

Chipsmall Limited consists of a professional team with an average of over 10 year of expertise in the distribution of electronic components. Based in Hongkong, we have already established firm and mutual-benefit business relationships with customers from, Europe, America and south Asia, supplying obsolete and hard-to-find components to meet their specific needs.

With the principle of "Quality Parts, Customers Priority, Honest Operation, and Considerate Service", our business mainly focus on the distribution of electronic components. Line cards we deal with include Microchip, ALPS, ROHM, Xilinx, Pulse, ON, Everlight and Freescale. Main products comprise IC, Modules, Potentiometer, IC Socket, Relay, Connector. Our parts cover such applications as commercial, industrial, and automotives areas.

We are looking forward to setting up business relationship with you and hope to provide you with the best service and solution. Let us make a better world for our industry!



Contact us

Tel: +86-755-8981 8866 Fax: +86-755-8427 6832

Email & Skype: info@chipsmall.com Web: www.chipsmall.com

Address: A1208, Overseas Decoration Building, #122 Zhenhua RD., Futian, Shenzhen, China







Power Factor Corrected Quasi-Resonant Primary Side Current-Mode Controller for LED Lighting with Thermal Foldback

The NCL30088 is a power factor corrected flyback controller targeting isolated and non–isolated constant current LED drivers. The controller operates in a quasi–resonant mode to provide optimal efficiency. Thanks to a novel control method, the device is able to tightly regulate a constant LED current from the primary side. This removes the need for secondary side feedback circuitry, biasing and an optocoupler.

The device is highly integrated with a minimum number of external components. A robust suite of safety protection is built in to simplify the design. This device is specifically intended for very compact, space efficient designs.

Features

- Quasi-resonant Peak Current-mode Control Operation
- Constant Current Control with Primary Side Feedback
- Tight LED Constant Current Regulation of ±2% Typical
- Power Factor Correction
- Line Feedforward for Enhanced Regulation Accuracy
- Low Start-up Current (13 µA typ.)
- Wide V_{cc} Range
- 300 mA / 500 mA Totem Pole Driver with 12 V Gate Clamp
- Robust Protection Features
 - OVP on V_{CC}
 - Programmable Over Voltage / LED Open Circuit Protection
 - ♦ Cycle-by-cycle Peak Current Limit
 - Winding Short Circuit Protection
 - Secondary Diode Short Protection
 - Output Short Circuit Protection
 - Shorted Current Sense Protection
 - User Programmable NTC Based Thermal Foldback
 - Thermal Shutdown
 - V_{cc} Undervoltage Lockout
 - ♦ Brown-out Protection
- Pb-Free, Halide-Free Product
- Four Versions: NCL30088A, B, C and D (See Table 1)

Typical Applications

- Integral LED Bulbs and Tubes
- LED Light Engines
- LED Drivers/Power Supplies
- Electronic Control Gear for LED Lighting



ON Semiconductor®

www.onsemi.com



MARKING DIAGRAM



L30088x = Specific Device Code

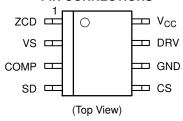
x = A, B, C, D

A = Assembly Location

L = Wafer Lot Y = Year W = Work Week

PIN CONNECTIONS

= Pb-Free Package



ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page 25 of this data sheet.

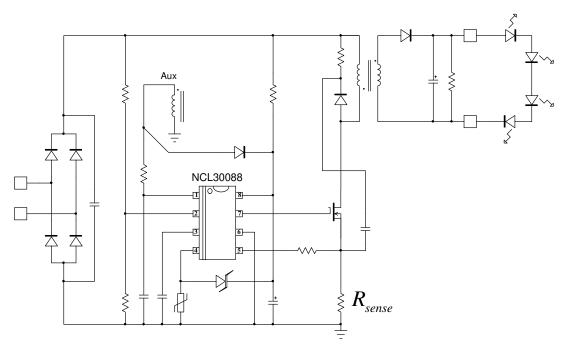


Figure 1. Typical Application Schematic in a Flyback Converter

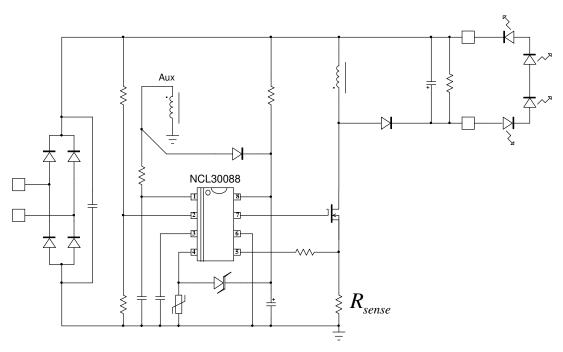


Figure 2. Typical Application Schematic in a Buck-Boost Converter

Table 1. FOUR NCL30088 VERSIONS

| Part Number | Protection Mode | Current Regulation Reference Voltage (V _{REF}) | Recommended for (*): |
|-------------|-----------------|--|--|
| NCL30088A | Latching-off | 250 mV | Isolated converters. Non–isolated converters with $V_{out} \leq \sqrt{2} \cdot (V_{in,rms})_{LL}$ |
| NCL30088B | Auto-recovery | 250 mV | Isolated converters. Non–isolated converters with $V_{out} \leq \sqrt{2} \cdot (V_{in,rms})_{LL}$ |
| NCL30088C | Latching-off | 200 mV | Non–isolated converters with $V_{out} > \sqrt{2} \cdot (V_{in,rms})_{LL}$ |
| NCL30088D | Auto-recovery | 200 mV | Non–isolated converters with $\label{eq:vout} V_{out} > \sqrt{2} \cdot (V_{in,rms})_{LL}$ |

^{*(}V_{in,rms})_{LL} designates the lowest line rms voltage. Refer to AND9200/D for more details. (http://www.onsemi.com/pub_link/Collateral/AND9200–D.PDF).

Table 2. PIN FUNCTION DESCRIPTION

| Pin No. | Pin Name | Function | Pin Description | |
|---------|-----------------|----------------------------------|--|--|
| 1 | ZCD | Zero Crossing Detection | Connected to the auxiliary winding, this pin detects the core reset event. | |
| 2 | VS | Input Voltage Sensing | This pin observes the input voltage rail and protects the LED driver in case of too low mains conditions (brown–out). | |
| | | | This pin also observes the input voltage rail for: - Power Factor Correction - Valley lockout | |
| 3 | COMP | Filtering Capacitor | This pin receives a filtering capacitor for power factor correction. Typical values ranges from 1 – 4.70 μF | |
| 4 | SD | Thermal Foldback and Shutdown | Connecting an NTC to this pin allows the user to program thermal current fold-back threshold and slope. A Zener diode can also be used to pull-up the pin and stop the controller for adjustable OVP protection. | |
| 5 | CS | Current Sense | This pin monitors the primary peak current. | |
| 6 | GND | - | Controller ground pin. | |
| 7 | DRV | Driver Output | The driver's output to an external MOSFET | |
| 8 | V _{CC} | IC Supply Pin | This pin is the positive supply of the IC. The circuit starts to operate when V_{CC} exceeds 18 V and turns off when V_{CC} goes below 8.8 V (typical values). After start–up, the operating range is 9.4 V up to 25.5 V ($V_{CC(OVP)}$ minimum level). | |

Internal Circuit Architecture

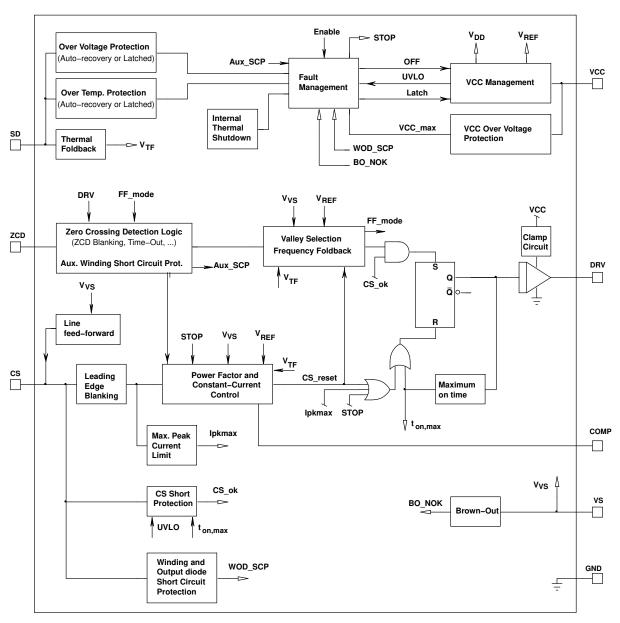


Figure 3. Internal Circuit Architecture

Table 3. MAXIMUM RATINGS TABLE

| Symbol | Rating | Value | Unit |
|--|--|---|---------|
| V _{CC(MAX)} | Maximum Power Supply voltage, V_{CC} pin, continuous voltage Maximum current for V_{CC} pin | -0.3 to 30 Internally limited | V mA |
| V _{DRV(MAX)} I _{DRV(MAX)} | Maximum driver pin voltage, DRV pin, continuous voltage Maximum current for DRV pin | -0.3, V _{DRV} (Note 1) -300, +500 | V mA |
| V _{MAX} I _{MAX} | Maximum voltage on low power pins (except DRV and V_{CC} pins) Current range for low power pins (except DRV and V_{CC} pins) | -0.3, 5.5 (Notes 2 and 5) -2, +5 | V mA |
| $R_{\theta J-A}$ | Thermal Resistance Junction-to-Air | 180 | °C/W |
| T _{J(MAX)} | Maximum Junction Temperature | 150 | °C |
| | Operating Temperature Range | -40 to +125 | °C |
| | Storage Temperature Range | -60 to +150 | °C |
| | ESD Capability, HBM model (Note 3) | | kV |
| | ESD Capability, MM model (Note 3) | | V |
| | ESD Capability, CDM model (Note 3) | 2 | kV |

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

- V_{DRV} is the DRV clamp voltage V_{DRV(high)} when V_{CC} is higher than V_{DRV(high)}. V_{DRV} is V_{CC} otherwise.
 This level is low enough to guarantee not to exceed the internal ESD diode and 5.5–V Zener diode. More positive and negative voltages can be applied if the pin current stays within the -2-mA / 5-mA range.
- 3. This device contains ESD protection and exceeds the following tests: Human Body Model 3500 V per JEDEC Standard JESD22-A114E, Machine Model Method 250 V per JEDEC Standard JESD22-A115B, Charged Device Model 2000 V per JEDEC Standard JESD22-C101E.
- 4. This device contains latch-up protection and has been tested per JEDEC Standard JESD78D, Class I and exceeds ±100 mA
- 5. Recommended maximum V_S voltage for optimal operation is 4 V. -0.3 V to +4.0 V is hence, the V_S pin recommended range.

Table 4. ELECTRICAL CHARACTERISTICS (Unless otherwise noted: For typical values T_J = 25°C, V_{CC} = 12 V, V_{ZCD} = 0 V, $V_{CS} = 0 \text{ V}, V_{SD} = 1.5 \text{ V}$) For min/max values $T_1 = -40^{\circ}\text{C}$ to $+125^{\circ}\text{C}$. $V_{CC} = 12 \text{ V}$

| Description | Test Condition | Symbol | Min | Тур | Max | Unit |
|---|---|--|-----------------------|-----------------------|-----------------------|------|
| STARTUP AND SUPPLY CIRCUITS | <u>.</u> | | | | | |
| Supply Voltage Startup Threshold Minimum Operating Voltage Hysteresis V _{CC(on)} – V _{CC(off)} Internal logic reset | V _{CC} rising V _{CC} rising V _{CC} falling | V _{CC(on)} V _{CC(off)} V _{CC(HYS)} V _{CC(reset)} | 16.0 8.2 8 4 | 18.0 8.8 - 5 | 20.0 9.4 - 6 | V |
| V _{CC} Over Voltage Protection Threshold | | V _{CC(OVP)} | 25.5 | 26.8 | 28.5 | V |
| $V_{CC(off)}$ noise filter $V_{CC(reset)}$ noise filter | | $t_{VCC(off)}$ $t_{VCC(reset)}$ | | 5 20 | - | μS |
| Startup current | | I _{CC(start)} | - | 13 | 30 | μΑ |
| Startup current in fault mode | | I _{CC(sFault)} | | 58 | 75 | μΑ |
| Supply Current Device Disabled/Fault Device Enabled/No output load on pin 7 Device Switching (F _{SW} = 65 kHz) | $V_{CC} > V_{CC(off)}$ $F_{sw} = 65 \text{ kHz}$ $C_{DRV} = 470 \text{ pF, } F_{sw} = 65 \text{ kHz}$ | I _{CC1} I _{CC2} I _{CC3} | 0.8 - - | 1.0 2.6 3.0 | 1.2 4.0 4.5 | mA |
| CURRENT SENSE | • | | | | | |
| Maximum Internal current limit | | V_{ILIM} | 0.95 | 1.00 | 1.05 | V |
| Leading Edge Blanking Duration for V _{ILIM} | | t _{LEB} | 240 | 300 | 360 | ns |

Guaranteed by Design

A NTC is generally placed between the SD and GND pins. Parameters R_{TF(start)}, R_{TF(stop)}, R_{OTP(off)} and R_{OTP(on)} give the resistance the NTC must exhibit to respectively, enter thermal foldback, stop thermal foldback, trigger the OTP limit and allow the circuit recovery after

At startup, when V_{CC} reaches $V_{CC(on)}$, the controller blanks OTP for more than 250 μ s to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

| Propagation delay from current detection to gate of in-state Italian | Description | Test Condition | Symbol | Min | Тур | Max | Unit |
|--|--|---|---------------------------|------|------|------|------|
| off—state ton(MAXX) 2.6 3.6 4.6 μs Maximum on–time ton(MAXX) 2.6 3.6 4.6 μs Threshold for immediate fault protection activation VCS(slosp) 1.35 1.50 1.5 1.0 1.5 1.0 | CURRENT SENSE | | | | | | |
| Threshold for immediate fault protection activation VCS(stop) 1.35 1.50 1.65 V | | | t _{ILIM} | - | 100 | 150 | ns |
| Leading Edge Blanking Duration for V _{CS(6000)} ns Le _{CS} - 150 - ns Current source for CS to GND short detection lC _{CS(60001)} d00 500 600 μA Current sense threshold for CS to GND short detection V _{CS} rising V _{CS(10001)} 30 65 100 mV mV cotton mV mV cotton mV mV mV cotton mV mV mV mV cotton mV mV mV mV cotton mV mV mV mV mV mV mV m | Maximum on-time | | t _{on(MAX)} | 26 | 36 | 46 | μS |
| Current source for CS to GND short detection VCS rising VCS(tow) 30 650 100 mV | Threshold for immediate fault protection activation | | V _{CS(stop)} | 1.35 | 1.50 | 1.65 | V |
| Current sense threshold for CS to GND short detection V _{CS} rising V _{CS} (iow) So 65 100 mV | Leading Edge Blanking Duration for V _{CS(stop)} | | t _{BCS} | - | 150 | _ | ns |
| Table Tab | Current source for CS to GND short detection | | I _{CS(short)} | 400 | 500 | 600 | μΑ |
| Drive Resistance DRV Sink DRV Source RSNK C 13 C C C C C C C C C | | V _{CS} rising | V _{CS(low)} | 30 | 65 | 100 | mV |
| DRV Sink DRV Source Pasink Pasink DRV Source Pasink (Note 6) Pasink (Note 6 | GATE DRIVE | | | | | | |
| DRV Sink (Note 6) DRV Source (Note 6) Sink (Israc 1 | DRV Sink DRV Source | | | | | | |
| Fall Time (90% to 10%) CDRV = 470 pF t ₁ - 30 - 10 NS | DRV Sink (Note 6) | | | | | | ma |
| | Rise Time (10% to 90%) | C _{DRV} = 470 pF | t _r | _ | 40 | - | ns |
| DRV High Voltage $V_{CC} = V_{CC(MAX)}$ $C_{DRV} = 470 pF, R_{DRV} = 33 kΩ$ $V_{DRV(high)}$ 10 12 14 V ZERO VOLTAGE DETECTION CIRCUIT Upper ZCD threshold voltage V_{ZCD} rising $V_{ZCD(ising)}$ - 90 150 mV Lower ZCD threshold voltage V_{ZCD} falling $V_{ZCD(Halling)}$ 35 55 - mV ZCD hysteresis V_{ZCD} falling $V_{ZCD(HAYS)}$ 15 - - mV Propagation Delay from valley detection to DRV high V_{ZCD} falling T_{DEM} - 100 300 ns Blanking delay after on–time $T_{ZCD(blank1)}$ 1.12 1.50 1.88 μs Timeout after last DEMAG transition T_{IIMO} 5.0 6.5 8.0 μs Pulling–down resistor $V_{ZCD} = V_{ZCD}(talling)$ $R_{ZCD(PD)}$ - 200 - kΩ CONSTANT CURRENT AND POWER FACTOR CONTROL Reference Voltage at $T_J = 25^{\circ}C$ A and B versions V_{REF} 245.5 | Fall Time (90% to 10%) | C _{DRV} = 470 pF | t _f | _ | 30 | - | ns |
| ZERO VOLTAGE DETECTION CIRCUITUpper ZCD threshold voltage V_{ZCD} rising $V_{ZCD(fising)}$ -90150mVLower ZCD threshold voltage V_{ZCD} falling $V_{ZCD(falling)}$ 3555-mVZCD hysteresis $V_{ZCD(HYS)}$ 15mVPropagation Delay from valley detection to DRV high V_{ZCD} falling T_{DEM} -100300nsBlanking delay after on-time $T_{ZCD(blank1)}$ 1.121.501.88μsTimeout after last DEMAG transition T_{TIMO} 5.06.58.0μsPulling-down resistor $V_{ZCD} = V_{ZCD(falling)}$ $R_{ZCD(PD)}$ -200-kΩCONSTANT CURRENT AND POWER FACTOR CONTROLReference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} 245 192.5250 200.0255 200.0mVReference Voltage $T_J = 25^{\circ}C$ to 100°CA and B versions | DRV Low Voltage | $V_{CC} = V_{CC(off)} + 0.2 \text{ V}$ $C_{DRV} = 470 \text{ pF}, R_{DRV} = 33 \text{ k}\Omega$ | $V_{DRV(low)}$ | 8 | _ | ı | ٧ |
| Upper ZCD threshold voltage V_{ZCD} rising V_{ZCD} (rising)-90150mVLower ZCD threshold voltage V_{ZCD} falling V_{ZCD} (falling)3555-mVZCD hysteresis V_{ZCD} falling V_{ZCD} falling15mVPropagation Delay from valley detection to DRV high V_{ZCD} falling V_{DEM} -100300nsBlanking delay after on–time V_{ZCD} falling V_{ZCD} falling1.121.501.88μsTimeout after last DEMAG transition V_{ZCD} e V_{ZCD} falling V_{ZCD} falling V_{ZCD} falling-200-kΩPulling–down resistor V_{ZCD} e V_{ZCD} falling V_{ZCD} for V_{ZCD} falling V_{ZCD} for V_{ZCD} f | DRV High Voltage | $V_{CC} = V_{CC(MAX)}$ $C_{DRV} = 470 \text{ pF, R}_{DRV} = 33 \text{ k}\Omega$ | $V_{DRV(high)}$ | 10 | 12 | 14 | V |
| Lower ZCD threshold voltage V_{ZCD} falling $V_{ZCD(ftalling)}$ 3555-mVZCD hysteresis V_{ZCD} falling $V_{ZCD(HYS)}$ 15mVPropagation Delay from valley detection to DRV high V_{ZCD} falling T_{DEM} -100300nsBlanking delay after on–time $T_{ZCD(blank1)}$ 1.121.501.88 μ_S Timeout after last DEMAG transition T_{TIMO} 5.06.58.0 μ_S Pulling–down resistor $V_{ZCD} = V_{ZCD}(ftalling)$ $R_{ZCD(PD)}$ -200- $k\Omega$ CONSTANT CURRENT AND POWER FACTOR CONTROLReference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} 245 195250 200255 200.0mVReference Voltage $T_J = 25^{\circ}C$ to 100°CA and B versions | ZERO VOLTAGE DETECTION CIRCUIT | | | | | | |
| ZCD hysteresis $V_{ZCD(HYS)}$ 15mVPropagation Delay from valley detection to DRV high V_{ZCD} falling T_{DEM} -100300nsBlanking delay after on-time $T_{ZCD(blank1)}$ 1.121.501.88 μ_S Timeout after last DEMAG transition T_{TIMO} 5.06.58.0 μ_S Pulling-down resistor $V_{ZCD} = V_{ZCD(falling)}$ $R_{ZCD(PD)}$ -200- $k\Omega$ CONSTANT CURRENT AND POWER FACTOR CONTROLReference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} 245 250 255 200255 205 205mVReference Voltage $T_J = 25^{\circ}C$ to 100°CA and B versions C and D versions V_{REF} 242.5 250.0 200.0 257.5 207.5 207.5mVReference Voltage $T_J = -40^{\circ}C$ to 125°CA and B versions C and D versions V_{REF} 240 250 200.0 210 207.5200.0 210Current sense lower threshold V_{CS} falling V_{CS} (low)2055100mV $V_{control}$ to current setpoint division ratio $V_{REF} = V_{REF} = $ | Upper ZCD threshold voltage | V _{ZCD} rising | V _{ZCD(rising)} | _ | 90 | 150 | mV |
| Propagation Delay from valley detection to DRV high V_{ZCD} falling T_{DEM} - 100 300 ns Blanking delay after on–time $T_{ZCD(blank1)}$ 1.12 1.50 1.88 μ_S Timeout after last DEMAG transition T_{TIMO} 5.0 6.5 8.0 μ_S Pulling–down resistor $V_{ZCD} = V_{ZCD(falling)}$ $R_{ZCD(PD)}$ - 200 - κ_D CONSTANT CURRENT AND POWER FACTOR CONTROL Reference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D | Lower ZCD threshold voltage | V _{ZCD} falling | V _{ZCD(falling)} | 35 | 55 | - | mV |
| Blanking delay after on-time $T_{ZCD(blank1)}$ 1.121.501.88μsTimeout after last DEMAG transition T_{TIMO} 5.06.58.0μsPulling-down resistor $V_{ZCD} = V_{ZCD(falling)}$ $R_{ZCD(PD)}$ -200- $k\Omega$ CONSTANT CURRENT AND POWER FACTOR CONTROLReference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} $\frac{245}{195}$ $\frac{250}{200}$ $\frac{255}{205}$ mVReference Voltage $T_J = 25^{\circ}C$ to 100°CA and B versions C and D versions V_{REF} $\frac{242.5}{192.5}$ $\frac{250.0}{200.0}$ $\frac{257.5}{207.5}$ mVReference Voltage $T_J = -40^{\circ}C$ to 125°CA and B versions C and D versions V_{REF} $\frac{240}{190}$ $\frac{250}{200}$ $\frac{260}{210}$ mVCurrent sense lower threshold V_{CS} falling V_{CS} (low) $\frac{20}{200}$ $\frac{250}{210}$ $\frac{250}{21$ | ZCD hysteresis | | V _{ZCD(HYS)} | 15 | - | - | mV |
| Timeout after last DEMAG transition | Propagation Delay from valley detection to DRV high | V _{ZCD} falling | T _{DEM} | - | 100 | 300 | ns |
| Pulling-down resistor $V_{ZCD} = V_{ZCD(falling)}$ $R_{ZCD(PD)}$ -200-kΩCONSTANT CURRENT AND POWER FACTOR CONTROLReference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} 245 250 205 205 205 205mVReference Voltage $T_J = 25^{\circ}C$ to 100°CA and B versions C and D versions V_{REF} 242.5 250.0 257.5 200.0 207.5 207.5 200.0 207.5mVReference Voltage $T_J = -40^{\circ}C$ to 125°CA and B versions C and D versions V_{REF} 240 250 260 210 210 200 210mVCurrent sense lower threshold V_{CS} falling V_{CS} (low)20 55 100 mV $V_{control}$ to current setpoint division ratio V_{ratio} -4Error amplifier gain $V_{REFX} = V_{REF}$ G_{EA} 40 50 60 μ S | Blanking delay after on-time | | T _{ZCD(blank1)} | 1.12 | 1.50 | 1.88 | μs |
| CONSTANT CURRENT AND POWER FACTOR CONTROLReference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} $245 \\ 195$ $250 \\ 200$ $255 \\ 205$ mVReference Voltage $T_J = 25^{\circ}C$ to $100^{\circ}C$ A and B versions C and D versions V_{REF} $242.5 \\ 192.5$ $250.0 \\ 200.0$ $257.5 \\ 207.5$ mVReference Voltage $T_J = -40^{\circ}C$ to $125^{\circ}C$ A and B versions C and D versions V_{REF} $240 \\ 190$ $250 \\ 200$ $260 \\ 210$ mVCurrent sense lower threshold V_{CS} falling V_{CS} (low) 20 55 100 mV $V_{control}$ to current setpoint division ratio V_{REF} V_{REF} V_{REF} V_{REF} V_{REF} V_{REF} V_{CS} falling <td< td=""><td>Timeout after last DEMAG transition</td><td></td><td>T_{TIMO}</td><td>5.0</td><td>6.5</td><td>8.0</td><td>μS</td></td<> | Timeout after last DEMAG transition | | T _{TIMO} | 5.0 | 6.5 | 8.0 | μS |
| Reference Voltage at $T_J = 25^{\circ}C$ A and B versions C and D versions V_{REF} 245 195 200 205 205 205mVReference Voltage $T_J = 25^{\circ}C$ to 100°CA and B versions C and D versions V_{REF} 242.5 250.0 257.5 200.0 207.5 207.5mVReference Voltage $T_J = -40^{\circ}C$ to 125°CA and B versions C and D versions V_{REF} 240 250 260 210 210 210mVCurrent sense lower threshold V_{CS} falling V_{CS} (low)20 55 100 mV $V_{Control}$ to current setpoint division ratio V_{REF} V_{REF} V_{REF} Error amplifier gain V_{REF} V_{REF} V_{REF} V_{REF} | Pulling-down resistor | $V_{ZCD} = V_{ZCD(falling)}$ | R _{ZCD(PD)} | - | 200 | - | kΩ |
| Reference Voltage $T_J = 25^{\circ}\text{C}$ to 100°C A and B versions C and D versions V_{REF} 242.5 250.0 207.5 mVReference Voltage $T_J = -40^{\circ}\text{C}$ to 125°C A and B versions C and D versions V_{REF} 240 250 200.0 260 210 Current sense lower threshold V_{CS} falling V_{CS} (low) 20 20 20 20 20 20 20 20 | CONSTANT CURRENT AND POWER FACTOR CON | TROL | | | | | |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | Reference Voltage at T _J = 25°C | | V_{REF} | | | | mV |
| | Reference Voltage T _J = 25°C to 100°C | | V _{REF} | | | | mV |
| $V_{control}$ to current setpoint division ratio V_{ratio} $V_{$ | Reference Voltage $T_J = -40^{\circ}C$ to $125^{\circ}C$ | | V _{REF} | | | | mV |
| Error amplifier gain $V_{REFX}=V_{REF}$ G_{EA} 40 50 60 μ S | Current sense lower threshold | V _{CS} falling | V _{CS(low)} | 20 | 55 | 100 | mV |
| 1 | V _{control} to current setpoint division ratio | | V _{ratio} | - | 4 | - | - |
| Error amplifier current capability $V_{REFX}=V_{REF}$ I_{EA} ± 60 μA | Error amplifier gain | $V_{REFX}=V_{REF}$ | G _{EA} | 40 | 50 | 60 | μS |
| | Error amplifier current capability | $V_{REFX}=V_{REF}$ | I _{EA} | | ±60 | | μА |

^{6.} Guaranteed by Design

^{7.} A NTC is generally placed between the SD and GND pins. Parameters R_{TF(start)}, R_{TF(stop)}, R_{OTP(off)} and R_{OTP(on)} give the resistance the NTC must exhibit to respectively, enter thermal foldback, stop thermal foldback, trigger the OTP limit and allow the circuit recovery after an OTP situation.

At startup, when V_{CC} reaches V_{CC(on)}, the controller blanks OTP for more than 250 μs to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

 $\begin{tabular}{ll} \textbf{Table 4. ELECTRICAL CHARACTERISTICS} & (Unless otherwise noted: For typical values $T_J=25^{\circ}C$, $V_{CC}=12$ V, $V_{ZCD}=0$ V, $V_{CS}=0$ V, $V_{SD}=1.5$ V) For min/max values $T_J=-40^{\circ}C$ to $+125^{\circ}C$, $V_{CC}=12$ V) $ (V_{CS}=12$ V) $ (V_{CS}=12$$

| Description | Test Condition | Symbol | Min | Тур | Max | Unit |
|--|--|--------------------------|------|------|----------|------|
| CONSTANT CURRENT AND POWER FACTOR CON | TROL | • | | | <u> </u> | |
| COMP Pin Start-up Current Source | COMP pin grounded | I _{EA_STUP} | | 140 | | μΑ |
| LINE FEED FORWARD | | • | | | | |
| V _{VS} to I _{CS(offset)} conversion ratio | | K _{LFF} | 18 | 20 | 22 | μS |
| Line feed-forward current on CS pin | DRV high, V _{VS} = 2 V | I _{FF} | 35 | 40 | 45 | μΑ |
| Offset current maximum value | V _{VS} > 5 V | I _{offset(MAX)} | 80 | 100 | 120 | μΑ |
| VALLEY LOCKOUT SECTION | | | | | | |
| Threshold for high- line range (HL) detection | V _{VS} rising | V_{HL} | 2.28 | 2.40 | 2.52 | V |
| Threshold for low-line range (LL) detection | V _{VS} falling | V_{LL} | 2.18 | 2.30 | 2.42 | V |
| Blanking time for line range detection | | t _{HL(blank)} | 15 | 25 | 35 | ms |
| FAULT PROTECTION | | | | | | |
| Thermal Shutdown (Note 6) | F _{SW} = 65 kHz | T _{SHDN} | 130 | 150 | 170 | °C |
| Thermal Shutdown Hysteresis | | T _{SHDN(HYS)} | - | 50 | - | °C |
| Threshold voltage for output short circuit or auxiliary winding short circuit detection | | V _{ZCD(short)} | 0.8 | 1.0 | 1.2 | V |
| Short circuit detection Timer | $V_{ZCD} < V_{ZCD(short)}$ | t _{OVLD} | 70 | 90 | 110 | ms |
| Auto-recovery timer duration | | t _{recovery} | 3 | 4 | 5 | s |
| SD pin Clamp series resistor | | R _{SD(clamp)} | | 1.6 | | kΩ |
| Clamped voltage | SD pin open | V _{SD(clamp)} | 1.13 | 1.35 | 1.57 | V |
| SD pin detection level for OVP | V _{SD} rising | V _{OVP} | 2.35 | 2.50 | 2.65 | V |
| Delay before OVP or OTP confirmation (OVP and OTP) | | T _{SD(delay)} | 22.5 | 30.0 | 37.5 | μS |
| Reference current for direct connection of an NTC (Note 8) | | I _{OTP(REF)} | 80 | 85 | 90 | μΑ |
| Fault detection level for OTP (Note 7) | V _{SD} falling | V _{OTP(off)} | 0.47 | 0.50 | 0.53 | V |
| SD pin level for operation recovery after an OTP detection | V _{SD} rising | V _{OTP(on)} | 0.66 | 0.70 | 0.74 | V |
| OTP blanking time when circuit starts operating (Note 8) | | t _{OTP(start)} | 250 | | 370 | μS |
| SD pin voltage at which thermal fold–back starts (V _{REF} is decreased) | | V _{TF(start)} | 0.94 | 1.00 | 1.06 | V |
| SD pin voltage at which thermal fold–back stops (V _{REF} is clamped to V _{REF50}) | | V _{TF(stop)} | 0.64 | 0.69 | 0.74 | V |
| V _{TF(start)} over I _{OTP(REF)} ratio (Note 7) | T _J = +25°C to +125°C | R _{TF(start)} | 10.8 | 11.7 | 12.6 | kΩ |
| V _{TF(stop)} over I _{OTP(REF)} ratio (Note 7) | $T_J = +25^{\circ}C \text{ to } +125^{\circ}C$ | R _{TF(stop)} | 7.4 | 8.1 | 8.8 | kΩ |
| V _{OTP(off)} over I _{OTP(REF)} ratio (Note 7) | $T_{J} = +25^{\circ}\text{C to } +125^{\circ}\text{C}$ | R _{OTP(off)} | 5.4 | 5.9 | 6.4 | kΩ |
| V _{OTP(on)} over I _{OTP(REF)} ratio (Note 7) | $T_{J} = +25^{\circ}\text{C to } +125^{\circ}\text{C}$ | R _{OTP(on)} | 7.5 | 8.1 | 8.7 | kΩ |
| V_{REF} @ V_{SD} = 600 mV (SD pin falling no OTP detection) (percent of V_{REF}) | | V _{REF(50)} | 40 | 50 | 60 | % |

^{6.} Guaranteed by Design

A NTC is generally placed between the SD and GND pins. Parameters R_{TF(start)}, R_{TF(stop)}, R_{OTP(off)} and R_{OTP(on)} give the resistance the NTC must exhibit to respectively, enter thermal foldback, stop thermal foldback, trigger the OTP limit and allow the circuit recovery after an OTP situation.

^{8.} At startup, when V_{CC} reaches $V_{CC(on)}$, the controller blanks OTP for more than 250 μs to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

 $\begin{tabular}{ll} \textbf{Table 4. ELECTRICAL CHARACTERISTICS} & (Unless otherwise noted: For typical values $T_J=25^{\circ}C$, $V_{CC}=12$ V, $V_{ZCD}=0$ V, $V_{CS}=0$ V, $V_{SD}=1.5$ V) For min/max values $T_J=-40^{\circ}C$ to $+125^{\circ}C$, $V_{CC}=12$ V) $ (V_{CS}=12$ V) $ (V_{CS}=12$$

| Description | Test Condition | Symbol | Min | Тур | Max | Unit | |
|---|------------------------|------------------------|------|------|------|------|--|
| BROWN-OUT | BROWN-OUT | | | | | | |
| Brown-Out ON level (IC start pulsing) | V _S rising | V _{BO(on)} | 0.95 | 1.00 | 1.05 | V | |
| Brown-Out OFF level (IC shuts down) | V _S falling | V _{BO(off)} | 0.85 | 0.90 | 0.95 | V | |
| BO comparators delay | | t _{BO(delay)} | | 30 | | μs | |
| Brown-Out blanking time | | t _{BO(blank)} | 15 | 25 | 35 | ms | |
| V _S pin Pulling-down Current | $V_S = V_{BO(on)}$ | I _{BO(bias)} | 50 | 250 | 450 | nA | |

- 6. Guaranteed by Design
- A NTC is generally placed between the SD and GND pins. Parameters R_{TF(start)}, R_{TF(stop)}, R_{OTP(off)} and R_{OTP(on)} give the resistance the NTC must exhibit to respectively, enter thermal foldback, stop thermal foldback, trigger the OTP limit and allow the circuit recovery after an OTP situation.
- 8. At startup, when V_{CC} reaches $V_{CC(on)}$, the controller blanks OTP for more than 250 μ s to avoid detecting an OTP fault by allowing the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin.

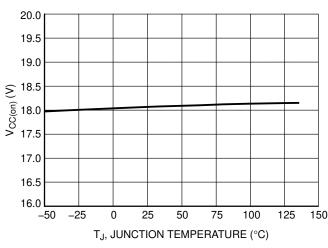


Figure 4. V_{CC} Start-up Threshold vs. Temperature

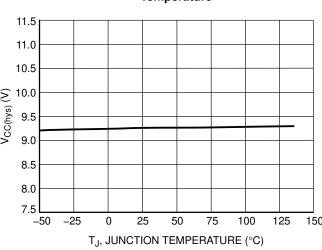


Figure 6. Hysteresis (V_{CC(on)} – V_{CC(off)}) vs. Temperature

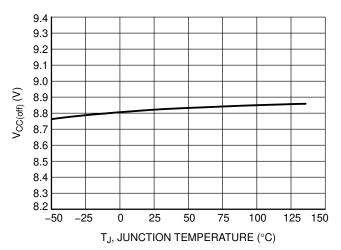


Figure 5. V_{CC} Minimum Operating Voltage vs. Temperature

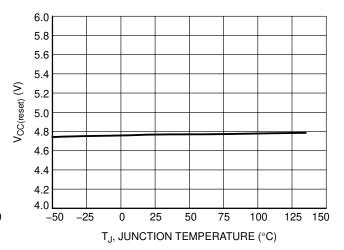
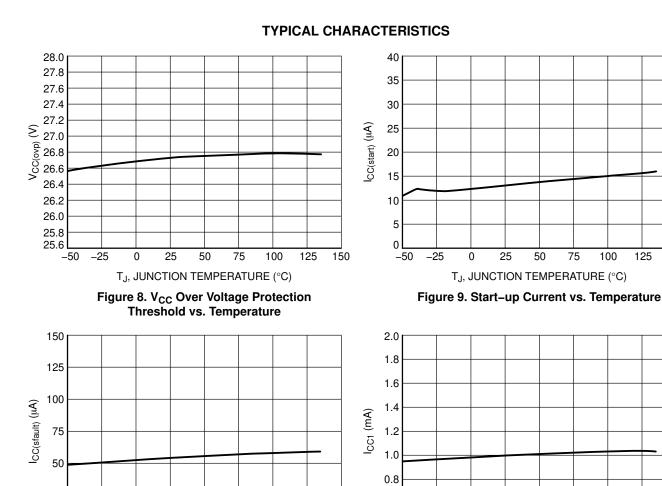


Figure 7. V_{CC(reset)} vs. Temperature



T_J, JUNCTION TEMPERATURE (°C) Figure 10. Start-up Current in Fault Mode vs. **Temperature**

50

75

100

125

150

25

-50

-25

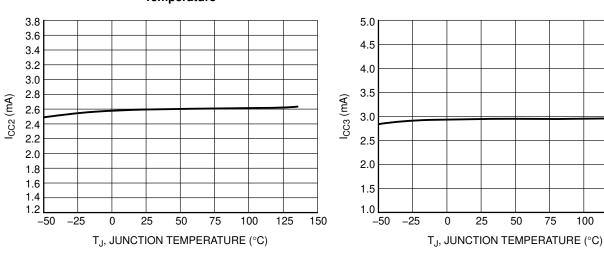


Figure 12. I_{CC2} vs. Temperature

100 125 150 50 75

25

50

 T_J , JUNCTION TEMPERATURE (°C)

Figure 11. I_{CC1} vs. Temperature

100

75

125 150

125 150

Figure 13. I_{CC3} vs. Temperature

0.6

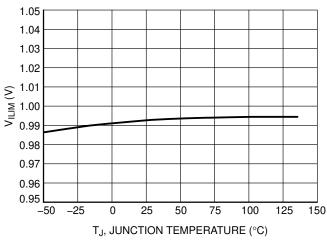
-50

-25

TYPICAL CHARACTERISTICS

400 380

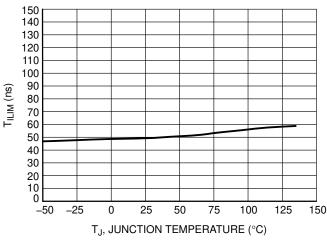
360



340 320 300 280 260 240 220 200 -25 25 50 75 100 125 150 -50 T_J, JUNCTION TEMPERATURE (°C)

Figure 14. Maximum Internal Current Limit vs.
Temperature

Figure 15. Leading Edge Blanking vs. Temperature



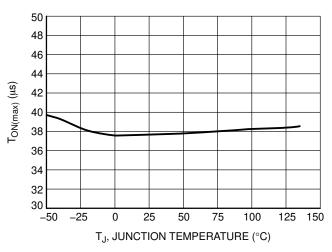
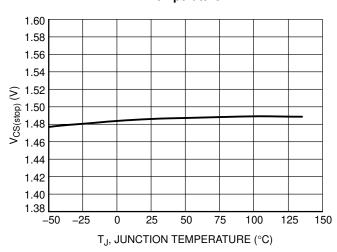


Figure 16. Current Limit Propagation Delay vs.
Temperature

Figure 17. Maximum On-time vs. Temperature



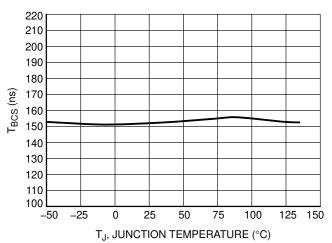
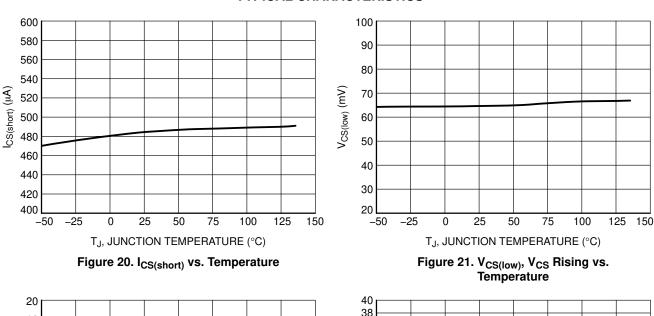
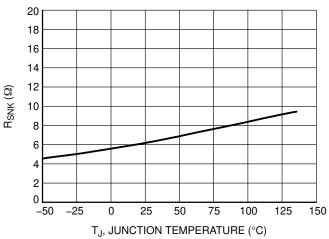


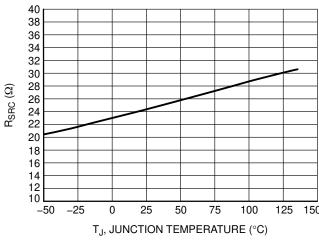
Figure 18. V_{CS(stop)} vs. Temperature

Figure 19. Leading Edge Blanking Duration for $V_{CS(stop)}$ vs. Temperature

TYPICAL CHARACTERISTICS







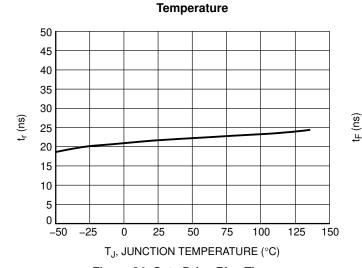


Figure 22. Sink Gate Drive Resistance vs.

Figure 23. Source Gate Drive Resistance vs. Temperature

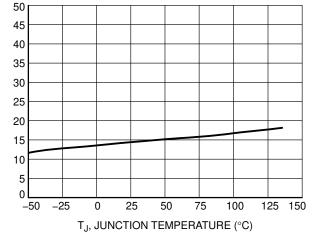


Figure 24. Gate Drive Rise Time vs. Temperature

Figure 25. Gate Drive Fall Time (C_{DRV} = 470 pF) vs. Temperature

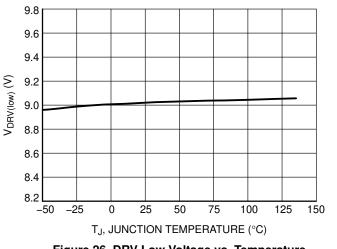


Figure 26. DRV Low Voltage vs. Temperature

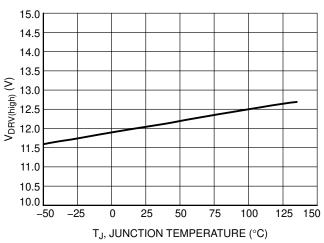


Figure 27. DRV High Voltage vs. Temperature

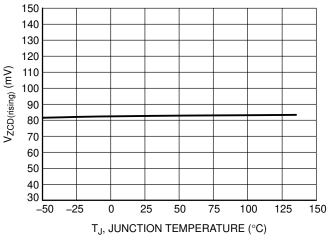


Figure 28. Upper ZCD Threshold Voltage vs. Temperature

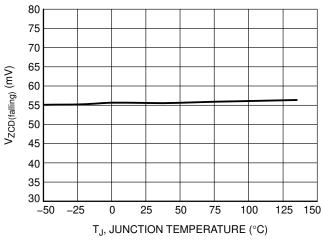


Figure 29. Lower ZCD Threshold vs. Temperature

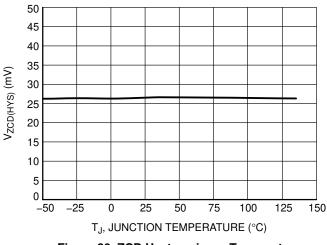


Figure 30. ZCD Hysteresis vs. Temperature

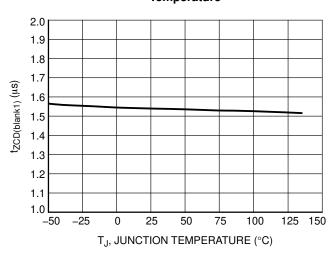


Figure 31. ZCD Blanking Delay vs. Temperature

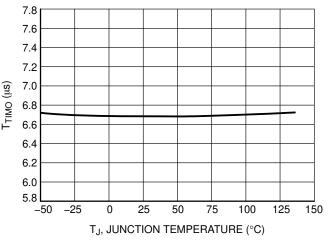


Figure 32. ZCD Time-out vs. Temperature

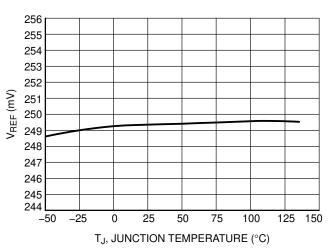


Figure 33. Reference Voltage vs. Temperature (A and B versions)

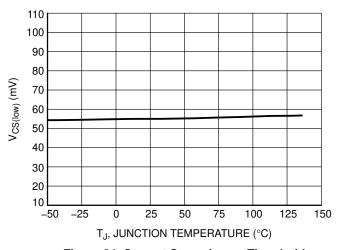


Figure 34. Current Sense Lower Threshold (V_{CS} Falling) vs. Temperature

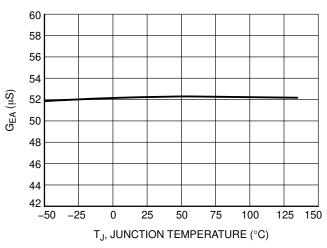


Figure 35. Error Amplifier Trans-conductance
Gain vs. Temperature

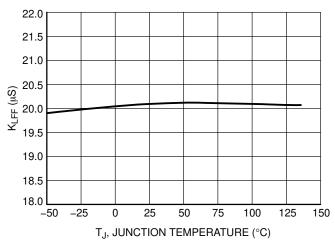


Figure 36. Feedforward V_{VS} to I_{CS(offset)} Conversion Ratio vs. Temperature

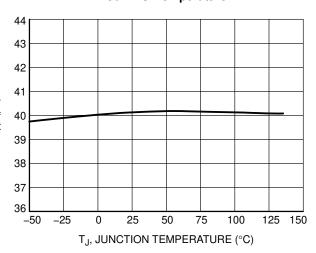


Figure 37. Line Feedforward Current on CS Pin (@ V_{VS} = 2 V) vs. Temperature

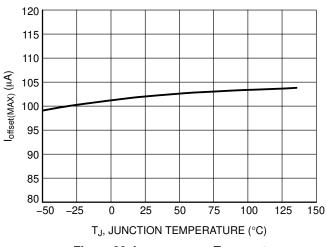


Figure 38. I_{offset(MAX)} vs. Temperature

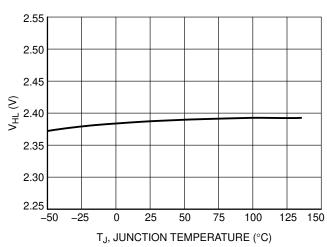


Figure 39. Threshold for High-line Range Detection vs. Temperature

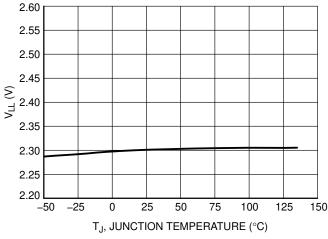


Figure 40. Threshold for Low-line Range Detection vs. Temperature

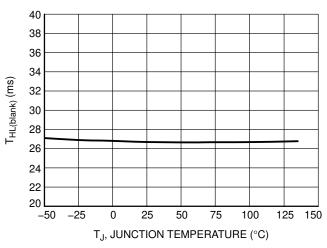


Figure 41. Blanking Time for Low-line Range Detection vs. Temperature

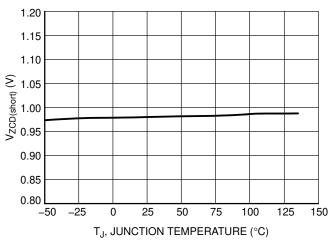


Figure 42. Threshold Voltage for Output Short Circuit Detection vs. Temperature

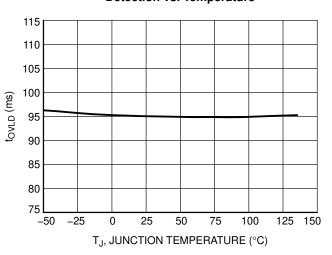
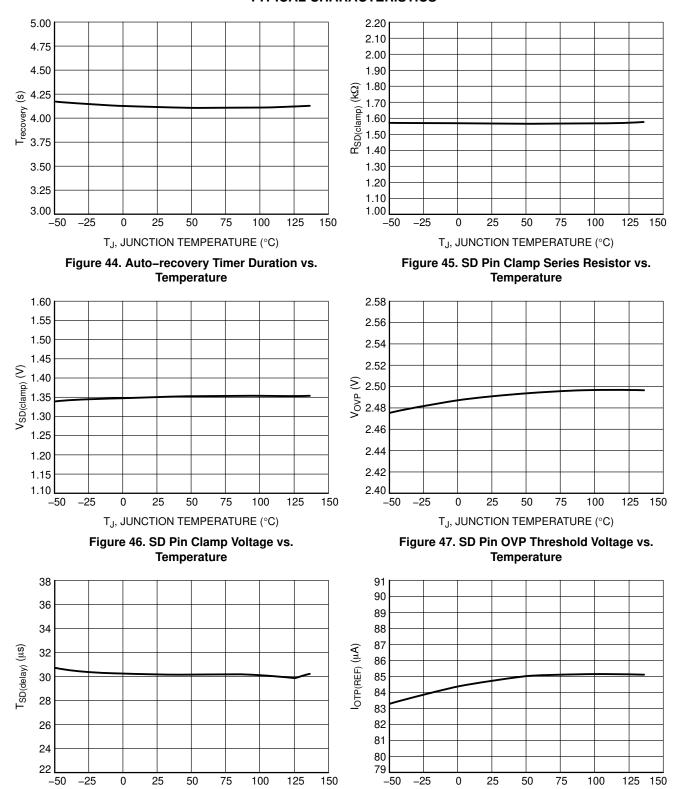
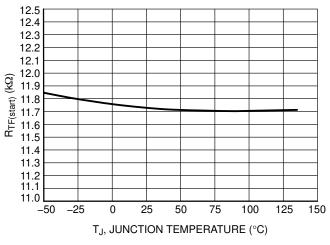


Figure 43. Short Circuit Detection Timer vs. Temperature



 $\label{eq:tj} T_J, \, \text{JUNCTION TEMPERATURE (°C)} \\ \textbf{Figure 48. } T_{\textbf{SD(delay)}} \, \textbf{vs. Temperature}$

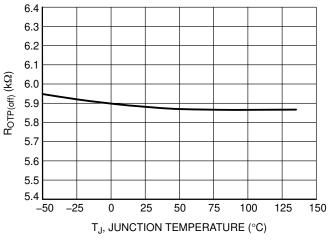
 T_J , JUNCTION TEMPERATURE (°C) Figure 49. $I_{OTP(REF)}$ vs. Temperature



8.8 8.7 8.6 8.5 8.4 $\mathsf{R}_\mathsf{TF(stop)}$ (k Ω) 8.3 8.2 8.1 8.0 7.9 7.8 7.7 7.6 -25 25 50 75 100 125 150 -50 T_J, JUNCTION TEMPERATURE (°C)

Figure 50. R_{TF(start)} vs. Temperature

Figure 51. R_{TF(stop)} vs. Temperature



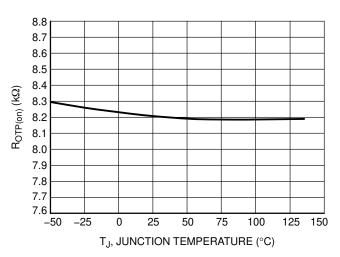
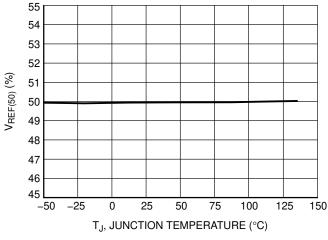


Figure 52. R_{OTP(off)} vs. Temperature

Figure 53. $R_{OTP(on)}$ vs. Temperature



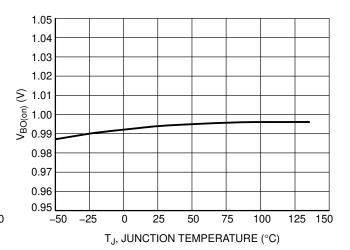


Figure 54. Ratio $V_{REF(50)}$ over V_{REF} vs. Temperature

Figure 55. Brown-out ON Level vs. Temperature

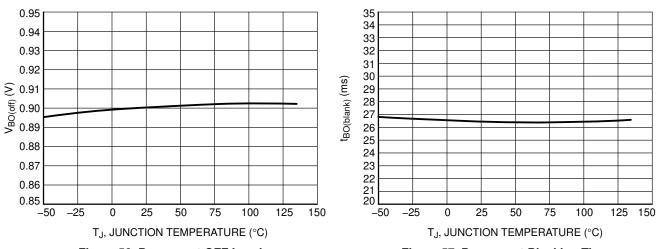


Figure 56. Brown-out OFF Level vs. Temperature

Figure 57. Brown-out Blanking Time vs. Temperature

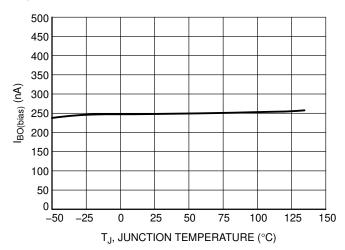


Figure 58. V_S Pin Pulling-down Current vs. Temperature

Application Information

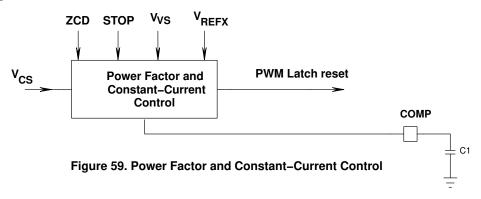
The NCL30088 is a driver for power-factor corrected flyback and non-isolated buck-boost and SEPIC converters. Its current-mode, quasi-resonant architecture optimizes the efficiency by turning on the MOSFET when its drain-source voltage is minimal (valley). At high line, the circuit delays the MOSFET turn on until the second valley is detected to reduce the switching losses. A proprietary circuitry ensures both accurate regulation of the output current (without the need for a secondary-side feedback) and near-unity power factor correction. The circuit contains a suite of powerful protections to ensure a robust LED driver design without the need for extra components or overdesign.

- Quasi-Resonance Current-Mode Operation: implementing quasi-resonance operation in peak current-mode control, the NCL30088 optimizes the efficiency by turning on the MOSFET when its drain-source voltage is minimal (valley). In light-load conditions, the circuit changes valleys to reduce the switching losses. For stable operation, the valley at which the MOSFET switches on remains locked until the input voltage or the output current set-point significantly changes.
- Primary–Side Constant–Current Control with Power Factor Correction: a proprietary circuitry allows the LED driver to achieve both near–unity power factor correction and accurate regulation of the output current without requiring any secondary–side feedback (no optocoupler needed). A power factor as high as 0.99 and an output current deviation below ±2% are typically obtained.
- Main protection features:
 - Over Temperature Thermal Fold–back /
 Shutdown/ Over Voltage Protection: the
 NCL30088 features a gradual current foldback to
 protect the driver from excessive temperature down
 to 50% of the programmed current. This represents a
 power reduction of the LED by more than 50%. If
 the temperature continues to rise after this point to a
 second level, the controller stops operating. This
 mode would only be expected to be reached if there
 is a severe fault. The first and second temperature
 thresholds depend on the value of the NTC

- connected to the SD pin. Note, the SD pin can also be used to shutdown the device by pulling this pin below the $V_{OTP(off)}$ min level. A Zener diode can also be used to pull-up the pin and stop the controller for adjustable OVP protection. Both protections are latching-off (A and C versions) or auto-recovery (the circuit can recover operation after 4–s delay has elapsed B and D versions).
- Cycle-by-cycle peak current limit: when the current sense voltage exceeds the internal threshold V_{ILIM}, the MOSFET is immediately turned off (cycle-by-cycle current limitation).
- Winding or Output Diode Short-Circuit
 Protection: an additional comparator senses the CS signal and stops the controller if it exceeds 150% x VILIM for 4 consecutive cycles. This feature can protect the converter if a winding is shorted or if the output diode is shorted or simply if the transformer saturates. This protection is latching-off (A and C versions) or auto-recovery (B and D versions).
- Output Short-circuit protection: if the ZCD pin voltage remains low for a 90-ms time interval, the controller detects that the output or the ZCD pin is grounded and hence, stops operation. This protection is latching-off (A and C versions) or auto-recovery (B and D versions).
- Open LED protection: if the V_{CC} pin voltage exceeds the OVP threshold, the controller shuts down and waits 4 seconds before restarting switching operation.
- Floating or Short Pin Detection: the circuit can detect most of these situations which helps pass safety tests.

Power Factor and Constant Current Control

The NCL30088 embeds an analog/digital block to control the power factor and regulate the output current by monitoring the ZCD, V_S and CS pin voltages (signals ZCD, V_S and V_{CS} of Figure 59). This circuitry generates the current setpoint ($V_{CONTROL}/4$) and compares it to the current sense signal (V_{CS}) to dictate the MOSFET turning off event when V_{CS} exceeds $V_{CONTROL}/4$.



As illustrated in Figure 59, the V_S pin provides the sinusoidal reference necessary for shaping the input current. The obtained current reference is further modulated so that when averaged over a half-line period, it is equal to the output current reference (V_{REFX}). This averaging process is made by an internal Operational Trans-conductance Amplifier (OTA) and the capacitor connected to the COMP pin (C1 of Figure 59). Typical COMP capacitance is 1 μ F and should not be less than 470 nF to ensure stability. The COMP ripple does not affect the power factor performance as the circuit digitally eliminates it when generating the current setpoint.

If the V_S pin properly conveys the sinusoidal shape, power factor will be close to unity and the Total Harmonic Distortion (THD) will be low. In any case, the output current will be well regulated following the equation below:

$$I_{out} = \frac{V_{REFX}}{2N_{PS}R_{sense}}$$
 (eq. 1)

Where:

- N_{PS} is the secondary to primary transformer turns
 N_{PS} = N_S/N_P. N_{PS} is 1 in the case of non-isolated buck-boost or SEPIC converter.
- R_{sense} is the current sense resistor (see Figure 1).
- V_{REFX} is the output current internal reference.
 V_{REFX} = V_{REF} (250 mV in A and B versions and 200 mV in C and D versions, typically) at full load.

The output current reference (V_{REFX}) is V_{REF} unless the temperature is high enough to activate the thermal fold–back (see "protections" section).

If a major fault is detected, the circuit enters the latched-off or auto-recovery mode and the COMP pin is grounded (except in an UVLO condition). This ensures a clean start-up when the circuit resumes operation.

Start-up Sequence

Generally an LED lamp is expected to emit light in < 1 sec and typically within 300 ms. The start–up phase consists of the time to charge the V_{CC} capacitor, begin switching and the time to charge the output capacitor until sufficient current flows into the LED string. To speed–up this phase, the following defines the start–up sequence:

- The COMP pin is grounded when the circuit is off. The average COMP voltage needs to exceed the V_S pin peak value to have the LED current properly regulated (whatever the current target is). To speed—up the COMP capacitance charge and shorten the start—up phase, an internal 80-μA current source adds to the OTA sourced current (60 μA max typically) to charge up the COMP capacitance. The 80-μA current source remains on until the OTA starts to sink current as a result of the COMP pin voltage sufficient rise. At that moment, the COMP pin being near its steady-state value, it is only driven by the OTA.
- If V_{CC} drops below the V_{CC(off)} threshold because the circuit fails to start—up properly on the first attempt, a new try takes place as soon as V_{CC} is recharged to V_{CC(on)}. The COMP voltage is not reset at that moment. Instead, the new attempt starts with the COMP level obtained at the end of the previous operating phase.
- If the load is shorted, the circuit will operate in hiccup mode with V_{CC} oscillating between V_{CC(off)} and V_{CC(on)} until the AUX_SCP protection trips (AUX_SCP is triggered if the ZCD pin voltage does not exceed 1 V within a 90–ms operation period of time thus indicating a short to ground of the ZCD pin or an excessive load preventing the output voltage from rising). The NCL30088A and NCL30088C latch off in this case. With the B and D versions, the AUX_SCP protection forces the 4–s auto–recovery delay to reduce the operation duty–ratio. Figure 60 illustrates a start–up sequence with the output shorted to ground, in this second case.

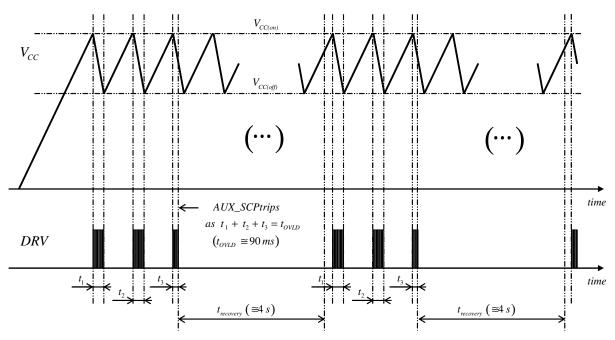


Figure 60. Start-up Sequence in a Load Short-circuit Situation (auto-recovery versions)

Zero Crossing Detection Block

The ZCD pin detects when the drain-source voltage of the power MOSFET reaches a valley by crossing below the 55-mV internal threshold. At startup or in case of extremely damped free oscillations, the ZCD comparator may not be able to detect the valleys. To avoid such a situation, the

NCL30088 features a time—out circuit that generates pulses if the voltage on ZCD pin stays below the 55–mV threshold for $6.5~\mu s$. The time—out also acts as a substitute clock for the valley detection and simulates a missing valley in case the free oscillations are too damped.

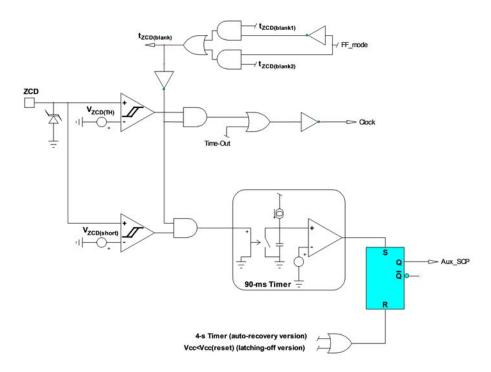


Figure 61. Zero Current Detection Block

If the ZCD pin or the auxiliary winding happen to be shorted, the time–out function would normally make the controller keep switching and hence lead to improper LED current value. The "AUX_SCP" protection prevents such a stressful operation: a secondary timer starts counting that is only reset when the ZCD voltage exceeds the V_{ZCD(short)} threshold (1 V typically). If this timer reaches 90 ms (no ZCD voltage pulse having exceeded V_{ZCD(short)} for this time period), the controller detects a fault and stops operation for 4 seconds (B and D versions) or latches off (A and C versions).

The "clock" shown in Figure 61 is used by the "valley selection frequency foldback" circuitry of the block diagram (Figure 3), to generate the next DRV pulse (if no fault prevents it):

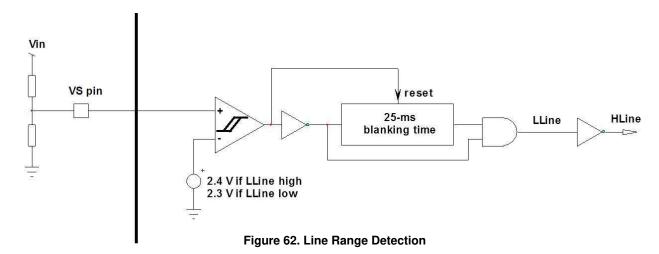
• Immediately when the clock occurs in QR mode at low line or valley 2 at high line (full load)

 After the appropriate number of "clock" pulses in thermal foldback mode

For an optimal operation, the maximum ZCD level should be maintained below 5 V to stay safely below the built in clamping voltage of the pin.

Line Range Detection

As sketched in Figure 62, this circuit detects the low–line range if the V_S pin remains below the V_{LL} threshold (2.3 V typical) for more than the 25–ms blanking time. High–line is detected as soon as the V_S pin voltage exceeds V_{HL} (2.4 V typical). These levels roughly correspond to 184–V rms and 192–V rms line voltages if the external resistors divider applied to the V_S pin is designed to provide a 1–V peak value at 80 V rms.



In the low-line range, conduction losses are generally dominant. Adding a dead-time would further increase these losses. Hence, only a short dead-time is necessary to reach the MOSFET valley. In high-line conditions, switching losses generally are the most critical. It is thus efficient to skip one valley to lower the switching frequency. Hence, under normal operation, the NCL30088 optimizes the

efficiency over the line range by turning on the MOSFET at the first valley in low-line conditions and at the second valley in the high-line case. This is illustrated by Figure 63 that sketches the MOSFET Drain-source voltage in both cases. In the event that thermal foldback is activated, additional valleys can be skipped as the power is reduced.

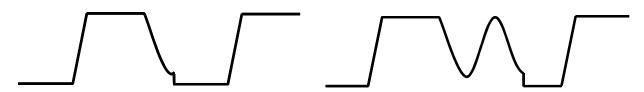


Figure 63. Full-load Operation - Quasi-resonant Mode in low line (left), turn on at valley 2 when in high line (right)

Line Feedforward

As illustrated by Figure 64, the input voltage is sensed by the V_S pin and converted into a current. By adding an

external resistor in series between the sense resistor and the CS pin, a voltage offset proportional to the input voltage is added to the CS signal for the MOSFET on–time.

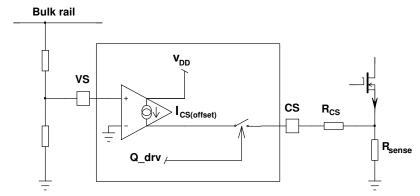


Figure 64. Line Feed-Forward Schematic

In Figure 64, Q_drv designates the output of the PWM latch which is high for the on-time and low otherwise.

Protections

The circuit incorporates a large variety of protections to make the LED driver very rugged. Among them, we can list:

Output Short Circuit Situation

An overload fault is detected if the ZCD pin voltage remains below $V_{ZCD(short)}$ for 90 ms. In such a situation, the circuit stops generating pulses until the 4–s delay auto–recovery time has elapsed (B and D versions) or latches off (A and C versions).

Winding or Output Diode Short Circuit Protection

If a transformer winding happens to be shorted, the primary inductance will collapse leading the current to ramp up in a very abrupt manner. The V_{ILIM} comparator (current limitation threshold) will trip to open the MOSFET and eventually stop the current rise. However, because of the

abnormally steep slope of the current, internal propagation delays and the MOSFET turn–off time will make possible the current rise up to 50% or more of the nominal maximum value set by V_{ILIM} . As illustrated in Figure 65, the circuit uses this current overshoot to detect a winding short circuit. The leading edge blanking (LEB) time for short circuit protection (LEB2) is significantly faster than the LEB time for cycle–by–cycle protection (LEB1). Practically, if four consecutive switching periods lead the CS pin voltage to exceed ($V_{CS(stop)}$ =150% * V_{ILIM}), the controller enters auto–recovery mode in B and D versions (4–s operation interruption between active bursts) and latches off in A and C versions. Similarly, this function can also protect the power supply if the output diode is shorted or if the transformer simply saturates.

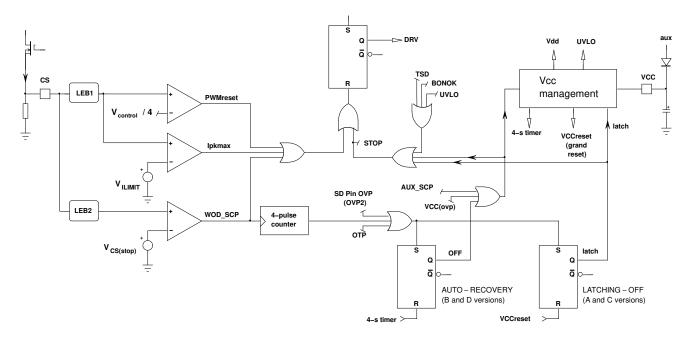


Figure 65. Winding Short Circuit Protection, Max. Peak Current Limit Circuits

V_{CC} Over Voltage Protection

The circuit stops generating pulses if V_{CC} exceeds $V_{CC(OVP)}$ and enters auto-recovery mode. This feature protects the circuit if the output LED string happens to open or is disconnected.

Programmable Over Voltage Protection (OVP2)

Connect a Zener diode between V_{CC} and the SD pin to set a programmable V_{CC} OVP (D_Z of Figure 66). The triggering level is (V_Z+V_{OVP}) where V_{OVP} is the 2.5–V internal threshold. If this protection trips, the NCL30088A and NCL30088C latch off while the NCL30088B and NCL30088D enter the auto-recovery mode.

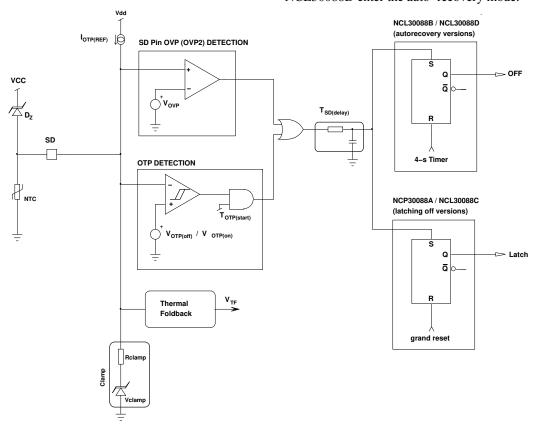


Figure 66. Thermal Foldback and OVP/OTP Circuitry

The SD pin is clamped to about 1.35 V (V_{clamp}) through a 1.6–k Ω resistor (R_{clamp}). It is then necessary to inject about

$$\left(\frac{\mathsf{V}_{\mathsf{OVP}} - \mathsf{V}_{\mathsf{clamp}}}{\mathsf{R}_{\mathsf{clamp}}}\right)$$

that is

$$\left(\frac{2.50-1.35}{1.6 \text{ k}} \cong 700 \,\mu\text{A}\right)$$

typically, to trigger the OVP protection. This current helps ensure an accurate detection by using the Zener diode far from its knee region.

Programmable Over Temperature Foldback Protection (OTP)

Connect an NTC between the SD pin and ground to detect an over–temperature condition. In response to a high temperature (detected if V_{SD} drops below $V_{TF(start)}$), the

circuit gradually reduces the LED current down 50% of its nominal value when V_{SD} reaches $V_{TF(stop)}$, in accordance with the characteristic of Figure 67.

If this thermal foldback cannot prevent the temperature from rising (testified by V_{SD} drop below V_{OTP}), the circuit latches off (A and C versions) or enters auto—recovery mode (B and D versions) and cannot resume operation until V_{SD} exceeds $V_{OTP(on)}$ to provide some temperature hysteresis (around 10°C typically). The OTP thresholds nearly correspond to the following resistances of the NTC:

- Thermal foldback starts when $R_{NTC} \le R_{TF(start)}$ (11.7 k Ω , typically)
- Thermal foldback stops when $R_{NTC} \le R_{TF(stop)}$ (8.0 k Ω , typically)
- OTP triggers when $R_{NTC} \le R_{OTP(off)}$ (5.9 k Ω , typically)
- OTP is removed when $R_{NTC} \ge R_{OTP(on)}$ (8.0 k Ω , typically) (Note 9)
- 9. This condition is sufficient for operation recovery of the B and D versions. For the A and C versions which latch off when OTP triggers, the circuit further needs to be reset by a V_{CC} drop below V_{CC(reset)}. An online EXCEL[®]-based design tool is available to aid in selecting the appropriate NTC value.

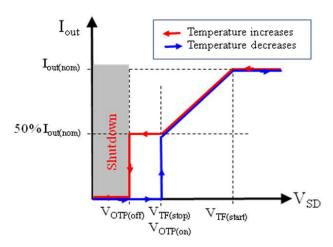


Figure 67. Output Current Reduction versus SD Pin Voltage

At startup, when V_{CC} reaches $V_{CC(on)}$, the OTP comparator is blanked for at least 250 μs in order to allow the SD pin voltage to reach its nominal value if a filtering capacitor is connected to the SD pin. This avoids flickering of the LED light during turn on.

Brown-Out Protection

The NCL30088 prevents operation when the line voltage is too low for proper operation. As illustrated in Figure 68, the circuit detects a brown–out situation if the V_S pin remains below the $V_{BO(off)}$ threshold (0.9 V typical) for more than the 25–ms blanking time. In this case, the controller stops operating. Operation resumes as soon as the V_S pin voltage exceeds $V_{BO(on)}$ (1.0 V typical) and V_{CC} is higher than $V_{CC(on)}$. To ease recovery, the circuit overrides the V_{CC} normal sequence (no need for V_{CC} cycling down below $V_{CC(off)}$). Instead, its consumption immediately reduces to $I_{CC(start)}$ so that V_{CC} rapidly charges up to $V_{CC(on)}$. Once done, the circuit re–starts operating.

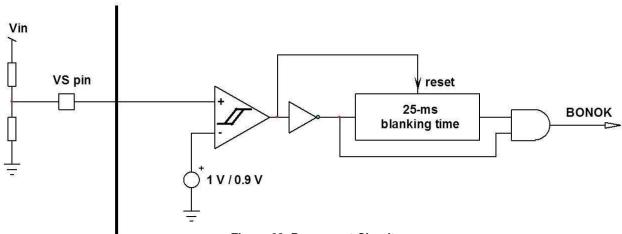


Figure 68. Brown-out Circuit

Die Over Temperature (TSD)

The circuit stops operating if the junction temperature (T_J) exceeds 150°C typically. The controller remains off until T_J goes below nearly 100°C.

Pin Connection Faults

The circuit addresses most pin connection fault cases:

• CS pin short to ground

The circuit senses the CS pin impedance every time it starts—up and after DRV pulses terminated by the 36–µs maximum on–time. If the measured impedance does not exceed 120 ohm typically, the circuit stops operating. In practice, it is recommended to place a minimum of 250–ohm in series between the CS pin and the current sense resistor to take into account possible parametric deviations.

• Fault of the GND connection

If the GND pin is properly connected, the supply current drawn from the positive terminal of the V_{CC} capacitor, flows out of the GND pin to return to the negative terminal of the V_{CC} capacitor. If the GND pin is not connected, the circuit ESD diodes offer another return path. The accidental non–connection of the GND pin is monitored by detecting that one of the ESD diode is conducting. Practically, the ESD diode of CS pin is monitored. If such a fault is detected for 200 μ s, the circuit stops generating DRV pulses.

More generally, incorrect pin connection situations (open, grounded, shorted to adjacent pin) are covered by AND9204/D.

Fault Modes

The circuit turns off whenever a major faulty condition prevents it from operating:

- Severe OTP (V_{SD} level below $V_{OTP(off)}$)
- V_{CC} OVP
- OVP2 (additional OVP provided by SD pin)
- Output diode short circuit protection: "WOD_SCP high"
- Output / Auxiliary winding Short circuit protection: "Aux_SCP high"
- Die over temperature (TSD)

In this mode, the DRV pulses generation is interrupted.

In the case of a latching–off fault, the circuit stops pulsing until the LED driver is unplugged and V_{CC} drops below $V_{CC(reset)}$. At that moment, the fault is cleared and the circuit could resume operation.

In the auto-recovery case, the circuit cannot generate DRV pulses for the auto-recovery 4–s delay. When this time has elapsed, the circuit recovers operation as soon as the V_{CC} voltage has exceeded $V_{CC(on)}$.

In the B and D versions, all these protections are auto-recovery. The SD pin OTP and OVP, WOD_SCP and AUX_SCP are latching off in the A and C versions (see Table 5).

Table 5. PROTECTION MODES

| | AUX_SCP | WOD_SCP | SD Pin OTP | SD Pin OVP |
|------------|---------------|---------------|---------------|---------------|
| NCL30088A* | Latching off | Latching off | Latching off | Latching off |
| NCL30088B | Auto-recovery | Auto-recovery | Auto-recovery | Auto-recovery |
| NCL30088C* | Latching off | Latching off | Latching off | Latching off |
| NCL30088D | Auto-recovery | Auto-recovery | Auto-recovery | Auto-recovery |

ORDERING INFORMATION

| Device | Package Type | Shipping |
|----------------|-----------------------|--------------------|
| NCL30088ADR2G* | | |
| NCL30088BDR2G | SOIC-8 | 2500 / Tana % Daal |
| NCL30088CDR2G* | (Pb–Free/Halide Free) | 2500 / Tape & Reel |
| NCL30088DDR2G | | |

^{*}Please contact local sales representative for availability.