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MPM3830
6V Input, 3A Module
Synchronous Step-Down Converter
with Integrated Inductor

DESCRIPTION

The MPM3830 is a step-down module converter with built-in power MOSFETs and inductor. The DC-DC module comes in a small surface-mount QFN-20(3mm x 5mm x 1.6mm) package and achieves 3A continuous output current from a 2.7V to 6V input voltage with excellent load and line regulation. The MPM3830 is ideal for powering portable equipment that runs from a single cell Lithium-Ion (Li+) Battery. The output voltage is regulated as low as 0.6V. Only FB resistors and input and output capacitors are needed to complete the design.

The Constant-on-time control (COT) scheme provides fast transient response, high light-load efficiency and easy loop stabilization.

Fault condition protection includes cycle-by-cycle current limit and thermal shutdown (TSD).

The MPM3830 requires a minimum number of readily available standard external components and is available in an ultra-small QFN20 (3mmx5mm) package.

FEATURES

- Wide 2.7V to 6V Operating Input Range
- Adjustable Output from 0.6V
- 3.0mm x 5.0mm x 1.6mm QFN Package
- Total Solution Size 8.5mm x 4.5 mm
- Low Radiated Emissions (EMI) Complies with EN55022 Class B Standard
- Up to 3A Continuous Output Current
- 100% Duty Cycle in Dropout
- Ultra Low IQ: 40µA
- EN and Power Good for Power Sequencing
- Cycle-by-Cycle Over-Current Protection
- Short-Circuit Protection with Hiccup Mode
- Adjustable Output Only Needs 4 External Components : 2 Ceramic Capacitors and FB Divider Resistors
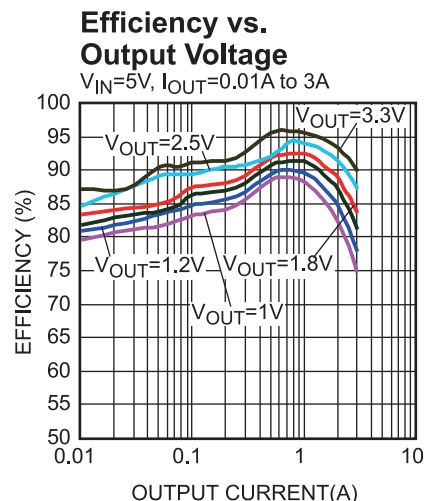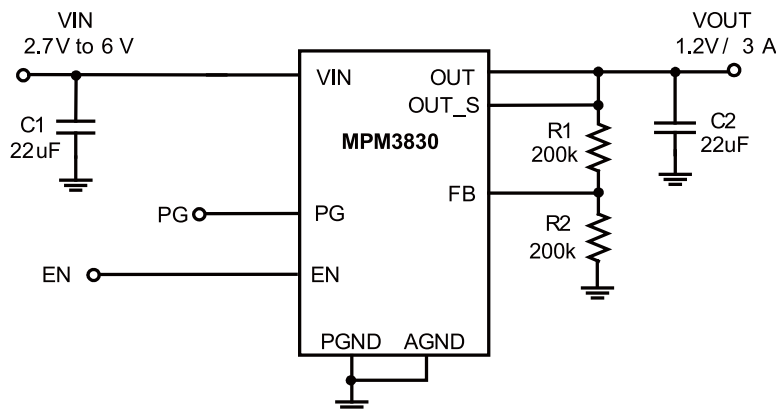
APPLICATIONS

- Low Voltage I/O System Power
- LDO Replacement
- Power for Portable Products
- Storage (SSD/HDD)
- Space-Limited Applications

TYPICAL APPLICATION

Efficiency vs. Output Voltage
V_{IN}=5V, I_{OUT}=0.01A to 3A

ORDERING INFORMATION

Part Number*	Package	Top Marking
MPM3830GQV	QFN-20 (3mmx5mm)	3830 M

* For Tape & Reel, add suffix –Z (e.g. MPM3830GQV–Z);

PACKAGE REFERENCE

TOP VIEW

AGND AGND PGND NC IN IN

| 18 | 17 | 16 | 15 | 14 | 13 |

EN — 1   12 — IN

OUT_S — 2   11 — PG

FB — 3   19   20   10 — NC
          NC   NC

SW — 4   9 — OUT

SW — 5   8 — OUT

SW — 6   7 — OUT

All "NC" pins must be left floating

QFN20 (3mmx5mm)
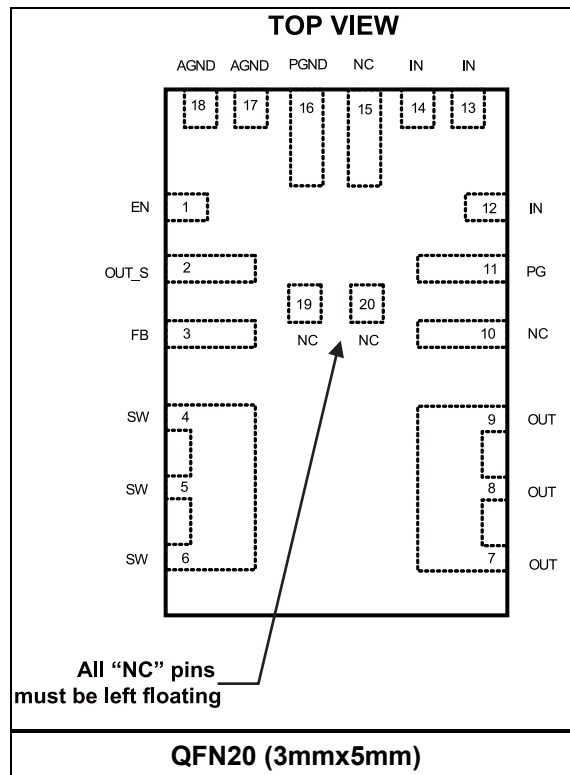
ABSOLUTE MAXIMUM RATINGS [1]

Supply Voltage V_{IN} 6.5V
V_{SW} ....
   -0.3V (-6V for <10ns) to 6.5V (10V for <10ns)
All Other Pins .... -0.3V to 6.5V
Junction Temperature .... 150°C
Lead Temperature .... 260°C
Continuous Power Dissipation (T_A = +25°C) [2]
…………….. .... 2.8W
Storage Temperature............... -65°C to +150°C

Recommended Operating Conditions [3]

Supply Voltage V_{IN} .... 2.7V to 6V
Operating Junction Temp. (T_J). -40°C to +125°C

Thermal Resistance [4] θ_{JA} θ_{JC}

QFN-20 (3mmx5mm)…………..46……10 °C/W

Notes:
1) Exceeding these ratings may damage the device.
2) The maximum allowable power dissipation is a function of the maximum junction temperature T_J (MAX), the junction-to-ambient thermal resistance θ_{JA}, and the ambient temperature T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D (MAX) = (T_J (MAX)-T_A)/θ_{JA}. Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
3) The device is not guaranteed to function outside of its operating conditions.
4) Measured on JESD51-7, 4-layer PCB.

ELECTRICAL CHARACTERISTICS

V_{IN} = 3.6V, T_J = -40°C to +125°C, Typical value is tested at T_J = +25°C. The limit over temperature is guaranteed by characterization, unless otherwise noted.

Parameter	Symbol	Condition	Min	Typ	Max	Units
Feedback Voltage	V_{FB}	2.7V ≤ V_{IN} ≤ 6V	591	600	609	mV
Feedback Current	I_{FB}	V_{FB} = 0.6V		10		nA
PFET Switch-On Resistance	R_{DSON_P}			50		mΩ
NFET Switch-On Resistance	R_{DSON_N}			40		mΩ
Inductor L Value	L	Inductance value at 1MHz		1		µH
Inductor DC Resistance	R_{DCR}			50		mΩ
Dropout Resistance	R_{DR}	100% on duty		100		mΩ
Switch Leakage		V_{EN} = 0V, V_{IN} = 6V V_{SW} = 0V and 6V, T_J=25°C		0	2	µA
PFET Peak Current Limit			3.6	4.5	6	A
NFET Valley Current Limit				4		A
NFET Switch Sinking Current	I_{NSW}	V_{OUT}=1.2V, V_{FB}=0.7V		100		µA
On Time	T_{ON}	V_{IN}=5V, V_{OUT}=1.2V		200		ns
		V_{IN}=3.6V, V_{OUT}=1.2V		280		
Switching Frequency	F_s	V_{OUT}=1.2V	960	1200	1440	kHz
Minimum Off Time	$T_{MIN-OFF}$			30		ns
Minimum On Time[5]	T_{MIN-On}			50		ns
Soft-Start Time	T_{SS-ON}			1.5		ms
Soft-Stop Time	T_{SS-OFF}			1		ms
Power Good Upper Trip Threshold		FB Voltage in Respect to the Regulation		+10		%
Power Good Lower Trip Threshold				-10		%
Power Good Delay				90		µs
Power Good Sink Current Capability	V_{PG_LO}	Sink 1mA			0.4	V
Power Good Logic High Voltage	V_{PG_HI}	V_{IN}=5V, V_{FB}=0.6V	4.9			V
Power Good Internal Pull Up Resistor	R_{PG}			500		kΩ
Under Voltage Lockout Threshold Rising			2.35	2.5	2.65	V
Under Voltage Lockout Threshold Hysteresis				400		mV
EN Input Logic Low Voltage					0.35	V
EN Input Logic High Voltage			1.2			V
EN Input Current		V_{EN}=2V		2		µA
		V_{EN}=0V		0		µA

ELECTRICAL CHARACTERISTICS *(continued)*

V_{IN} = 3.6V, T_J = -40°C to +125°C, Typical value is tested at T_J = +25°C. The limit over temperature is guaranteed by characterization, unless otherwise noted.

| Parameter	Symbol	Condition	Min	Typ	Max	Units
Supply Current (Shutdown)		V_{EN}=0V, T_J=25°C		0	1	µA
Supply Current (Quiescent)		V_{EN}=2V, V_{FB}=0.63V, V_{IN}=3.6V		40		µA
Thermal Shutdown[5]				160		°C
Thermal Hysteresis[5]				30		°C

Notes:
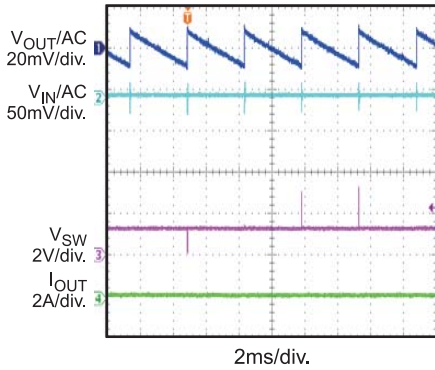5) Guaranteed by design.

TYPICAL PERFORMANCE CHARACTERISTICS

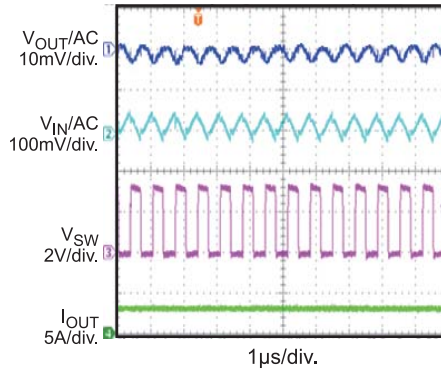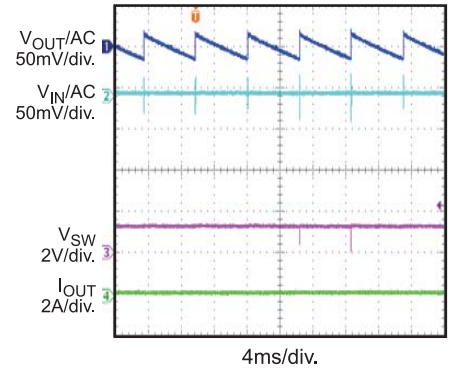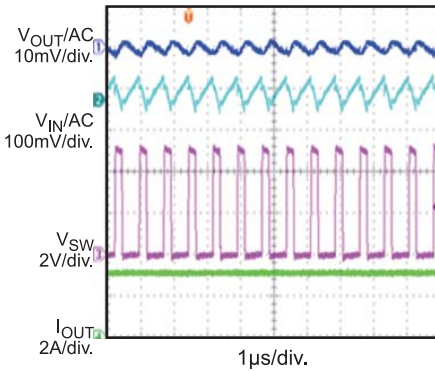V_{IN} = 5V, V_{OUT} = 1.2V, C_{OUT}=22µF, T_A = +25ºC, unless otherwise noted.
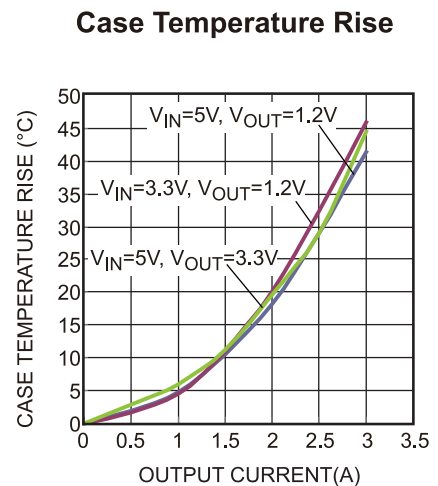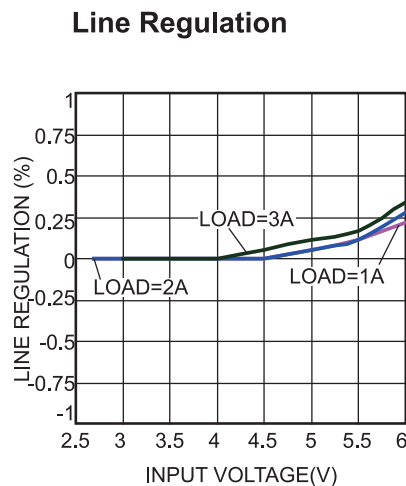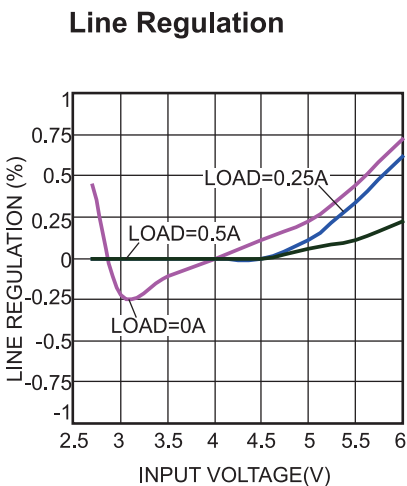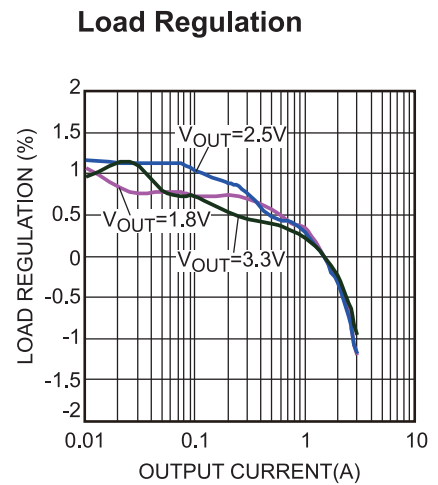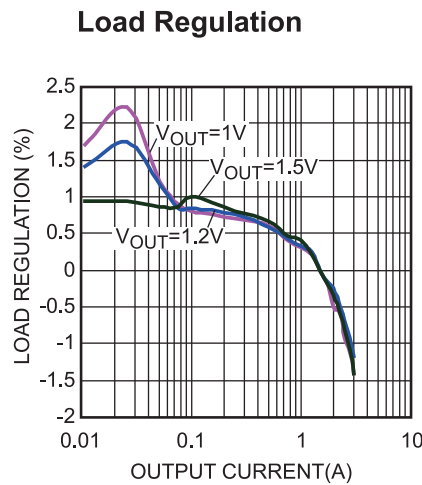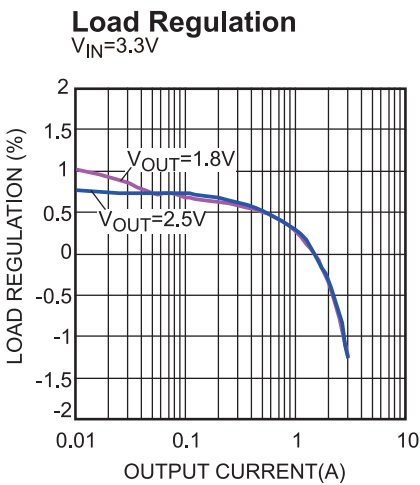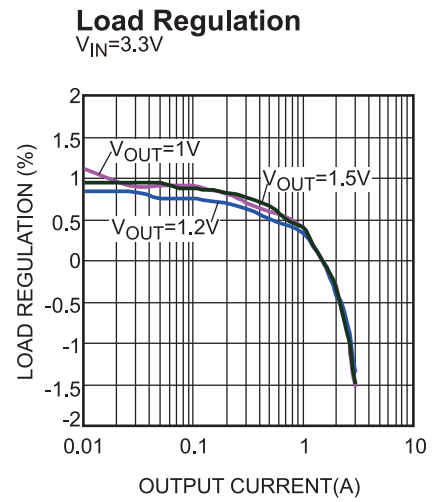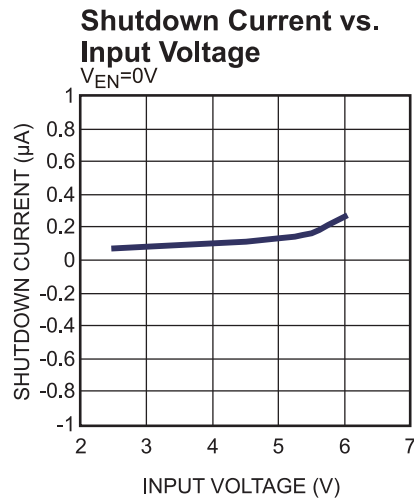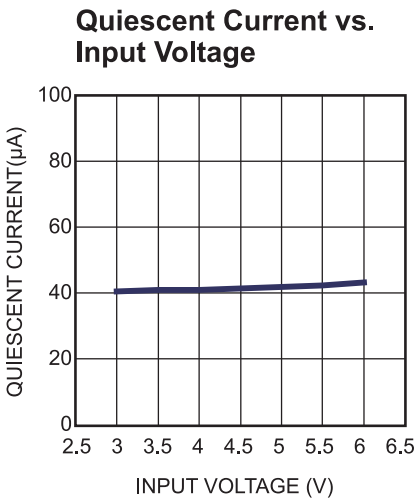
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

V_{IN} = 5V, V_{OUT} = 1.2V, C_{OUT}=22µF, T_A = +25ºC, unless otherwise noted.

Efficiency vs. Output Voltage
V_{IN}=3.3V
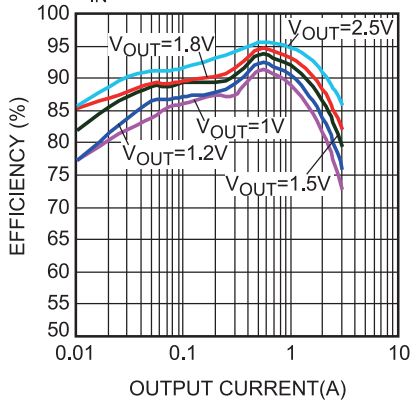
Efficiency vs. Output Voltage
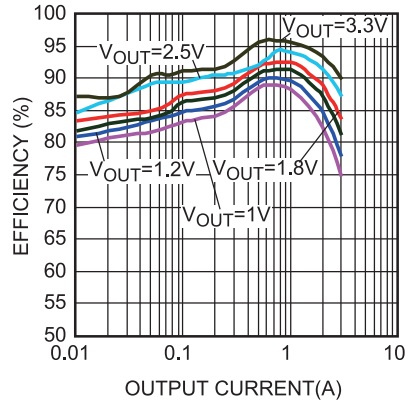
EN Rising vs. Temperature
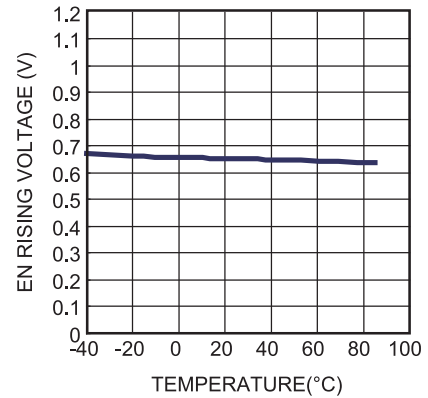
Reference Voltage vs. Temperature
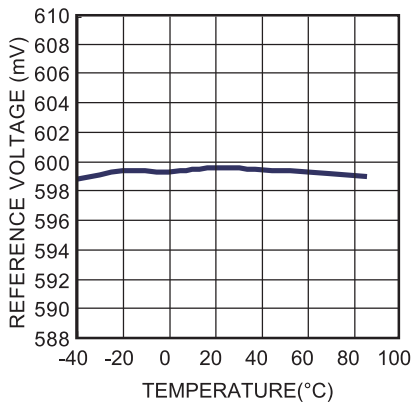
Quiescent Current vs. Temperature
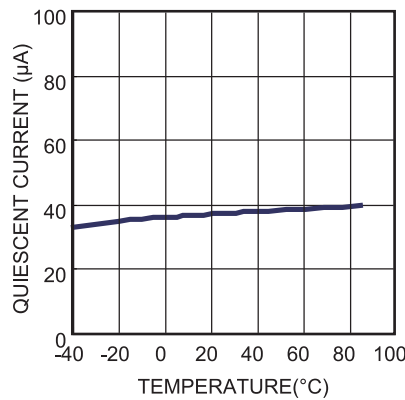
EN Falling vs. Temperature
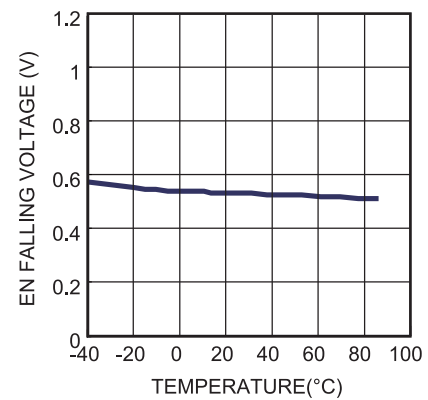
Radiated Emission
I_{OUT}=3A, C_{OUT}=22µFx2
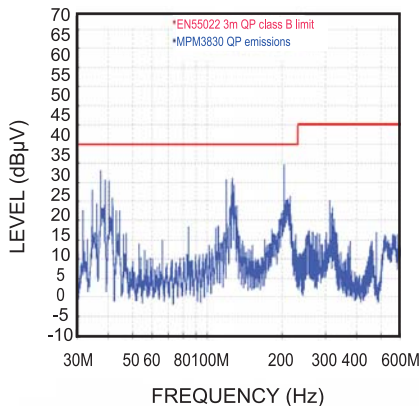
Output Current Derating vs. Output Voltage
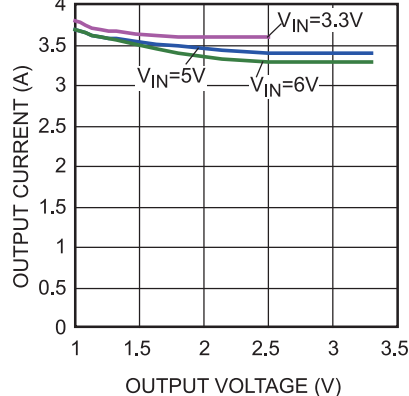
TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*
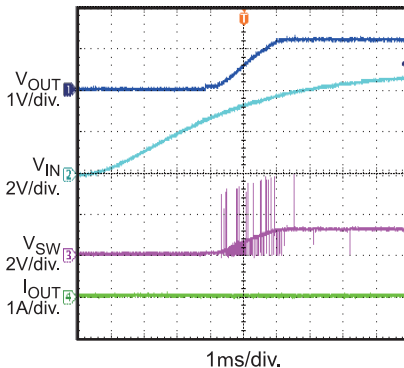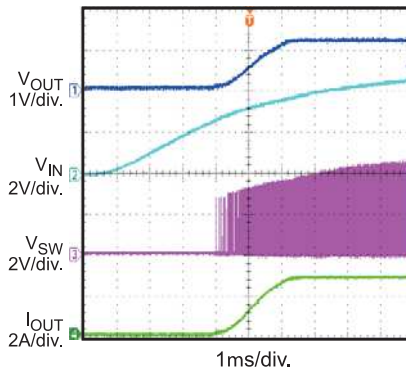
V_{IN} = 5V, V_{OUT} = 1.2V, C_{OUT}=22μF, T_A = +25ºC, unless otherwise noted.

Output Ripple
V_{IN} = 3.3V, V_{OUT} = 1.2V, I_{OUT}=0A

Output Ripple
V_{IN} = 3.3V, V_{OUT} = 1.2V, I_{OUT}=3A

Output Ripple
V_{IN} = 5V, V_{OUT} = 1.2V, I_{OUT}=0A

Output Ripple
V_{IN} = 5V, V_{OUT} = 1.2V, I_{OUT}=3A

Output Ripple
V_{IN} = 5V, V_{OUT} = 3.3V, I_{OUT}=0A
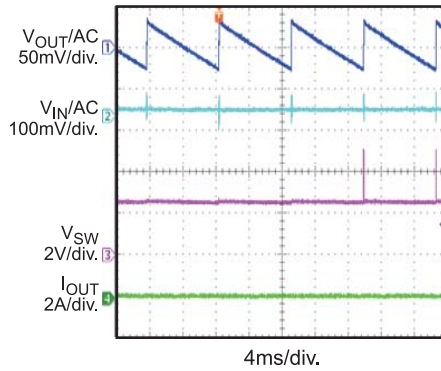
Output Ripple
V_{IN} = 5V, V_{OUT} = 3.3V, I_{OUT}=3A
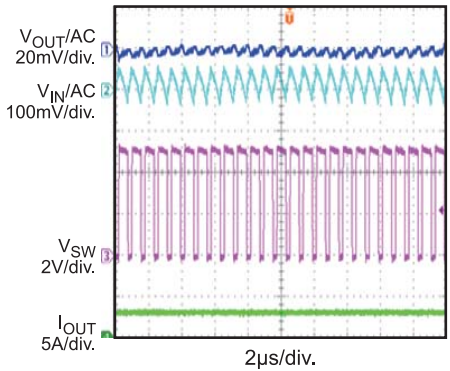
**V_{IN} Power Up
without Load**

**V_{IN} Power Up
with 3A Load**

**V_{IN} Shutdown
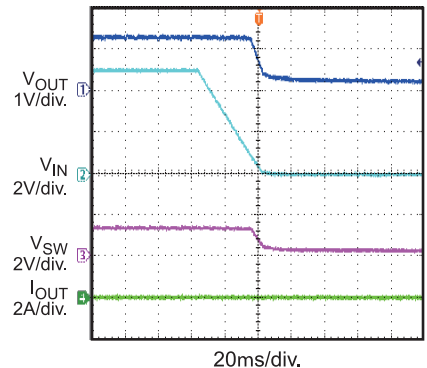without Load**

TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

V_{IN} = 5V, V_{OUT} = 1.2V, C_{OUT}=22µF, T_A = +25ºC, unless otherwise noted.

**V_{IN} Shutdown
with 3A Load**
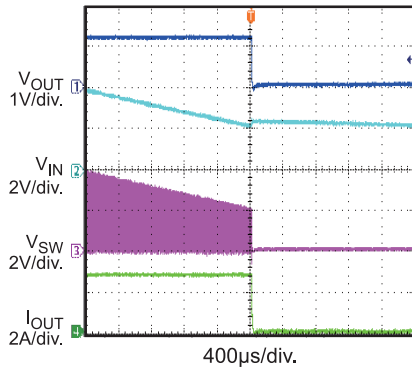
**EN Startup
without Load**
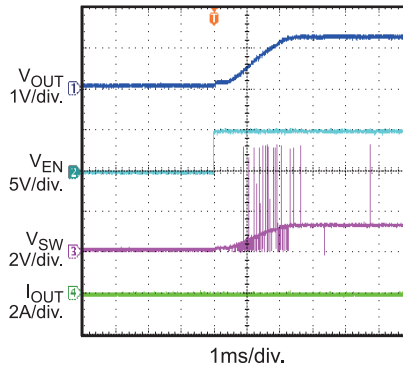
**EN Shutdown
without Load**
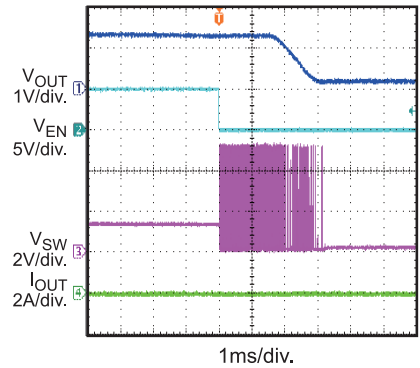
**EN Startup
with 3A Load**
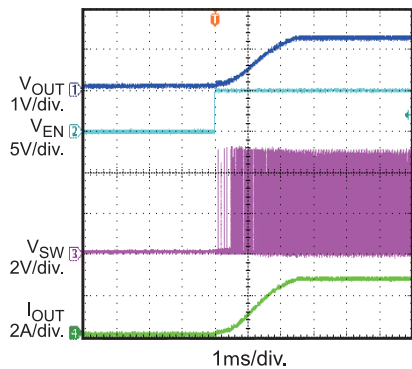
**EN Shutdown
with 3A Load**
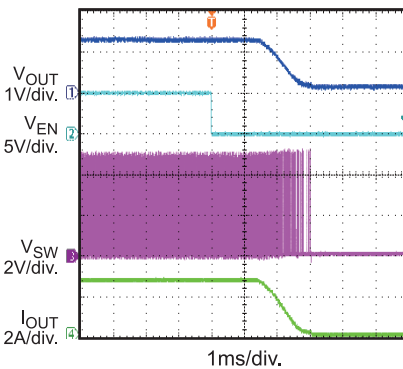
**Power Good
Through EN Startup**

**Power Good
Through EN Shutdown**

Transient Response
V_{IN} = 3.3V, V_{OUT} = 1V,
I_{OUT}=1.5A-3A, 0.25A/µs

Transient Response
V_{IN} = 5V, V_{OUT} = 1V,
I_{OUT}=1.5A-3A, 0.25A/µs

TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

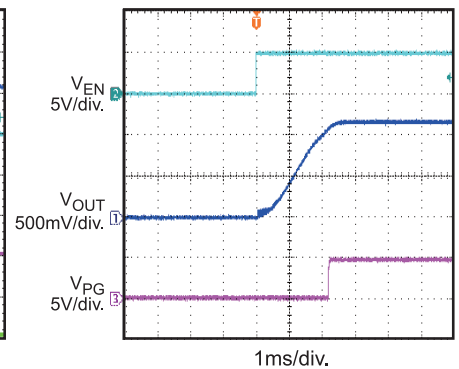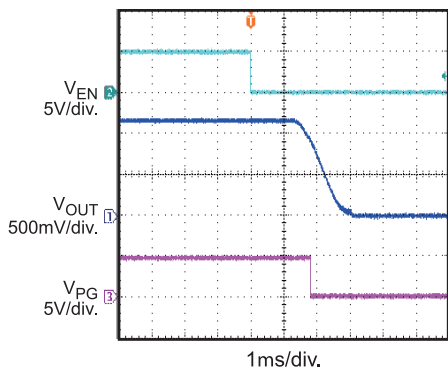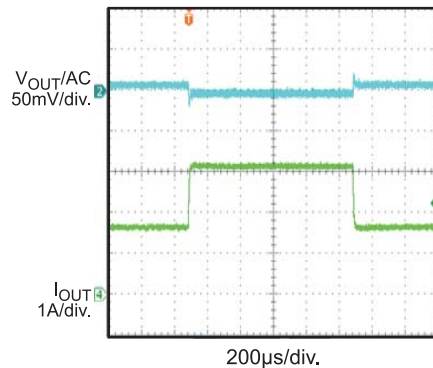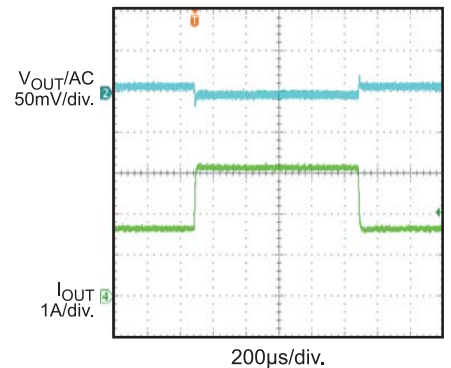V_{IN} = 5V, V_{OUT} = 1.2V, C_{OUT}=22µF, T_A = +25ºC, unless otherwise noted.

Transient Response
V_{IN} = 3.3V, V_{OUT} = 1.8V,
I_{OUT}=1.5A-3A, 0.25A/µs

V_{OUT}/AC
50mV/div.

I_{OUT}
1A/div.

200µs/div.
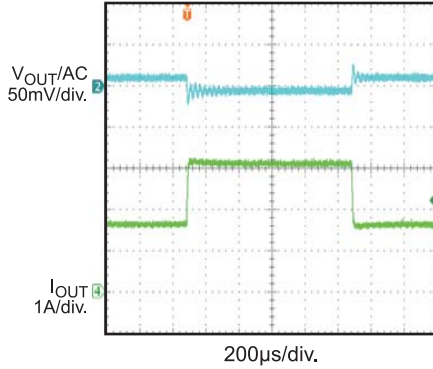
Transient Response
V_{IN} = 5V, V_{OUT} = 1.8V,
I_{OUT}=1.5A-3A, 0.25A/µs

V_{OUT}/AC
50mV/div.

I_{OUT}
1A/div.

200µs/div.
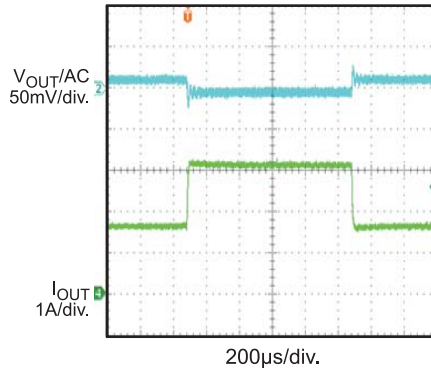
Transient Response
V_{IN} = 5V, V_{OUT} = 2.5V,
I_{OUT}=1.5A-3A, 0.25A/µs

V_{OUT}/AC
50mV/div.

I_{OUT}
1A/div.

200µs/div.
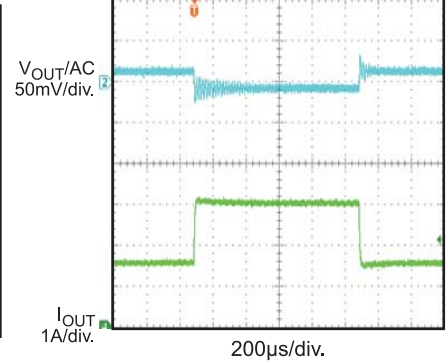
Transient Response
V_{IN} = 5V, V_{OUT} = 3.3V,
I_{OUT}=1.5A-3A, 0.25A/µs

V_{OUT}/AC
50mV/div.

I_{OUT}
1A/div.

200µs/div.

Short-Circuit Entry

V_{OUT}
1V/div.

V_{IN}
5V/div.

V_{SW}
2V/div.

I_{OUT}
5A/div.

2ms/div.

Short Circuit

V_{OUT}
1V/div.

V_{IN}
5V/div.

V_{SW}
2V/div.

I_{OUT}
5A/div.

2ms/div.

Short-Circuit Recovery

V_{OUT}
1V/div.

V_{IN}
5V/div.

V_{SW}
2V/div.

I_{OUT}
5A/div.

2ms/div.
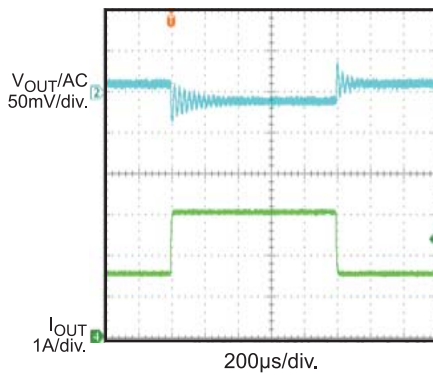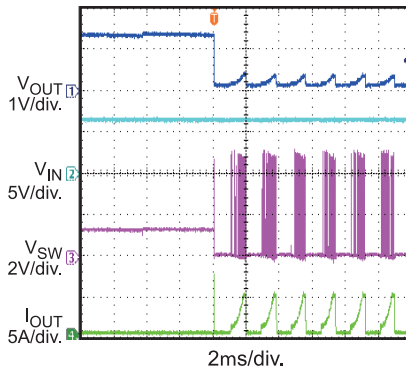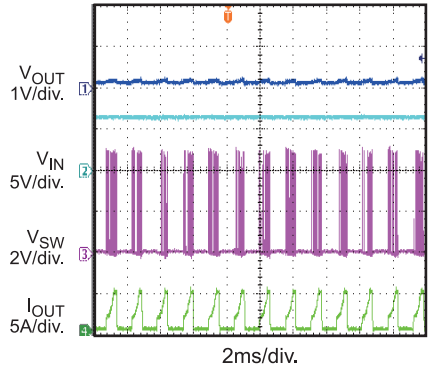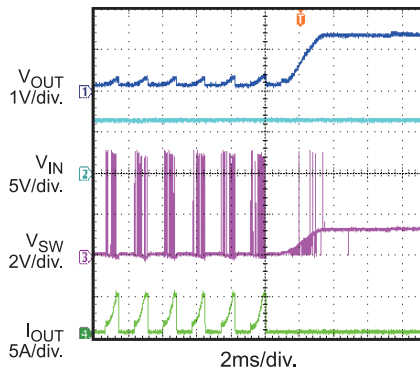
PIN FUNCTIONS

Pin #	Name	Description
1	EN	On/Off Control.
2	OUT_S	Output Voltage Sense.
3	FB	Feedback. An external resistor divider from the output to GND (tapped to the FB), sets the output voltage.
4, 5, 6	SW	Switch Output.
7, 8, 9	OUT	Power Output.
11	PG	Power Good Indicator. The output of PG is an open drain with an internal pull up resistor to IN. PG is pulled up to IN when the FB voltage is within 10% of the regulation level, otherwise PG is low.
12, 13, 14	IN	Supply Voltage to Internal Control Circuitry.
16	PGND	Power Ground.
17, 18	AGND	Analogy Ground for Internal Control Circuit.
10, 15, 19, 20	NC	DO NOT CONNECT. Pin must be left floating.

FUNCTIONAL BLOCK DIAGRAM

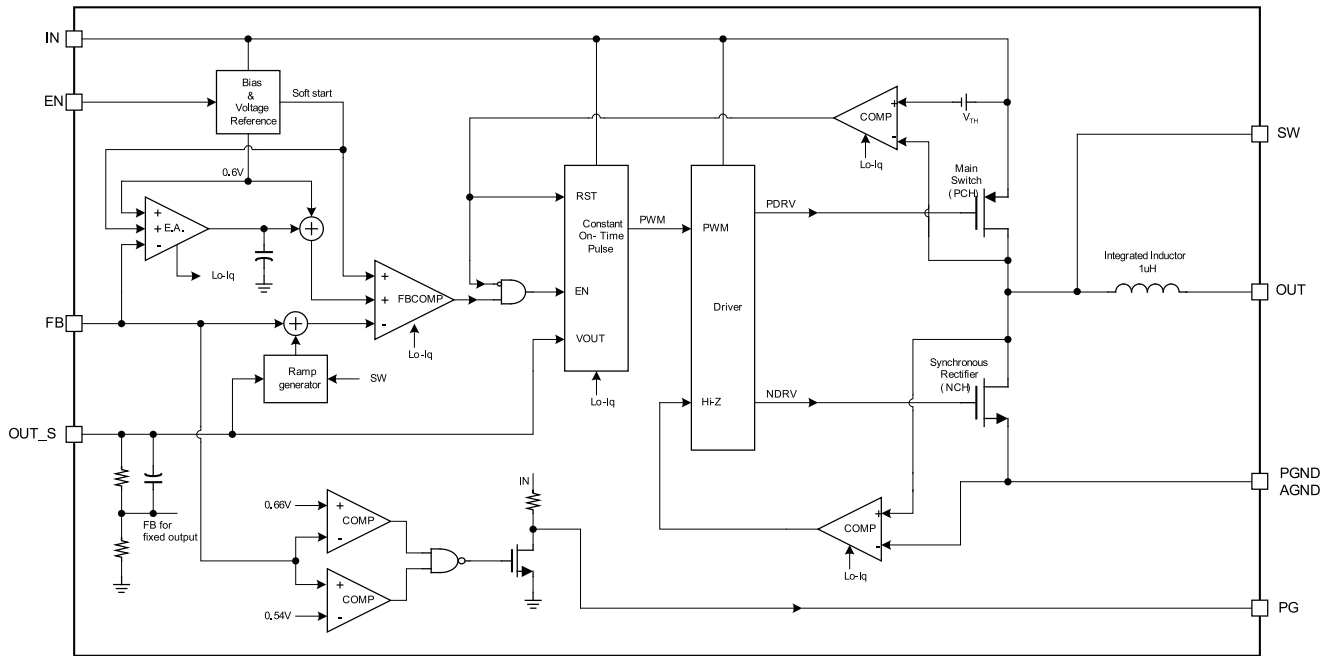Figure 1— Functional Block Diagram

OPERATION

The DC-DC module has a small surface-mount QFN-20(3mm x 5mm x 1.6mm) package. The module's integrated inductor simplifies the schematic and layout design. Only FB resistors and input and output capacitors are needed to complete the design. MPM3830 uses constant on-time control (COT) with input voltage feed forward to stabilize the switching frequency over a full-input range. At light load, MPM3830 employs a proprietary control of the low-side switch and inductor current on switching node and improve efficiency.

Constant On-Time Control (COT)

Compared to a fixed-frequency PWM control, constant on-time control (COT) offers the advantage of a simpler control loop and faster transient response. Using input voltage feed forward, the MPM3830 maintains a nearly constant switching frequency across the input and output voltage range. The on-time of the switching pulse is estimated as follows:

$$T_{ON} = \frac{V_{OUT}}{V_{IN}} \times 0.833\mu s$$

To prevent inductor current run away during load transition, MPM3830 fixes the minimum off time to 30ns. However, this minimum off-time limit does not affect operation in a steady state.

Light Load Operation

In a light-load condition, MPM3830 uses a proprietary control scheme to save power and improve efficiency. There is a zero current cross detect circuit (ZCD) to judge if the inductor current starts to reverse. When the inductor current touch ZCD threshold, the low side switch will start to be turned off.

The DCM mode happens only after low side switch turned off by ZCD circuit. Considering the ZCD circuit propagation time, the typical delay is 20ns. This means the inductor current continues to fall after the ZCD is triggered. If the inductor current falling slew rate is fast (Vo voltage is high or close to Vin), the low-side MOSFET turns off (this means the inductor current may be negative). This does not allow the MPM3830 to enter DCM.

If DCM is required, the off-time of the low-side MOSFET in continuous conduction mode (CCM) should be longer than 40ns. It means the maximum duty is 95% to guarantee DCM mode at light load.

For example, if Vin is 3.4V and Vo is 3.3V, the off-time in CCM is 25ns. It is difficult to enter DCM at light load.

Enable (EN)

If the input voltage is greater than the under-voltage lockout threshold (UVLO), typically 2.5V, MPM3830 is enabled by pulling EN above 1.2V. Leaving EN to float or be pulled down to ground disables MPM3830. There is an internal 1MΩ resistor from EN to ground.

Soft Start/Stop

MPM3830 has a built-in soft-start that ramps up the output voltage in a controlled slew rate. This avoids overshoot at startup. The soft-start time is about 1.5ms typically.

At disable, MPM3830 ramps down the internal reference thus allow the load to linearly discharge the output. During soft stop time, the low side internal MOSFET will switch to control the slew rate of output voltage which follows the internal reference. Under light load and large output capacitor condition, the large energy stored in output capacitor will be transferred to input capacitor through the inductor. The topology is changed into a boost converter after V_{OUT} and V_{IN} role exchange. The boost voltage causes an overshoot on input capacitor; sometimes this overshoot is higher than the V_{ABS} (the ABSOLUTE maximum value) of input pin and can damage the IC. To prevent this situation, the input capacitor needs to be large enough to absorb this energy.

The energy stored in the output capacitor will be transferred to input capacitor. Consider the conduction loss on inductor, HS/LS MOS and so on, estimate 80% transfer efficiency of boost converter. Therefore the transferred energy can be calculated by below equation:

$$W_{BOOST} = 0.5 \text{ x } C_{OUT} \text{ x } V_{OUT}^2 \text{ x } 0.8$$

Where W_{BOOST} is the transferred energy,

C_{OUT} is the output capacitor,

V_{OUT} is output voltage.

To absorb this energy and protect the IC, we should guarantee the current input voltage plus the overshoot voltage cannot be higher than the V_{ABS} on input pin. The required minimum input capacitor can be calculated below:

$$C_{IN(MIN)}=2 \times W_{BOOST} / (V_{ABS}^2 - V_{IN}^2)$$

Where $C_{IN(MIN)}$ is the minimum input capacitor,

V_{ABS} is the ABSOLUTE maximum value of input pin.

Power Good Indicator (PGOOD)

MPM3830 has an open drain with a 500kΩ pull-up resistor pin for the power good indicator (POODG). When FB is within +/-10% of regulation voltage (i.e. 0.6V), PGOOD is pulled up to IN by the internal resistor. If FB voltage is out of the +/-10% window, PGOOD is pulled down to ground by an internal MOS FET. The MOS FET has a maximum R_{dson} of less than 100Ω.

Current Limit

MPM3830 has a typical 4.5A current limit for the high-side switch. When the high-side switch reaches the current limit, MPM3830 hits the hiccup threshold until the current decreases. This prevents the inductor current from continuing to build which results in damage to the components.

Short Circuit and Recovery

MPM3830 enters short-circuit protection (SCP) mode when the current limit reached, then it tries to recover from the short circuit with hiccup mode. In SCP, MPM3830 disables the output power stage, discharges the soft-start cap and then automatically tries to soft-start again. If the short circuit remains after the soft-start ends, MPM3830 repeats the cycle until the short circuit disappears, and the output rises back to the regulation level.

APPLICATION INFORMATION

COMPONENT SELECTION

Setting the Output Voltage

The external resistor divider is used to set the output voltage (see Typical Application on page 1). The feedback resistor R1 cannot be too large or too small considering the trade-off for stability and dynamics. Choose R1 between 50kΩ to 200kΩ. R2 is given by:

$$R2 = \frac{R1}{\dfrac{V_{out}}{0.6} - 1}$$
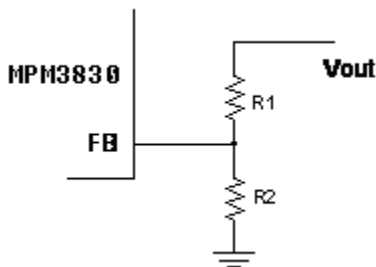
The feedback circuit is shown in Figure 2.

Figure 2— Feedback Network

Table 1 lists the recommended resistor values for common output voltages.

Table 1—Resistor Values for Common Output Voltages

V_{OUT} (V)	R1 (kΩ)	R2 (kΩ)
1.0	200(1%)	300(1%)
1.2	200(1%)	200(1%)
1.8	200(1%)	100(1%)
2.5	200(1%)	63.2(1%)
3.3	200(1%)	44.2(1%)

Load Regulation Improvement

The load regulation of MPM3830 will be influenced by feedback resistor.

The relationship between Vo and feedback network can be estimated as:

$$V_O \approx V_{FB} \times \frac{R_1 + R_2}{R_2} - I_O \times DCR \frac{R_1}{R_C}$$

The integrated inductor DCR is typical 50mΩ. The R_C is internal compensation resistor, it's typical 1MΩ-1.2MΩ.

Base on the equation, to get better load regulation, decreasing the feedback resistor are the effective way. But too small feedback resistor will cause the steady problem.

For most applications, the 200kΩ R1 and 22µF output capacitor is sufficient, but for better load regulation, 100kΩ R1 and 2x22µF output capacitors are suggested.

Table 2 lists the recommended resistors and output capacitors value for better load regulation.

Table 2—Resistor and Capacitor Selection for Better Load Regulation

V_{OUT} (V)	R1 (kΩ)	R2 (kΩ)	Cout(uF)
1.0	100(1%)	150(1%)	44
1.2	100(1%)	100(1%)	44
1.8	150(1%)	75(1%)	44
2.5	200(1%)	63.2(1%)	44
3.3	200(1%)	44.2(1%)	44

Selecting the Input Capacitor

The input current to the step-down converter is discontinuous, therefore a capacitor is required to supply the AC current while maintaining the DC input voltage. For optimal performance, use low ESR capacitors. Ceramic capacitors with X5R or X7R dielectrics are highly recommended due to their low ESR and small temperature coefficients. For most applications, a 22µF capacitor is sufficient

Since the input capacitor absorbs the input switching current it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated by:

$$I_{C1} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}$$

The worst case condition occurs at $V_{IN} = 2V_{OUT}$, where:

$$I_{C1} = \frac{I_{LOAD}}{2}$$

For simplification, choose the input capacitor that has a RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum or ceramic. When using electrolytic or tantalum capacitors, a small, high quality ceramic capacitor (i.e. 0.1µF), should be placed as close to the IC as possible. When using ceramic capacitors, check that they have enough capacitance to provide sufficient charge to prevent an excessive voltage ripple at input. The input-voltage ripple caused by capacitance is estimated by:

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_S \times C1} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Selecting the Output Capacitor

The output capacitor (C2) is required to maintain the DC output voltage.

Low ESR ceramic capacitors can be used with MPM3830 to keep the output-ripple low. Generally, 22µF output ceramic capacitor is enough for most of the cases. In higher output voltage condition, 47µF might be needed for a stable system.

When using ceramic capacitors, the impedance at the switching frequency is dominated by the capacitance. The output-voltage ripple is mainly caused by the capacitance. For simplification, the output-voltage ripple is estimated by:

$$\Delta V_{OUT} = \frac{V_{OUT}}{8 \times f_S^2 \times L_1 \times C2} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

When using tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output ripple can be approximated by:

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_S \times L_1} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times R_{ESR}$$

The L1 is 1µH integrated inductor.

The characteristics of the output capacitor affect the stability of the regulation system.

Layout Recommendation of MPM3830

Proper layout of the switching power supplies is very important, and sometimes critical to make it work properly. Especially, for the high switching converter, if the layout is not carefully done, the regulator could show poor line or load regulation, stability issues.

For MPM3830, the high speed step-down regulator, the input capacitor should be placed as close as possible to the IC pins. As shown in Figure 3, the 0805 size ceramic capacitor is used, please make sure the two ends of the ceramic capacitor be directly connected to PIN12-14 (the Power Input Pin) and PIN 16 (the Power GND Pin).
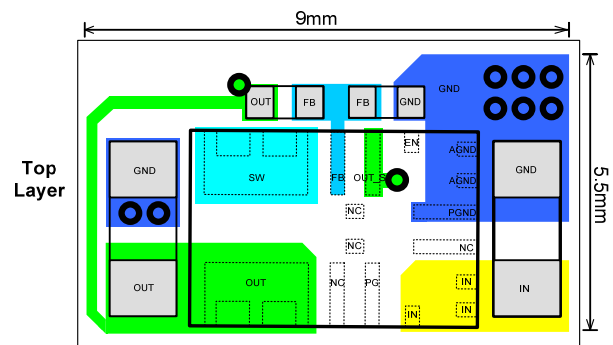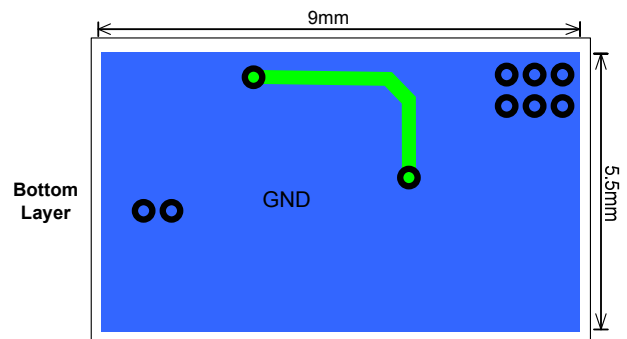

Figure 3— Top Layer
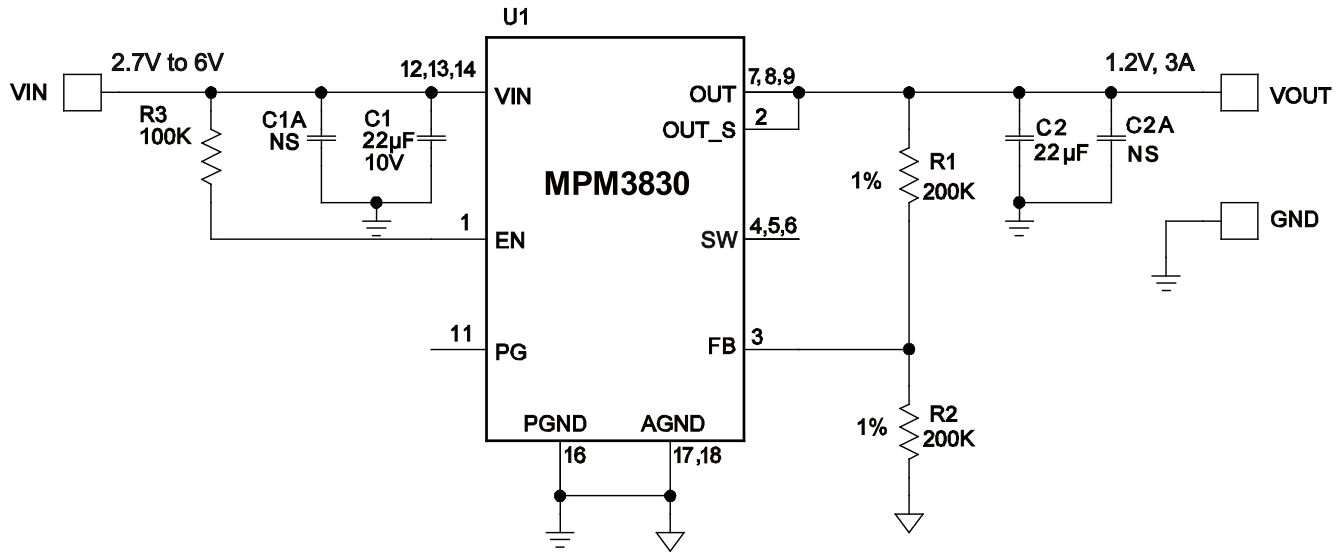

Figure 4— Bottom Layer

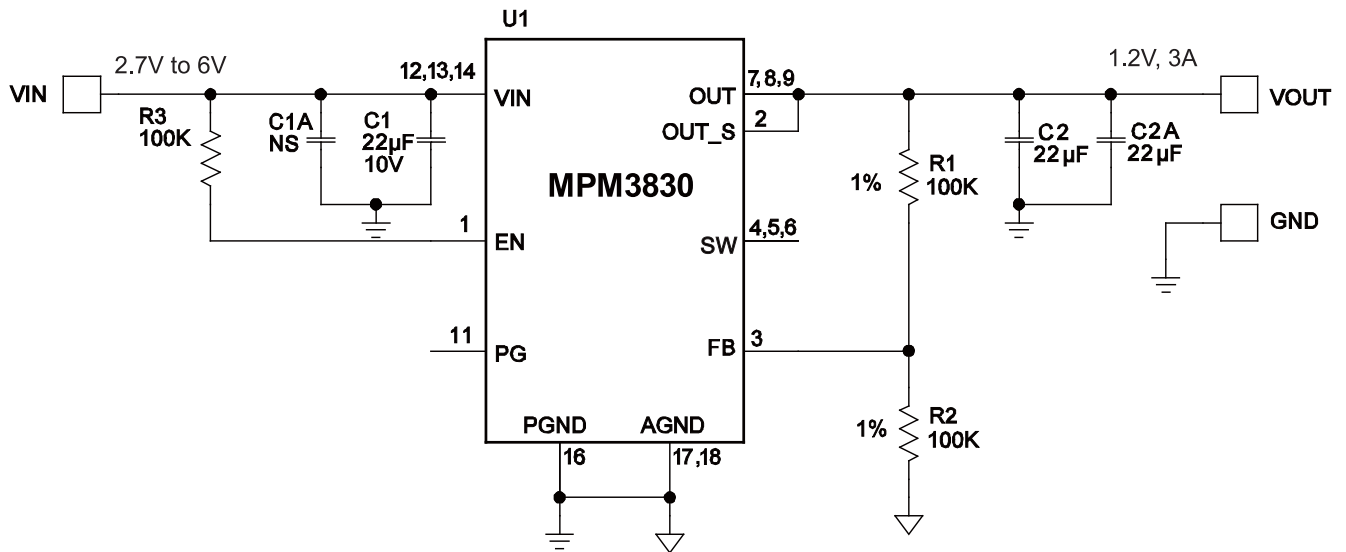## TYPICAL APPLICATION CIRCUITS

Figure 5: Typical Application Circuit

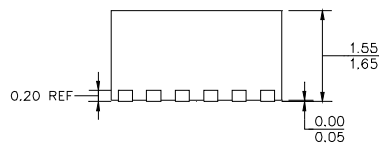**Figure 6: Better Load Regulation Circuit**

PACKAGE INFORMATION

QFN-20 (3mmx5mm)

PIN 1 ID MARKING

PIN 1 ID INDEX AREA

2.90
3.10

4.90
5.10

TOP VIEW

0.20
0.30

0.35
0.45

0.50
BSC

0.45
0.55

PIN 1 ID
0.125 X 45° TYP

0.35
0.45

13   18

NOTE 2

12

1.15
TYP

0.75
0.85

1.55

0.97
0.90

0.20
0.30

0.25
0.18
0.00

0.40

0.20
0.30

1.25

7   6

2.10

0.75
0.85

0.20
REF

BOTTOM VIEW

1.55
1.65

0.20 REF

0.00
0.05

SIDE VIEW

0.80

0.25

0.70
2.80

0.125 X 45°

2.1
1.7
1.55

NOTE 2

1.15

0.97
0.90

0.25

0.25
0.18
0.00

0.40

0.25

1.25

2.10

1.80 1.30 0.70 0.00 0.70 1.30 1.80
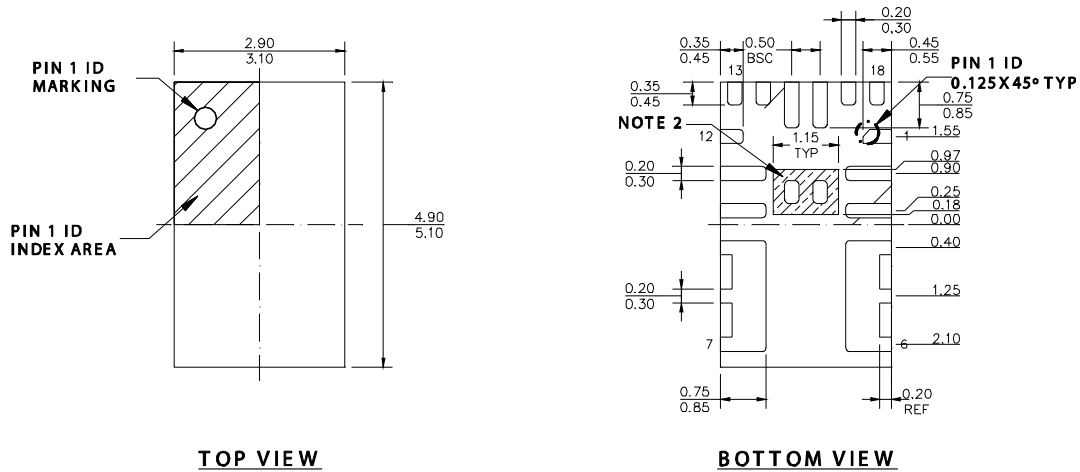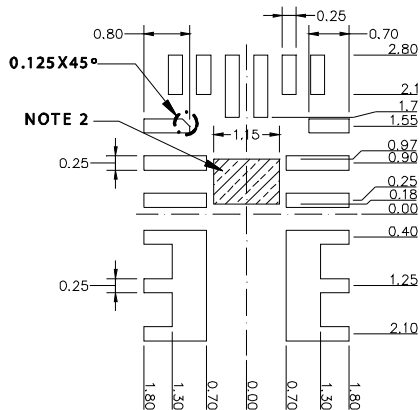
RECOMMENDED LAND PATTERN

NOTE:

1) ALL DIMENSIONS ARE IN MILLIMETERS.
2) SHADED AREA IS THE KEEP-OUT ZONE. THE EXPOSED BOTTOM METAL PADS ENCLOSED BY THIS ZONE IS NOT TO BE CONNECTED TO ANY PCB METAL TRACE & VIA ELECTRICALLY OR MECHANICALLY.
3) EXPOSED PADDLE SIZE DOES NOT INCLUDE MOLD FLASH.
4) LEAD COPLANARITY SHALL BE 0.10 MILLIMETERS MAX.
5) JEDEC REFERENCE IS MO-220.
6) DRAWING IS NOT TO SCALE.