4		+4	mV	
Current-Limit Threshold Voltage (Zero Crossing)	$V_{ZERO}$	$V_{GND} - V_{LX\_}$ , $DPRSLPVR = 5V$		1		mV	

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = V_{SHDN} = V_{PGDIN} = V_{PSI} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from  $FBAC$  to  $CSN1$ ,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $V_{SLOW} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = 0^\circ C$  to  $+85^\circ C$ , unless otherwise noted. Typical values are at  $T_A = +25^\circ C$ .)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
CSP_, CSN_ Common-Mode Input Range			0		2	V
Phase 2 Disable Threshold		Measured at CSP2	3	$V_{CC} - 1$	$V_{CC} - 0.4$	V
CSP_, CSN_ Input Current	$I_{CSP\_}$ , $I_{CSN\_}$	$T_A = +25^\circ C$	-0.2		+0.2	$\mu A$
ILIM Input Current	$I_{LIM}$	$T_A = +25^\circ C$	-0.1		+0.1	$\mu A$
Droop Amplifier Offset		$(1/N) \times \sum (V_{CSP\_} - V_{CSN\_})$ at $I_{FBAC} = 0$ ; $\sum$ indicates summation over all phases from 1 to N, $N = 2$	$T_A = +25^\circ C$	-0.5	+0.5	mV/phase
			$T_A = 0^\circ C$ to $+85^\circ C$	-0.75	+0.75	
Droop Amplifier Transconductance	$G_m(FBAC)$	$\Delta I_{FBAC} / \Delta [\sum (V_{CSP\_} - V_{CSN\_})]$ ; $\sum$ indicates summation over all phases from 1 to N, $N = 2$ , $V_{FBAC} = V_{CSN-} = 0.45V$ to $2V$	590	600	608	$\mu S$
Current-Balance Amplifier Offset		$(V_{CSP1} - V_{CSN1}) - (V_{CSP2} - V_{CSN2})$ at $I_{CCI} = 0$	-1.0		+1.0	mV
Current-Balance Amplifier Transconductance	$G_m(CCI)$	$I_{CCI} / [(V_{CSP1} - V_{CSN1}) - (V_{CSP2} - V_{CSN2})]$		200		$\mu S$
<b>CURRENT MONITOR (MAX17082/MAX17482 Only)</b>						
Current-Monitor Output Current at Full Load Condition	$I_{IMON}$	$V_{CSP1} - V_{CSN1} = V_{CSP2} - V_{CSN2} = 20mV$ , $V_{CSN-} = 0.45V$ to $2.0V$	93.12	96	98.88	$\mu A$
Current-Monitor Transconductance	$G_m(IMON)$	$\Delta I_{IMON} / \Delta [\sum (V_{CSP\_} - V_{CSN\_})]$ ; $\sum$ indicates summation over all phases from 1 to N, $N = 2$ , $CSN- = 0.45V$ to $2V$	2.2	2.4	2.6	mS
IMON Clamp Voltage	$V_{IMON,max}$	$I_{SINK} = 10mA$	1.05	1.10	1.15	V
IMON Pulldown Resistance in Shutdown		$\overline{SHDN} = 0$ , measured after soft-shutdown completed ( $DL- = low$ )		10		$\Omega$
<b>GATE DRIVERS</b>						
DH_ Gate Driver On-Resistance	$R_{ON(DH_)}$	BST_ - LX_ forced to 5V	High state (pullup)	0.9	2.5	$\Omega$
			Low state (pulldown)	0.7	2.0	
DL_ Gate Driver On-Resistance	$R_{ON(DL_)}$		High state (pullup)	0.7	2.0	$\Omega$
			Low state (pulldown)	0.25	0.7	
DH_ Gate Driver Source Current	$I_{DH_(SOURCE)}$	DH_ forced to 2.5V, BST_ - LX_ forced to 5V		2.2		A
DH_ Gate Driver Sink Current	$I_{DH_(SINK)}$	DH_ forced to 2.5V, BST_ - LX_ forced to 5V		2.7		A
DL_ Gate Driver Source Current	$I_{DL_(SOURCE)}$	DL_ forced to 2.5V		2.7		A

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

MAX17021/MAX17082/MAX17482

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = \overline{V_{SHDN}} = V_{PGDIN} = \overline{V_{PSI}} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $\overline{V_{SLOW}} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = 0^\circ C$  to  $+85^\circ C$ , unless otherwise noted. Typical values are at  $T_A = +25^\circ C$ .)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
DL_ Gate Driver Sink Current	$I_{DL(SINK)}$	DL_ forced to 2.5V		8		A
Internal BST_ Switch On-Resistance	$R_{ON(BST_)}$			10	20	$\Omega$
<b>LOGIC AND I/O</b>						
Logic Input High Voltage	$V_{IH}$	$\overline{SHDN}$ , PGDIN MAX17021: DPRSLPVR	2.3			V
Logic Input Low Voltage	$V_{IL}$	$\overline{SHDN}$ , PGDIN MAX17021: DPRSLPVR			1.0	V
$\overline{SHDN}$ No-Fault Level		To enable no-fault mode	11		13	V
Low-Voltage Logic Input High Voltage	$V_{IHLV}$	$\overline{PSI}$ , D0-D6; MAX17082/MAX17482: DPRSLPVR, $\overline{SLOW}$ , MAX17021: $\overline{DPRSTP}$	0.67			V
Low-Voltage Logic Input Low Voltage	$V_{ILLV}$	$\overline{PSI}$ , D0-D6; MAX17082/MAX17482: DPRSLPVR, $\overline{SLOW}$ , MAX17021: $\overline{DPRSTP}$			0.33	V
Logic Input Current		$T_A = +25^\circ C$ , $\overline{SHDN}$ , DPRSLPVR, PGDIN, $\overline{PSI}$ , $\overline{DPRSTP}$ , $\overline{SLOW}$ , D0-D6 = 0 or 5V	-1		+1	$\mu A$

## ELECTRICAL CHARACTERISTICS

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = \overline{V_{SHDN}} = V_{PGDIN} = \overline{V_{PSI}} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $\overline{V_{SLOW}} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = -40^\circ C$  to  $+105^\circ C$ , unless otherwise noted.) (Note 4)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS	
<b>PWM CONTROLLER</b>							
Input-Voltage Range		$V_{CC}$ , $V_{DD}$	4.5		5.5	V	
		$V_{3P3}$	3.0		3.6		
DC Output-Voltage Accuracy	$V_{OUT}$	Measured at FB with respect to GNDS; includes load-regulation error (Note 2)	DAC codes from 0.8125V to 1.5000V	-0.75		+0.75	%
		DAC codes from 0.3750V to 0.8000V	-10		+10	mV	
		DAC codes from 0 to 0.3625V	-25		+25		
Boot Voltage	$V_{BOOT}$	MAX17021: IMVP-6+	1.19		1.21	V	
		MAX17082/MAX17482: IMVP-6.5	1.09		1.11		



# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = \overline{V_{SHDN}} = V_{PGDIN} = \overline{V_{PSI}} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GND = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $\overline{V_{SLOW}} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = -40^{\circ}C$  to  $+105^{\circ}C$ , unless otherwise noted.) (Note 4)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS	
GNDS Input Range			-200		+200	mV	
GNDS Gain	$A_{GNDS}$	$\Delta V_{OUT}/\Delta V_{GNDS}$	0.97		1.03	V/V	
TIME Regulation Voltage	$V_{TIME}$	$R_{TIME} = 71.5k\Omega$	1.985		2.015	V	
TIME Slew-Rate Accuracy		$R_{TIME} = 71.5k\Omega$ (12.5mV/ $\mu$ s nominal)	-10		+10	%	
		$R_{TIME} = 35.7k\Omega$ (25mV/ $\mu$ s nominal) to 178k $\Omega$ (5mV/ $\mu$ s nominal)	-15		+15		
		Soft-start and soft-shutdown: $R_{TIME} = 35.7k\Omega$ (3.125mV/ $\mu$ s nominal) to 178k $\Omega$ (0.625mV/ $\mu$ s nominal)	-25		+25		
		Slow: IMVP-6.5 (MAX17082/MAX17482): $\overline{V_{SLOW}} = 0V$ , 1/2 of nominal slew rate, $R_{TIME} = 71.5k\Omega$ (6.25mV/ $\mu$ s nominal); IMVP-6+ (MAX17021): $\overline{V_{DPRSTP}} = \overline{V_{DPRSLPVR}} = 5V$ , 1/4 of nominal slew rate, $R_{TIME} = 71.5k\Omega$ (3.125mV/ $\mu$ s nominal)	-15		+15		
TIME Slew-Rate Accuracy		Slow: IMVP-6.5 (MAX17082/MAX17482): $\overline{V_{SLOW}} = 0V$ , 1/2 of nominal slew rate, $R_{TIME} = 35.7k\Omega$ (12.5mV/ $\mu$ s nominal) to 178k $\Omega$ (2.5mV/ $\mu$ s nominal); IMVP-6+ (MAX17021): $\overline{V_{DPRSTP}} = \overline{V_{DPRSLPVR}} = 5V$ , 1/4 of nominal slew rate, $R_{TIME} = 35.7k\Omega$ (6.25mV/ $\mu$ s nominal) to 178k $\Omega$ (1.25mV/ $\mu$ s nominal)	-17		+17	%	
On-Time	$t_{ON}$	Measured at DH_ (Note 3)	$R_{TON} = 96.75k\Omega$ (600kHz per phase), 167ns nominal	-15		+15	%
			$R_{TON} = 200k\Omega$ (300kHz per phase), 333ns nominal	-15		+15	
			$R_{TON} = 303.25k\Omega$ (200kHz per phase), 500ns nominal	-15		+15	
Minimum Off-Time	$t_{OFF(MIN)}$	Measured at DH_ (Note 3)			350	ns	
<b>BIAS CURRENTS</b>							
Quiescent Supply Current ( $V_{CC}$ )	$I_{CC}$	Measured at $V_{CC}$ , $\overline{V_{DPRSLPVR}} = 5V$ , FB forced above the regulation point			5	mA	
Quiescent Supply Current ( $V_{3P3}$ )	$I_{3P3}$	Measured at $V_{3P3}$ , FB forced within the $\overline{CLKEN}$ power-good window			4	$\mu$ A	

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = V_{SHDN} = V_{PGDIN} = V_{PSI} = V_{LIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $V_{SLOW} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = -40^\circ C$  to  $+105^\circ C$ , unless otherwise noted.) (Note 4)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS	
<b>FAULT PROTECTION</b>							
Output Overvoltage-Protection Threshold (MAX17021/MAX7082 Only)	$V_{OVP}$	Skip mode after output reaches the regulation voltage or PWM mode, measured at FB with respect to the voltage target set by the VID code (see Table 4)	250		350	mV	
		Soft-start, soft-shutdown, skip mode, and output have not reached the regulation voltage, measured at FB	IMVP-6.5 (MAX17082)	1.45		1.55	V
			IMVP-6+ (MAX17021)	1.75		1.85	
Output Undervoltage-Protection Threshold	$V_{UVP}$	Measured at FB with respect to the voltage target set by the VID code (see Table 4)	-450		-350	mV	
$\overline{CLKEN}$ Startup Delay and Boot Time Period	$t_{BOOT}$	Measured from the time when FB reaches the boot target voltage (Note 3)	20		100	$\mu s$	
PWRGD Startup Delay		Measured at startup from the time when $\overline{CLKEN}$ goes low	3		10	ms	
$\overline{CLKEN}$ and PWRGD Threshold		Measured at FB with respect to the voltage target set by the VID code (see Table 4), 20mV hysteresis (typ)	Lower threshold, falling edge (undervoltage)	-350		-250	mV
			Upper threshold, rising edge (overvoltage)	+150		+250	
$\overline{CLKEN}$ Output Low Voltage		Low state, $I_{SINK} = 3mA$			0.4	V	
$\overline{CLKEN}$ Output High Voltage		High state, $I_{SOURCE} = 3mA$	$V_{3P3} - 0.4$			V	
PWRGD, PHASEGD Output Low Voltage		Low state, $I_{SINK} = 3mA$			0.4	V	
$V_{CC}$ Undervoltage-Lockout Threshold (UVLO)	$V_{UVLO(VCC)}$	Rising edge, 65mV typical hysteresis, controller disabled below this level	4.0		4.5	V	
<b>THERMAL PROTECTION</b>							
$\overline{VRHOT}$ Trip Threshold		Measured at THRM as a percentage of $V_{CC}$ , falling edge, typical hysteresis = 75mV	28		32	%	
$\overline{VRHOT}$ Output On-Resistance	$R_{ON(\overline{VRHOT})}$	Low state			10	$\Omega$	

MAX17021/MAX17082/MAX17482

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## ELECTRICAL CHARACTERISTICS (continued)

(Circuit of Figure 1,  $V_{IN} = 10V$ ,  $V_{CC} = V_{DD} = \overline{V_{SHDN}} = V_{PGDIN} = \overline{V_{PS1}} = V_{ILIM} = 5V$ ,  $V_{3P3} = 3.3V$ ,  $DPRSLPVR = GNDS = GND$ ,  $V_{CSP1} = V_{CSN1} = V_{CSP2} = V_{CSN2} = 1.0000V$ ,  $FB = FBAC$ ,  $R_{FBAC} = 3.57k\Omega$  from FBAC to CSN1,  $D6-D0 = [0101000]$ ; MAX17082/MAX17482:  $\overline{V_{SLOW}} = 5V$ ; MAX17021:  $\overline{DPRSTP} = GND$ ;  $T_A = -40^\circ C$  to  $+105^\circ C$ , unless otherwise noted.) (Note 4)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
<b>VALLEY CURRENT LIMIT, DROOP, AND CURRENT BALANCE</b>						
Current-Limit Threshold Voltage (Positive)	$V_{LIMIT}$	$V_{CSP\_} - V_{CSN\_}$	$V_{TIME} - V_{ILIM} = 100mV$	7	13	mV
			$V_{TIME} - V_{ILIM} = 500mV$	40	60	
			$ILIM = V_{CC}$	19	26	
CSP_, CSN_ Common-Mode Input Range			0		2	V
Droop Amplifier Transconductance	$G_m(FBAC)$	$\Delta I_{FBAC}/\Delta[\sum(V_{CSP\_} - V_{CSN\_})]$ , $\sum$ indicates summation over all phases from 1 to N, $N = 2$ , $V_{FBAC} = V_{CSN\_} = 0.45V$ to $2V$	585		610	$\mu S$
Current-Balance Amplifier Offset		$(V_{CSP1} - V_{CSN1}) - (V_{CSP2} - V_{CSN2})$ at $I_{CCI} = 0$	-1.25		+1.25	mV
<b>CURRENT MONITOR (MAX17082/MAX17482 Only)</b>						
Current-Monitor Transconductance	$G_m(IMON)$	$\Delta I_{IMON}/\Delta[\sum(V_{CSP\_} - V_{CSN\_})]$ , $\sum$ indicates summation over all phases from 1 to N, $N = 2$ , $V_{CSN\_} = 0.45V$ to $2V$	2.2		2.6	mS
IMON Clamp Voltage	$V_{IMON,max}$	$I_{SINK} = 10mA$	1.05		1.15	V
<b>GATE DRIVERS</b>						
DH_ Gate Driver On-Resistance	$R_{ON(DH\_)}$	BST_ - LX_ forced to 5V	High state (pullup)		2.5	$\Omega$
			Low state (pulldown)		2.0	
DL_ Gate Driver On-Resistance	$R_{ON(DL\_)}$		High state (pullup)		2.0	$\Omega$
			Low state (pulldown)		0.7	
<b>LOGIC AND I/O</b>						
Logic Input High Voltage	$V_{IH}$	$\overline{SHDN}$ , PGDIN: MAX17021: DPRSLPVR	2.3			V
Logic Input Low Voltage	$V_{IL}$	$\overline{SHDN}$ , PGDIN: MAX17021: DPRSLPVR			1.0	V
Low-Voltage Logic Input High Voltage	$V_{IHLV}$	$\overline{PS1}$ , D0-D6: MAX17082/MAX17482: DPRSLPVR, $\overline{SLOW}$ MAX17021: $\overline{DPRSTP}$	0.67			V
Low-Voltage Logic Input Low Voltage	$V_{ILLV}$	$\overline{PS1}$ , D0-D6: MAX17082/MAX17482: DPRSLPVR, $\overline{SLOW}$ MAX17021: $\overline{DPRSTP}$			0.33	V

**Note 2:** When pulse skipping, the output rises by approximately 1.5% when transitioning from continuous conduction to no load.

**Note 3:** On-time and minimum off-time specifications are measured from 50% to 50% at the DH\_ and DL\_ pins, with LX\_ forced to GND, BST\_ forced to 5V, and a 500pF capacitor from DH\_ to LX\_ to simulate external MOSFET gate capacitance. Actual in-circuit times might be different due to MOSFET switching speeds.

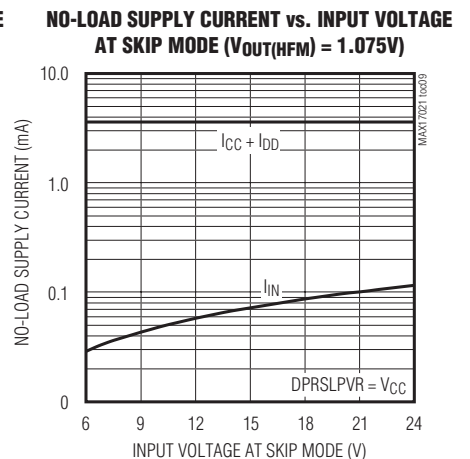
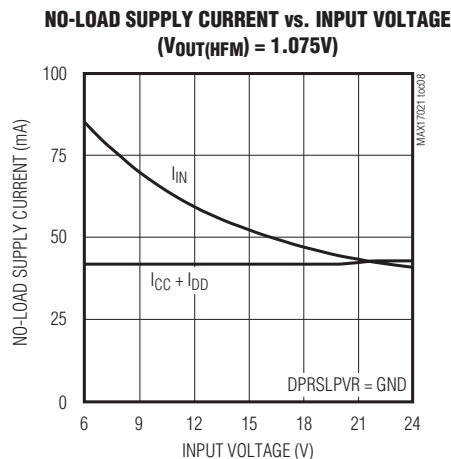
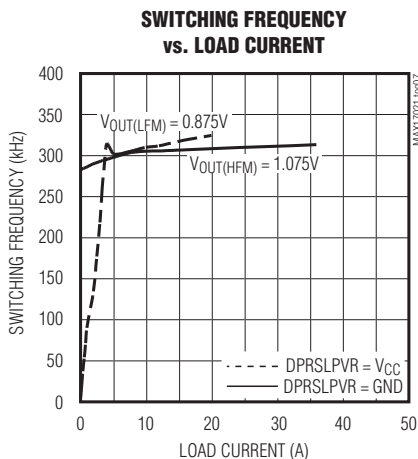
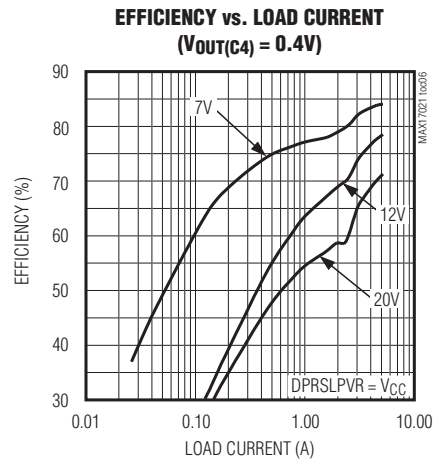
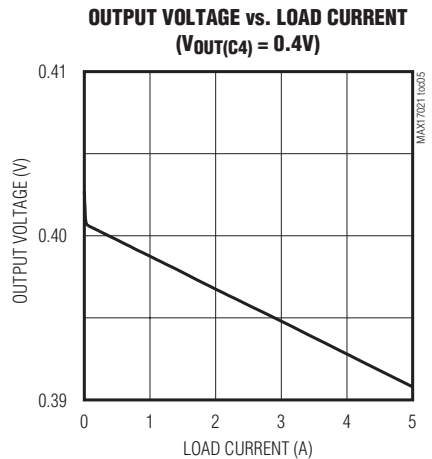
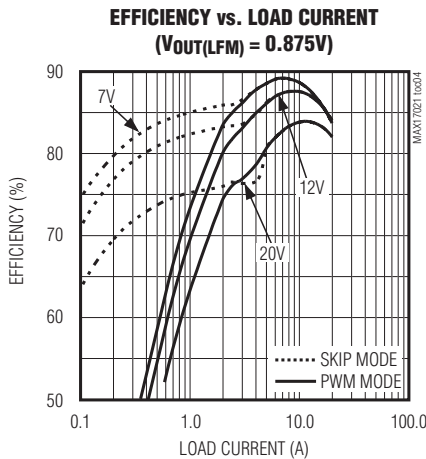
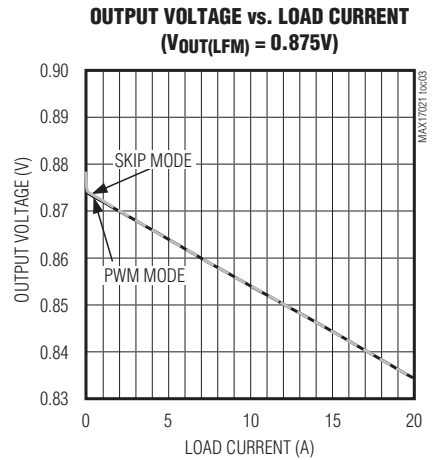
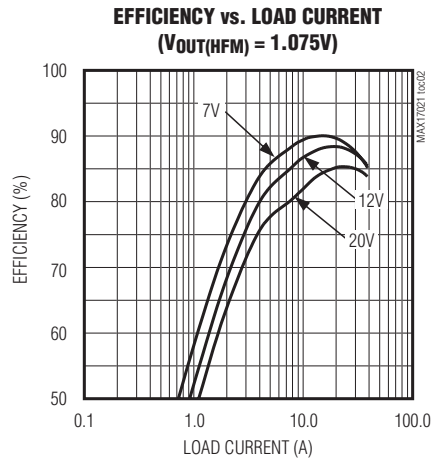
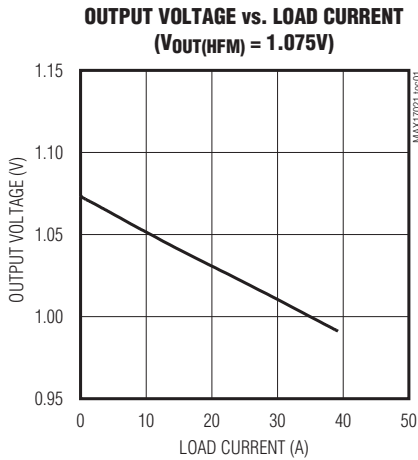
**Note 4:** Specifications to  $T_A = -40^\circ C$  and  $+105^\circ C$  are guaranteed by design and are not production tested.

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Typical Operating Characteristics

(Circuit of Figure 1.  $V_{IN} = 12V$ ,  $V_{CC} = V_{DD} = 5V$ ,  $\overline{SHDN} = V_{CC}$ , D0–D6 set for 1.075V,  $T_A = +25^\circ C$ , unless otherwise specified.)

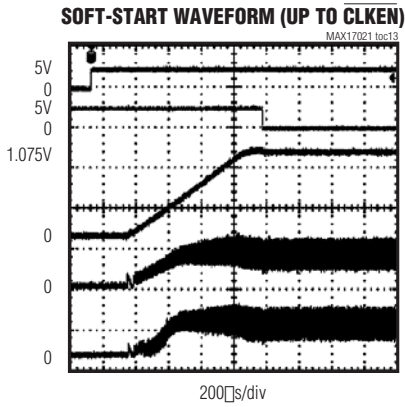
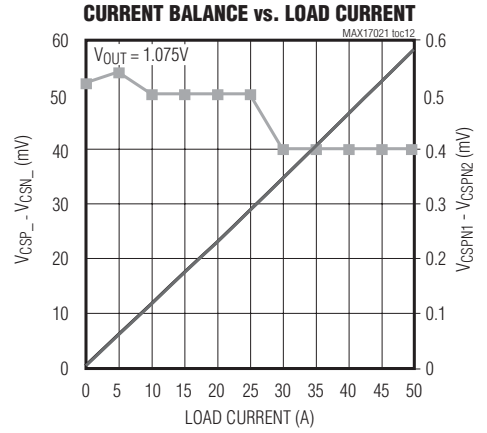
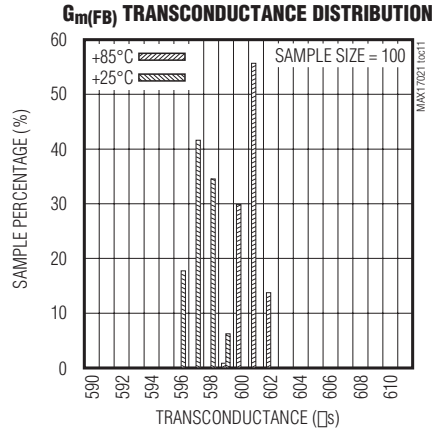
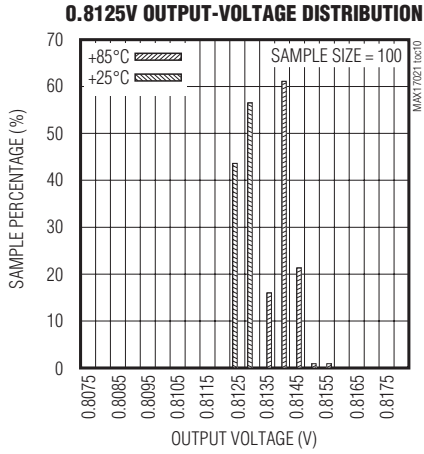
MAX17021/MAX17082/MAX17482



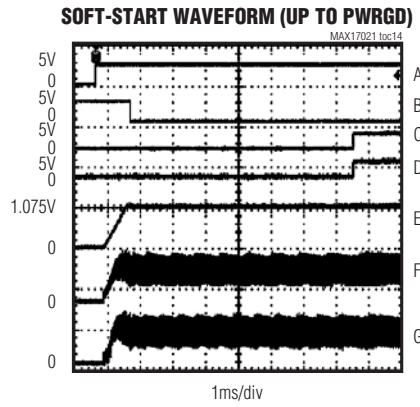
# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Typical Operating Characteristics (continued)

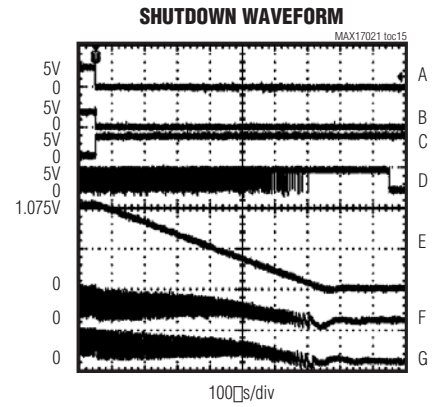
(Circuit of Figure 1.  $V_{IN} = 12V$ ,  $V_{CC} = V_{DD} = 5V$ ,  $\overline{SHDN} = V_{CC}$ , D0–D6 set for 1.075V,  $T_A = +25^\circ C$ , unless otherwise specified.)



A.  $\overline{SHDN}$ , 10V/div  
 B. CLKEN, 10V/div  
 C.  $V_{OUT}$ , 500mV/div  
 D.  $I_{LX1}$ , 10A/div  
 E.  $I_{LX2}$ , 10A/div  
 $I_{OUT} = 15A$



A.  $\overline{SHDN}$ , 10V/div  
 B. PWRGD, 10V/div  
 C. PHASEGD, 10V/div  
 D. CLKEN, 10V/div  
 E.  $V_{OUT}$ , 1V/div  
 F.  $I_{LX1}$ , 10A/div  
 G.  $I_{LX2}$ , 10A/div  
 $I_{OUT} = 15A$



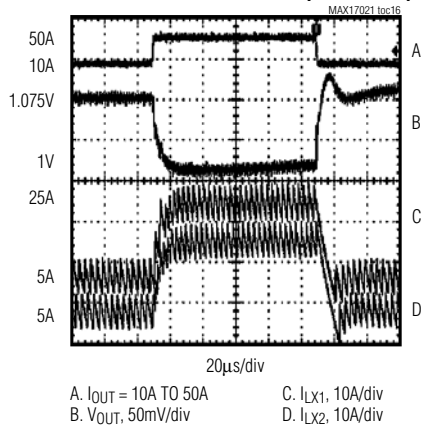
A.  $\overline{SHDN}$ , 10V/div  
 B. CLKEN, 10V/div  
 C. PWRGD, 10V/div  
 D.  $DL_-$ , 10V/div  
 E.  $V_{OUT}$ , 500mV/div  
 F.  $I_{LX1}$ , 10A/div  
 G.  $I_{LX2}$ , 10A/div

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

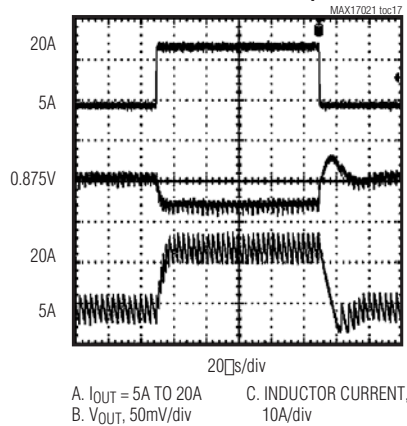
## Typical Operating Characteristics (continued)

(Circuit of Figure 1.  $V_{IN} = 12V$ ,  $V_{CC} = V_{DD} = 5V$ ,  $\overline{SHDN} = V_{CC}$ , D0–D6 set for 1.075V,  $T_A = +25^\circ C$ , unless otherwise specified.)

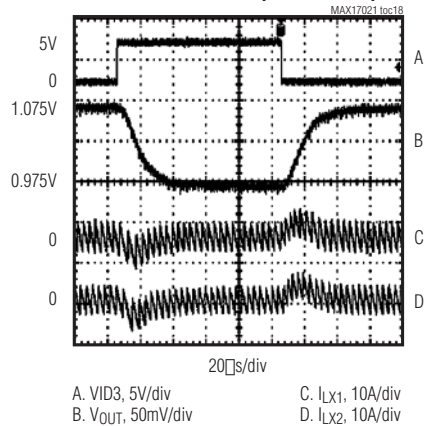
**LOAD TRANSIENT RESPONSE (HFM MODE)**



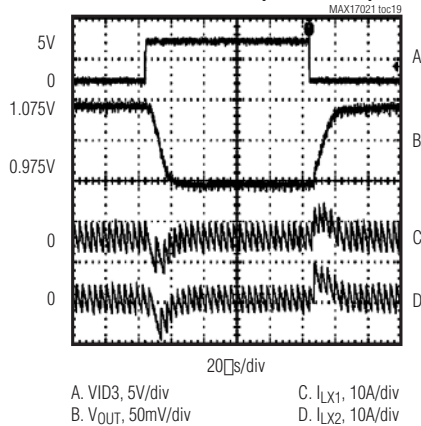
**LOAD-TRANSIENT RESPONSE (LFM MODE)**



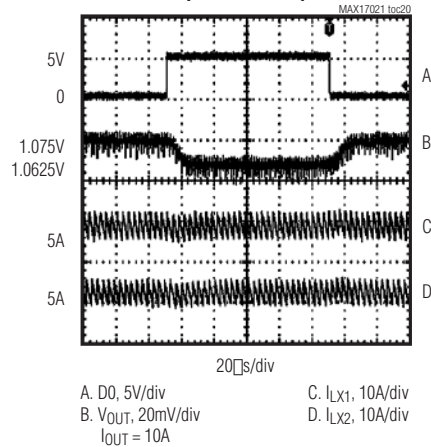
**VID CODE CHANGE ( $\overline{SLOW} = GND$ )**



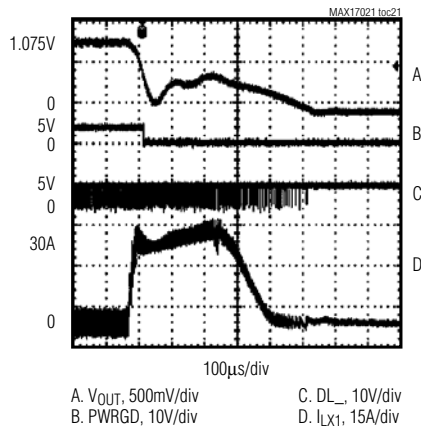
**VID CODE CHANGE ( $\overline{SLOW} = V_{DD}$ )**



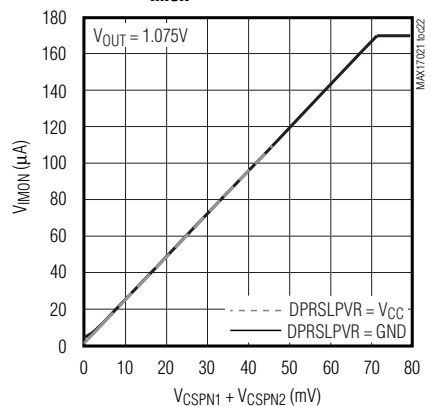
**DYNAMIC VID CODE CHANGE ( $D0 = 12.5mV$ )**



**OUTPUT UNDERVOLTAGE FAULT**



**VIMON vs. LOAD CURRENT**

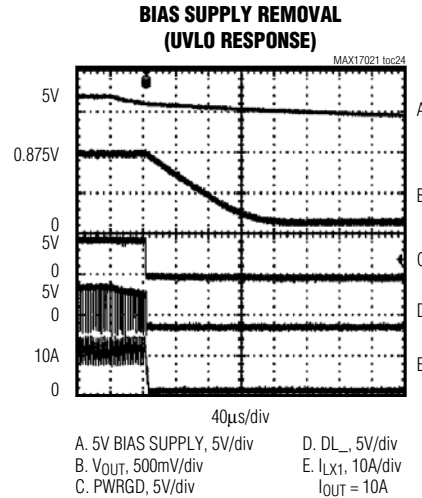
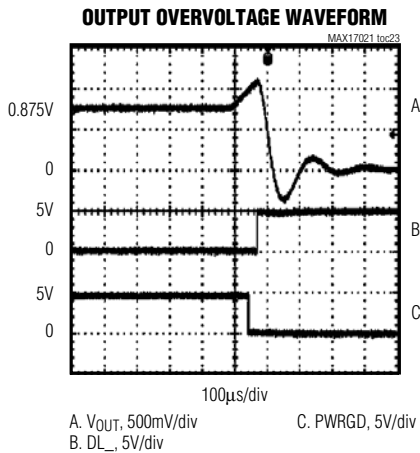


MAX17021/MAX17082/MAX17482

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Typical Operating Characteristics (continued)

(Circuit of Figure 1.  $V_{IN} = 12V$ ,  $V_{CC} = V_{DD} = 5V$ ,  $\overline{SHDN} = V_{CC}$ , D0–D6 set for 1.075V,  $T_A = +25^\circ C$ , unless otherwise specified.)



## Pin Description

PIN	NAME	FUNCTION
1	PGDIN	System Power-Good Logic Input. PGDIN indicates the power status of other system rails and is used for power-supply sequencing. After power-up to the boot voltage, the output voltage remains at V <sub>BOOT</sub> , CLKEN remains high, and PWRGD remains low as long as the PGDIN stays low. When PGDIN is pulled high, the output transitions to selected VID voltage, and CLKEN is pulled low. If the system pulls PGDIN low during normal operation, the MAX17021/MAX17082/MAX17482 immediately drive CLKEN high, pull PWRGD low, and slew the output to the boot voltage (using two-phase pulse-skipping mode). The controller remains at the boot voltage until PGDIN goes high again, SHDN is toggled, or the V <sub>CC</sub> input power supply is cycled.
2	THRM	Input of Internal Comparator. Connect the output of a resistor- and thermistor-divider (between V <sub>CC</sub> and GND) to THRM. Select the components such that the voltage at THRM falls below 1.5V (30% of V <sub>CC</sub> ) at the desired high temperature.
3	IMON (MAX17082/ MAX17482 only)	Current-Monitor Output. The MAX17082/MAX17482 IMON output source a current that is directly proportional to the current-sense voltage as defined by: $I_{IMON} = G_m(IMON) \times (V_{CSP\_} - V_{CSN\_})$ where $G_m(IMON) = 2.4mS$ (typ). The IMON current is unidirectional (sources current out of IMON only) for positive current-sense values. For negative current-sense voltages, the IMON current is zero. Connect an external resistor between IMON and VSS_SENSE to create the desired IMON gain based on the following equation: $R_{IMON} = 0.999V / (IMAX \times R_{SENSE} \times G_m(IMON))$ where IMAX is defined in the <i>Current Monitor</i> section of the Intel IMVP-6.5 specification and based on discrete increments (20A, 30A, 40A, etc.), R <sub>SENSE</sub> is the typical effective value of the current-sense element (sense resistor or inductor DCR) that is used to provide the current-sense voltage, and G <sub>m</sub> (IMON) is the typical transconductance amplifier gain as defined in the <i>Electrical Characteristics</i> table. The IMON voltage is internally clamped to a maximum of 1.1V (typ). The transconductance amplifier and voltage clamp are internally compensated, so IMON cannot directly drive large capacitance values. To filter the IMON signal, use an RC filter as shown in Figure 2. IMON is pulled to ground when MAX17082/MAX17482 are in shutdown.

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Pin Description (continued)

PIN	NAME	FUNCTION
4	ILIM	Valley Current-Limit Adjustment Input. The valley current-limit threshold voltage at CSP_ to CSN_ equals precisely 1/10 of the differential TIME to ILIM voltage over a 0.1V to 0.5V range (10mV to 50mV current-sense range). The negative current-limit threshold is nominally -125% of the corresponding valley current-limit threshold. Connect ILIM directly to V <sub>CC</sub> to set the default current-limit threshold setting of 22.5mV (typ) nominal.
5	TIME	Slew-Rate Adjustment Pin. TIME regulates to 2.0V and the load current determines the slew rate of the internal error-amplifier target. The sum of the resistance between TIME and GND (R <sub>TIME</sub> ) determines the nominal slew-rate: $\text{SLEW RATE} = (12.5\text{mV}/\mu\text{s}) \times (71.5\text{k}\Omega/\text{RTIME})$ The guaranteed R <sub>TIME</sub> range is between 35.7k $\Omega$ and 178k $\Omega$ . This “nominal” slew rate applies to VID transitions and to the transition from boot mode to VID. If the VID DAC inputs are clocked, the slew rate for all other VID transitions is set by the rate at which they are clocked, up to a maximum slew rate equal to the nominal slew rate defined above. The startup and shutdown slew rates are always 1/8 of nominal slew rate in order to minimize surge currents. MAX17021: If both DPRSLPVR and $\overline{\text{DPRSTP}}$ are pulled high, then the slew rate is reduced to 1/4 of nominal. MAX17082/MAX17482: If $\overline{\text{SLOW}}$ is low, then the slew rate is reduced to 1/2 of nominal.
6	V <sub>CC</sub>	Controller Analog Bias Supply Voltage. Connect to a 4.5V to 5.5V source. Bypass to GND with 1 $\mu$ F minimum.
7	CCI	Current-Balance Compensation. Connect a 470pF capacitor between CCI and the positive side of the feedback remote sense. CCI is internally forced low in shutdown.
8	FB	Remote Feedback-Sense Input. Normally shorted to FBAC and connected to the V <sub>CC</sub> _SENSE pin of the CPU socket through the load-line gain resistor (see the FBAC pin description). FB internally connects to the error amplifier and integrator.
9	FBAC	Voltage-Positioning Transconductance Amplifier Output. Connect a resistor R <sub>FB</sub> between FBAC and the positive side of the feedback remote sense to set the DC steady-state droop based on the voltage-positioning gain requirement: $R_{\text{FB}} = R_{\text{DROOP}} / (R_{\text{SENSE}} \times G_{\text{m(FBAC)}})$ where R <sub>DROOP</sub> is the desired voltage-positioning slope and G <sub>m(FBAC)</sub> = 600 $\mu$ S (typ). R <sub>SENSE</sub> is the value of the current-sense resistors that are used to provide the (CSP_, CSN_) current-sense voltages. If lossless sensing is used, R <sub>SENSE</sub> = R <sub>L</sub> . In this case, consider making R <sub>FB</sub> a resistor network that includes an NTC thermistor to minimize the temperature dependence of the voltage-positioning slope. FBAC is high impedance in shutdown.
10	GNDS	Remote Ground-Sense Input. Normally connected to the V <sub>SS</sub> _SENSE pin of the CPU socket. GNDS internally connects to a transconductance amplifier that fine tunes the output voltage—compensating for voltage drops from the regulator ground to the load ground.
11	CSN2	Negative Current-Sense Input for Phase 2. Connect CSN2 to the negative terminal of the inductor current-sensing resistor or directly to the negative terminal of the inductor if the lossless DCR sensing method is used (see Figure 4).
12	CSP2	Positive Current-Sense Input for Phase 2. Connect CSP2 to the positive terminal of the inductor current-sensing resistor or directly to the positive terminal of the filtering capacitor used when the lossless DCR sensing method is used (see Figure 4). Short CSP2 to V <sub>CC</sub> for dedicated one-phase operation.

MAX17021/MAX17082/MAX17482



# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Pin Description (continued)

PIN	NAME	FUNCTION															
13	$\overline{\text{SHDN}}$	Shutdown Control Input. This input cannot withstand the battery voltage. Connect to $V_{CC}$ for normal operation. Connect to ground to put the IC into its 1 $\mu$ A max shutdown state. During startup, the output voltage is ramped up to the boot voltage slowly at a slew rate that is 1/8 the slew rate set by the TIME resistor. During the transition from normal operation to shutdown, the output voltage is ramped down at the same slow slew rate. Forcing $\overline{\text{SHDN}}$ to 11V~13V disables both overvoltage-protection and undervoltage-protection circuits, clears the fault latch, disables transient phase overlap, and disables the BST_ charging switches. Do not connect $\overline{\text{SHDN}}$ to > 13V.															
14	DPRSLPVR	<p>Pulse-Skipping Control Input. This 1.0V logic input signal indicates power usage and sets the operating mode of MAX17021/MAX17082/MAX17482. When DPRSLPVR is forced high, the controller immediately enters the automatic pulse-skipping mode. The controller returns to forced-PWM mode when DPRSLPVR is forced low and the output is in regulation. The PWRGD upper threshold is blanked during any downward output-voltage transition that occurs when the controller is in pulse-skipping mode, and stays blanked until the transition-related PWRGD blanking period is complete and the output reaches regulation. The output overvoltage fault threshold is changed from a tracking [VID + 300mV] threshold to a fixed-default transitional OVP threshold during the period for which the PWRGD upper threshold is blanked.</p> <p>The MAX17082 is in two-phase pulse-skipping mode during startup and while in boot mode, but is in forced-PWM mode during the transition from boot mode to VID mode plus 20<math>\mu</math>s, and during soft-shutdown, irrespective of the DPRSLPVR logic level.</p> <p>DPRSLPVR and <math>\overline{\text{PSI}}</math> together determine the operating mode and the number of active phases as shown in the following truth table:</p> <table border="1"> <thead> <tr> <th>DPRSLPVR</th> <th><math>\overline{\text{PSI}}</math></th> <th>MODE AND PHASES</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>0</td> <td>Very low current (one-phase pulse skipping)</td> </tr> <tr> <td>1</td> <td>1</td> <td>Low current (approx 3A) (one-phase pulse skipping)</td> </tr> <tr> <td>0</td> <td>0</td> <td>Intermediate power potential (one-phase PWM)</td> </tr> <tr> <td>0</td> <td>1</td> <td>Max power potential (two- or one-phase PWM as configured at CSP2)</td> </tr> </tbody> </table>	DPRSLPVR	$\overline{\text{PSI}}$	MODE AND PHASES	1	0	Very low current (one-phase pulse skipping)	1	1	Low current (approx 3A) (one-phase pulse skipping)	0	0	Intermediate power potential (one-phase PWM)	0	1	Max power potential (two- or one-phase PWM as configured at CSP2)
DPRSLPVR	$\overline{\text{PSI}}$	MODE AND PHASES															
1	0	Very low current (one-phase pulse skipping)															
1	1	Low current (approx 3A) (one-phase pulse skipping)															
0	0	Intermediate power potential (one-phase PWM)															
0	1	Max power potential (two- or one-phase PWM as configured at CSP2)															
15	$\overline{\text{PSI}}$	Power-State Indicator Input. DPRSLPVR and $\overline{\text{PSI}}$ together determine the operating mode and the number of active phases as shown in the truth table included under the $\overline{\text{PSI}}$ pin description above.															
16	TON	<p>Switching Frequency Setting Input. An external resistor between the input power source and TON sets the switching period (<math>T_{SW} = 1/f_{SW}</math>) per phase according to the following equation:</p> $T_{SW} = 16.3\text{pF} \times (R_{TON} + 6.5\text{k}\Omega)$ <p>TON becomes high impedance in shutdown to reduce the input quiescent current. If the TON current is less than 10<math>\mu</math>A, the MAX17021/MAX17082/MAX17482 disable the controller, set the TON open fault latch, and pull DL_ and DH_ low.</p>															
17	V3P3	3.3V CLKEN Input Supply. V3P3 input supplies the $\overline{\text{CLKEN}}$ CMOS push-pull logic output. Connect to the system's standard 3.3V supply voltage before $\overline{\text{SHDN}}$ is pulled high for proper IMVP-6.5 operation.															
18	$\overline{\text{CLKEN}}$	Clock Enable Push-Pull Logic Output. This inverted logic output indicates when the output voltage sensed at FB is in regulation. During soft-start, shutdown, and when the FB is out of regulation, the MAX17021/MAX17082/MAX17482 pull $\overline{\text{CLKEN}}$ up to V3P3. During VID transitions, the controller forces $\overline{\text{CLKEN}}$ low. Except during the power-up sequence, $\overline{\text{CLKEN}}$ is the inverse of PWRGD. See the <i>Startup Timing Diagram</i> (Figure 10). When in pulse-skipping mode (DPRSLPVR high), the upper $\overline{\text{CLKEN}}$ threshold is disabled.															
19	PWRGD	<p>Open-Drain Power-Good Output. After output-voltage transitions, except during power-up and power-down; if FB is in regulation then PWRGD is high impedance.</p> <p>During startup, PWRGD is held low and continues to be low while the part is in boot mode and until 5ms (typ) after <math>\overline{\text{CLKEN}}</math> goes low.</p> <p>PWRGD is forced low in shutdown.</p> <p>PWRGD is forced high impedance whenever the slew-rate controller is active (output-voltage transitions). When in pulse-skipping mode (DPRSLPVR high), the upper PWRGD threshold comparator is blanked during downward transitions.</p> <p>A pullup resistor on PWRGD causes additional finite shutdown current.</p>															

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Pin Description (continued)

MAX17021/MAX17082/MAX17482

PIN	NAME	FUNCTION															
20	PHASEGD	Phase-Good Current-Balance Open-Drain Output. Used to signal the system that one of the two phases either has a fault condition or is not matched with the other. Detection is done by identifying the need for a large on-time difference between phases in order to achieve or move towards current balance. PHASEGD is low in shutdown. PHASEGD is forced high impedance whenever the slew-rate controller is active (output-voltage transitions). PHASEGD is forced high impedance while in one-phase operation (DPRSLPVR = high or $\overline{PSI}$ = low).															
21	BST2	Boost Flying-Capacitor Connection for Phase 2. BST2 provides the upper supply rail for the DH2 high-side gate driver. An internal switch between $V_{DD}$ and BST2 charges the flying capacitor while the low-side MOSFET is on (DL2 pulled high and LX2 pulled to ground).															
22	LX2	Inductor Connection for Phase 2. LX2 is the internal lower supply rail for the DH2 high-side gate driver. Also used as an input to the controller's zero-crossing comparator for phase 2.															
23	DH2	High-Side Gate-Driver Output for Phase 2. DH2 swings from LX2 to BST2. The controller pulls DH2 low in shutdown.															
24	DL2	Low-Side Gate-Driver Output for Phase 2. DL2 swings from GND to $V_{DD}$ . DL2 is forced low in skip mode after detecting an inductor current zero crossing. DL2 is forced low during one-phase operation ( $\overline{PSI}$ = GND or CSP2 = $V_{CC}$ ).															
25	$\overline{VRHOT}$	Open-Drain Output of Internal Comparator. $\overline{VRHOT}$ is pulled low when the voltage at THRM goes below 1.5V (30% of $V_{CC}$ ). $\overline{VRHOT}$ is high impedance in shutdown.															
26	$V_{DD}$	Driver Supply Voltage Input. $V_{DD}$ is the supply voltage used to internally power the low-side gate drivers and refresh the BST_ flying capacitors during the off-times. Connect $V_{DD}$ to the 4.5V to 5.5V system supply voltage. Bypass $V_{DD}$ to the system power ground with a 1 $\mu$ F each or greater ceramic capacitor.															
27	DL1	Low-Side Gate-Driver Output for Phase 1. DL1 swings from GND to $V_{DD}$ . DL1 is forced high when an output overvoltage fault is detected, overriding any negative current-limit condition that might be present. DL1 is forced low after soft-shutdown or in skip mode after detecting an inductor current zero crossing.															
28	DH1	High-Side Gate-Driver Output for Phase 1. DH1 swings from LX1 to BST1. The controller pulls DH1 low in shutdown.															
29	LX1	Inductor Connection for Phase 1. LX1 is the internal lower supply rail for the DH1 high-side gate driver. Also used as an input to the controller's zero-crossing comparator for phase 1.															
30	BST1	Boost Flying-Capacitor Connection for Phase 1. BST1 provides the upper supply rail for the DH1 high-side gate driver. An internal switch between $V_{DD}$ and BST1 charges the flying capacitor while the low-side MOSFET is on (DL1 is pulled high and LX1 is pulled to ground).															
31	$\overline{DPRSTP}$ (MAX17021)	IMVP-6+ Slew-Rate Select Input. This 1.0V logic input signal from the IMVP-6+ system is usually the logical complement of the DPRSLPVR signal. However, the IMVP-6+ specification supports a special slow C4 exit condition that allows both $\overline{DPRSTP}$ and DPRSLPVR to be pulled high simultaneously. When this occurs, the voltage-transition slew rate reduces to 1/4 the nominal ( $R_{TIME}$ -based) slew rate for the duration of this logic condition. The slew rate returns to normal when either DPRSLPVR or $\overline{DPRSTP}$ is pulled low: <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th>DPRSLPVR</th> <th><math>\overline{DPRSTP}</math></th> <th>SLEW RATE</th> </tr> </thead> <tbody> <tr> <td>0</td> <td>0</td> <td>Nominal slew rate</td> </tr> <tr> <td>0</td> <td>1</td> <td>Nominal slew rate</td> </tr> <tr> <td>1</td> <td>0</td> <td>Nominal slew rate</td> </tr> <tr> <td>1</td> <td>1</td> <td>Slew rate reduced to 1/4 of nominal</td> </tr> </tbody> </table>	DPRSLPVR	$\overline{DPRSTP}$	SLEW RATE	0	0	Nominal slew rate	0	1	Nominal slew rate	1	0	Nominal slew rate	1	1	Slew rate reduced to 1/4 of nominal
	DPRSLPVR	$\overline{DPRSTP}$	SLEW RATE														
0	0	Nominal slew rate															
0	1	Nominal slew rate															
1	0	Nominal slew rate															
1	1	Slew rate reduced to 1/4 of nominal															
$\overline{SLOW}$ (MAX17082/ MAX17482)	IMVP-6.5 Slew-Rate Select Input. This 1.0V logic input signal selects between the nominal and "slow" (half of nominal rate) slew rates. When $\overline{SLOW}$ is forced high, the selected nominal slew rate is set by the TIME resistance as defined above. When $\overline{SLOW}$ is forced low, the slew rate is reduced to half the nominal slew rate.																

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Pin Description (continued)

PIN	NAME	FUNCTION
32–38	D0–D6	Low-Voltage VID DAC Code Input. The D0–D6 inputs do not have internal pullups. These 1.0V logic inputs are designed to interface directly with the CPU. The output voltage is set by the VID code indicated by the logic-level voltages on D0–D6 (see Table 4).
39	CSP1	Positive Current-Sense Input for Phase 1. Connect CSP1 to the positive terminal of the inductor current-sensing resistor or directly to the positive terminal of the filtering capacitor used when the lossless DCR sensing method is used (see Figure 4).
40	CSN1	Negative Current-Sense Input for Phase 1. Connect CSN1 to the negative terminal of the inductor current-sensing resistor or directly to the negative terminal of the inductor if the lossless DCR sensing method is used (see Figure 4). Under $V_{CC}$ UVLO conditions and after soft-shutdown is completed, CSN1 is internally pulled to GND through a $10\Omega$ FET to discharge the output.
—	EP	Exposed Pad. Internally connected to GND. Connect to the ground plane through a thermally enhanced via. <b>For the MAX17021/MAX17082/MAX17482, the exposed pad is the only GND connection and must be properly soldered.</b>

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

MAX17021/MAX17082/MAX17482

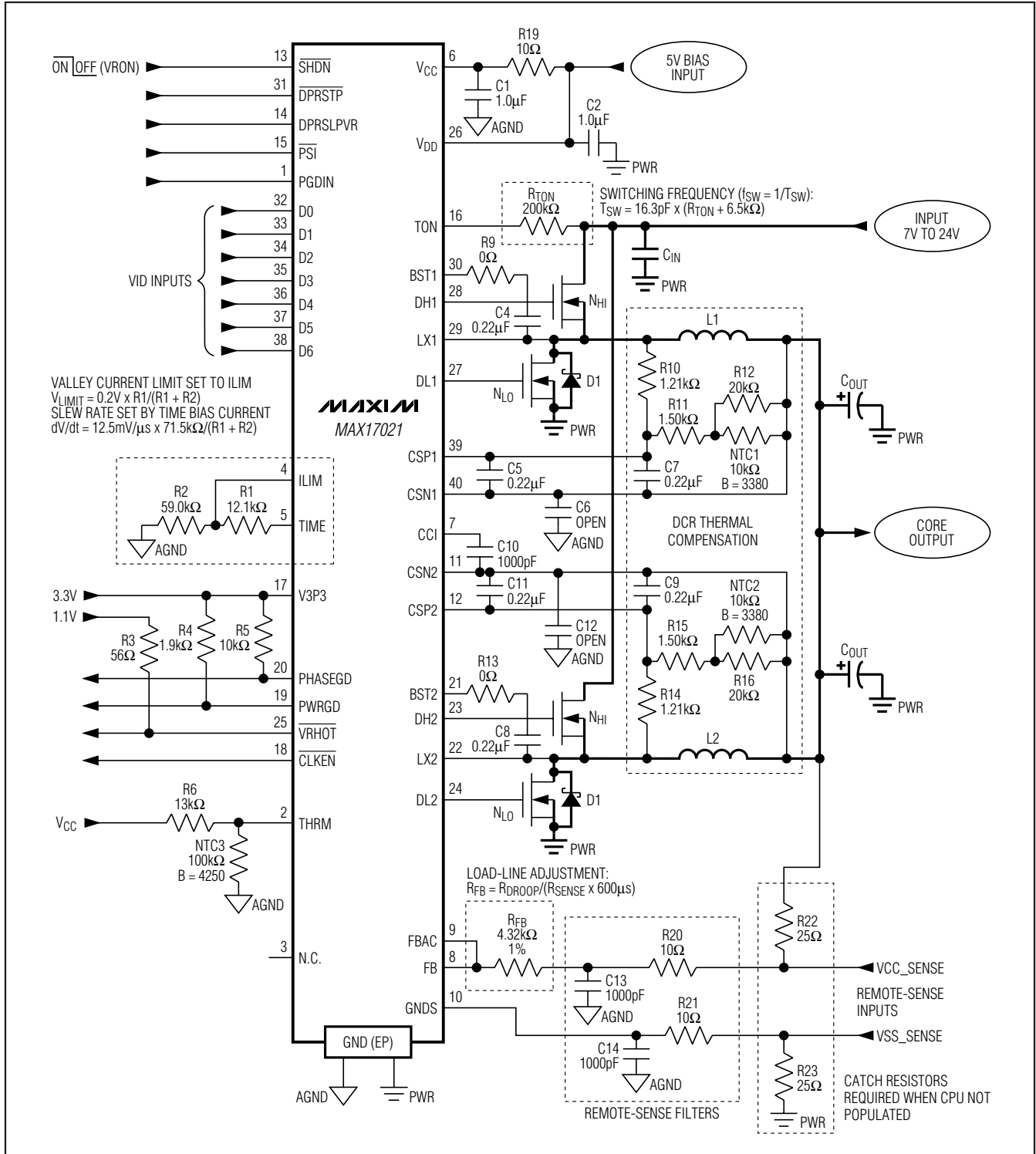


Figure 1. Standard 2-Phase IMVP-6+ Application Circuit

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Detailed Description

Table 1 lists the component selection for standard applications. Table 2 lists component suppliers for the MAX17021/MAX17082/MAX17482/MAX17482.

### Free-Running, Constant-On-Time PWM Controller with Input Feed-Forward

The Quick-PWM control architecture is a pseudo-fixed-frequency, constant-on-time, current-mode regulator with voltage feed-forward (Figure 3). This architecture relies on the output filter capacitor's ESR to act as the current-sense resistor, so the output ripple voltage provides the PWM ramp signal. The control algorithm is

simple: the high-side switch on-time is determined solely by a one-shot whose period is inversely proportional to input voltage, and directly proportional to output voltage or the difference between the main and secondary inductor currents (see the *On-Time One-Shot* section). Another one-shot sets a minimum off-time. The on-time one-shot triggers when the error comparator goes low, the inductor current of the selected phase is below the valley current-limit threshold, and the minimum off-time one-shot times out. The controller maintains 180° out-of-phase operation by alternately triggering the main and secondary phases after the error comparator drops below the output-voltage set point.

Table 1. Component Selection for Standard Applications

DESIGN PARAMETERS	IMVP-6+ SV	IMVP-6+ LV	IMVP-6.5 AUBURNDALE SV CORE	IMVP-6.5 AUBURNDALE LV CORE
CIRCUIT	FIGURE 1	FIGURE 1	FIGURE 2	FIGURE 2
Input-Voltage Range	7V to 20V	7V to 20V	7V to 20V	7V to 20V
Maximum Load Current (TDC Current)	44A (34A)	23A (19A)	50A (37A)	28A (19A)
Transient Load Current	35A (10A/μs)	18A (10A/μs)	35A (10A/μs)	23A (10A/μs)
Load Line	-2.1mV/A	-4mV/A	-1.9mV/A	-3mV/A
<b>COMPONENTS</b>				
TON Resistance (R <sub>TON</sub> )	200kΩ (f <sub>SW</sub> = 300kHz)	200kΩ (f <sub>SW</sub> = 300kHz)	200kΩ (f <sub>SW</sub> = 300kHz)	200kΩ (f <sub>SW</sub> = 300kHz)
Inductance (L)	NEC/TOKIN MPC1055LR36 0.36μH, 32A, 0.8mΩ	NEC/TOKIN MPC1055LR36 0.36μH, 32A, 0.8mΩ	NEC/TOKIN MPC1055LR36 0.36μH, 32A, 0.8mΩ	NEC/TOKIN MPC1055LR36 0.36μH, 32A, 0.8mΩ
High-Side MOSFET (N <sub>H</sub> )	Siliconix 1x Si4386DY 7.8m /9.5mΩ (typ/max)	Siliconix 1x Si4386DY 7.8m /9.5mΩ (typ/max)	Siliconix 1x Si4386DY 7.8m /9.5mΩ (typ/max)	Siliconix 1x Si4386DY 7.8m /9.5mΩ (typ/max)
Low-Side MOSFET (N <sub>L</sub> )	Siliconix 2x Si4642DY 3.9m /4.7mΩ (typ/max)	Siliconix 2x Si4642DY 3.9m /4.7mΩ (typ/max)	Siliconix 2x Si4642DY 3.9m /4.7mΩ (typ/max)	Siliconix 2x Si4642DY 3.9m /4.7mΩ (typ/max)
Output Capacitors (C <sub>OUT</sub> )	4x 330μF, 6mΩ, 2.5V Panasonic EEFSX0D0D331XR 28x 10μF, 6V ceramic (0805)	3x 330μF, 6mΩ, 2.5V Panasonic EEFSX0D0D331XR 28x 10μF, 6V ceramic (0805)	4x 330μF, 6mΩ, 2.5V Panasonic EEFSX0D0D331XR 28x 10μF, 6V ceramic (0805)	3x 330μF, 6mΩ, 2.5V Panasonic EEFSX0D0D331XR 28x 10μF, 6V ceramic (0805)
Input Capacitors (C <sub>IN</sub> )	4x 10μF, 25V ceramic (1210)	4x 10μF, 25V ceramic (1210)	4x 10μF, 25V ceramic (1210)	4x 10μF, 25V ceramic (1210)

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

MAX17021/MAX17082/MAX17482

**Table 1. Component Selection for Standard Applications (continued)**

DESIGN PARAMETERS	IMVP-6+ SV	IMVP-6+ LV	IMVP-6.5 AUBURNDALE SV CORE	IMVP-6.5 AUBURNDALE LV CORE
TIME-ILIM Resistance (R1)	10kΩ	10kΩ	10kΩ	10kΩ
ILIM-GND Resistance (R2)	59kΩ	59kΩ	59kΩ	59kΩ
FB Resistance (R <sub>FB</sub> )	4.32kΩ	8.45kΩ	4.02kΩ	6.34kΩ
IMON Resistance	N/A	N/A	9.09kΩ	18.2kΩ
LX_-CSP_ Resistance	1.21kΩ	1.21kΩ	1.21kΩ	1.21kΩ
CSP_-CSN_ Series Resistance (R6)	1.50kΩ	1.50kΩ	1.50kΩ	1.50kΩ
Parallel NTC Resistance	20kΩ	20kΩ	20kΩ	20kΩ
DCR Sense NTC (NTC1)	10kΩ NTC B = 3380 TDK NTCG163JH103F	10kΩ NTC B = 3380 TDK NTCG163JH103F	10kΩ NTC B = 3380 TDK NTCG163JH103F	10kΩ NTC B = 3380 TDK NTCG163JH103F
DCR Sense Capacitance (C <sub>SENSE</sub> )	2x 0.22μF, 6V ceramic (0805)	2x 0.22μF, 6V ceramic (0805)	2x 0.22μF, 6V ceramic (0805)	2x 0.22μF, 6V ceramic (0805)

**Table 2. Component Suppliers**

SUPPLIER	WEBSITE
AVX Corp.	<a href="http://www.avxcorp.com">www.avxcorp.com</a>
BI Technologies	<a href="http://www.bitechnologies.com">www.bitechnologies.com</a>
Central Semiconductor Corp.	<a href="http://www.centrasemi.com">www.centrasemi.com</a>
Fairchild Semiconductor	<a href="http://www.fairchildsemi.com">www.fairchildsemi.com</a>
International Rectifier	<a href="http://www.irf.com">www.irf.com</a>
KEMET Corp	<a href="http://www.kemet.com">www.kemet.com</a>
NEC/TOKIN Corp.	<a href="http://www.nec-tokin.com">www.nec-tokin.com</a>
Panasonic Corp.	<a href="http://www.panasonic.com">www.panasonic.com</a>

SUPPLIER	WEBSITE
Pulse Engineering	<a href="http://www.pulseeng.com">www.pulseeng.com</a>
Renesas Technology Corp.	<a href="http://www.renesas.com">www.renesas.com</a>
SANYO Electric Co, Ltd.	<a href="http://www.sanyodevice.com">www.sanyodevice.com</a>
Siliconix (Vishay)	<a href="http://www.vishay.com">www.vishay.com</a>
Sumida	<a href="http://www.sumida.com">www.sumida.com</a>
Taiyo Yuden	<a href="http://www.t-yuden.com">www.t-yuden.com</a>
TDK Corp.	<a href="http://www.component.tdk.com">www.component.tdk.com</a>
TOKO America, Inc.	<a href="http://www.tokoam.com">www.tokoam.com</a>

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

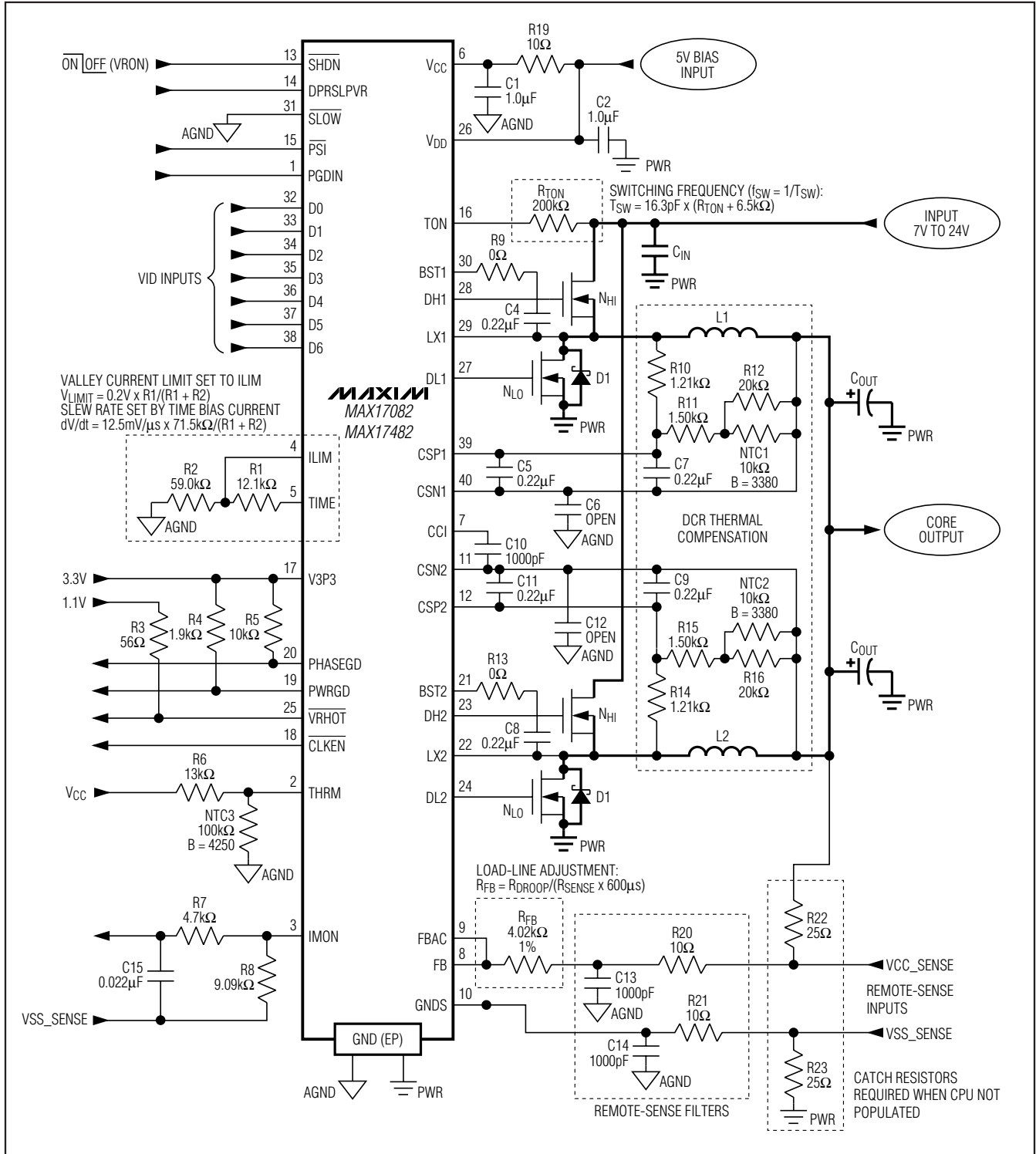


Figure 2. Standard 2-Phase IMVP-6.5 (Calpella) Application Circuit

# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

MAX17021/MAX17082/MAX17482

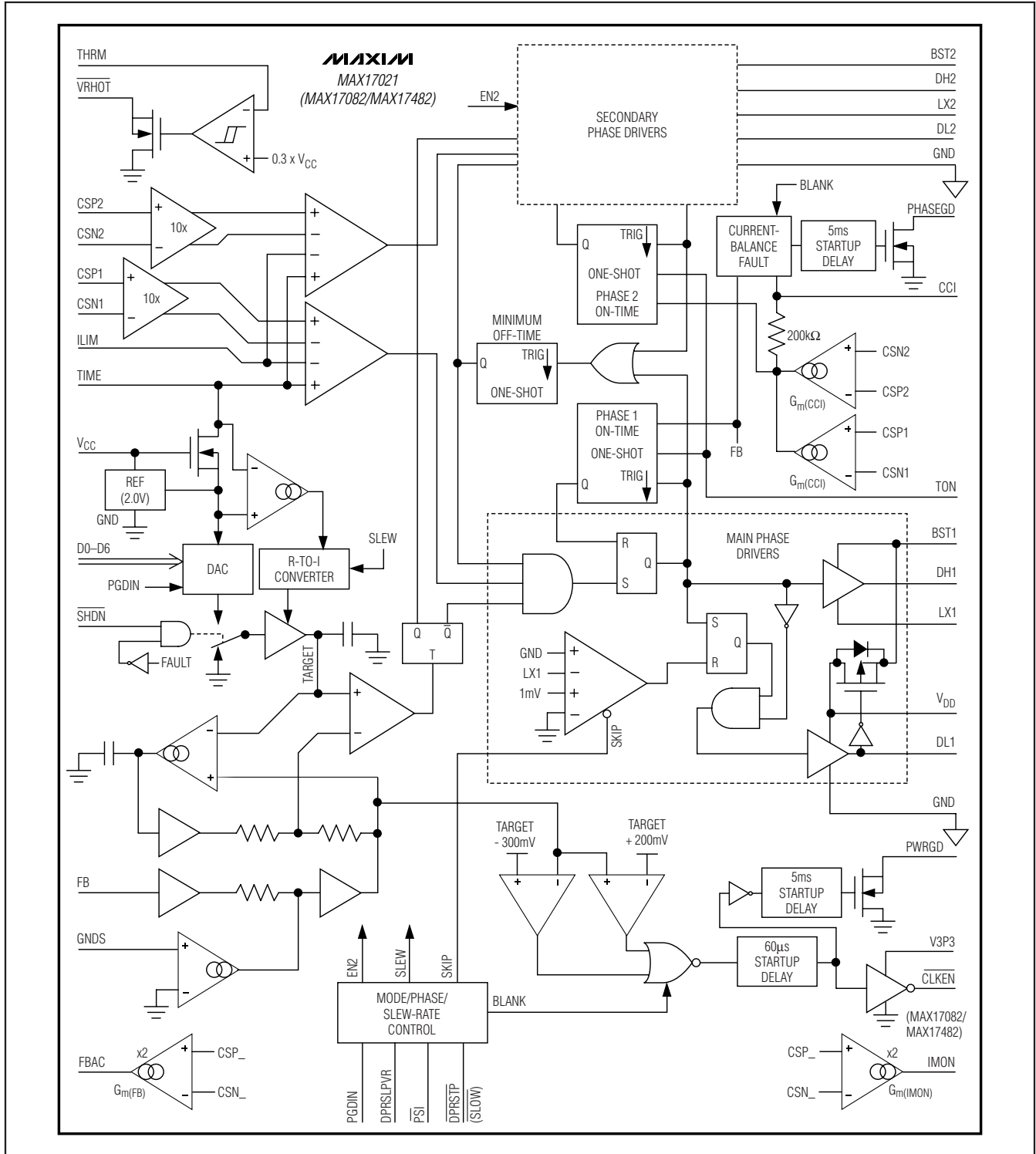


Figure 3. Functional Diagram



# Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

## Dual 180° Out-of-Phase Operation

The two phases in the MAX17021/MAX17082/MAX17482 operate 180° out-of-phase to minimize input and output filtering requirements, reduce electromagnetic interference (EMI), and improve efficiency. This effectively lowers component count—reducing cost, board space, and component power requirements—making the MAX17021/MAX17082/MAX17482 ideal for high-power, cost-sensitive applications.

Typically, switching regulators provide power using only one phase instead of dividing the power among several phases. In these applications, the input capacitors must support high instantaneous current requirements. The high RMS ripple current can lower efficiency due to I<sup>2</sup>R power loss associated with the input capacitor's effective series resistance (ESR). Therefore, the system typically requires several low-ESR input capacitors in parallel to minimize input-voltage ripple, to reduce ESR-related power losses, and to meet the necessary RMS ripple current rating.

With the MAX17021/MAX17082/MAX17482, the controller shares the current between two phases that operate 180° out-of-phase, so the high-side MOSFETs never turn on simultaneously during normal operation. The instantaneous input current of either phase is effectively halved, resulting in reduced input-voltage ripple, ESR power loss, and RMS ripple current (see the *Input Capacitor Selection* section). Therefore, the same performance can be achieved with fewer or less-expensive input capacitors.

## +5V Bias Supply (V<sub>CC</sub> and V<sub>DD</sub>)

The Quick-PWM controller requires an external +5V bias supply in addition to the battery. Typically, this +5V bias supply is the notebook's 95% efficient +5V system supply. Keeping the bias supply external to the IC improves efficiency and eliminates the cost associated with the +5V linear regulator that would otherwise be needed to supply the PWM circuit and gate drivers. If stand-alone capability is needed, the +5V bias supply can be generated with an external linear regulator.

The +5V bias supply must provide V<sub>CC</sub> (PWM controller) and V<sub>DD</sub> (gate-drive power), so the maximum current drawn is:

$$I_{BIAS} = I_{CC} + f_{SW} (Q_{G(LOW)} + Q_{G(HIGH)})$$

where I<sub>CC</sub> is provided in the *Electrical Characteristics* table, f<sub>SW</sub> is the switching frequency, and Q<sub>G(LOW)</sub> and Q<sub>G(HIGH)</sub> are the MOSFET data sheet's total gate-charge specification limits at V<sub>GS</sub> = 5V.

V<sub>IN</sub> and V<sub>DD</sub> can be tied together if the input power source is a fixed +4.5V to +5.5V supply. If the +5V bias supply is powered-up prior to the battery supply, the

enable signal ( $\overline{SHDN}$  going from low to high) must be delayed until the battery voltage is present to ensure startup.

## Switching Frequency (TON)

Connect a resistor (R<sub>TON</sub>) between TON and V<sub>IN</sub> to set the switching period T<sub>SW</sub> = 1/f<sub>SW</sub>, per phase:

$$T_{SW} = 16.3\text{pF} \times (R_{TON} + 6.5\text{k}\Omega)$$

A 96.75kΩ to 303.25kΩ corresponds to switching periods of 167ns (600kHz) to 500ns (200kHz), respectively. High-frequency (600kHz) operation optimizes the application for the smallest component size, trading off efficiency due to higher switching losses. This might be acceptable in ultra-portable devices where the load currents are lower and the controller is powered from a lower voltage supply. Low-frequency (200kHz) operation offers the best overall efficiency at the expense of component size and board space.

## TON Open-Circuit Protection

The TON input includes open-circuit protection to avoid long, uncontrolled on-times that could result in an over-voltage condition on the output. The MAX17021/MAX17082/MAX17482 detect an open-circuit fault if the TON current drops below 10μA for any reason—the TON resistor (R<sub>TON</sub>) is unpopulated, a high resistance value is used, the input voltage is low, etc. Under these conditions, the MAX17021/MAX17082/MAX17482 stop switching (DH<sub>-</sub> and DL<sub>-</sub> pulled low) and immediately set the fault latch. Toggle SHDN or cycle the V<sub>CC</sub> power supply below 0.5V to clear the fault latch and reactivate the controller.

## On-Time One-Shot

The core of each phase contains a fast, low-jitter, adjustable one-shot that sets the high-side MOSFETs on-time. The one-shot for the main phase varies the on-time in response to the input and feedback voltages. The main high-side switch on-time is inversely proportional to the input voltage as measured by the TON input, and proportional to the feedback voltage (V<sub>FB</sub>):

$$t_{ON(MAIN)} = \frac{T_{SW} (V_{FB} + 0.075V)}{V_{IN}}$$

where the switching period (T<sub>SW</sub> = 1/f<sub>SW</sub>) is set by the resistor at the TON pin, and 0.075V is an approximation to accommodate the expected drop across the low-side MOSFET switch.

The one-shot for the secondary phase varies the on-time in response to the input voltage and the difference between the main and secondary inductor currents. Two identical transconductance amplifiers integrate the

## Dual-Phase, Quick-PWM Controllers for IMVP-6+/IMVP-6.5 CPU Core Power Supplies

difference between the master and slave current-sense signals. The summed output is internally connected to CCI, allowing adjustment of the integration time constant with a compensation network connected between CCI and FB. The resulting compensation current and voltage are determined by the following equations:

$$I_{CCI} = G_m(V_{CSP1} - V_{CSN1}) - G_m(V_{CSP2} - V_{CSN2})$$

$$V_{CCI} = V_{FB} + I_{CCI}Z_{CCI}$$

where  $Z_{CCI}$  is the impedance at the CCI output. The secondary on-time one-shot uses this integrated signal ( $V_{CCI}$ ) to set the secondary high-side MOSFETs on-time. When the main and secondary current-sense signals ( $V_{CM} = V_{CSP1} - V_{CSN1}$  and  $V_{CS} = V_{CSP2} - V_{CSN2}$ ) become unbalanced, the transconductance amplifiers adjust the secondary on-time, which increases or decreases the secondary inductor current until the current-sense signals are properly balanced:

$$t_{ON(SEC)} = T_{SW} \left( \frac{V_{CCI} + 0.075V}{V_{IN}} \right)$$

$$= T_{SW} \left( \frac{V_{FB} + 0.075V}{V_{IN}} \right) + T_{SW} \left( \frac{I_{CCI}Z_{CCI}}{V_{IN}} \right)$$

$$= (\text{Main On-time}) + (\text{Secondary Current Balance Correction})$$

This algorithm results in a nearly constant switching frequency and balanced inductor currents despite the lack of a fixed-frequency clock generator. The benefits of a constant switching frequency are twofold: first, the frequency can be selected to avoid noise-sensitive regions such as the 455kHz IF band; second, the inductor ripple-current operating point remains relatively constant, resulting in easy design methodology and predictable output-voltage ripple. The on-time one-shots have good accuracy at the operating points specified in the *Electrical Characteristics* table. On-times at operating points far removed from the conditions specified in the *Electrical Characteristics* table can vary over a wider range.

On-times translate only roughly to switching frequencies. The on-times guaranteed in the *Electrical Characteristics* table are influenced by switching delays in the external high-side MOSFET. Resistive losses, including the inductor, both MOSFETs, output capacitor ESR, and PCB copper losses in the output and ground tend to raise the switching frequency at higher output currents. Also, the dead-time effect increases the effective on-time, reducing the switching frequency. It occurs only during forced-PWM operation and dynamic output-voltage transitions when the induc-

tor current reverses at light- or negative-load currents. With reversed inductor current, the inductor's EMF causes  $LX_{-}$  to go high earlier than normal, extending the on-time by a period equal to the  $DH_{-}$ -rising dead time. For loads above the critical conduction point, where the dead-time effect is no longer a factor, the actual switching frequency (per phase) is:

$$f_{SW} = \frac{(V_{OUT} + V_{DIS})}{t_{ON}(V_{IN} + V_{DIS} - V_{CHG})}$$

where  $V_{DIS}$  is the sum of the parasitic voltage drops in the inductor discharge path, including synchronous rectifier, inductor, and PCB resistances;  $V_{CHG}$  is the sum of the parasitic voltage drops in the inductor charge path, including high-side switch, inductor, and PCB resistances; and  $t_{ON}$  is the on-time as determined above.

### Current Sense

The output current of each phase is sensed. Low-offset amplifiers are used for current balance, voltage-positioning gain, and current limit. Sensing the current at the output of each phase offers advantages, including less noise sensitivity, more accurate current sharing between phases, and the flexibility of using either a current-sense resistor or the DC resistance of the output inductor.

Using the DC resistance ( $R_{DCR}$ ) of the output inductor allows higher efficiency. In this configuration, the initial tolerance and temperature coefficient of the inductor's DCR must be accounted for in the output-voltage droop-error budget and power monitor. This current-sense method uses an RC filtering network to extract the current information from the output inductor (see Figure 4). The resistive divider used should provide a current-sense resistance ( $R_{CS}$ ) low enough to meet the current-limit requirements, and the time constant of the RC network should match the inductor's time constant ( $L/R_{CS}$ ):

$$R_{CS} = \left( \frac{R_2}{R_1 + R_2} \right) R_{DCR}$$

and:

$$R_{CS} = \frac{L}{C_{EQ}} \left[ \frac{1}{R_1} + \frac{1}{R_2} \right]$$

where  $R_{CS}$  is the required current-sense resistance and  $R_{DCR}$  is the inductor's series DC resistance.