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## 620 $\mu$ A, 2 MHz Auto-Zeroed Op Amps

### Features

- High DC Precision:
  - $V_{OS}$  Drift:  $\pm 50$  nV/ $^{\circ}$ C (maximum)
  - $V_{OS}$ :  $\pm 2$   $\mu$ V (maximum)
  - $A_{OL}$ : 125 dB (minimum)
  - PSRR: 125 dB (minimum)
  - CMRR: 120 dB (minimum)
  - $E_{ni}$ : 1.0  $\mu$ V<sub>P-P</sub> (typical),  $f = 0.1$  Hz to 10 Hz
  - $E_{ni}$ : 0.32  $\mu$ V<sub>P-P</sub> (typical),  $f = 0.01$  Hz to 1 Hz
- Low Power and Supply Voltages:
  - $I_Q$ : 620  $\mu$ A/amplifier (typical)
  - Wide Supply Voltage Range: 2.3V to 5.5V
- Easy to Use:
  - Rail-to-Rail Input/Output
  - Gain Bandwidth Product: 2 MHz (typical)
  - Unity Gain Stable
  - Available in Single and Dual
  - Single with Chip Select ( $\overline{CS}$ ): MCP6V28
- Extended Temperature Range:  $-40^{\circ}$ C to  $+125^{\circ}$ C

### Typical Applications

- Portable Instrumentation
- Sensor Conditioning
- Temperature Measurement
- DC Offset Correction
- Medical Instrumentation

### Design Aids

- SPICE Macro Models
- FilterLab<sup>®</sup> Software
- Microchip Advanced Part Selector (MAPS)
- Analog Demonstration and Evaluation Boards
- Application Notes

### Related Parts

Parts with lower power, lower bandwidth and higher noise:

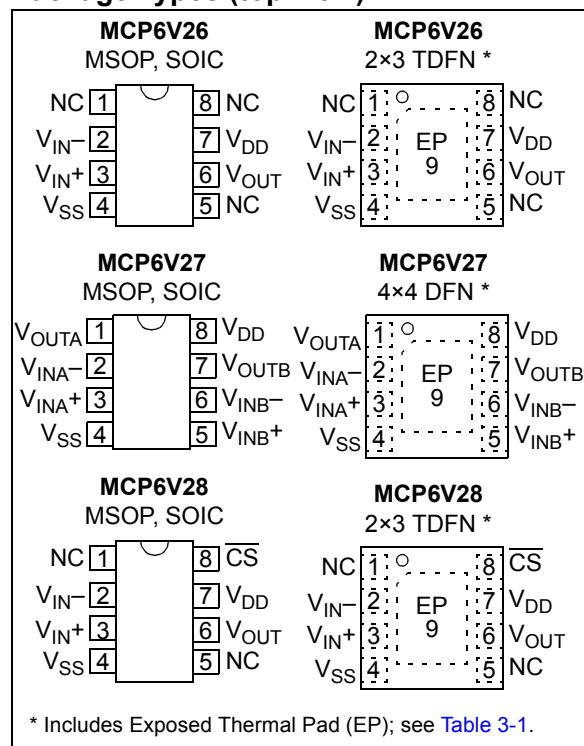
- MCP6V01/2/3: Spread clock
- MCP6V06/7/8: Non-spread clock

### Description

The Microchip Technology Inc. MCP6V26/7/8 family of operational amplifiers provides input offset voltage correction for very low offset and offset drift. These devices have a wide gain bandwidth product (2 MHz, typical) and strongly reject switching noise. They are unity gain stable, have no 1/f noise, and have good power supply rejection ratio (PSRR) and common mode rejection ratio (CMRR). These products operate with a single supply voltage as low as 2.3V, while drawing 620  $\mu$ A/amplifier (typical) of quiescent current.

The Microchip Technology Inc. MCP6V26/7/8 op amps are offered as a single (MCP6V26), single with Chip Select ( $\overline{CS}$ ) (MCP6V28) and dual (MCP6V27). They were designed using an advanced CMOS process.

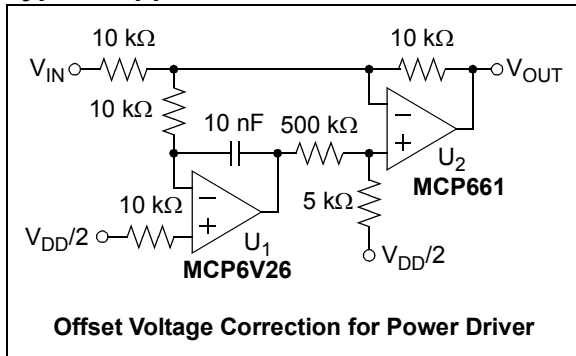
### Package Types (top view)



# MCP6V26/7/8

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## Typical Application Circuit



## 1.0 ELECTRICAL CHARACTERISTICS

### 1.1 Absolute Maximum Ratings †

$V_{DD} - V_{SS}$ .....	6.5V
Current at Input Pins †† .....	±2 mA
Analog Inputs ( $V_{IN+}$ and $V_{IN-}$ ) †† .....	$V_{SS} - 1.0V$ to $V_{DD} + 1.0V$
All other Inputs and Outputs .....	$V_{SS} - 0.3V$ to $V_{DD} + 0.3V$
Difference Input voltage .....	$ V_{DD} - V_{SS} $
Output Short Circuit Current .....	Continuous
Current at Output and Supply Pins .....	±30 mA
Storage Temperature .....	-65°C to +150°C
Max. Junction Temperature .....	+150°C
ESD protection on all pins (HBM, CDM, MM) ≥	4 kV, 1.5 kV, 300V

† **Notice:** Stresses above those listed under “Absolute Maximum Ratings” may cause permanent damage to the device. This is a stress rating only and functional operation of the device at those or any other conditions above those indicated in the operational listings of this specification is not implied. Exposure to maximum rating conditions for extended periods may affect device reliability.

†† See [Section 4.2.1, Rail-to-Rail Inputs](#).

### 1.2 Specifications

**TABLE 1-1: DC ELECTRICAL SPECIFICATIONS**

<b>Electrical Characteristics:</b> Unless otherwise indicated, $T_A = +25^\circ\text{C}$ , $V_{DD} = +2.3V$ to $+5.5V$ , $V_{SS} = \text{GND}$ , $V_{CM} = V_{DD}/3$ , $V_{OUT} = V_{DD}/2$ , $V_L = V_{DD}/2$ , $R_L = 10\text{ k}\Omega$ to $V_L$ and $\overline{\text{CS}} = \text{GND}$ (refer to <a href="#">Figure 1-5</a> and <a href="#">Figure 1-6</a> ).						
Parameters	Sym	Min	Typ	Max	Units	Conditions
<b>Input Offset</b>						
Input Offset Voltage	$V_{OS}$	-2	—	+2	$\mu\text{V}$	$T_A = +25^\circ\text{C}$ ( <a href="#">Note 1</a> )
Input Offset Voltage Drift with Temperature (linear Temp. Co.)	$TC_1$	-50	—	+50	$\text{nV}/^\circ\text{C}$	$T_A = -40$ to $+125^\circ\text{C}$ ( <a href="#">Note 1</a> )
Input Offset Voltage Quadratic Temperature Coefficient	$TC_2$	—	±0.2	—	$\text{nV}/^\circ\text{C}^2$	$T_A = -40$ to $+125^\circ\text{C}$
Power Supply Rejection	PSRR	125	142	—	dB	( <a href="#">Note 1</a> )
<b>Input Bias Current and Impedance</b>						
Input Bias Current	$I_B$	—	+7	—	pA	
Input Bias Current across Temperature	$I_B$	—	+110	—	pA	$T_A = +85^\circ\text{C}$
	$I_B$	—	+1.2	+5	nA	$T_A = +125^\circ\text{C}$
Input Offset Current	$I_{OS}$	—	±70	—	pA	
Input Offset Current across Temperature	$I_{OS}$	—	±50	—	pA	$T_A = +85^\circ\text{C}$
	$I_{OS}$	—	±60	—	pA	$T_A = +125^\circ\text{C}$
Common Mode Input Impedance	$Z_{CM}$	—	$10^{13}  12$	—	$\Omega  \text{pF}$	
Differential Input Impedance	$Z_{DIFF}$	—	$10^{13}  12$	—	$\Omega  \text{pF}$	

**Note 1:** Set by design and characterization. Due to thermal junction and other effects in the production environment, these parts can only be screened in production (except  $TC_1$ ; see [Appendix B: “Offset Related Test Screens”](#)).

**2:** [Figure 2-18](#) shows how  $V_{CML}$  and  $V_{CMH}$  changed across temperature for the first production lot.

# MCP6V26/7/8

**TABLE 1-1: DC ELECTRICAL SPECIFICATIONS (CONTINUED)**

<b>Electrical Characteristics:</b> Unless otherwise indicated, $T_A = +25^\circ\text{C}$ , $V_{DD} = +2.3\text{V}$ to $+5.5\text{V}$ , $V_{SS} = \text{GND}$ , $V_{CM} = V_{DD}/3$ , $V_{OUT} = V_{DD}/2$ , $V_L = V_{DD}/2$ , $R_L = 10\text{ k}\Omega$ to $V_L$ and $\overline{\text{CS}} = \text{GND}$ (refer to <a href="#">Figure 1-5</a> and <a href="#">Figure 1-6</a> ).						
Parameters	Sym	Min	Typ	Max	Units	Conditions
<b>Common Mode</b>						
Common-Mode Input Voltage Range Low	$V_{CML}$	—	—	$V_{SS} - 0.15$	V	(Note 2)
Common-Mode Input Voltage Range High	$V_{CMH}$	$V_{DD} + 0.2$	—	—	V	(Note 2)
Common-Mode Rejection	CMRR	120	136	—	dB	$V_{DD} = 2.3\text{V}$ , $V_{CM} = -0.15\text{V}$ to $2.5\text{V}$ (Note 1, Note 2)
	CMRR	125	142	—	dB	$V_{DD} = 5.5\text{V}$ , $V_{CM} = -0.15\text{V}$ to $5.7\text{V}$ (Note 1, Note 2)
<b>Open-Loop Gain</b>						
DC Open-Loop Gain (large signal)	$A_{OL}$	125	147	—	dB	$V_{DD} = 2.3\text{V}$ , $V_{OUT} = 0.2\text{V}$ to $2.1\text{V}$ (Note 1)
	$A_{OL}$	133	155	—	dB	$V_{DD} = 5.5\text{V}$ , $V_{OUT} = 0.2\text{V}$ to $5.3\text{V}$ (Note 1)
<b>Output</b>						
Minimum Output Voltage Swing	$V_{OL}$	—	$V_{SS} + 5$	$V_{SS} + 15$	mV	$G = +2$ , $0.5\text{V}$ input overdrive
Maximum Output Voltage Swing	$V_{OH}$	$V_{DD} - 15$	$V_{DD} - 5$	—	mV	$G = +2$ , $0.5\text{V}$ input overdrive
Output Short Circuit Current	$I_{SC}$	—	$\pm 12$	—	mA	$V_{DD} = 2.3\text{V}$
	$I_{SC}$	—	$\pm 22$	—	mA	$V_{DD} = 5.5\text{V}$
<b>Power Supply</b>						
Supply Voltage	$V_{DD}$	2.3	—	5.5	V	
Quiescent Current per amplifier	$I_Q$	450	620	800	$\mu\text{A}$	$I_O = 0$
POR Trip Voltage	$V_{POR}$	1.15	—	1.65	V	

**Note 1:** Set by design and characterization. Due to thermal junction and other effects in the production environment, these parts can only be screened in production (except  $TC_1$ ; see [Appendix B: “Offset Related Test Screens”](#)).

**2:** [Figure 2-18](#) shows how  $V_{CML}$  and  $V_{CMH}$  changed across temperature for the first production lot.

**TABLE 1-2: AC ELECTRICAL SPECIFICATIONS**

**Electrical Characteristics:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $+5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$  (refer to [Figure 1-5](#) and [Figure 1-6](#)).

Parameters	Sym	Min	Typ	Max	Units	Conditions
<b>Amplifier AC Response</b>						
Gain Bandwidth Product	GBWP	—	2.0	—	MHz	
Slew Rate	SR	—	1.0	—	V/ $\mu\text{s}$	
Phase Margin	PM	—	65	—	$^\circ$	G = +1
<b>Amplifier Noise Response</b>						
Input Noise Voltage	$E_{ni}$	—	0.32	—	$\mu\text{V}_{P-P}$	f = 0.01 Hz to 1 Hz
	$E_{ni}$	—	1.0	—	$\mu\text{V}_{P-P}$	f = 0.1 Hz to 10 Hz
Input Noise Voltage Density	$e_{ni}$	—	50	—	nV/ $\sqrt{\text{Hz}}$	f < 5 kHz
	$e_{ni}$	—	29	—	nV/ $\sqrt{\text{Hz}}$	f = 100 kHz
Input Noise Current Density	$i_{ni}$	—	0.6	—	fA/ $\sqrt{\text{Hz}}$	
<b>Amplifier Distortion (Note 1)</b>						
Intermodulation Distortion (AC)	IMD	—	40	—	$\mu\text{V}_{PK}$	$V_{CM}$ tone = 50 mV <sub>PK</sub> at 1 kHz, $G_N = 1$
<b>Amplifier Step Response</b>						
Start Up Time	$t_{STR}$	—	75	—	$\mu\text{s}$	G = +1, $V_{OS}$ within 50 $\mu\text{V}$ of its final value <b>(Note 2)</b>
Offset Correction Settling Time	$t_{STL}$	—	150	—	$\mu\text{s}$	G = +1, $V_{IN}$ step of 2V, $V_{OS}$ within 50 $\mu\text{V}$ of its final value
Output Overdrive Recovery Time	$t_{ODR}$	—	45	—	$\mu\text{s}$	G = -100, $\pm 0.5\text{V}$ input overdrive to $V_{DD}/2$ , $V_{IN}$ 50% point to $V_{OUT}$ 90% point <b>(Note 3)</b>

- Note 1:** These parameters were characterized using the circuit in [Figure 1-7](#). In [Figure 2-37](#) and [Figure 2-38](#), there is an IMD tone at DC, a residual tone at 1 kHz, other IMD tones and clock tones.
- 2:** High gains behave differently; see [Section 4.3.3, Offset at Power Up](#).
- 3:**  $t_{ODR}$  includes some uncertainty due to clock edge timing.

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**TABLE 1-3: DIGITAL ELECTRICAL SPECIFICATIONS**

**Electrical Characteristics:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $+5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$ , and  $\overline{\text{CS}} = \text{GND}$  (refer to [Figure 1-5](#) and [Figure 1-6](#)).

Parameters	Sym	Min	Typ	Max	Units	Conditions
<b><math>\overline{\text{CS}}</math> Pull-Down Resistor (MCP6V28)</b>						
$\overline{\text{CS}}$ Pull-Down Resistor	$R_{PD}$	3	5	—	$\text{M}\Omega$	
<b><math>\overline{\text{CS}}</math> Low Specifications (MCP6V28)</b>						
$\overline{\text{CS}}$ Logic Threshold, Low	$V_{IL}$	$V_{SS}$	—	$0.3V_{DD}$	V	
$\overline{\text{CS}}$ Input Current, Low	$I_{CSL}$	—	5	—	$\mu\text{A}$	$\overline{\text{CS}} = V_{SS}$
<b><math>\overline{\text{CS}}</math> High Specifications (MCP6V28)</b>						
$\overline{\text{CS}}$ Logic Threshold, High	$V_{IH}$	$0.7V_{DD}$	—	$V_{DD}$	V	
$\overline{\text{CS}}$ Input Current, High	$I_{CSH}$	—	$V_{DD}/R_{PD}$	—	$\mu\text{A}$	$\overline{\text{CS}} = V_{DD}$
$\overline{\text{CS}}$ Input High, GND Current per amplifier	$I_{SS}$	—	-0.4	—	$\mu\text{A}$	$\overline{\text{CS}} = V_{DD}$ , $V_{DD} = 2.3\text{V}$
	$I_{SS}$	—	-1	—	$\mu\text{A}$	$\overline{\text{CS}} = V_{DD}$ , $V_{DD} = 5.5\text{V}$
Amplifier Output Leakage, $\overline{\text{CS}}$ High	$I_{O\_LEAK}$	—	20	—	$\mu\text{A}$	$\overline{\text{CS}} = V_{DD}$
<b><math>\overline{\text{CS}}</math> Dynamic Specifications (MCP6V28)</b>						
$\overline{\text{CS}}$ Low to Amplifier Output On Turn-on Time	$t_{ON}$	—	4	50	$\mu\text{s}$	$\overline{\text{CS}}$ Low = $V_{SS} + 0.3\text{ V}$ , $G = +1\text{ V/V}$ , $V_{OUT} = 0.9 V_{DD}/2$
$\overline{\text{CS}}$ High to Amplifier Output High-Z	$t_{OFF}$	—	1	—	$\mu\text{s}$	$\overline{\text{CS}}$ High = $V_{DD} - 0.3\text{ V}$ , $G = +1\text{ V/V}$ , $V_{OUT} = 0.1 V_{DD}/2$
Internal Hysteresis	$V_{HYST}$	—	0.2	—	V	

**TABLE 1-4: TEMPERATURE SPECIFICATIONS**

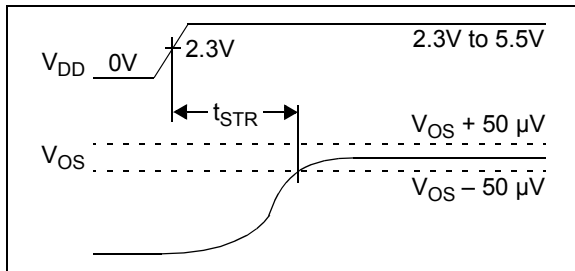
**Electrical Characteristics:** Unless otherwise indicated, all limits are specified for:  $V_{DD} = +2.3\text{V}$  to  $+5.5\text{V}$ ,  $V_{SS} = \text{GND}$ .

Parameters	Sym	Min	Typ	Max	Units	Conditions
<b>Temperature Ranges</b>						
Specified Temperature Range	$T_A$	-40	—	+125	$^\circ\text{C}$	
Operating Temperature Range	$T_A$	-40	—	+125	$^\circ\text{C}$	(Note 1)
Storage Temperature Range	$T_A$	-65	—	+150	$^\circ\text{C}$	
<b>Thermal Package Resistances</b>						
Thermal Resistance, 8L-4x4 DFN	$\theta_{JA}$	—	48	—	$^\circ\text{C/W}$	(Note 2)
Thermal Resistance, 8L-MSOP	$\theta_{JA}$	—	211	—	$^\circ\text{C/W}$	
Thermal Resistance, 8L-SOIC	$\theta_{JA}$	—	150	—	$^\circ\text{C/W}$	
Thermal Resistance, 8L-2x3 TDFN	$\theta_{JA}$	—	53	—	$^\circ\text{C/W}$	(Note 2)

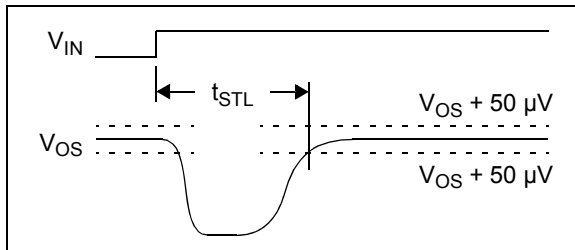
**Note 1:** Operation must not cause  $T_J$  to exceed Maximum Junction Temperature specification (+150 $^\circ\text{C}$ ).

**Note 2:** Measured on a standard JC51-7, four layer printed circuit board with ground plane and vias.

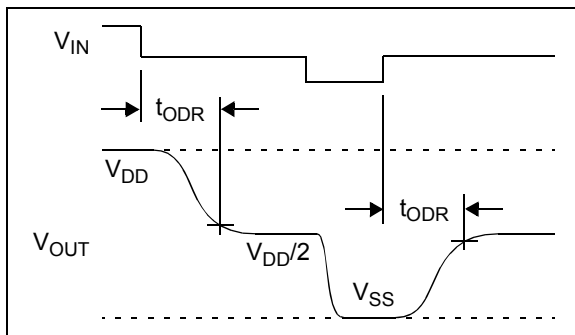
## 1.3 Timing Diagrams



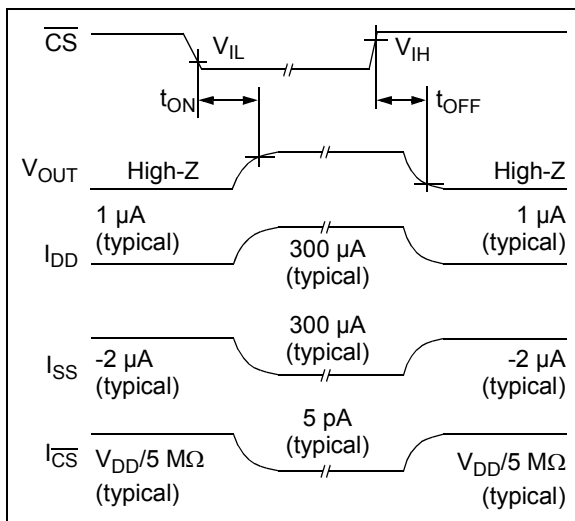
**FIGURE 1-1:** Amplifier Start Up.



**FIGURE 1-2:** Offset Correction Settling Time.



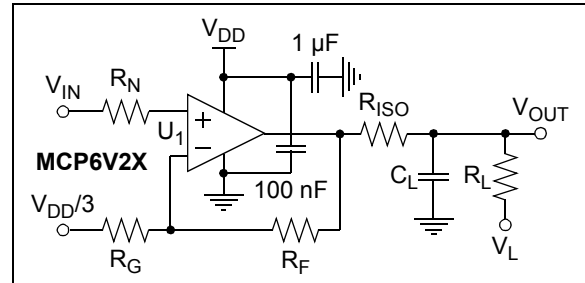
**FIGURE 1-3:** Output Overdrive Recovery.



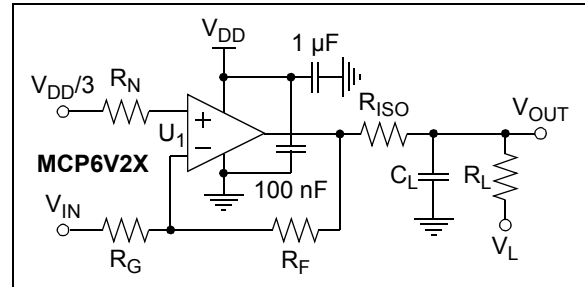
**FIGURE 1-4:** Chip Select (MCP6V28).

## 1.4 Test Circuits

The circuits used for the DC and AC tests are shown in [Figure 1-5](#) and [Figure 1-6](#). Lay the bypass capacitors out as discussed in [Section 4.3.10, Supply Bypassing and Filtering](#).  $R_N$  is equal to the parallel combination of  $R_F$  and  $R_G$  to minimize bias current effects.

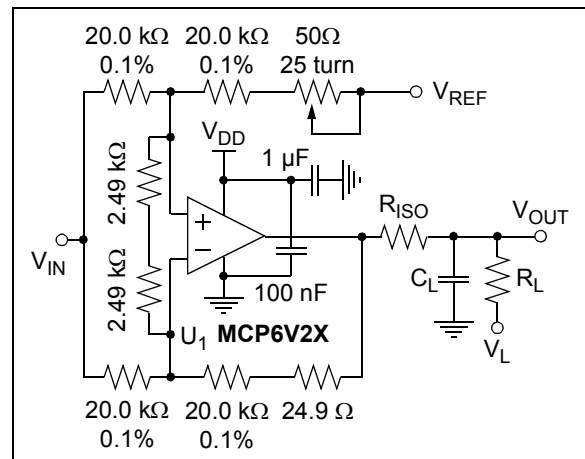


**FIGURE 1-5:** AC and DC Test Circuit for Most Non-Inverting Gain Conditions.



**FIGURE 1-6:** AC and DC Test Circuit for Most Inverting Gain Conditions.

The circuit in [Figure 1-7](#) tests the op amp input's dynamic behavior (i.e., IMD,  $t_{STR}$ ,  $t_{STL}$  and  $t_{ODR}$ ). The potentiometer balances the resistor network ( $V_{OUT}$  should equal  $V_{REF}$  at DC). The op amp's common mode input voltage is  $V_{CM} = V_{IN}/2$ . The error at the input ( $V_{ERR}$ ) appears at  $V_{OUT}$  with a noise gain of 10 V/V.



**FIGURE 1-7:** Test Circuit for Dynamic Input Behavior.



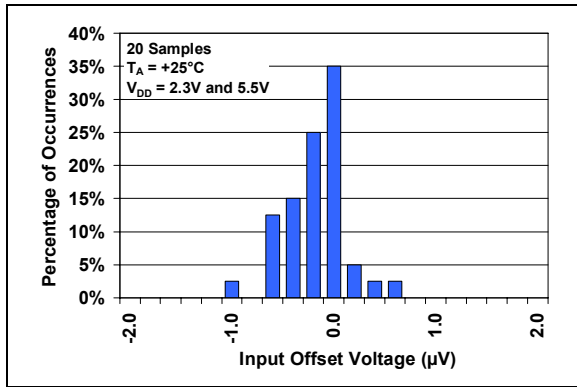
# MCP6V26/7/8

## 2.0 TYPICAL PERFORMANCE CURVES

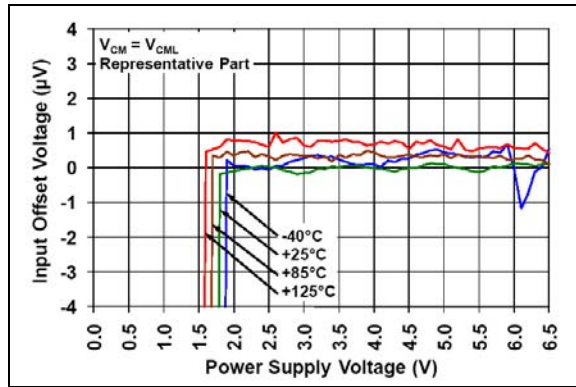
**Note:** The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .

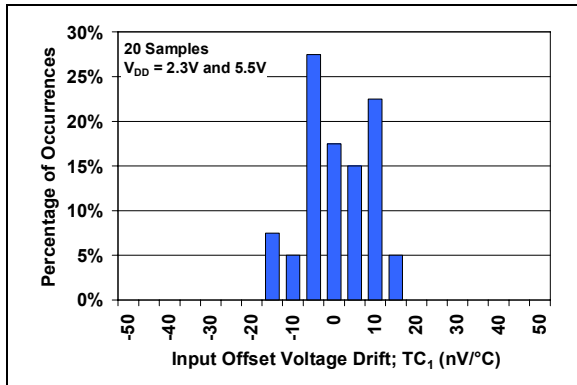
### 2.1 DC Input Precision



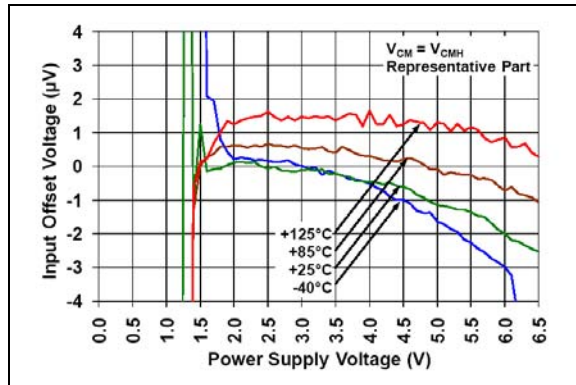
**FIGURE 2-1:** Input Offset Voltage.



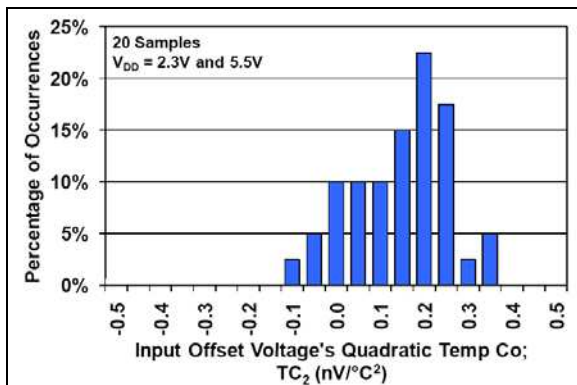
**FIGURE 2-4:** Input Offset Voltage vs. Power Supply Voltage with  $V_{CM} = V_{CM_L}$ .



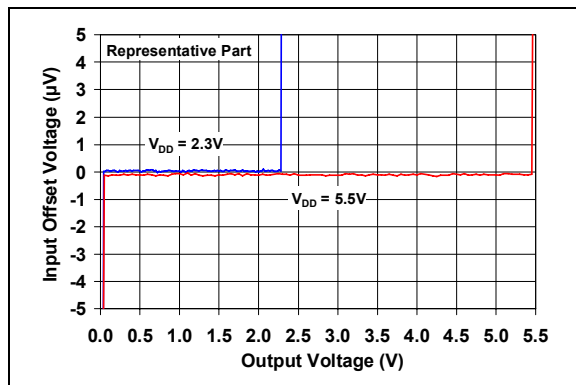
**FIGURE 2-2:** Input Offset Voltage Drift.



**FIGURE 2-5:** Input Offset Voltage vs. Power Supply Voltage with  $V_{CM} = V_{CM_H}$ .

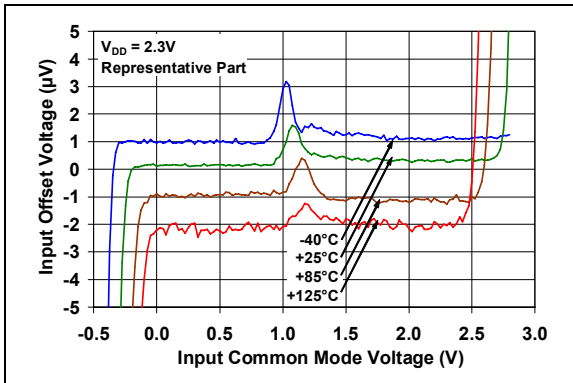


**FIGURE 2-3:** Input Offset Voltage Quadratic Temperature Coefficient.

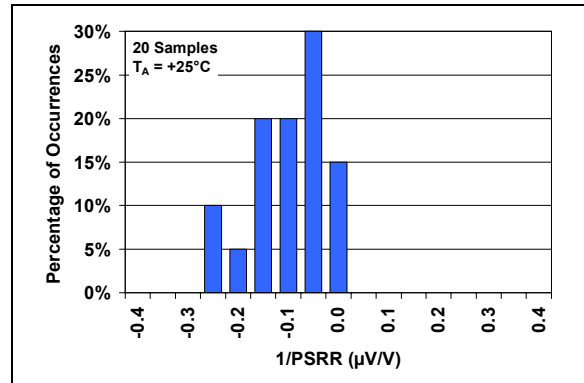


**FIGURE 2-6:** Input Offset Voltage vs. Output Voltage.

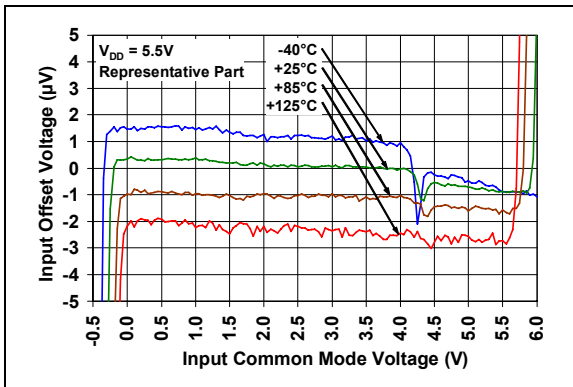
**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .



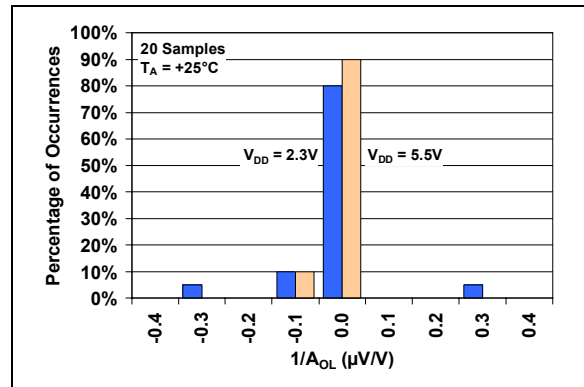
**FIGURE 2-7:** Input Offset Voltage vs. Common Mode Voltage with  $V_{DD} = 2.3\text{V}$ .



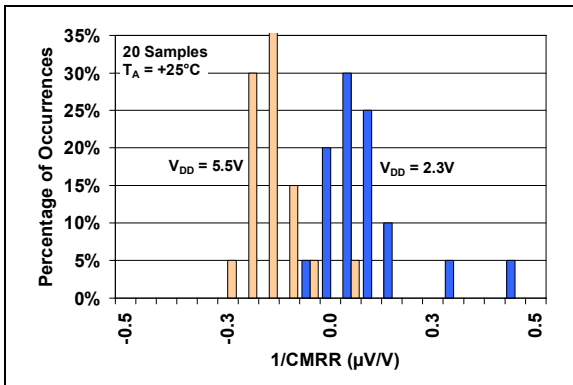
**FIGURE 2-10:** PSRR.



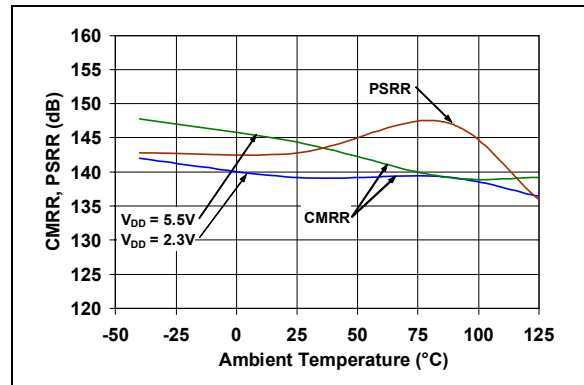
**FIGURE 2-8:** Input Offset Voltage vs. Common Mode Voltage with  $V_{DD} = 5.5\text{V}$ .



**FIGURE 2-11:** DC Open-Loop Gain.



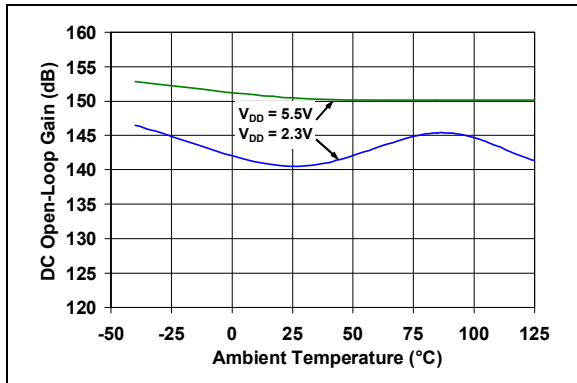
**FIGURE 2-9:** CMRR.



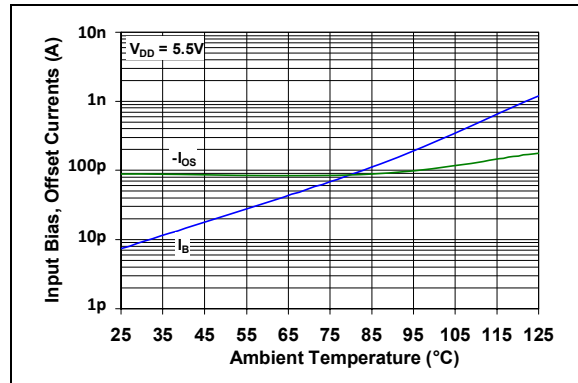
**FIGURE 2-12:** CMRR and PSRR vs. Ambient Temperature.

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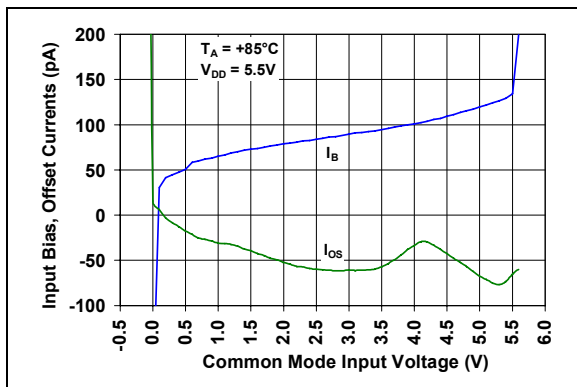
**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .



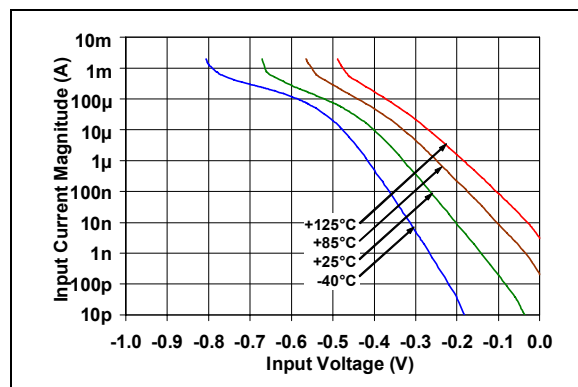
**FIGURE 2-13:** DC Open-Loop Gain vs. Ambient Temperature.



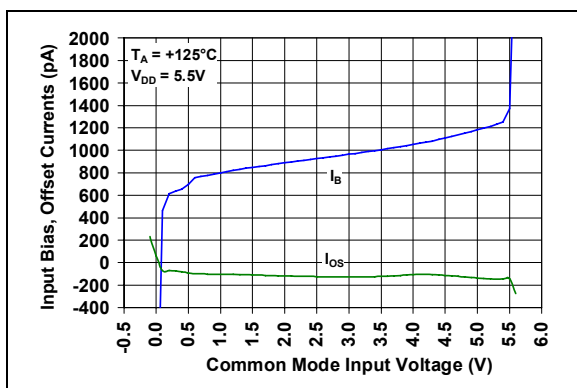
**FIGURE 2-16:** Input Bias and Offset Currents vs. Ambient Temperature with  $V_{DD} = +5.5\text{V}$ .



**FIGURE 2-14:** Input Bias and Offset Currents vs. Common Mode Input Voltage with  $T_A = +85^\circ\text{C}$ .



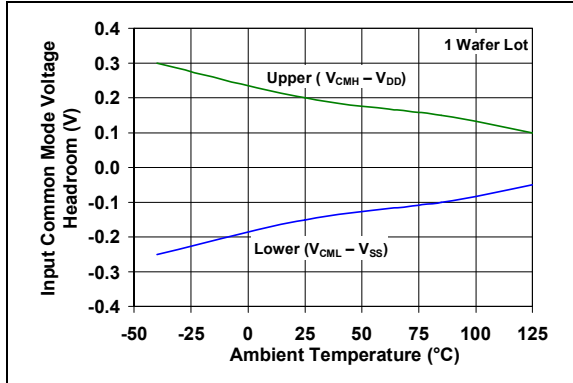
**FIGURE 2-17:** Input Bias Current vs. Input Voltage (below  $V_{SS}$ ).



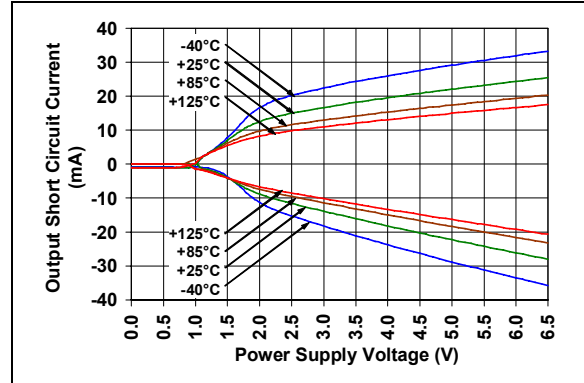
**FIGURE 2-15:** Input Bias and Offset Currents vs. Common Mode Input Voltage with  $T_A = +125^\circ\text{C}$ .

**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .

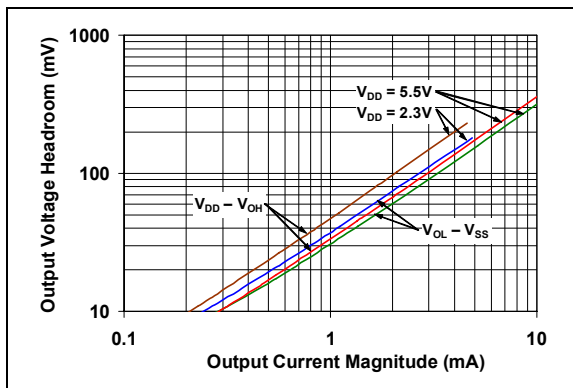
## 2.2 Other DC Voltages and Currents



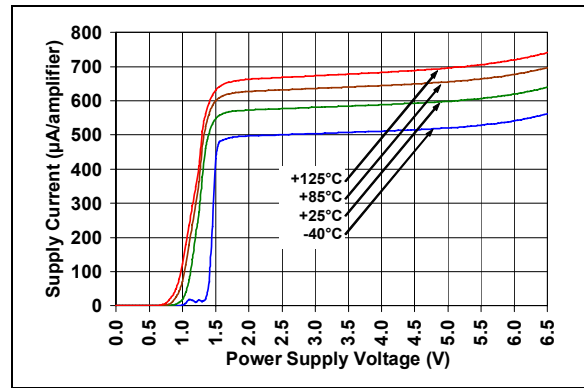
**FIGURE 2-18:** Input Common Mode Voltage Headroom (Range) vs. Ambient Temperature.



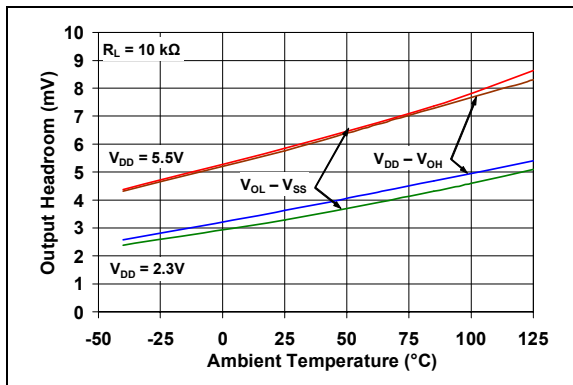
**FIGURE 2-21:** Output Short Circuit Current vs. Power Supply Voltage.



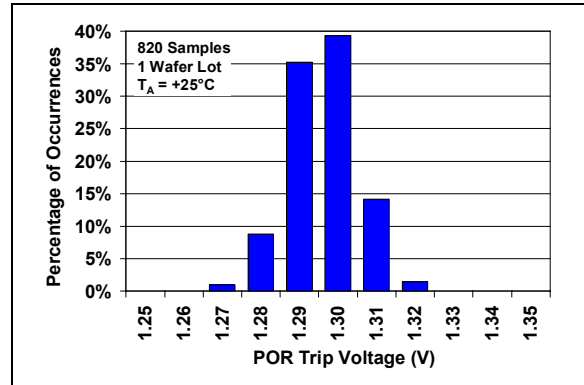
**FIGURE 2-19:** Output Voltage Headroom vs. Output Current.



**FIGURE 2-22:** Supply Current vs. Power Supply Voltage.



**FIGURE 2-20:** Output Voltage Headroom vs. Ambient Temperature.

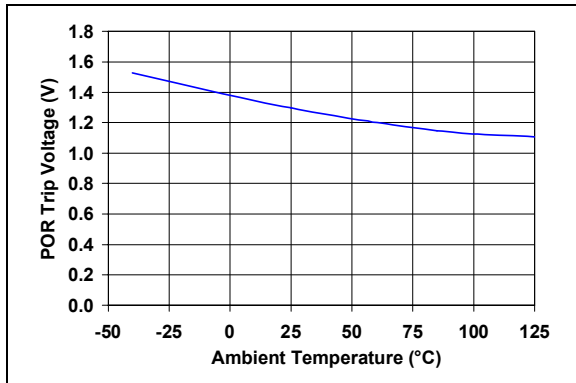


**FIGURE 2-23:** Power On Reset Trip Voltage.

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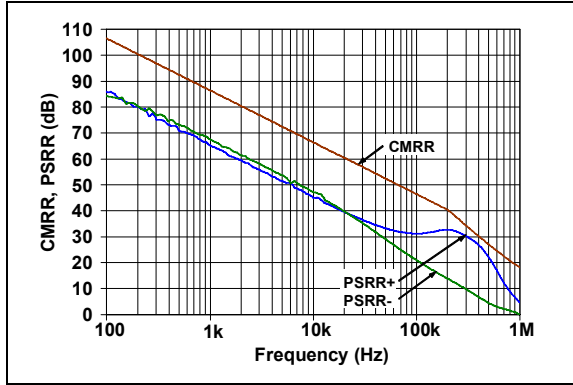
**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .



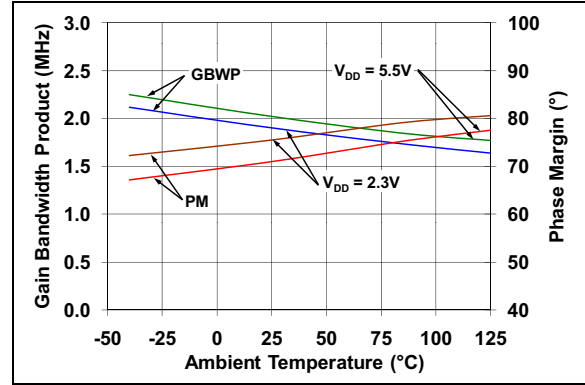
**FIGURE 2-24:** Power On Reset Voltage vs. Ambient Temperature.

**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .

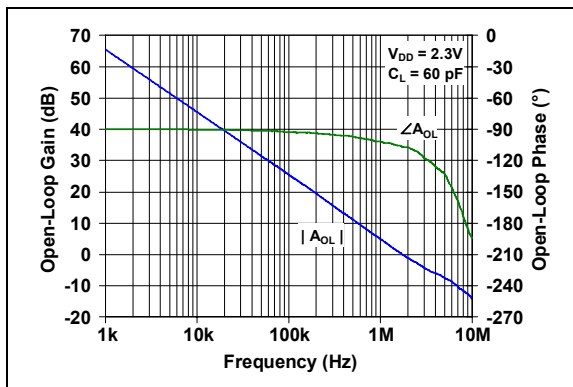
## 2.3 Frequency Response



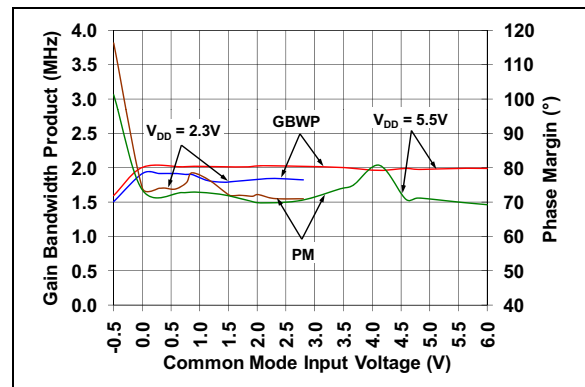
**FIGURE 2-25:** CMRR and PSRR vs. Frequency.



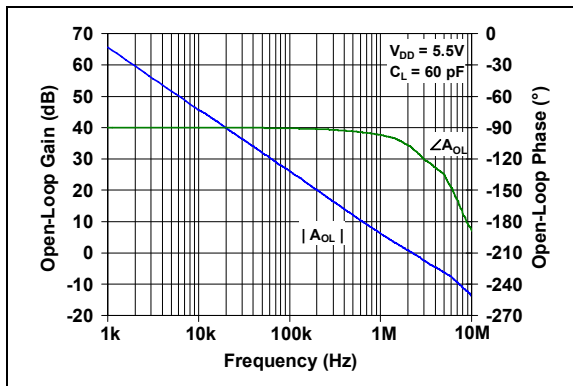
**FIGURE 2-28:** Gain Bandwidth Product and Phase Margin vs. Ambient Temperature.



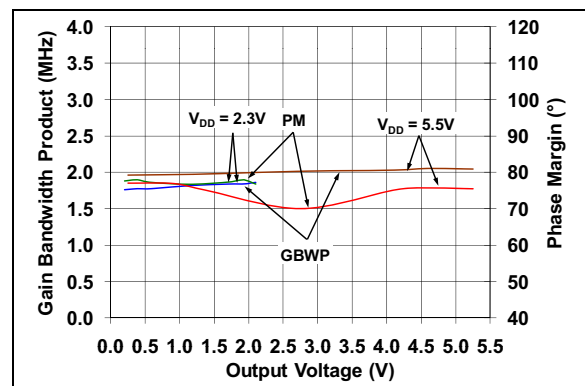
**FIGURE 2-26:** Open-Loop Gain vs. Frequency with  $V_{DD} = 2.3\text{V}$ .



**FIGURE 2-29:** Gain Bandwidth Product and Phase Margin vs. Common Mode Input Voltage.



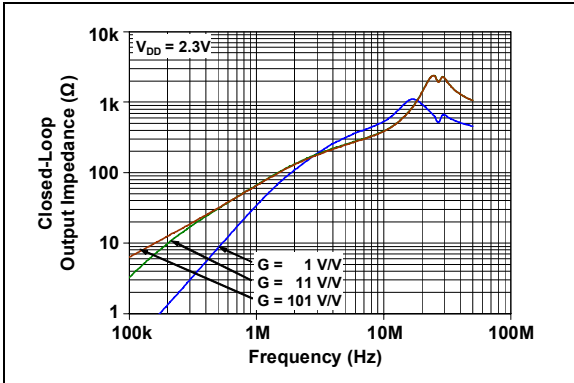
**FIGURE 2-27:** Open-Loop Gain vs. Frequency with  $V_{DD} = 5.5\text{V}$ .



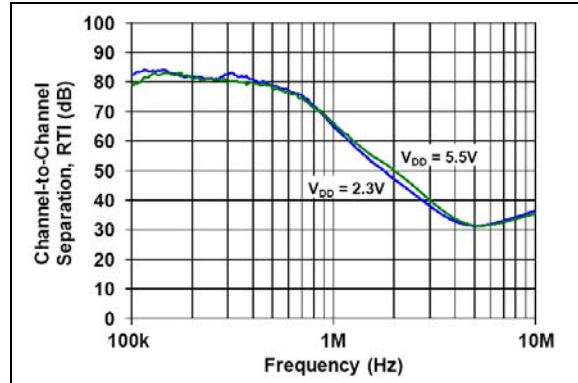
**FIGURE 2-30:** Gain Bandwidth Product and Phase Margin vs. Output Voltage.

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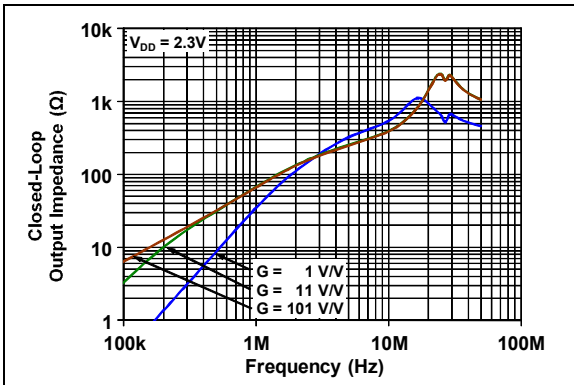
**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .



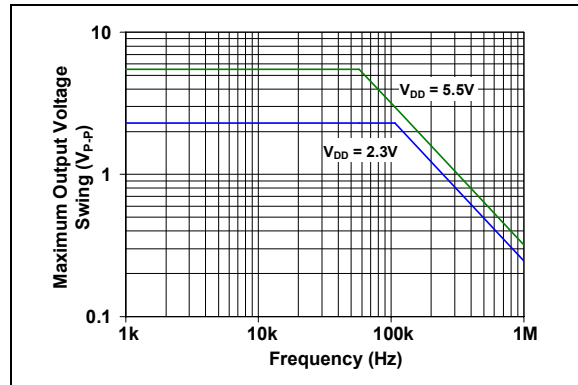
**FIGURE 2-31:** Closed-Loop Output Impedance vs. Frequency with  $V_{DD} = 2.3\text{V}$ .



**FIGURE 2-33:** Channel-to-Channel Separation vs. Frequency.



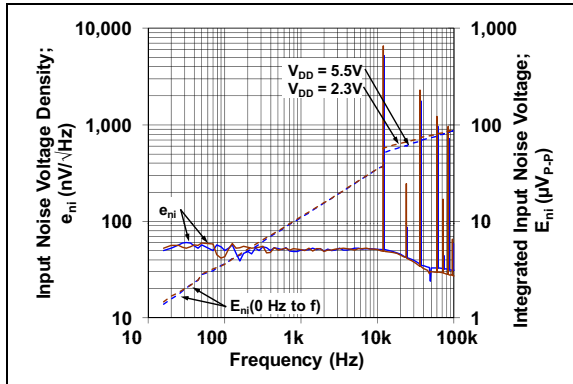
**FIGURE 2-32:** Closed-Loop Output Impedance vs. Frequency with  $V_{DD} = 5.5\text{V}$ .



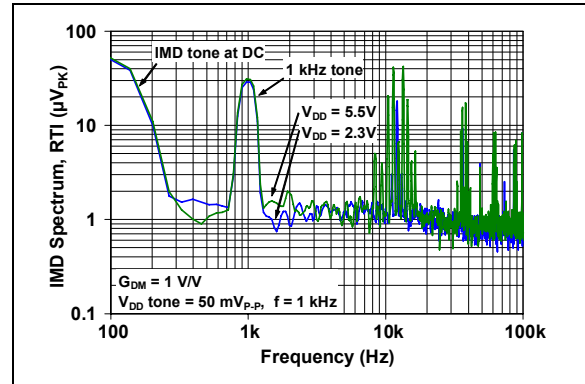
**FIGURE 2-34:** Maximum Output Voltage Swing vs. Frequency.

**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $CS = \text{GND}$ .

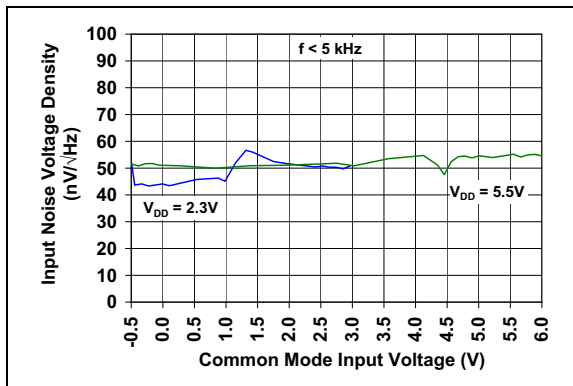
## 2.4 Input Noise and Distortion



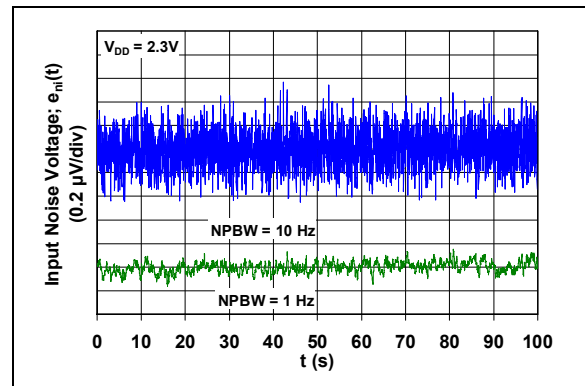
**FIGURE 2-35:** Input Noise Voltage Density and Integrated Input Noise Voltage vs. Frequency.



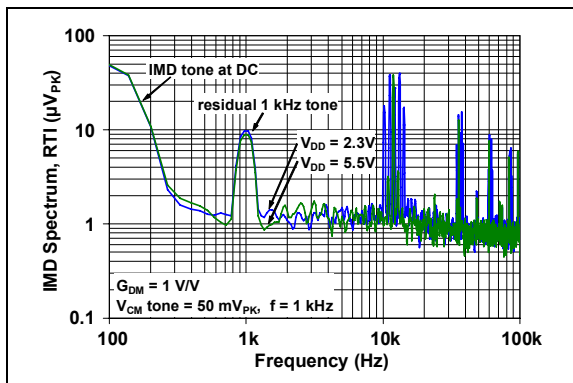
**FIGURE 2-38:** Intermodulation Distortion vs. Frequency with  $V_{DD}$  Disturbance (see Figure 1-7).



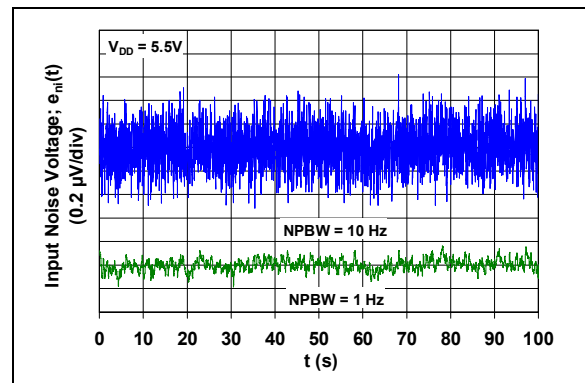
**FIGURE 2-36:** Input Noise Voltage Density vs. Input Common Mode Voltage.



**FIGURE 2-39:** Input Noise vs. Time with 1 Hz and 10 Hz Filters and  $V_{DD} = 2.3\text{V}$ .



**FIGURE 2-37:** Intermodulation Distortion vs. Frequency with  $V_{CM}$  Disturbance (see Figure 1-7).



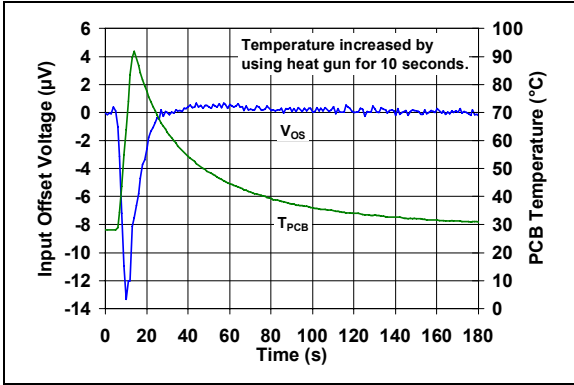
**FIGURE 2-40:** Input Noise vs. Time with 1 Hz and 10 Hz Filters and  $V_{DD} = 5.5\text{V}$ .



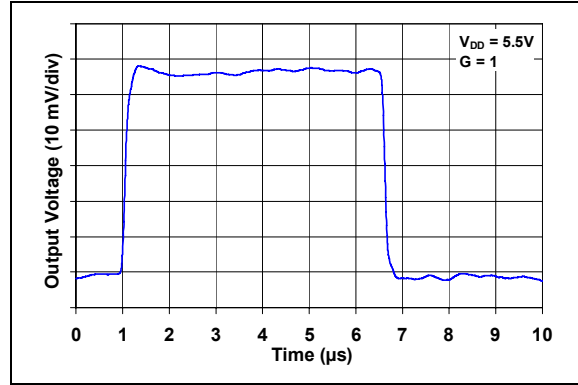
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**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .

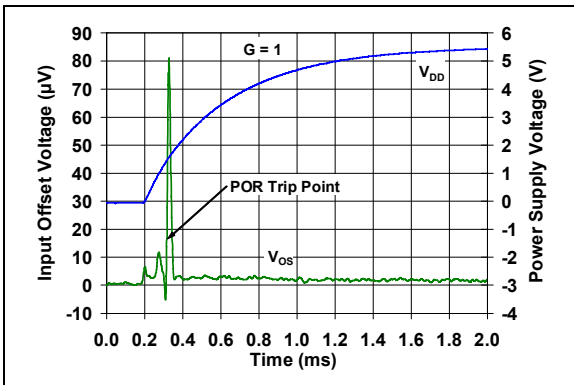
## 2.5 Time Response



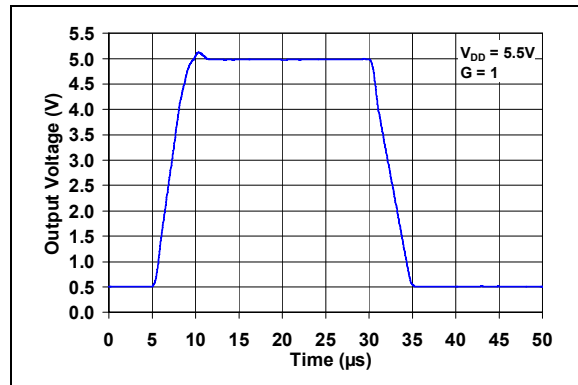
**FIGURE 2-41:** Input Offset Voltage vs. Time with Temperature Change.



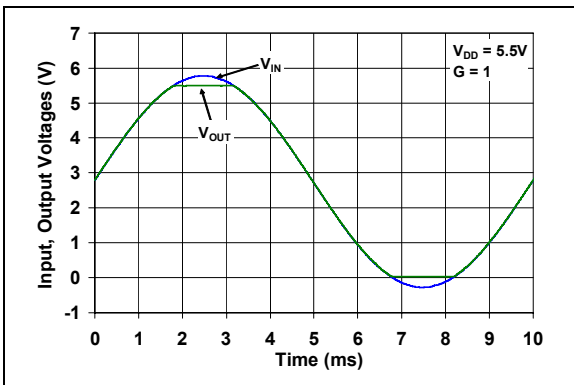
**FIGURE 2-44:** Non-inverting Small Signal Step Response.



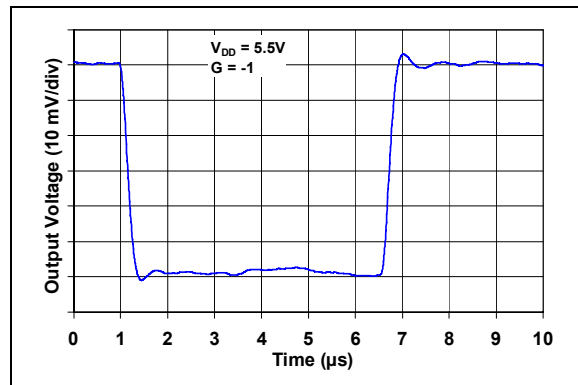
**FIGURE 2-42:** Input Offset Voltage vs. Time at Power Up.



**FIGURE 2-45:** Non-inverting Large Signal Step Response.

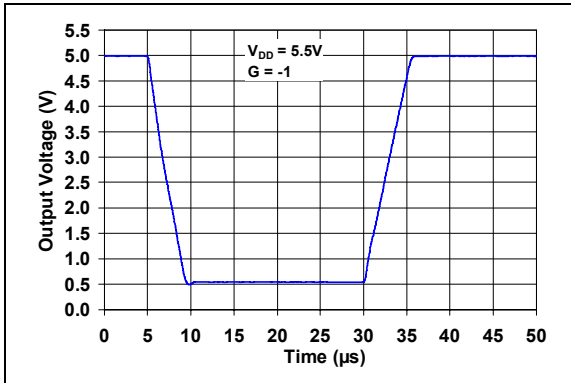


**FIGURE 2-43:** The MCP6V26/7/8 Device Shows No Input Phase Reversal with Overdrive.

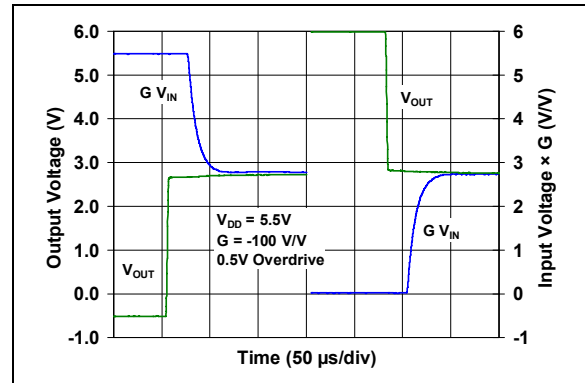


**FIGURE 2-46:** Inverting Small Signal Step Response.

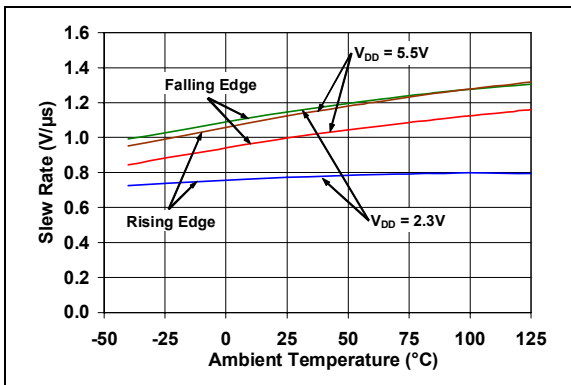
**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$  and  $\overline{\text{CS}} = \text{GND}$ .



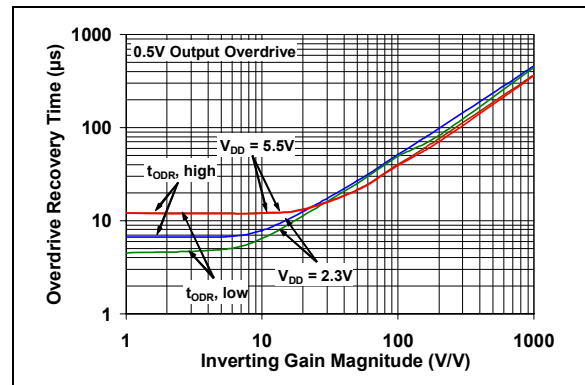
**FIGURE 2-47:** Inverting Large Signal Step Response.



**FIGURE 2-49:** Output Overdrive Recovery vs. Time with  $G = -100\text{ V/V}$ .



**FIGURE 2-48:** Slew Rate vs. Ambient Temperature.

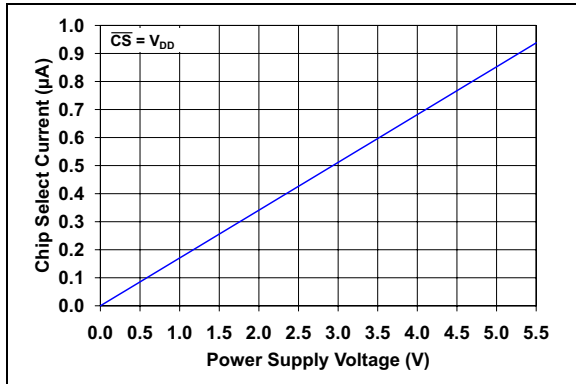


**FIGURE 2-50:** Output Overdrive Recovery Time vs. Inverting Gain.

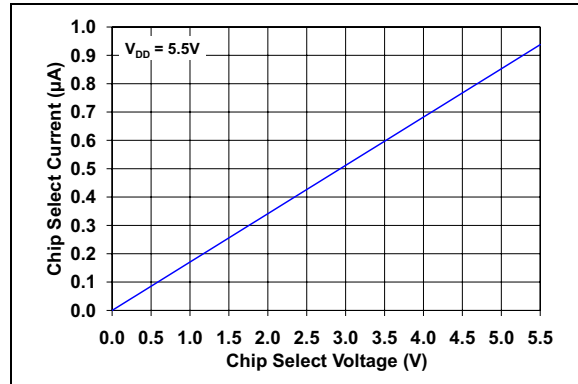
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**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$ , and  $\overline{\text{CS}} = \text{GND}$ .

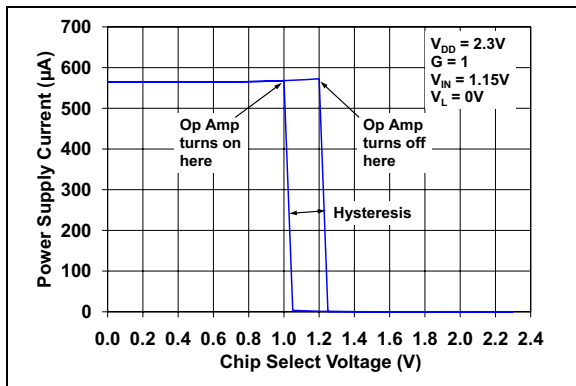
## 2.6 Chip Select Response (MCP6V28 only)



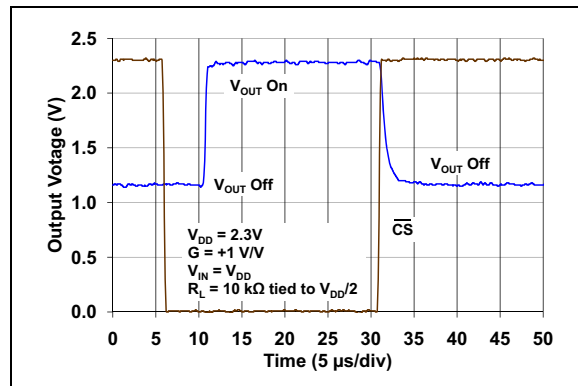
**FIGURE 2-51:** Chip Select Current vs. Power Supply Voltage.



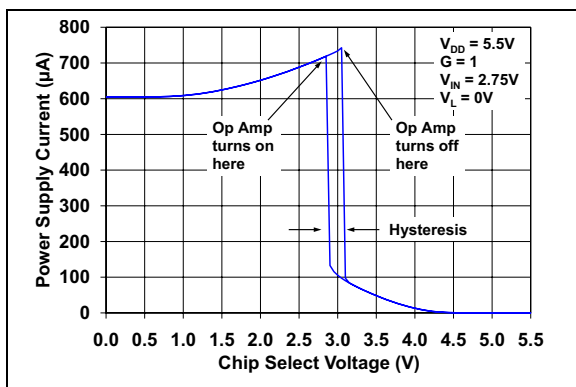
**FIGURE 2-54:** Chip Select Current vs. Chip Select Voltage.



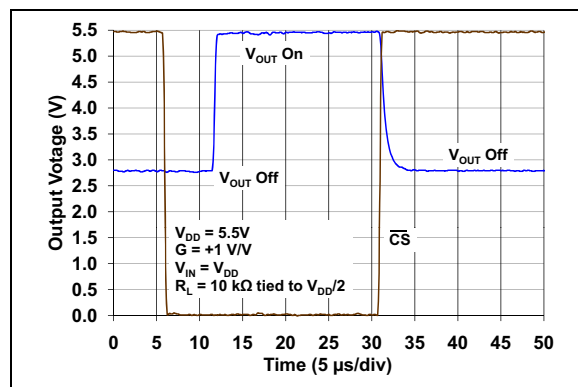
**FIGURE 2-52:** Power Supply Current vs. Chip Select Voltage with  $V_{DD} = 2.3\text{V}$ .



**FIGURE 2-55:** Chip Select Voltage, Output Voltage vs. Time with  $V_{DD} = 2.3\text{V}$ .

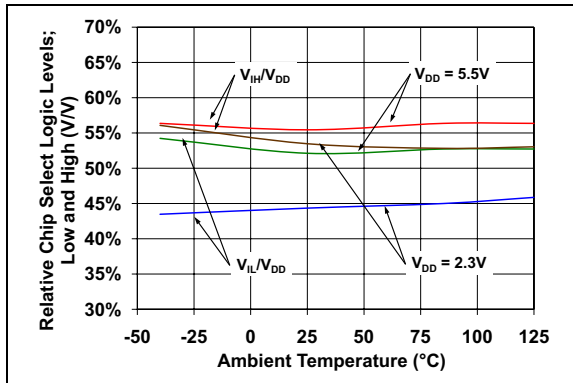


**FIGURE 2-53:** Power Supply Current vs. Chip Select Voltage with  $V_{DD} = 5.5\text{V}$ .

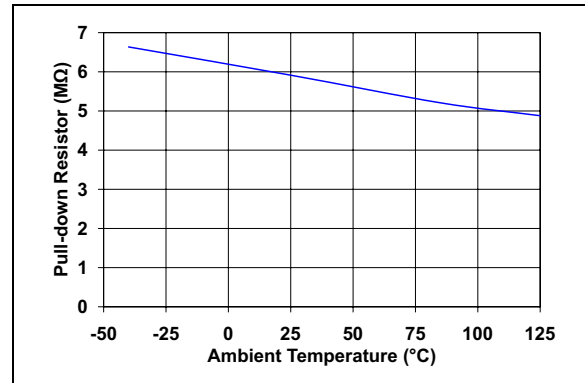


**FIGURE 2-56:** Chip Select Voltage, Output Voltage vs. Time with  $V_{DD} = 5.5\text{V}$ .

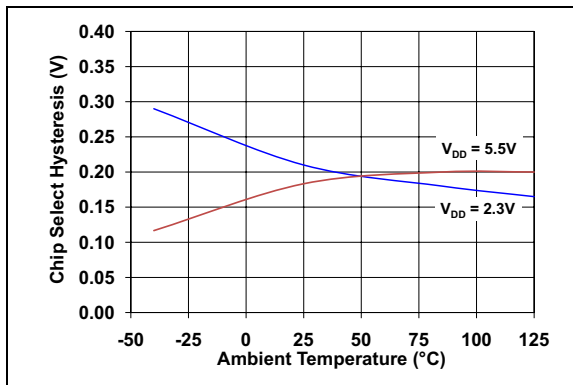
**Note:** Unless otherwise indicated,  $T_A = +25^\circ\text{C}$ ,  $V_{DD} = +2.3\text{V}$  to  $5.5\text{V}$ ,  $V_{SS} = \text{GND}$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 10\text{ k}\Omega$  to  $V_L$ ,  $C_L = 60\text{ pF}$ , and  $\overline{\text{CS}} = \text{GND}$ .



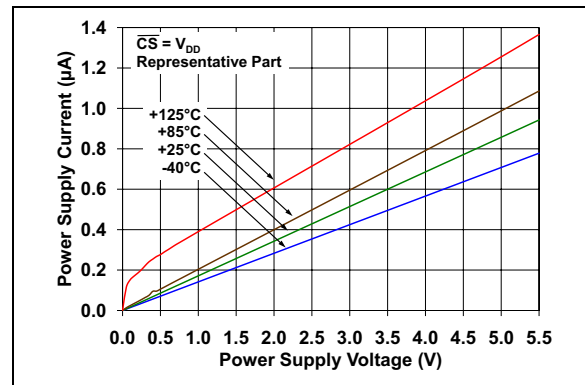
**FIGURE 2-57:** Chip Select Relative Logic Thresholds vs. Ambient Temperature.



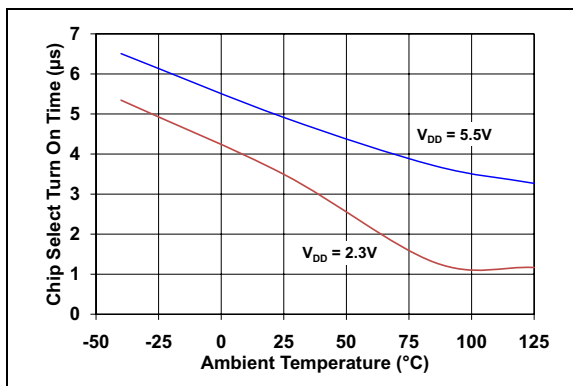
**FIGURE 2-60:** Chip Select's Pull-down Resistor ( $R_{PD}$ ) vs. Ambient Temperature.



**FIGURE 2-58:** Chip Select Hysteresis.



**FIGURE 2-61:** Quiescent Current in Shutdown vs. Power Supply Voltage.



**FIGURE 2-59:** Chip Select Turn On Time vs. Ambient Temperature.

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## 3.0 PIN DESCRIPTIONS

Descriptions of the pins are listed in [Table 3-1](#).

**TABLE 3-1: PIN FUNCTION TABLE**

MCP6V26		MCP6V27		MCP6V28		Symbol	Description
TDFN	MSOP, SOIC	DFN	MSOP, SOIC	TDFN	MSOP, SOIC		
6	6	1	1	6	6	$V_{OUT}, V_{OUTA}$	Output (op amp A)
2	2	2	2	2	2	$V_{IN-}, V_{INA-}$	Inverting Input (op amp A)
3	3	3	3	3	3	$V_{IN+}, V_{INA+}$	Non-inverting Input (op amp A)
4	4	4	4	4	4	$V_{SS}$	Negative Power Supply
—	—	5	5	—	—	$V_{INB+}$	Non-inverting Input (op amp B)
—	—	6	6	—	—	$V_{INB-}$	Inverting Input (op amp B)
—	—	7	7	—	—	$V_{OUTB}$	Output (op amp B)
7	7	8	8	7	7	$V_{DD}$	Positive Power Supply
—	—	—	—	8	8	$\overline{CS}$	Chip Select (op amp A)
1, 5, 8	1, 5, 8	—	—	1, 5	1, 5	NC	No Internal Connection
9	—	9	—	9	—	EP	Exposed Thermal Pad (EP); must be connected to $V_{SS}$

### 3.1 Analog Outputs

The analog output pins ( $V_{OUT}$ ) are low-impedance voltage sources.

### 3.2 Analog Inputs

The non-inverting and inverting inputs ( $V_{IN+}$ ,  $V_{IN-}$ , ...) are high-impedance CMOS inputs with low bias currents.

### 3.3 Power Supply Pins

The positive power supply ( $V_{DD}$ ) is 2.3V to 5.5V higher than the negative power supply ( $V_{SS}$ ). For normal operation, the other pins are between  $V_{SS}$  and  $V_{DD}$ .

Typically, these parts are used in a single (positive) supply configuration. In this case,  $V_{SS}$  is connected to ground and  $V_{DD}$  is connected to the supply.  $V_{DD}$  will need bypass capacitors.

### 3.4 Chip Select ( $\overline{CS}$ ) Digital Input

This pin ( $\overline{CS}$ ) is a CMOS, Schmitt-triggered input that places the MCP6V28 op amp into a low power mode of operation.

### 3.5 Exposed Thermal Pad (EP)

There is an internal connection between the Exposed Thermal Pad (EP) and the  $V_{SS}$  pin; they must be connected to the same potential on the Printed Circuit Board (PCB).

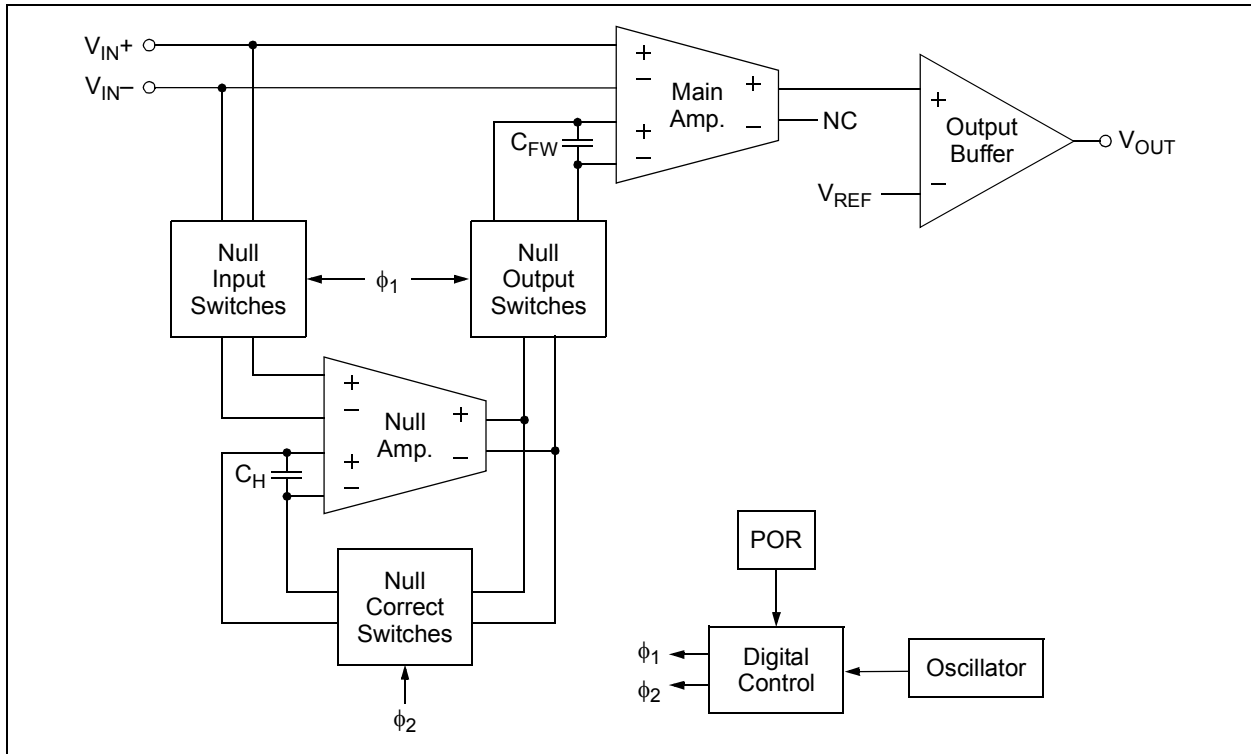
This pad can be connected to a PCB ground plane to provide a larger heat sink. This improves the package thermal resistance ( $\theta_{JA}$ ).

## 4.0 APPLICATIONS

The MCP6V26/7/8 family of auto-zeroed op amps are manufactured using Microchip's state-of-the-art CMOS process. This family is designed for low cost, low power and high precision applications. Its low supply voltage, low quiescent current and wide bandwidth make the MCP6V26/7/8 devices ideal for battery-powered applications.

## 4.1 Overview of Auto-Zeroing Operation

Figure 4-1 shows a simplified diagram of the MCP6V26/7/8 auto-zeroed op amps. This will be used to explain how the DC voltage errors are reduced in this architecture.



**FIGURE 4-1:** Simplified Auto-Zeroed Op Amp Functional Diagram.

### 4.1.1 BUILDING BLOCKS

The Null Amplifier and Main Amplifier are designed for high gain and accuracy using a differential topology. They have a main input pair (+ and - pins at their top left) used for the signal. They have an auxiliary input pair (+ and - pins at their bottom left) used for correcting the offset voltages. Both input pairs are added together internally. The capacitors at the auxiliary inputs ( $C_{FW}$  and  $C_H$ ) hold the corrected values during normal operation.

The Output Buffer is designed to drive external loads at the  $V_{OUT}$  pin. It also produces a single-ended output voltage ( $V_{REF}$  is an internal reference voltage).

All of these switches are make-before-break in order to minimize glitch-induced errors. They are driven by two clock phases ( $\phi_1$  and  $\phi_2$ ) that select between normal mode and auto-zeroing mode.

The clock is derived from an internal R-C oscillator running at a rate of  $f_{OSC1} = 850$  kHz. The oscillator's output is divided down to the desired rate.

The internal POR ensures the part starts up in a known good state. It also provides protection against power supply brown-out events.

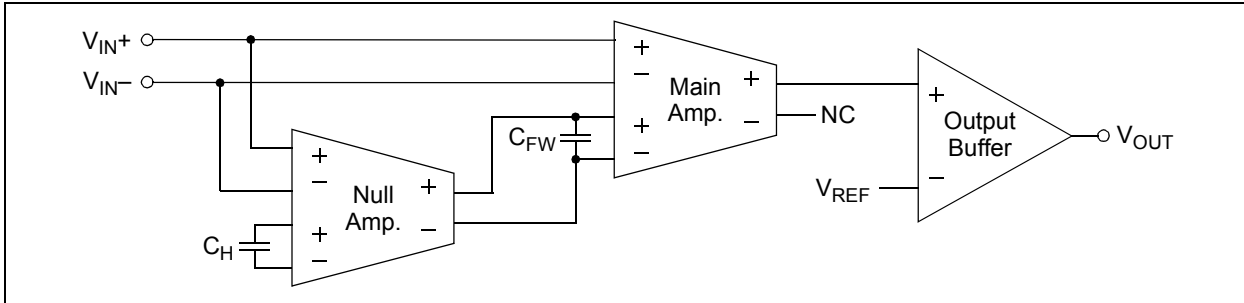
The Digital Control circuitry takes care of all of the housekeeping details of the switching operation. It also takes care of POR events.

# MCP6V26/7/8

## 4.1.2 AUTO-ZEROING ACTION

Figure 4-2 shows the connections between amplifiers during the Normal Mode of operation ( $\phi_1$ ). The hold capacitor ( $C_H$ ) corrects the Null Amplifier's input offset. Since the Null Amplifier has very high gain, it dominates the signal seen by the Main Amplifier. This greatly reduces the impact of the Main Amplifier's input

offset voltage on overall performance. Essentially, the Null Amplifier and Main Amplifier behave as a regular op amp with very high gain ( $A_{OL}$ ) and very low offset voltage ( $V_{OS}$ ).

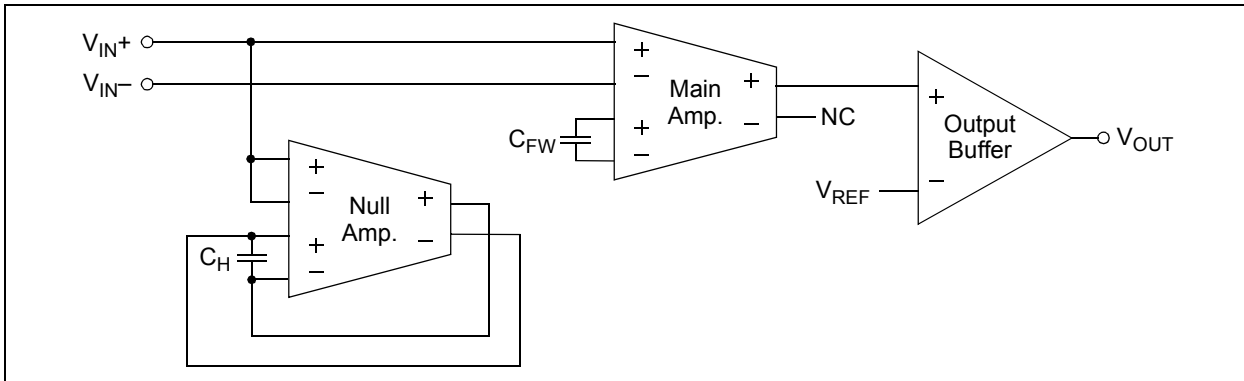


**FIGURE 4-2:** Normal Mode of Operation ( $\phi_1$ ); Equivalent Amplifier Diagram.

Figure 4-3 shows the connections between amplifiers during the Auto-zeroing Mode of operation ( $\phi_2$ ). The signal goes directly through the Main Amplifier, and the flywheel capacitor ( $C_{FW}$ ) maintains a constant correction on the Main Amplifier's offset.

Since these corrections happen every 40  $\mu$ s, or so, we also minimize slow errors, including offset drift with temperature ( $\Delta V_{OS}/\Delta T_A$ ), 1/f noise, and input offset aging.

The Null Amplifier uses its own high open loop gain to drive the voltage across  $C_H$  to the point where its input offset voltage is almost zero. Because the signal input pair is connected to  $V_{IN+}$ , the auto-zeroing action corrects the offset at the current common mode input voltage ( $V_{CM}$ ) and supply voltage ( $V_{DD}$ ). This makes the DC CMRR and PSRR very high also.



**FIGURE 4-3:** Auto-zeroing Mode of Operation ( $\phi_2$ ); Equivalent Diagram.

## 4.1.3 INTERMODULATION DISTORTION (IMD)

The MCP6V26/7/8 op amps will show intermodulation distortion (IMD), products when an AC signal is present.

The signal and clock can be decomposed into sine wave tones (Fourier series components). These tones interact with the auto-zeroing circuitry's non-linear response to produce IMD tones at sum and difference

frequencies. Each of the square wave clock's harmonics has a series of IMD tones centered on it. See Figure 2-37 and Figure 2-38.

## 4.2 Other Functional Blocks

### 4.2.1 RAIL-TO-RAIL INPUTS

The input stage of the MCP6V26/7/8 op amps use two differential CMOS input stages in parallel. One operates at low common mode input voltage ( $V_{CM}$ , which is approximately equal to  $V_{IN+}$  and  $V_{IN-}$  in normal operation) and the other at high  $V_{CM}$ . With this topology, the input operates with  $V_{CM}$  up to  $V_{DD} + 0.2V$ , and down to  $V_{SS} - 0.15V$ , at  $+25^{\circ}C$  (see Figure 2-18). The input offset voltage ( $V_{OS}$ ) is measured at  $V_{CM} = V_{SS} - 0.15V$  and  $V_{DD} + 0.2V$  to ensure proper operation.

The transition between the input stages occurs when  $V_{CM} \approx V_{DD} - 1.2V$  (see Figure 2-7 and Figure 2-8). For the best distortion and gain linearity, with non-inverting gains, avoid this region of operation.

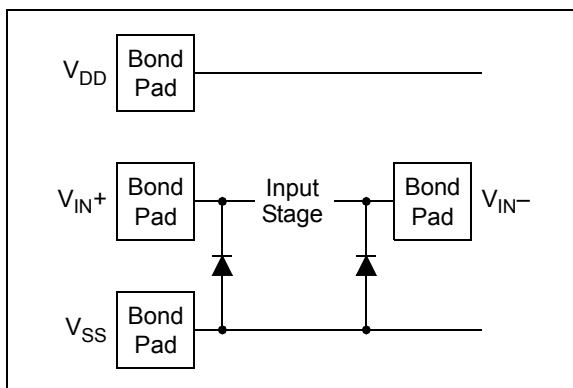
#### 4.2.1.1 Phase Reversal

The input devices are designed to not exhibit phase inversion when the input pins exceed the supply voltages. Figure 2-43 shows an input voltage exceeding both supplies with no phase inversion.

#### 4.2.1.2 Input Voltage Limits

In order to prevent damage and/or improper operation of these amplifiers, the circuit must limit the voltages at the input pins (see Section 1.1, Absolute Maximum Ratings †). This requirement is independent of the current limits discussed later on.

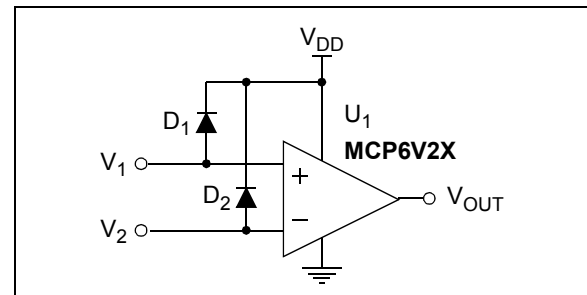
The ESD protection on the inputs can be depicted as shown in Figure 4-4. This structure was chosen to protect the input transistors against many (but not all) over-voltage conditions, and to minimize input bias current ( $I_B$ ).



**FIGURE 4-4:** Simplified Analog Input ESD Structures.

The input ESD diodes clamp the inputs when they try to go more than one diode drop below  $V_{SS}$ . They also clamp any voltages that are well above  $V_{DD}$ ; their breakdown voltage is high enough to allow normal operation, but not low enough to protect against slow over-voltage (beyond  $V_{DD}$ ) events. Very fast ESD events (that meet the spec) are limited so that damage does not occur.

In some applications, it may be necessary to prevent excessive voltages from reaching the op amp inputs; Figure 4-5 shows one approach to protecting these inputs.  $D_1$  and  $D_2$  may be small signal silicon diodes, Schottky diodes for lower clamping voltages or diode-connected FETs for low leakage.

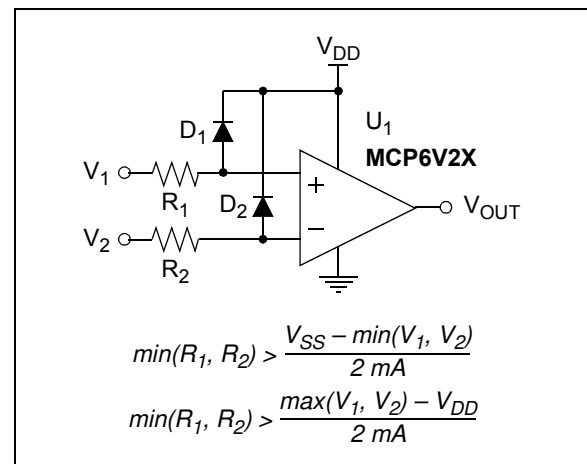


**FIGURE 4-5:** Protecting the Analog Inputs Against High Voltages.

#### 4.2.1.3 Input Current Limits

In order to prevent damage and/or improper operation of these amplifiers, the circuit must limit the currents into the input pins (see Section 1.1, Absolute Maximum Ratings †). This requirement is independent of the voltage limits previously discussed.

Figure 4-6 shows one approach to protecting these inputs. The resistors  $R_1$  and  $R_2$  limit the possible current in or out of the input pins (and into  $D_1$  and  $D_2$ ). The diode currents will dump onto  $V_{DD}$ .



**FIGURE 4-6:** Protecting the Analog Inputs Against High Currents.



# MCP6V26/7/8

It is also possible to connect the diodes to the left of resistors  $R_1$  and  $R_2$ . In this case, the currents through diodes  $D_1$  and  $D_2$  need to be limited by some other mechanism. The resistors then serve as in-rush current limiters; the DC current into the input pins ( $V_{IN+}$  and  $V_{IN-}$ ) should be very small.

A significant amount of current can flow out of the inputs (through the ESD diodes) when the common mode voltage ( $V_{CM}$ ) is below ground ( $V_{SS}$ ); see [Figure 2-17](#).

## 4.2.2 RAIL-TO-RAIL OUTPUT

The output voltage range of the MCP6V26/7/8 zero-drift op amps is  $V_{DD} - 15\text{ mV}$  (minimum) and  $V_{SS} + 15\text{ mV}$  (maximum) when  $R_L = 10\text{ k}\Omega$  is connected to  $V_{DD}/2$  and  $V_{DD} = 5.5\text{ V}$ . Refer to [Figure 2-19](#) and [Figure 2-20](#).

This op amp is designed to drive light loads; use another amplifier to buffer the output from heavy loads.

## 4.2.3 CHIP SELECT ( $\overline{CS}$ )

The single MCP6V28 has a Chip Select ( $\overline{CS}$ ) pin. When  $\overline{CS}$  is pulled high, the supply current for the corresponding op amp drops to about  $1\text{ }\mu\text{A}$  (typical), and is pulled through the  $\overline{CS}$  pin to  $V_{SS}$ . When this happens, the amplifier is put into a high impedance state. By pulling  $\overline{CS}$  low, the amplifier is enabled. If the  $\overline{CS}$  pin is left floating, the internal pull-down resistor (about  $5\text{ M}\Omega$ ) will keep the part on. [Figure 1-4](#) shows the output voltage and supply current response to a  $\overline{CS}$  pulse.

## 4.3 Application Tips

### 4.3.1 INPUT OFFSET VOLTAGE OVER TEMPERATURE

[Table 1-1](#) gives both the linear and quadratic temperature coefficients ( $TC_1$  and  $TC_2$ ) of input offset voltage. The input offset voltage, at any temperature in the specified range, can be calculated as follows:

#### EQUATION 4-1:

$$V_{OS}(T_A) = V_{OS} + TC_1\Delta T + TC_2\Delta T^2$$

Where:

$\Delta T$	=	$T_A - 25^\circ\text{C}$
$V_{OS}(T_A)$	=	input offset voltage at $T_A$
$V_{OS}$	=	input offset voltage at $+25^\circ\text{C}$
$TC_1$	=	linear temperature coefficient
$TC_2$	=	quadratic temperature coefficient

### 4.3.2 DC GAIN PLOTS

[Figure 2-9](#), [Figure 2-10](#) and [Figure 2-11](#) are histograms of the reciprocals (in units of  $\mu\text{V/V}$ ) of CMRR, PSRR and  $A_{OL}$ , respectively. They represent the change in input offset voltage ( $V_{OS}$ ) with a change in common mode input voltage ( $V_{CM}$ ), power supply voltage ( $V_{DD}$ ) and output voltage ( $V_{OUT}$ ).

The  $1/A_{OL}$  histogram is centered near  $0\text{ }\mu\text{V/V}$  because the measurements are dominated by the op amp's input noise. The negative values shown represent noise, *not* unstable behavior. We validate the op amps' stability by making multiple measurements of  $V_{OS}$ ; an unstable part would fail, because it would show either greater variability in  $V_{OS}$ , or the output stuck at one of the rails.

### 4.3.3 OFFSET AT POWER UP

When these parts power up, the input offset ( $V_{OS}$ ) starts at its uncorrected value (usually less than  $\pm 5\text{ mV}$ ). Circuits with high DC gain can cause the output to reach one of the two rails. In this case, the time to a valid output is delayed by an output overdrive time (like  $t_{ODR}$ ), in addition to the startup time (like  $t_{STR}$ ).

It can be simple to avoid this extra startup time. Reducing the gain is one method. Adding a capacitor across the feedback resistor ( $R_F$ ) is another method.

### 4.3.4 SOURCE RESISTANCES

The input bias currents have two significant components; switching glitches that dominate at room temperature and below, and input ESD diode leakage currents that dominate at  $+85^\circ\text{C}$  and above.

Make the resistances seen by the inputs small and equal. This minimizes the output offset caused by the input bias currents.

The inputs should see a resistance on the order of  $10\Omega$  to  $1\text{ k}\Omega$  at high frequencies (i.e., above  $1\text{ MHz}$ ). This helps minimize the impact of switching glitches, which are very fast, on overall performance. In some cases, it may be necessary to add resistors in series with the inputs to achieve this improvement in performance.

Small input resistances are needed for high gains. Without them, parasitic capacitances can cause positive feedback and instability.

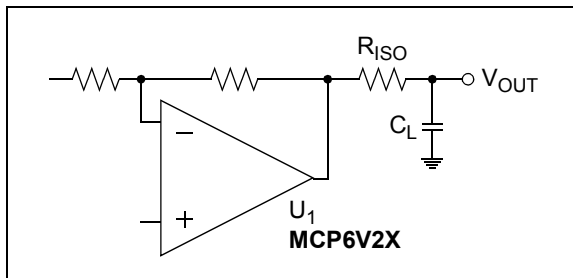
### 4.3.5 SOURCE CAPACITANCE

The capacitances seen by the two inputs should be small and matched. The internal switches connected to the inputs dump charges on these capacitors; an offset can be created if the capacitances do not match. Large input capacitances and source resistances, together with high gain, can lead to positive feedback and instability.

## 4.3.6 CAPACITIVE LOADS

Driving large capacitive loads can cause stability problems for voltage feedback op amps. As the load capacitance increases, the feedback loop's phase margin decreases and the closed-loop bandwidth is reduced. This produces gain peaking in the frequency response, with overshoot and ringing in the step response. These auto-zeroed op amps have a different output impedance than most op amps, due to their unique topology.

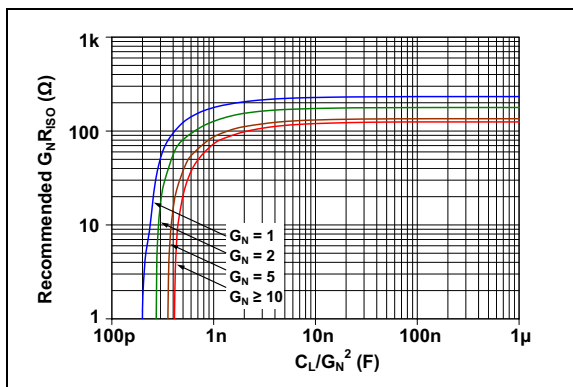
When driving a capacitive load with these op amps, a series resistor at the output ( $R_{ISO}$  in Figure 4-7) improves the feedback loop's phase margin (stability) by making the output load resistive at higher frequencies. The bandwidth will be generally lower than the bandwidth with no capacitive load.



**FIGURE 4-7:** Output Resistor,  $R_{ISO}$ , Stabilizes Capacitive Loads.

Figure 4-8 gives recommended  $R_{ISO}$  values for different capacitive loads and gains. The x-axis is the normalized load capacitance ( $C_L/G_N^2$ ). The y-axis is the normalized resistance ( $G_N R_{ISO}$ ).

$G_N$  is the circuit's noise gain. For non-inverting gains,  $G_N$  and the Signal Gain are equal. For inverting gains,  $G_N$  is  $1+|\text{Signal Gain}|$  (e.g.,  $-1$  V/V gives  $G_N = +2$  V/V).



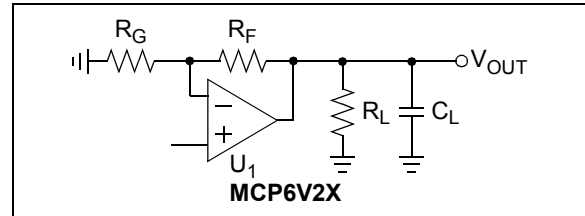
**FIGURE 4-8:** Recommended  $R_{ISO}$  values for Capacitive Loads.

After selecting  $R_{ISO}$  for your circuit, double check the resulting frequency response peaking and step response overshoot. Modify  $R_{ISO}$ 's value until the response is reasonable. Bench evaluation and simulations with the MCP6V26/7/8 SPICE macro model are helpful.

## 4.3.7 STABILIZING OUTPUT LOADS

This family of auto-zeroed op amps has an output impedance (Figure 2-31 and Figure 2-32) that has a double zero when the gain is low. This can cause a large phase shift in feedback networks that have low resistance near the part's bandwidth. This large phase shift can cause stability problems.

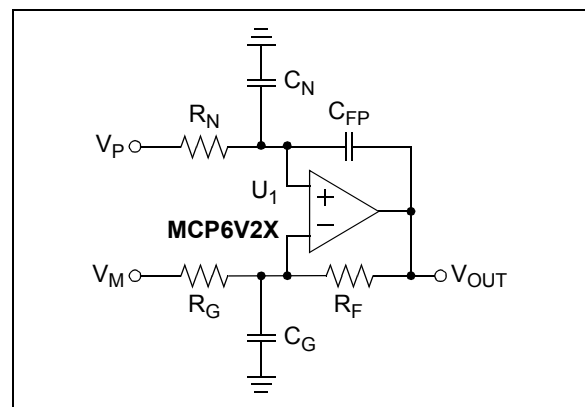
Figure 4-9 shows that the load on the output is  $(R_L + R_{ISO}) || (R_F + R_G)$ , where  $R_{ISO}$  is before the load (like Figure 4-7). This load needs to be large enough to maintain stability; it should be at least  $(2 \text{ k}\Omega)/G_N$ .



**FIGURE 4-9:** Output Load.

## 4.3.8 GAIN PEAKING

Figure 4-10 shows an op amp circuit that represents non-inverting amplifiers ( $V_M$  is a DC voltage and  $V_P$  is the input) or inverting amplifiers ( $V_P$  is a DC voltage and  $V_M$  is the input). The capacitances  $C_N$  and  $C_G$  represent the total capacitance at the input pins; they include the op amp's common mode input capacitance ( $C_{CM}$ ), board parasitic capacitance and any capacitor placed in parallel. The capacitance  $C_{FP}$  represents the parasitic capacitance coupling the output and non-inverting input pins.



**FIGURE 4-10:** Amplifier with Parasitic Capacitance.

$C_G$  acts in parallel with  $R_G$  (except for a gain of  $+1$  V/V), which causes an increase in gain at high frequencies.  $C_G$  also reduces the phase margin of the feedback loop, which becomes less stable. This effect can be reduced by either reducing  $C_G$  or  $R_F || R_G$ .

$C_N$  and  $R_N$  form a low-pass filter that affects the signal at  $V_P$ . This filter has a single real pole at  $1/(2\pi R_N C_N)$ .