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## 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5

## General Description

The MAX4104/MAX4105/MAX4304/MAX4305 op amps feature ultra-high speed, low noise, and low distortion in a SOT23 package. The unity-gain-stable MAX4104 requires only 20 mA of supply current while delivering 625 MHz bandwidth and $400 \mathrm{~V} / \mu$ s slew rate. The MAX4304, compensated for gains of $+2 \mathrm{~V} / \mathrm{V}$ or greater, delivers a 730 MHz bandwidth and a $1000 \mathrm{~V} / \mu \mathrm{s}$ slew rate. The MAX4105 is compensated for a minimum gain of $+5 \mathrm{~V} / \mathrm{V}$ and delivers a 410 MHz bandwidth and a $1400 \mathrm{~V} / \mathrm{sec}$ slew rate. The MAX4305 has $+10 \mathrm{~V} / \mathrm{V}$ minimum gain compensation and delivers a 340 MHz bandwidth and a $1400 \mathrm{~V} / \mathrm{\mu s}$ slew rate.

Low voltage noise density of $2.1 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ and -88 dBc spurious-free dynamic range make these devices ideal for low-noise/low-distortion video and telecommunications applications. These op amps also feature a wide output voltage swing of $\pm 3.7 \mathrm{~V}$ and $\pm 70 \mathrm{~mA}$ output currentdrive capability. For space-critical applications, they are available in a miniature 5-pin SOT23 package.

Applications
Video ADC Preamp
Pulse/RF Telecom Applications
Video Buffers and Cable Drivers
Ultrasound
Active Filters
ADC Input Buffers

Typical Application Circuit


Features

- Low 2.1nV $/ \sqrt{\mathrm{Hz}}$ Voltage Noise Density
- Ultra-High 740MHz -3dB Bandwidth (MAX4304, Avcl $=2 \mathrm{~V} / \mathrm{V}$ )
- 100MHz 0.1dB Gain Flatness (MAX4104/4105)
- 1400V/ $\mu$ s Slew Rate (MAX4105/4305)
- -88dBc SFDR (5MHz, RL = 100 $)$ (MAX4104/4304)
- High Output Current Drive: $\pm 70 \mathrm{~mA}$
- Low Differential Gain/Phase Error: 0.01\%/0.01 (MAX4104/4304)
- Low $\pm 1 m \mathrm{~V}$ Input Offset Voltage
- Available in Space-Saving 5-Pin SOT23 Package

Selector Guide

| PART | MINIMUM <br> STABLE <br> GAIN (V/V) | BANDWIDTH <br> (MHz) | PIN-PACKAGE |
| :---: | :---: | :---: | :--- |
| MAX4104 | 1 | 625 | 5-pin SOT23, 8-pin SO |
| MAX4304 | 2 | 740 | 5-pin SOT23, 8-pin SO |
| MAX4105 | 5 | 410 | 5-pin SOT23, 8-pin SO |
| MAX4305 | 10 | 340 | 5-pin SOT23, 8-pin SO |

Ordering Information

| PART | TEMP. RANGE | PIN- <br> PACKAGE | SOT <br> TOP MARK |
| :--- | :--- | :--- | :---: |
| MAX4104ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO | - |
| MAX4104EUK-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5 SOT $23-5$ | ACCO |

Ordering Information continued at end of data sheet.
Pin Configurations


## 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5

## ABSOLUTE MAXIMUM RATINGS

Supply Voltage ( $\mathrm{V}_{\mathrm{CC}}$ to $\mathrm{V}_{E E}$ ).
Voltage on Any Pin to Ground..........(VEE -0.3 V ) to ( $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$ )
Short-Circuit Duration (Vout to GND) $\qquad$ Continuous Continuous Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ )

$$
5 \text {-pin SOT23 (derate } 7.1 \mathrm{~mW} /{ }^{\circ} \mathrm{C} \text { above }+70^{\circ} \mathrm{C} \text { ) ........... } 571 \mathrm{~mW}
$$

8 -pin SO (derate $5.9 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ ) $\qquad$ .471 mW

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## DC ELECTRICAL CHARACTERISTICS

$\left(V_{C C}=+5 \mathrm{~V}, \mathrm{~V}_{E E}=-5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0, R_{\mathrm{L}}=100 \mathrm{k} \Omega, \mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{MIN}}\right.$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Supply Voltage Range | $\mathrm{V}_{\mathrm{Cc}} / \mathrm{V}_{\text {EE }}$ | Guaranteed by PSRR test |  | $\pm 3.5$ | $\pm 5$ | $\pm 5.5$ | V |
| Input Offset Voltage | Vos | VOUT $=0$ | MAX4_0_ESA |  | 1 | 6 | mV |
|  |  |  | MAX4_0_EUK |  | 1 | 8 |  |
| Input Offset-Voltage Drift | TCVos |  |  |  | 2.5 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | IB |  |  |  | 32 | 70 | $\mu \mathrm{A}$ |
| Input Offset Current | los |  |  |  | 0.5 | 5.0 | $\mu \mathrm{A}$ |
| Differential Input Resistance | RiN | $-0.8 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq 0.8 \mathrm{~V}$ |  |  | 6 |  | $\mathrm{k} \Omega$ |
| Common-Mode Input Resistance | RIN | Either input |  |  | 1.5 |  | $\mathrm{M} \Omega$ |
| Input Common-Mode Voltage Range | VCM | Guaranteed by CMRR test |  | -2.8 |  | +4.1 | V |
| Common-Mode Rejection Ratio | CMRR | $-2.8 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CM}} \leq 4.1 \mathrm{~V}$ |  | 80 | 95 |  | dB |
| Positive Power-Supply Rejection Ratio | PSSR+ | $\mathrm{V}_{\mathrm{CC}}=3.5 \mathrm{~V}$ to 5.5 V |  | 75 | 85 |  | dB |
| Negative Power-Supply Rejection Ratio | PSRR- | $\mathrm{V}_{\mathrm{EE}}=-3.5 \mathrm{~V}$ to -5.5V |  | 55 | 65 |  | dB |
| Quiescent Supply Current | Is | VOUT $=0$ |  |  | 20 | 27 | mA |
| Open-Loop Gain | Avol | $-2.8 \mathrm{~V} \leq \mathrm{V}_{\text {OUT }} \leq 2.8 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=100 \Omega$ |  | 55 | 65 |  | dB |
| Output Voltage Swing | Vout | $\mathrm{RL}=100 \mathrm{k} \Omega$ |  | $\pm 3.5$ | to + |  | V |
|  |  | $\mathrm{R}_{\mathrm{L}}=100 \Omega$ |  | $\pm 3.0$ | to + |  |  |
| Output Current Drive | Iout | $\mathrm{RL}=30 \Omega$ |  | $\pm 53$ | $\pm 70$ |  | mA |
| Short-Circuit Output Current | Isc | RL = short to ground |  |  | 80 |  | mA |
| Open-Loop Output Impedance | ZOUT |  |  |  | 9 |  | $\Omega$ |

## 740MHz, Low-Noise, Low-Distortion Op Amps in SOT23-5

## AC ELECTRICAL CHARACTERISTICS

$\left(V_{C C}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0, \mathrm{R}_{\mathrm{L}}=100 \Omega\right.$; $\mathrm{A} \mathrm{V}=+1 \mathrm{~V} / \mathrm{V}$ for MAX4104, $+2 \mathrm{~V} / \mathrm{V}$ for MAX4304, $+5 \mathrm{~V} / \mathrm{V}$ for MAX4105, $+10 \mathrm{~V} / \mathrm{V}$ for MAX4305; $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$; unless otherwise noted.)

| PARAMETER | SYMBOL | CONDITIONS |  |  |  | MIN TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -3dB Bandwidth | $\mathrm{BW}_{(-3 \mathrm{~dB})}$ | VOUT $=100 \mathrm{mVp}-\mathrm{p}$ |  |  | MAX4104 | 625 |  | MHz |
|  |  |  |  |  | MAX4304 | 740 |  |  |
|  |  |  |  |  | MAX4105 | 410 |  |  |
|  |  |  |  |  | MAX4305 | 340 |  |  |
| 0.1dB Bandwidth | $\mathrm{BW}_{(0.1)}$ | VOUT $=100 \mathrm{mVp}-\mathrm{p}$ |  |  | MAX4104 | 100 |  | MHz |
|  |  |  |  |  | MAX4304 | 60 |  |  |
|  |  |  |  |  | MAX4105 | 80 |  |  |
|  |  |  |  |  | MAX4305 | 70 |  |  |
| Full-Power Bandwidth | FPBW | $\mathrm{V}_{\text {OUT }}=2 \mathrm{Vp}-\mathrm{p}$ |  |  | MAX4104 | 115 |  | MHz |
|  |  |  |  |  | MAX4304 | 285 |  |  |
|  |  |  |  |  | MAX4105 | 370 |  |  |
|  |  |  |  |  | MAX4305 | 320 |  |  |
| Slew Rate | SR | VOUT $=2 \mathrm{Vp}-\mathrm{p}$ |  |  | MAX4104 | 400 |  | V/ $/ \mathrm{s}$ |
|  |  |  |  |  | MAX4304 | 1000 |  |  |
|  |  |  |  |  | MAX4105 | 1400 |  |  |
|  |  |  |  |  | MAX4305 | 1400 |  |  |
| Settling Time to 0.1\% | ts | VOUT $=2 \mathrm{Vp}-\mathrm{p}$ |  |  | to 0.1\% | 20 |  | ns |
|  |  |  |  |  | to 0.01\% | 25 |  |  |
| Spurious-Free Dynamic Range | SFDR | VOUT $=2 \mathrm{Vp}$-p | MAX4104/ MAX4304 |  | $\mathrm{f}_{\mathrm{C}}=5 \mathrm{MHz}$ | -88 |  | dBc |
|  |  |  |  |  | $\mathrm{f}_{\mathrm{C}}=20 \mathrm{MHz}$ | -67 |  |  |
|  |  |  | MAX4105/ <br> MAX4305 |  | $\mathrm{fC}_{\mathrm{C}}=5 \mathrm{MHz}$ | -74 |  |  |
|  |  |  |  |  | $\mathrm{fC}=20 \mathrm{MHz}$ | -61 |  |  |
| Differential Gain Error | DG | NTSC, RL = $150 \Omega$ |  | MAX | 04/MAX4304 | 0.01 |  | \% |
|  |  |  |  | MAX | 05/MAX4305 | 0.02 |  |  |
| Differential Phase Error | DP | NTSC, RL = $150 \Omega$ |  | MAX | 04/MAX4304 | 0.01 |  | degrees |
|  |  |  |  | MAX | 05/MAX4305 | 0.02 |  |  |
| Input Voltage Noise Density | $\mathrm{e}_{n}$ | $\mathrm{f}=1 \mathrm{MHz}$ |  |  |  | 2.1 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| Input Current Noise Density | in | $\mathrm{f}=1 \mathrm{MHz}$ |  |  |  | 3.1 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
| Output Impedance | ZOUT | $\mathrm{f}=10 \mathrm{MHz}$ |  |  |  | 1 |  | $\Omega$ |

## 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5

## Typical Operating Characteristics

$\left(\mathrm{V}_{C C}=+5 \mathrm{~V}, \mathrm{~V}_{E E}=-5 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=330 \Omega, \mathrm{R}_{\mathrm{L}}=100 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)


# 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5 

Typical Operating Characteristics (continued)
$\left(V_{C C}=+5 V, V_{E E}=-5 V, R_{F}=330 \Omega, R_{L}=100 \Omega, T_{A}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)


POSITIVE POWER-SUPPLY REJECTION vs. FREQUENCY


VOLTAGE NOISE DENSITY vs. FREQUENCY (INPUT REFERRED)


M AX4105
LARGE-SIGNAL GAIN
vs. FREQUENCY (AvCL $=+5$ )


NEGATIVE POWER-SUPPLY REJECTION
vs. FREQUENCY


CURRENT NOISE DENSITY vs. FREQUENCY (INPUT REFERRED)
clan

MAX4305
LARGE-SIGNAL GAIN vs. FREQUENCY (AvCL = +10)


COMMON-M ODE REJECTION
vs. FREQUENCY


CLOSED-LOOP OUTPUT IMPEDANCE
vs. FREQUENCY


## 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5

## Typical Operating Characteristics (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=330 \Omega, \mathrm{R}_{\mathrm{L}}=100 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)

MAX4104/MAX4304 DIFFERENTIAL GAIN AND PHASE



IRE
M AX4105/M AX4305 HARM ONIC DISTORTION vs. FREQUENCY


MAX4104/M AX4304 HARM ONIC DISTORTION vs. OUTPUT SWING


MAX4105/MAX4305 DIFFERENTIAL GAIN AND PHASE



M AX4104/M AX4304 HARM ONIC DISTORTION vs. LOAD


MAX4105/MAX4305 HARM ONIC DISTORTION
vs. OUTPUT SWING


MAX4104/M AX4304 HARM ONIC DISTORTION vs. FREQUENCY


M AX4105/M AX4305 HARM ONIC DISTORTION vs. LOAD



# 740MHz, Low-Noise, Low-Distortion Op Amps in SOT23-5 

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{C C}=+5 \mathrm{~V}, \mathrm{~V}_{E E}=-5 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=330 \Omega, \mathrm{R}_{\mathrm{L}}=100 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)


## 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{\mathrm{CC}}=+5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=-5 \mathrm{~V}, \mathrm{R}_{\mathrm{F}}=330 \Omega, \mathrm{R}_{\mathrm{L}}=100 \Omega, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted.)

MAX4305
SMALL-SIGNAL PULSE RESPONSE
( $A_{V}=+10$ )


MAX4305 LARGE-SIGNAL PULSE RESPONSE


MAX4104 LARGE-SIGNAL PULSE RESPONSE
( $A_{V}=+1$ )


MAX4105 LARGE-SIGNAL PULSE RESPONSE


MAX4305
LARGE-SIGNAL PULSE RESPONSE


# 740MHz，Low－Noise，Low－Distortion Op Amps in SOT23－5 

## Pin Description

| PIN |  | NAME | FUNCTION |  |
| :---: | :---: | :---: | :--- | :---: |
| SOT23－5 | SO |  |  |  |
| - | $1,5,8$ | N．C． | Not internally connected． |  |
| 4 | 2 | IN－ | Amplifier Inverting Input |  |
| 3 | 3 | IN＋ | Amplifier Noninverting <br> Input |  |
| 2 | 4 | VEE | Negative Power Supply |  |
| 1 | 6 | OUT | Amplifier Output |  |
| 5 | 7 | VCC | Positive Power Supply |  |

## Detailed Description

The MAX4104／MAX4105／MAX4304／MAX4305 are ultra－ high－speed，low－noise amplifiers featuring－3dB band－ widths up to $880 \mathrm{MHz}, 0.1 \mathrm{~dB}$ gain flatness up to 100 MHz ，and low differential gain and phase errors of $0.01 \%$ and $0.01^{\circ}$ ，respectively．These devices operate on dual power supplies ranging from $\pm 3.5 \mathrm{~V}$ to $\pm 5.5 \mathrm{~V}$ and require only 20 mA of supply current．
The MAX4104／MAX4304／MAX4105／MAX4305 are opti－ mized for minimum closed－loop gains of $+1 \mathrm{~V} / \mathrm{V},+2 \mathrm{~V} / \mathrm{V}$ ， $+5 \mathrm{~V} / \mathrm{V}$ and $+10 \mathrm{~V} / \mathrm{V}$（respectively）with corresponding -3 dB bandwidths of $880 \mathrm{MHz}, 730 \mathrm{MHz}, 430 \mathrm{MHz}$ ，and 350 MHz ．Each device in this family features a low input voltage noise density of only $2.1 \mathrm{nV} / \sqrt{\mathrm{Hz}}$（at 1 MHz ），an output current drive of $\pm 70 \mathrm{~mA}$ ，and spurious－free dynamic range as low as $-88 \mathrm{dBc}\left(5 \mathrm{MHz}, \mathrm{R}_{\mathrm{L}}=100 \Omega\right)$ ．

## Applications Information

## Layout and Power－Supply Bypassing

The MAX4104／MAX4105／MAX4304／MAX4305 have an extremely high bandwidth，and consequently require careful board layout，including the possible use of constant－impedance microstrip or stripline techniques．
To realize the full AC performance of these high－speed amplifiers，pay careful attention to power－supply bypassing and board layout．The PC board should have at least two layers：a signal and power layer on one side，and a large，low－impedance ground plane on the other side．The ground plane should be as free of voids as possible．With multilayer boards，locate the ground plane on a layer that incorporates no signal or power traces．

Regardless of whether or not a constant－impedance board is used，it is best to observe the following guide－ lines when designing the board：
1）Do not use wire－wrapped boards（they are much too inductive）or breadboards（they are much too capacitive）．
2）Do not use IC sockets．IC sockets increase reac－ tances．
3）Keep signal lines as short and straight as possible． Do not make $90^{\circ}$ turns；round all corners．
4）Observe high－frequency bypassing techniques to maintain the amplifier＇s accuracy and stability．
5）Bear in mind that，in general，surface－mount compo－ nents have shorter bodies and lower parasitic reac－ tance，resulting in greatly improved high－frequency performance over through－hole components．
The bypass capacitors should include 1 nF and $0.1 \mu \mathrm{~F}$ ceramic surface－mount capacitors between each sup－ ply pin and the ground plane，located as close to the package as possible．Optionally，place a $10 \mu \mathrm{~F}$ tantalum capacitor at the power supply pins＇point of entry to the PC board to ensure the integrity of incoming supplies． The power－supply trace should lead directly from the tantalum capacitor to the VCC and VEE pins．To mini－ mize parasitic inductance，keep PC traces short and use surface－mount components．
Input termination resistors and output back－termination resistors，if used，should be surface－mount types，and should be placed as close to the IC pins as possible．

## DC and Noise Errors

The MAX4104／MAX4105／MAX4304／MAX4305 output offset voltage，VOUT（Figure 1），can be calculated with the following equation：
VOUT $=\left[V_{O S}+\left(I_{B}+x R_{S}\right)+\left(\operatorname{lB}-x\left(R_{F} \| R_{G}\right)\right]\left[1+R_{F} / R_{G}\right]\right.$ where：
VOS＝input offset voltage（in volts）
$1+R_{F} / R_{G}=$ amplifier closed－loop gain（dimensionless）
$\mathrm{I}_{\mathrm{B}+}=$ noninverting input bias current（in amps）
$\mathrm{I}_{\mathrm{B}}-=$ inverting input bias current（in amps）
$\mathrm{R}_{\mathrm{G}}=$ gain－setting resistor（in ohms）
$\mathrm{RF}_{\mathrm{F}}=$ feedback resistor（in ohms）
RS＝source resistor at noninverting input（in ohms）
The following equation represents output noise density：
$e_{n(\text { OUT })}=\left[1+\frac{R_{F}}{R_{G}}\right] \sqrt{\left(i_{n} \times R_{S}\right)^{2}+\left[i_{n} \times\left(R_{F} \| R_{G}\right)\right]^{2}+e_{n}{ }^{2}}$

# 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5 



Figure 1. Output Offset Voltage
where:
$\mathrm{i}_{\mathrm{n}}=$ input current noise density (in $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ )
$\mathrm{e}_{\mathrm{n}}=$ input voltage noise density (in $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ )
The MAX4104/MAX4105/MAX4304/MAX4305 have a very low, $2.1 \mathrm{nV} / \sqrt{\mathrm{Hz}}$ input voltage noise density and $3.1 \mathrm{pA} / \sqrt{\mathrm{Hz}}$ input current noise density.
An example of DC-error calculations, using the MAX4304 typical data and the typical operating circuit with $R_{F}=R_{G}=330 \Omega\left(R_{F} \| R_{G}=165 \Omega\right)$ and $R_{S}=50 \Omega$ gives:

$$
\begin{aligned}
& V_{\text {OUT }}=\left[\left(32 \times 10^{-6}\right)(50)+\left(32 \times 10^{-6}\right)(165 \Omega)+1 \times 10^{-3}\right][1+1] \\
& V_{\text {OUT }}=15.8 \mathrm{mV}
\end{aligned}
$$

Calculating total output noise in a similar manner yields the following:

$$
\begin{aligned}
& \mathrm{e}_{\mathrm{n}(\text { OUT })}= \\
& {[1+1] \sqrt{\left(3.1 \times 10^{-12} \times 50\right)^{2}+\left(3.1 \times 10^{-12} \times 165\right)^{2}+\left(2.1 \times 10^{-9}\right)^{2}}} \\
& \mathrm{e}_{\mathrm{n}(\text { OUT })}=4.3 \mathrm{nV} \sqrt{\mathrm{~Hz}}
\end{aligned}
$$

With a 200 MHz system bandwidth, this calculates to $60.8 \mu \mathrm{~V}$ RMS (approximately $365 \mu \mathrm{Vp}-\mathrm{p}$, using the sixsigma calculation).

ADC Input Buffers Input buffer amplifiers can be a source of significant error in high-speed ADC applications. The input buffer is usually required to rapidly charge and discharge the ADC's input, which is often capacitive. In addition, the input impedance of a high-speed ADC often changes


Figure 2. Video Line Driver
very rapidly during the conversion cycle-a condition that demands an amplifier with very low output impedance at high frequencies to maintain measurement accuracy. The combination of high-speed, fast slew rate, low noise, and low-distortion available in the MAX4104/MAX4105/MAX4304/MAX4305 makes them ideally suited for use as buffer amplifiers in high-speed ADC applications.

Video Line Driver The MAX4104/MAX4105/MAX4304/MAX4305 are optimized to drive coaxial transmission lines when the cable is terminated at both ends, as shown in Figure 2. To minimize reflections and maximize power transfer, select the termination resistors to match the characteristic impedance of the transmission line. Cable frequency response can cause variations in the flatness of the signal.

Driving Capacitive Loads The MAX4104/MAX4105/MAX4304/MAX4305 provide maximum AC performance when driving no output load capacitance. This is the case when driving a correctly terminated transmission line (i.e., a back-terminated cable).
In most amplifier circuits, driving a large load capacitance increases the chance of oscillations occurring. The amplifier's output impedance and the load capacitor combine to add a pole and excess phase to the loop response. If the pole's frequency is low enough and phase margin is degraded sufficiently, oscillations may result.
A second concern when driving capacitive loads originates from the amplifier's output impedance, which

## 740MHz, Low-Noise, Low-Distortion Op Amps in SOT23-5



Figure 3a. MAX4104 Frequency Response with Capacitive Load and No Isolation Resistor


Figure 3c. MAX4105 Frequency Response with Capacitive Load and No Isolation Resistor
appears inductive at high frequencies. This inductance forms an L-C resonant circuit with the capacitive load, which causes peaking in the frequency response and degrades the amplifier's phase margin.
The MAX4104/MAX4105/MAX4304/MAX4305 drive capacitive loads up to 10 pF without oscillation. However, some peaking may occur in the frequency domain (Figure 3). To drive larger capacitance loads or to reduce ringing, add an isolation resistor between the amplifier's output and the load (Figure 4).
The value of RISO depends on the circuit's gain and the capacitive load (Figure 5). Figure 6 shows the MAX4104/MAX4105/MAX4304/MAX4305 frequency response with the isolation resistor and a capacitive


Figure 3b. MAX4304 Frequency Response with Capacitive Load and No Isolation Resistor


Figure 3d. MAX4305 Frequency Response with Capacitive Load and No Isolation Resistor
load. With higher capacitive values, bandwidth is dominated by the RC network formed by RISO and CL; the bandwidth of the amplifier itself is much higher. Also note that the isolation resistor forms a divider that decreases the voltage delivered to the load.

## Maxim's High-Speed Evaluation Boards

 The MAX4104 evaluation kit manual shows a suggested layout for Maxim's high-speed, single-amplifier evaluation boards. This board was developed using the techniques described previously (see Layout and Power-Supply Bypassing section). The smallest available surface-mount resistors were used for the feedback and back-termination resistors to minimize the
## 740 MHz , Low-Noise, Low-Distortion Op Amps in SOT23-5



Figure 4. Using an Isolation Resistor ( $R_{I S O}$ ) for High Capacitive Loads


Figure 5. Optimal Isolation Resistor (RISO) vs. Capacitive Load

## Pin Configurations (continued)




Figure 6. Frequency Responses vs. Capacitive Load with $15 \Omega$ Isolation Resistor
distance from the IC to these resistors, thus reducing the capacitance associated with longer lead lengths.
SMA connectors were used for best high-frequency performance. Because distances are extremely short, performance is unaffected by the fact that inputs and outputs do not match a $50 \Omega$ line. However, in applications that require lead lengths greater than $1 / 4$ of the wavelength of the highest frequency of interest, constant-impedance traces should be used.
Fully assembled evaluation boards are available for the MAX4104 in an 8-pin SO package.

## Ordering Information (continued)

| PART | TEMP. RANGE | PIN- <br> PACKAGE | SOT <br> TOP MARK |
| :--- | :--- | :--- | :---: |
| MAX4105ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO | - |
| MAX4105EUK-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5 SOT23-5 | ACCP |
| MAX4304ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO | - |
| MAX4304EUK-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5 SOT23-5 | ACCQ |
| MAX4305ESA | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SO | - |
| MAX4305EUK-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 5 SOT23-5 | ACCR |

*Future product-contact factory for availability.
Chip Information
TRANSISTOR COUNT: 44
SUBSTRATE CONNECTED TO VEE

