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# Fixed Frequency Current Mode Controller for Flyback Converters

The NCP1236 is a new fixed-frequency current-mode controller featuring Dynamic Self-Supply (DSS). This device is pin-to-pin compatible with the previous NCP12xx families.

The DSS function greatly simplifies the design of the auxiliary supply and the  $V_{CC}$  capacitor by activating the internal startup current source to supply the controller during transients.

Due to frequency foldback, the controller exhibits excellent efficiency in light load condition while still achieving very low standby power consumption. Internal frequency jittering, ramp compensation, and a versatile latch input make this controller an excellent candidate for converters where components cost is the key constraints.

In addition, the controller includes a new high voltage circuitry that combines a start—up current source and a brown—out detector able to sense the input voltage either from the rectified ac line or the dc filtered bulk voltage. The high voltage sensing circuitry is used for the overpower protection purposes as well. Overpower protection, overload protection, and next protective features increases safety level of the final application.

Finally, due to a careful design, the precision of critical parameters is well controlled over the entire temperature range  $(-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C})$ .

#### **Features**

- Fixed-Frequency Current-Mode Operation with Built-In Ramp Compensation
- 65 kHz or 100 kHz Oscillator Frequency
- Frequency Foldback then Skip Mode for Maximized Performance in Light Load and Standby Conditions
- Timer-Based Overload Protection with Latched (option A) or Auto-Recovery (option B) Operation, Shortened Overload Timer for Increased Safety (options C and D), (see all options on page 2)
- High-voltage Current Source with Brown-Out detection and Dynamic Self-Supply, Simplifying the Design of the V<sub>CC</sub> Capacitor
- Frequency Modulation for Softened EMI Signature, including during Frequency Foldback mode
- Adjustable Overpower Compensation
- Latch-off Input for Severe Fault Conditions, Allowing Direct Connection of an NTC for Overtemperature Protection (OTP)
- V<sub>CC</sub> Operation up to 28 V, with Overvoltage Detection
- ±500 mA Peak Source / Sink Current Drive Capability
- 4.0 ms Soft-Start



#### ON Semiconductor®

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#### MARKING DIAGRAM



SOIC-7 CASE 751U



36Xff = Specific Device Code

X = A, B, C or D

ff = 65 or 100 = Assembly Location

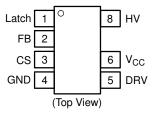
L = Wafer Lot

Y = Year

W = Work Week

■ = Pb-Free Package

#### PIN CONNECTIONS



#### ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page 33 of this data sheet.

- Internal Thermal Shutdown
- Pin-to-Pin Compatible with the Existing NCP12xx Series
- These Devices are Pb–Free, Halogen Free/BFR Free and are RoHS Compliant

#### **Typical Applications**

- AC-DC Adapters for Notebooks, LCD, and Printers
- Offline Battery Chargers
- Consumer Electronic Power Supplies
- Auxiliary/Housekeeping Power Supplies

# **TYPICAL APPLICATION EXAMPLE**

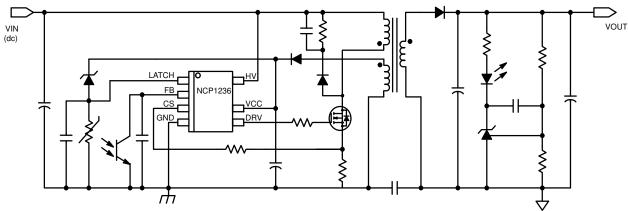


Figure 1. Flyback Converter Application Using the NCP1236

# **OPTIONS**

Part	Option	Frequency	OCP Fault	Fault Timer	Autorecovery Timer
	Α	65 kHz	Latched	128 ms	1 s
	А	100 kHz	Latched	128 ms	1 s
	В	65 kHz	Autorecovery	128 ms	1 s
NCP1236	В	100 kHz	Autorecovery	128 ms	1 s
	С	65 kHz	Latched	32 ms	1.5 s
	С	100 kHz	Latched	32 ms	1.5 s
	D	65 kHz	Autorecovery	32 ms	1.5 s
	D	100 kHz	Autorecovery	32 ms	1.5 s

## PIN FUNCTION DESCRIPTION

Pin No	Pin Name	Function	Pin Description
1	LATCH	Latch-Off Input	Pull the pin up or down to latch–off the controller. An internal current source allows the direct connection of an NTC for over temperature detection
2	FB	Feedback	An optocoupler collector to ground controls the output regulation.
3	CS	Current Sense	This Input senses the Primary Current for current–mode operation, and Offers an overpower compensation adjustment.
4	GND		IC Ground
5	DRV	Drive output	Drives external MOSFET
6	V <sub>CC</sub>	V <sub>CC</sub> input	This supply pin accepts up to 28 Vdc, with overvoltage detection
8	HV	High-voltage pin	Connects to the bulk capacitor or the rectified AC line to perform the functions of Start-up Current Source, Dynamic Self-Supply and brown-out detection

### SIMPLIFIED INTERNAL BLOCK SCHEMATIC

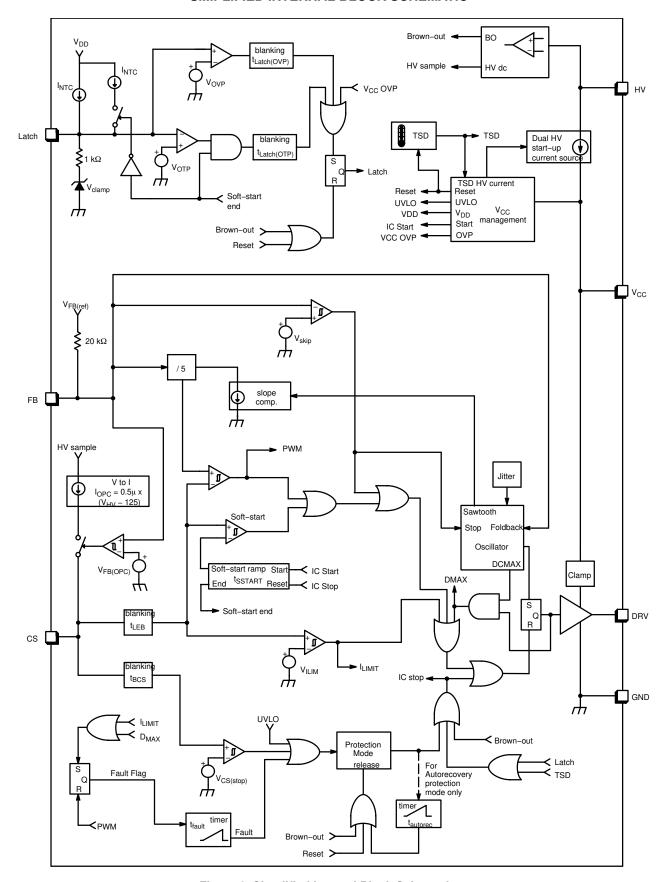


Figure 2. Simplified Internal Block Schematic

#### **MAXIMUM RATINGS**

Rating	Symbol	Value	Unit
Supply Pin (pin 6) (Note 2) Voltage range Current range	V <sub>CCMAX</sub>	-0.3 to 28 ±30	V mA
High Voltage Pin (pin 8) (Note 2) Voltage range Current range	V <sub>HVMAX</sub> I <sub>HVMAX</sub>	-0.3 to 500 ±20	V mA
Driver Pin (pin 5) (Note 2) Voltage range Current range	V <sub>DRVMAX</sub>	-0.3 to 20 ± 1000	V mA
All other pins (Note 2) Voltage range Current range	V <sub>MAX</sub> I <sub>MAX</sub>	-0.3 to 10 ±10	V mA
Thermal Resistance SOIC-7 Junction-to-Air, low conductivity PCB (Note 3) Junction-to-Air, medium conductivity PCB (Note 4) Junction-to-Air, high conductivity PCB (Note 5)	$R_{\theta J-A}$	162 147 115	°C/W
Temperature Range Operating Junction Temperature Storage Temperature Range	T <sub>JMAX</sub> T <sub>STRGMAX</sub>	-40 to +150 -60 to +150	°C
ESD Capability (Note 1) Human Body Model (All pins except HV) Machine Model		2000 200	V

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

- This device series contains ESD protection and exceeds the following tests: Human Body Model 2000 V per JEDEC standard JESD22, Method A114E Machine Model Method 200 V per JEDEC standard JESD22, Method A115A
- 2. This device contains latch-up protection and exceeds 100 mA per JEDEC Standard JESD78
- 3. As mounted on a 80 x 100 x 1.5 mm FR4 substrate with a single layer of 50 mm<sup>2</sup> of 2 oz copper traces and heat spreading area. As specified for a JEDEC 51–1 conductivity test PCB. Test conditions were under natural convection or zero air flow.
- 4. As mounted on a 80 x 100 x 1.5 mm FR4 substrate with a single layer of 100 mm<sup>2</sup> of 2 oz copper traces and heat spreading area. As specified for a JEDEC 51–2 conductivity test PCB. Test conditions were under natural convection or zero air flow.
- As mounted on a 80 x 100 x 1.5 mm FR4 substrate with a single layer of 650 mm<sup>2</sup> of 2 oz copper traces and heat spreading area. As specified for a JEDEC 51–3 conductivity test PCB. Test conditions were under natural convection or zero air flow.

### **ELECTRICAL CHARACTERISTICS**

(For typical values  $T_J = 25^{\circ}C$ , for min/max values  $T_J = -40^{\circ}C$  to  $+125^{\circ}C$ ,  $V_{HV} = 125$  V,  $V_{CC} = 11$  V unless otherwise noted)

Characteristics	Test Condition	Symbol	Min	Тур	Max	Unit
HIGH VOLTAGE CURRENT SOUR	DE					
Minimum voltage for current source operation		$V_{HV(min)}$	-	30	40	V
Current flowing out of V <sub>CC</sub> pin	$V_{CC} = 0 \text{ V} $ $V_{CC} = V_{CC(on)} - 0.5 \text{ V}$	I <sub>start1</sub> I <sub>start2</sub>	0.2 3	0.5 6	0.8 9	mA
Off-state leakage current	V <sub>HV</sub> = 500 V	I <sub>start(off)</sub>	-	25	50	μΑ
SUPPLY						
Turn-on threshold level, V <sub>CC</sub> going up HV current source stop threshold		V <sub>CC(on)</sub>	11.0	12.0	13.0	V
HV current source restart threshold		V <sub>CC(min)</sub>	9.5	10.5	11.5	V
Turn-off threshold		V <sub>CC(off)</sub>	8.5	9.5	10.5	V
Overvoltage threshold		V <sub>CC(ovp)</sub>	25	26.5	28	V
Blanking duration on $V_{CC(off)}$ and $V_{CC(ovp)}$ detection (Note 7)		t <sub>VCC(blank)</sub>	7	10	13	μS
V <sub>CC</sub> decreasing level at which the internal logic resets		V <sub>CC(reset)</sub>	3.6	5.0	6.0	V
V <sub>CC</sub> level for I <sub>START1</sub> to I <sub>START2</sub> transition		V <sub>CC(inhibit)</sub>	0.4	1.0	1.6	V
Internal current consumption (Note 6)	DRV open, $V_{FB} = 3$ V, 65 kHz DRV open, $V_{FB} = 3$ V, 100 kHz $C_{drv} = 1$ nF, $V_{FB} = 3$ V, 65 kHz $C_{drv} = 1$ nF, $V_{FB} = 3$ V, 100 kHz Off mode (skip or before start–up) Fault mode (fault or latch)	CC1  CC1  CC2  CC2  CC3  CC4	1.2 1.2 1.9 2.2 0.67 0.4	1.8 1.9 2.5 2.9 0.9 0.7	2.2 2.3 3.2 3.6 1.13 1.0	mA
BROWN-OUT			•		-	
Brown-Out thresholds	V <sub>HV</sub> going up V <sub>HV</sub> going down	V <sub>HV(start)</sub> V <sub>HV(stop)</sub>	92 79	107 92	122 105	V
Timer duration for line cycle drop-out		t <sub>HV</sub>	47	68	90	ms
OSCILLATOR						
Oscillator frequency		fosc	60 92	65 100	70 108	kHz
Maximum duty cycle		D <sub>MAX</sub>	75	80	85	%
Frequency jittering amplitude, in percentage of F <sub>OSC</sub>		A <sub>jitter</sub>	±4	±6	±8	%
Frequency jittering modulation frequency		F <sub>jitter</sub>	85	125	165	Hz
OUTPUT DRIVER				-	<u>-</u>	-
Rise time, 10% to 90 % of V <sub>CC</sub>	$V_{CC} = V_{CC(min)} + 0.2 \text{ V}, C_{DRV} = 1 \text{ nF}$	t <sub>rise</sub>	-	40	70	ns
Fall time, 90% to 10 % of V <sub>CC</sub>	$V_{CC} = V_{CC(min)} + 0.2 \text{ V}, C_{DRV} = 1 \text{ nF}$	t <sub>fall</sub>	-	40	70	ns
Current capability	$V_{CC} = V_{CC(min)} + 0.2 \text{ V}, C_{DRV} = 1 \text{ nF}$ DRV high, $V_{DRV} = 0 \text{ V}$ DRV low, $V_{DRV} = V_{CC}$	I <sub>DRV(source)</sub> I <sub>DRV(sink)</sub>	- -	500 500	- -	mA
Clamping voltage (maximum gate voltage)	$V_{CC} = V_{CCmax} - 0.2$ V, DRV high, R <sub>DRV</sub> = 33 kΩ, C <sub>load</sub> = 220 pF	V <sub>DRV(clamp)</sub>	11	13.5	16	V

<sup>6.</sup> Internal supply current only, current in FB pin not included (current flowing in GND pin only).7. Guaranteed by design.

 $\textbf{ELECTRICAL CHARACTERISTICS} \ ( \text{continued}) \\ ( \text{For typical values } T_J = 25^{\circ}\text{C}, \text{ for min/max values } T_J = -40^{\circ}\text{C to } +125^{\circ}\text{C}, \text{ } V_{\text{HV}} = 125 \text{ V}, \text{ } V_{\text{CC}} = 11 \text{ V unless otherwise noted})$ 

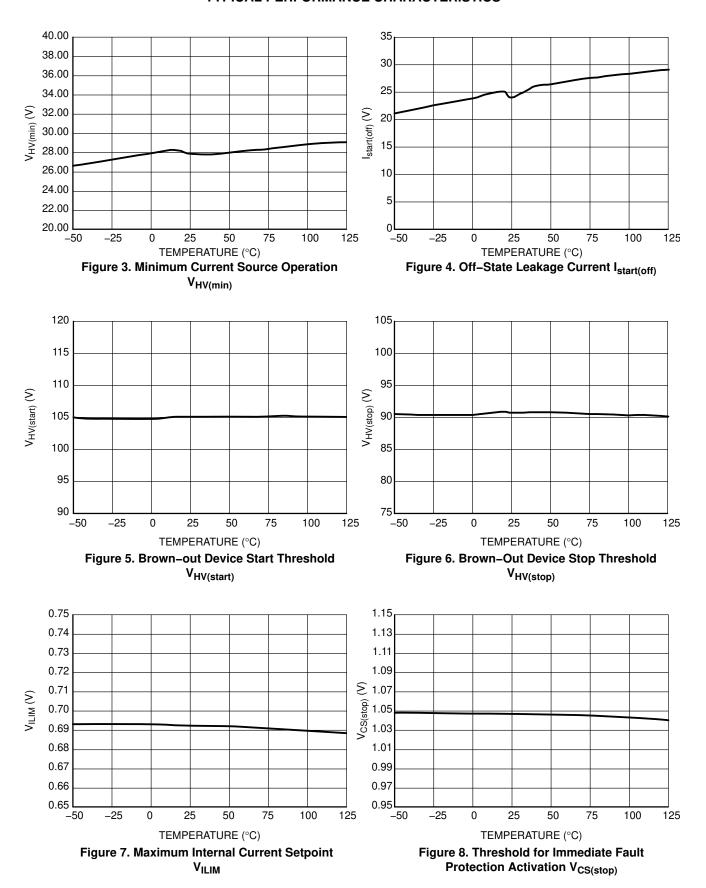
Characteristics	Test Condition	Symbol	Min	Тур	Max	Unit
OUTPUT DRIVER						
High-state voltage drop	$V_{CC}$ = $V_{CC(min)}$ + 0.2 V, $R_{DRV}$ = 33 k $\Omega$ , DRV high	V <sub>DRV(drop)</sub>	-	-	1	V
CURRENT SENSE						
Input Bias Current	V <sub>CS</sub> = 0.7 V	I <sub>bias</sub>	-	0.02	_	μΑ
Maximum internal current setpoint	V <sub>FB</sub> > 3.5 V	V <sub>ILIM</sub>	0.66	0.7	0.74	V
Propagation delay from V <sub>Ilimit</sub> detection to DRV off	V <sub>CS</sub> = V <sub>ILIM</sub>	t <sub>delay</sub>	-	80	110	ns
Leading Edge Blanking Duration for V <sub>ILIM</sub>		t <sub>LEB</sub>	190	250	310	ns
Threshold for immediate fault protection activation		V <sub>CS(stop)</sub>	0.95	1.05	1.15	V
Leading Edge Blanking Duration for V <sub>CS(stop)</sub>		t <sub>BCS</sub>	90	120	150	ns
Slope of the compensation ramp		S <sub>comp(65kHz)</sub> S <sub>comp(100kHz)</sub>	1 1	-32.5 -50		mV / μs
Soft-start duration	From 1 <sup>st</sup> pulse to V <sub>CS</sub> = V <sub>ILIM</sub>	t <sub>SSTART</sub>	2.8	4.0	5.2	ms
OVERPOWER COMPENSATION						
V <sub>HV</sub> to I <sub>OPC</sub> conversion ratio		K <sub>OPC</sub>	_	0.54	-	$\mu A / V$
Current flowing out of CS pin	V <sub>HV</sub> = 125 V V <sub>HV</sub> = 162 V V <sub>HV</sub> = 325 V V <sub>HV</sub> = 365 V	I <sub>OPC(125)</sub> I <sub>OPC(162)</sub> I <sub>OPC(325)</sub> I <sub>OPC(365)</sub>	- - - 105	0 20 110 130	- - - 150	μΑ
FB voltage above which I <sub>OPC</sub> is applied	V <sub>HV</sub> = 365 V	V <sub>FB(OPCF)</sub>	2.12	2.35	2.58	V
FB voltage below which is no I <sub>OPC</sub> applied	V <sub>HV</sub> = 365 V	V <sub>FB(OPCE)</sub>	-	2.15	-	V
Watchdog timer for dc operation		t <sub>WD(OPC)</sub>	-	32	-	ms
FEEDBACK						
Internal pull-up resistor	T <sub>J</sub> = 25°C	R <sub>FB(up)</sub>	15	20	25	kΩ
V <sub>FB</sub> to internal current setpoint division ratio		K <sub>FB</sub>	4.7	5	5.3	-
Internal pull-up voltage on the FB pin		V <sub>FB(ref)</sub>	4.3	5	5.7	V
OVERCURRENT PROTECTION	<u> </u>	I		1	<u> </u>	1
Fault timer duration	From CS reaching V <sub>ILIMIT</sub> to DRV stop	t <sub>fault</sub>	98	128	168	ms
Fault timer duration (for the C version only)	From CS reaching V <sub>ILIMIT</sub> to DRV stop	t <sub>fault</sub>	16	32	48	ms
Autorecovery mode latch-off time duration		t <sub>autorec</sub>	0.85	1.00	1.35	S
Autorecovery mode latch-off time duration (for the C version only)		t <sub>autorec</sub>	1.0	1.5	2.0	S

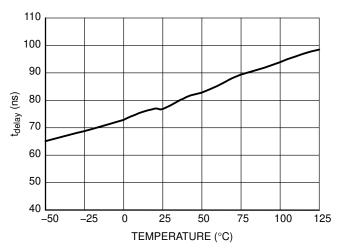
<sup>6.</sup> Internal supply current only, current in FB pin not included (current flowing in GND pin only).7. Guaranteed by design.

 $\textbf{ELECTRICAL CHARACTERISTICS} \ ( \text{continued}) \\ ( \text{For typical values } T_J = 25^{\circ}\text{C}, \text{ for min/max values } T_J = -40^{\circ}\text{C to } +125^{\circ}\text{C}, \text{ } V_{\text{HV}} = 125 \text{ V}, \text{ } V_{\text{CC}} = 11 \text{ V unless otherwise noted})$ 

Characteristics	Test Condition	Symbol	Min	Тур	Max	Unit
FREQUENCY FOLDBACK		•	ı			
Feedback voltage threshold below which frequency foldback starts		V <sub>FB(foldS)</sub>	1.8	2.0	2.2	V
Feedback voltage threshold below which frequency foldback is complete		V <sub>FB(foldE)</sub>	1.22	1.35	1.48	V
Minimum switching frequency	$V_{FB} = V_{Skip(in)} + 0.2$	f <sub>OSC(min)</sub>	22	27	32	kHz
SKIP-CYCLE MODE						
Feedback voltage thresholds for skip mode	V <sub>FB</sub> going down V <sub>FB</sub> going up	V <sub>skip(in)</sub> V <sub>skip(out)</sub>	0.63 0.72	0.7 0.80	0.77 0.88	V
LATCH-OFF INPUT						
High threshold	V <sub>Latch</sub> going up	V <sub>OVP</sub>	2.35	2.5	2.65	V
Low threshold	V <sub>Latch</sub> going down	V <sub>OTP</sub>	0.76	0.8	0.84	٧
Current source for direct NTC connection  During normal operation  During soft–start	V <sub>Latch</sub> = 0 V	I <sub>NTC</sub> I <sub>NTC(SSTART)</sub>	65 130	95 190	105 210	μΑ
Blanking duration on high latch detection	65 kHz version 100 kHz version	t <sub>Latch(OVP)</sub>	35 25	50 35	70 45	μS
Blanking duration on low latch detection		t <sub>Latch(OTP)</sub>	-	350	_	μS
Clamping voltage	I <sub>Latch</sub> = 0 mA I <sub>Latch</sub> = 1 mA	V <sub>clamp0</sub> (Latch) V <sub>clamp1</sub> (Latch)	1.0 2.0	1.2 2.4	1.4 3.0	V
TEMPERATURE SHUTDOWN			_		_	
Temperature shutdown (Note 7)	T <sub>J</sub> going up	T <sub>TSD</sub>	135	150	165	°C
Temperature shutdown hysteresis (Note 7)	T <sub>J</sub> going down	T <sub>TSD(HYS)</sub>	20	30	40	°C

<sup>6.</sup> Internal supply current only, current in FB pin not included (current flowing in GND pin only).7. Guaranteed by design.

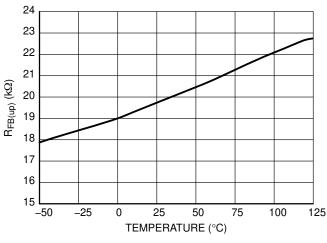




300 290 280 270 260 t<sub>LEB</sub> (ns) 250 240 230 220 210 200 25 50 75 -50 -25 0 100 125 TEMPERATURE (°C)

Figure 9. Propagation Delay t<sub>delay</sub>

Figure 10. Leading Edge Blanking Duration  $$t_{\mbox{\scriptsize LEB}}$$ 



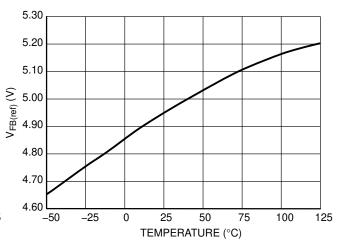
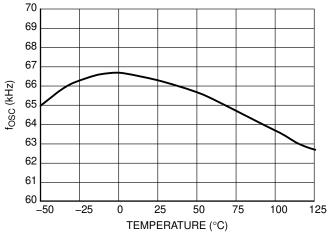


Figure 11. FB Pin Internal Pull-up Resistor  $R_{FB(up)}$ 

Figure 12. FB Pin Open Voltage V<sub>FB(ref)</sub>



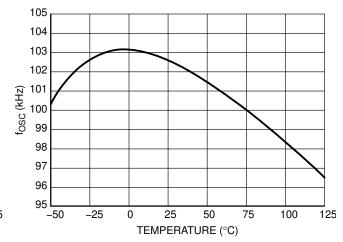


Figure 13. Oscillator Frequency f<sub>OSC</sub> for the 65 kHz version

Figure 14. Oscillator Frequency f<sub>OSC</sub> for the 100 kHz version

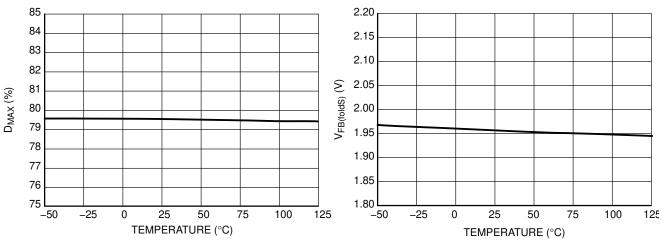


Figure 15. Maximum Duty Cycle  $D_{MAX}$ 

Figure 16. FB Pin Voltage Below Which Frequency Foldback Starts V<sub>FB(foldS)</sub>

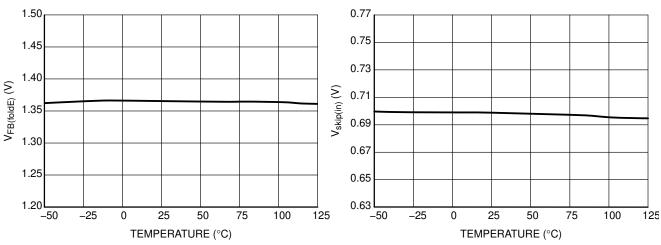


Figure 17. FB Pin Voltage Below Which Frequency Foldback is Complete  $V_{FB(foldE)}$ 

Figure 18. FB Pin Skip-in Level V<sub>skip(in)</sub>

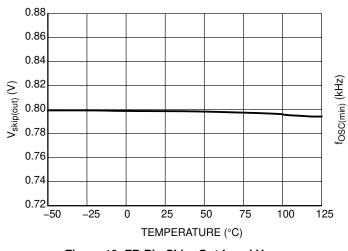


Figure 19. FB Pin Skip-Out Level V<sub>skip(out)</sub>

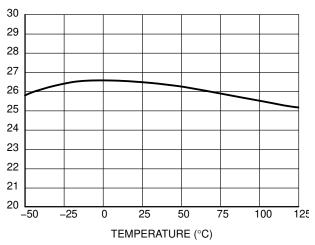
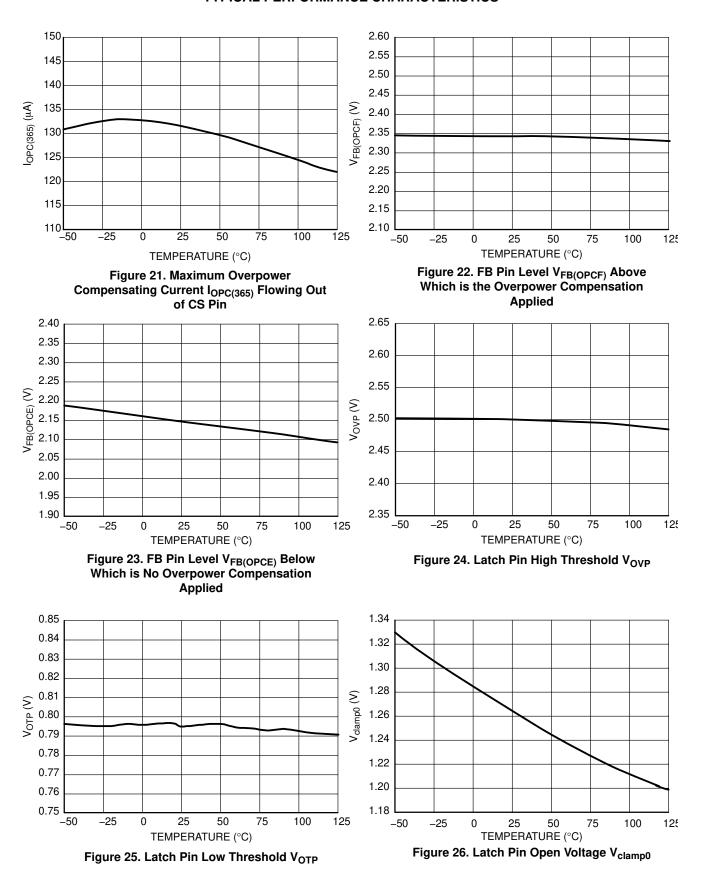
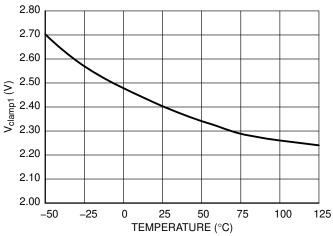


Figure 20. Minimum Switching Frequency f<sub>OSC(min)</sub>





TEMPERATURE (°C)

Figure 27. Latch Pin Voltage V<sub>clamp1</sub> (Latch-off Pin is Sinking 1 mA)

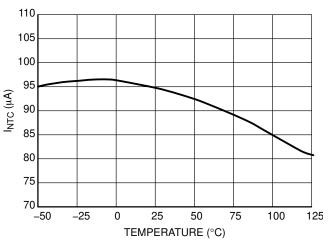


Figure 28. Current  $\rm I_{NTC}$  Sourced from the Latch Pin, Allowing Direct NTC Connection

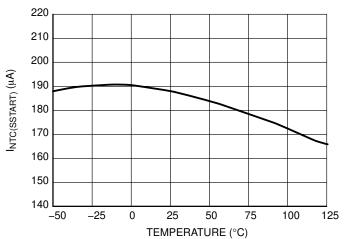


Figure 29. Current I<sub>NTC(SSTART)</sub> Sourced from the Latch Pin, During Soft-Start

#### **APPLICATION INFORMATION**

#### Introduction

The NCP1236 includes all necessary features to build a safe and efficient power supply based on a fixed–frequency flyback converter. It is particularly well suited for applications where low part count is a key parameter, without sacrificing safety.

- Current–Mode Operation with slope compensation:
  The primary peak current is permanently controlled by
  the FB voltage, ensuring maximum safety: the DRV
  turn–off event is dictated by the peak current setpoint.
  It also ensures that the frequency response of the
  system stays a first order if in DCM, which eases the
  design of the FB loop. The controller can be also used
  in CCM applications with a wide input voltage range
  thanks to its fixed ramp compensation that prevents the
  appearance of sub–harmonic oscillations.
- Fixed-Frequency Oscillator with Jittering: The NCP1236 is available in different frequency options to fit any application. The internal oscillator features a low-frequency jittering that helps passing the EMI limits by spreading out the energy content of frequency peaks in quasi-peak and average mode of measurement.
- Latched / Autorecovery Timer-Based Overload **Protection**: The overload protection depends only on the FB signal, making it able to work with any transformer, even with very poor coupling or high leakage inductance. When the fault timer elapses the device can be permanently latched in version A or the latch can be reset by an autorecovery restart of the device in version B. The power supply has to be stopped then restarted in order to resume operation, even if the overload condition disapears, in case of usage the A version of the NCP1236. The fault timer duration is internally fixed. The controller also latches off if the voltage on the CS pin reaches 1.5 times the maximum internal setpoint (allowing to detect winding short-circuits), with the same modes of releasing the latch in A or B version.
- High Voltage Start-Up Current Source with Brown-Out Detection: Due to ON Semiconductor's Very High Voltage technology, the NCP1236 can be directly connected to the high input voltage. The start-up current source ensures a clean start-up and the Dynamic Self-Supply (DSS) restarting the start-up current source to supply the controller if the V<sub>CC</sub>

- voltage transiently drops. The high voltage pin also features a high-voltage sensing circuitry, which is able to turn the controller off if the input voltage is too low (brown-out condition). This protection works either with a DC input voltage or a rectified AC input voltage, and is independent of the high voltage ripple.
- Adjustable Overpower Compensation: The high input voltage sensed on the HV pin is converted into a current to build on the current sense voltage an offset proportional to the input voltage. By choosing the value of the resistor in series with the CS pin, the amount of compensation can be adjusted to the application.
- Frequency foldback then skip mode for light load operation: In order to ensure a high efficiency under all load conditions, the NCP1236 implements a frequency foldback for light load condition and a skip mode for extremely low load condition. The switching frequency is decreased down to 27 kHz to reduce switching losses.
- Extended VCC range: The NCP1236 accepts a supply voltage as high as 28 V, with an overvoltage threshold V<sub>CC(ovp)</sub> (typically 26.5 V) that latches the controller off
- Clamped Driver Stage: Despite the high maximum supply voltage, the voltage on DRV pin is safely clamped below 16 V, allowing the use of any standard MOSFET, and reducing the current consumption of the controller.
- Dual Latch-off Input: The NCP1236 can be latched off by 2 ways: The voltage increase applied to its Latch pin (typically an overvoltage) or by a decrease this voltage. Thanks to the internal precise pull—up current source a NTC can be directly connected to the latch pin. This NTC will provide an overtemperature protection by decreasing its resistance and consequently the voltage at Latch pin,
- **Soft–Start**: At every start–up the peak current is gradually increased during 4.0 ms to minimize the stress on power components.
- Temperature Shutdown: The NCP1236 is internally protected against self-overheating: if the die temperature is too high, the controller shuts all circuitries down (including the HV start-up current source), allowing the silicon to cool down before attempting to restart. This ensures a safe behavior in case of failure.

#### **Typical Operation**

- Start-up: The HV start-up current source ensures the charging of the V<sub>CC</sub> capacitor up to the start-up threshold V<sub>CC(on)</sub>, until the input voltage is high enough (above V<sub>HV(start)</sub>) to allow the switching to start. The controller then delivers pulses, starting with a soft-start period t<sub>SSTART</sub> during which the peak current linearly increases before the current-mode control takes over. During the soft-start period, the low level latch is ignored, and the latch current is double, to ensure a fast pre-charge of the Latch pin decoupling capacitor.
- Normal operation: As long as the feedback voltage is within the regulation range and V<sub>CC</sub> is maintained above V<sub>CC(min)</sub>, the NCP1236 runs at a fixed frequency (with jittering) in current–mode control. The peak current (sensed on the CS pin) is set by the voltage on the FB pin. Fixed ramp compensation is applied internally to prevent sub–harmonic oscillations from occurring.
- **Light load operation**: When the FB voltage decreases below V<sub>FB(foldS)</sub>, typically corresponding to a load of 33 % of the maximum load (for a DCM design), the switching frequency starts to decrease down to f<sub>OSC(min)</sub>. By lowering the switching losses, this feature helps to improve the efficiency in light load conditions. The frequency jittering is enabled in light load operation as well.
- No load operation: When the FB voltage decreases below V<sub>skip(in)</sub>, typically corresponding to a load of 2 % of the maximum load, the controller enters skip mode. By completely stopping the switching while the feedback voltage is below V<sub>skip(out)</sub>, the losses are

- further reduced. This allows minimizing the power dissipation under extremely low load conditions. As the skip mode is entered at very light loads, for which the peak current is very small, there is no risk of audible noise.  $V_{CC}$  can be maintained between  $V_{CC(on)}$  and  $V_{CC(min)}$  by the DSS, if the auxiliary winding does not provide sufficient level of  $V_{CC}$  voltage under this condition
- Overload: The NCP1236 features timer-based overload detection, solely dependent on the feedback information: as soon as the internal peak current setpoint hits the V<sub>ILIM</sub> clamp, an internal timer starts to count. When the timer elapses, the controller stops and enter the protection mode, autorecovery for the B version (the controller initiates a new start-up after t<sub>autorec</sub> elapses), or latched for the A version (the latch is released if a brown-out event occurs or V<sub>CC</sub> is reset).
- **Brown–out**: The NCP1236 features a true AC line monitoring circuitry. It includes a minimum start–up threshold and an autorecovery brown–out protection; both of them independent of the ripple on the input voltage. It can even work with an unfiltered, rectified AC input. The thresholds are fixed, but they are designed to fit most of the standard AC–DC conversion applications.
- Latch-off: When the Latch input is pulled up (typically by an over-voltage condition), or pulled down (typically by an over-temperature condition, using the provided current source with an NTC), the controller latches off. A voltage higher than V<sub>CC(ovp)</sub> on the VCC pin has the same effect. The latch is released when a brown-out condition occurs, or when the V<sub>CC</sub> is reset.

#### **DETAILED DESCRIPTION**

# High-Voltage Current Source with Built-in Brown-out Detection

The NCP1236 HV pin can be connected either to the rectified bulk voltage, or to the ac line through a rectifier.

#### Start-up

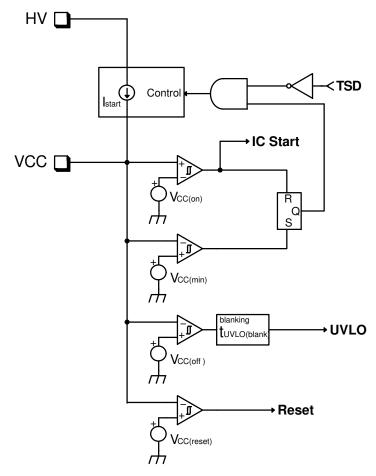


Figure 30. HV Start-up Current Source Functional Schematic

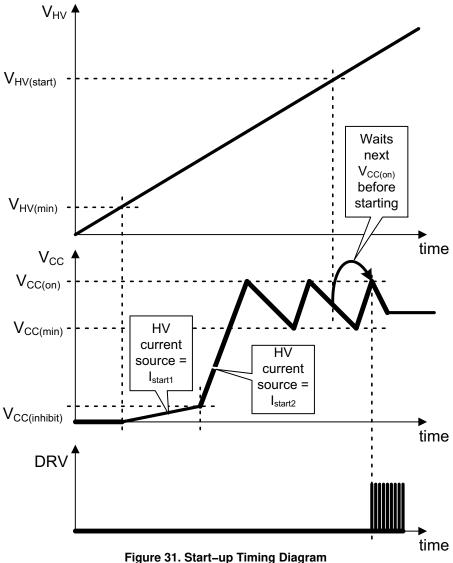
At start–up, the current source turns on when the voltage on the HV pin is higher than  $V_{HV(min)}$ , and turns off when  $V_{CC}$  reaches  $V_{CC(on)}$ , then turns on again when  $V_{CC}$  reaches  $V_{CC(min)}$ , until the input voltage is high enough to ensure a proper start–up, i.e. when  $V_{HV}$  reaches  $V_{HV(start)}$ . The controller actually starts the next time  $V_{CC}$  reaches  $V_{CC(on)}$ .

Even though the DSS is able to maintain the  $V_{CC}$  voltage between  $V_{CC(on)}$  and  $V_{CC(min)}$  by turning the HV start-up current source on and off, it can only be used in light load

condition, otherwise the power dissipation on the die would be too much. As a result, an auxiliary voltage source is needed to supply  $V_{CC}$  during normal operation.

The DSS is useful to keep the controller alive when no switching pulses are delivered, e.g. in brown–out condition, or to prevent the controller from stopping during load transients when the  $V_{CC}$  might drop.

If the voltage increases above the overvoltage protection threshold  $V_{CC(ovp)}$ , the controller is latched off.



For safety reasons, the start-up current is lowered when V<sub>CC</sub> is below V<sub>CC(inhibit)</sub>, to reduce the power dissipation in case the  $V_{CC}\,\text{pin}$  is shorted to GND (in case of  $V_{CC}\,\text{capacitor}$ failure, or external pull-down on V<sub>CC</sub> to disable the controller).

There are only two conditions for which the current source doesn't turn on when  $V_{CC}$  reaches  $V_{CC(min)}$ : the voltage on HV pin is too low (below  $V_{HV(min)}$ ), or a thermal shutdown condition (TSD) has been detected. In all other conditions, the HV current source will always turn on and off to maintain  $V_{CC}$  between  $V_{CC(min)}$  and  $V_{CC(on)}$ .

#### Brown-out protection

When the input voltage goes below V<sub>HV(stop)</sub>, a brown-out condition is detected, and the controller stops. The HV current source alternatively turns on and off to maintain  $V_{CC}$  between  $V_{CC(on)}$  and  $V_{CC(min)}$  until the input voltage is back above  $V_{HV(start)}$ .

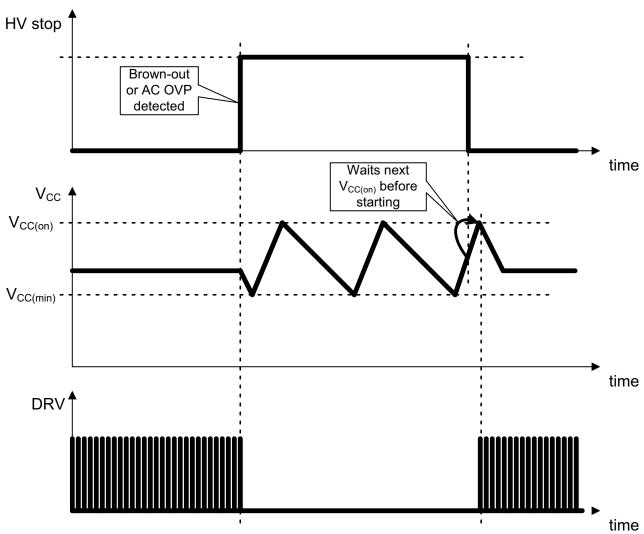


Figure 32. Brown-out Timing Diagram

When  $V_{HV}$  crosses the  $V_{HV(start)}$  threshold, the controller can start immediately. When it crosses  $V_{HV(stop)}$ , it triggers

a timer of duration  $t_{HV}$ : this ensures that the controller doesn't stop in case of line cycle drop—out.

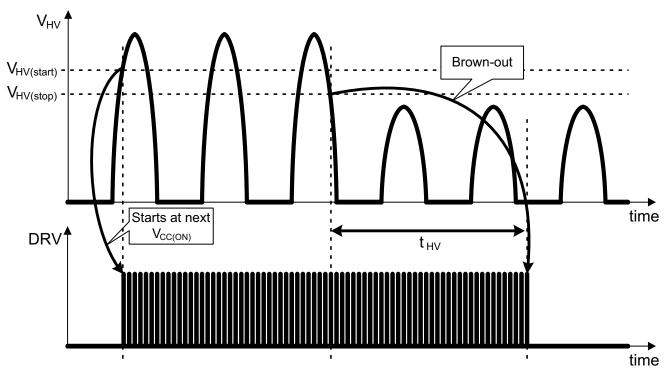


Figure 33. AC Input Brown-out Timing Diagram

#### Oscillator with Maximum Duty Cycle and Frequency Jittering

The NCP1236 includes an oscillator that sets the switching frequency with an accuracy of  $\pm 7\%$ . Two frequency options can be ordered: 65 kHz and 100 kHz. The maximum duty cycle of the DRV pin is 80%, with an accuracy of  $\pm 7\%$ .

In order to improve the EMI signature, the switching frequency jitters  $\pm 6\%$  around its nominal value, with a triangle—wave shape and at a frequency of 125 Hz. This frequency jittering is active even when the frequency is decreased to improve the EMI in light load condition.

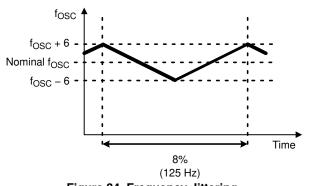


Figure 34. Frequency Jittering

#### **Clamped Driver**

The supply voltage for the NCP1236 can be as high as 28 V, but most of the MOSFETs that will be connected to the DRV pin cannot accept more than 20 V on their gate. The driver pin is therefore clamped safely below 16 V. This driver has a typical current capability of  $\pm 500$  mA.

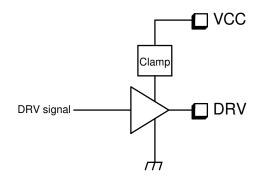


Figure 35. Clamped Driver

#### CURRENT-MODE CONTROL WITH OVERPOWER COMPENSATION AND SOFT-START

#### **Current sensing**

NCP1236 is a current—mode controller, which means that the FB voltage sets the peak current flowing in the inductance and the MOSFET. This is done through a PWM comparator: the current is sensed across a resistor and the resulting voltage is applied to the CS pin. It is applied to one input of the PWM comparator through a 250 ns LEB block. On the other input the FB voltage divided by 5 sets the threshold: when the voltage ramp reaches this threshold, the output driver is turned off.

The maximum value for the current sense is 0.7 V, and it is set by a dedicated comparator.

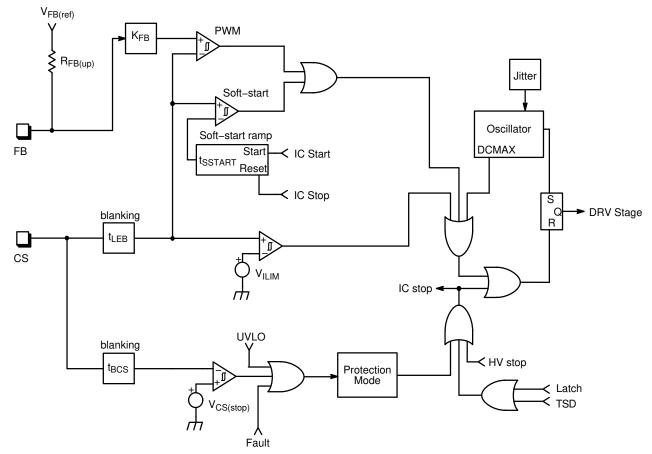


Figure 36. Current Sense Block Schematic

Each time the controller is starting, i.e. the controller was off and starts – or restarts – when  $V_{CC}$  reaches  $V_{CC(on)}$ , a soft–start is applied: the current sense setpoint is linearly increased from 0 (the minimum level can be higher than 0 because of the LEB and propagation delay) until it reaches  $V_{ILIM}$  (after a duration of  $t_{SSTART}$ ), or until the FB loop

imposes a setpoint lower than the one imposed by the soft–start (the 2 comparators outputs are OR'ed). The soft–start ramp signal is generated by the D/A converter in the NCP1236, that's why there are observable 15 discrete steps instead the truly linearly increasing current setpoint ramp.

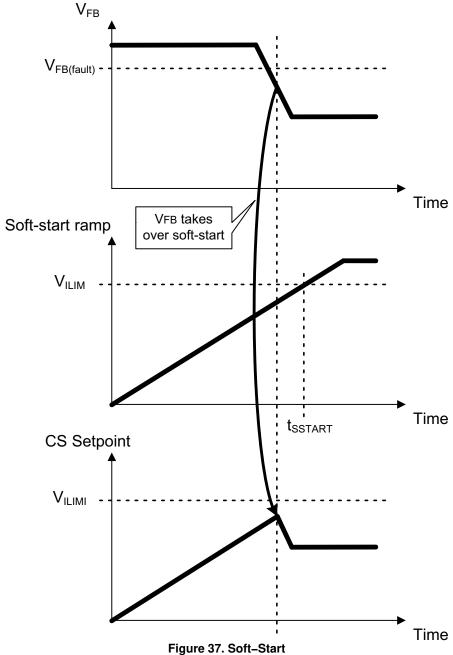


Figure 37. Soft-Start

Under some conditions, like a winding short–circuit for instance, not all the energy stored during the on time is transferred to the output during the off time, even if the on time duration is at its minimum (imposed by the propagation delay of the detector added to the LEB duration). As a result, the current sense voltage keeps on increasing above  $V_{ILIM}$ , because the controller is blind during the LEB blanking time. Dangerously high current can grow in the system if nothing is done to stop the controller. That's what the additional comparator, that senses when the current sense voltage on CS pin reaches  $V_{CS(stop)}$  (= 1.5 x  $V_{ILIM}$ ), does: as soon as this comparator toggles, the controller immediately enters the protection mode (latched or autorecovery according to the chosen option).

#### Overpower compensation

The power delivered by a flyback power supply is proportional to the square of the peak current in the discontinuous conduction mode:

$$P_{OUT} = \frac{1}{2} \cdot \eta \cdot L_p \cdot F_{SW} \cdot I_p^2 \qquad (eq. 1)$$

Unfortunately, due to the inherent propagation delay of the logic, the actual peak current is higher at high input voltage than at low input voltage, leading to a significant difference in the maximum output power delivered by the power supply.

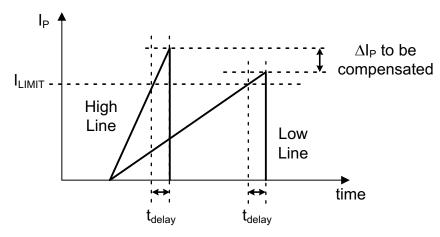


Figure 38. Line Compensation for True Overpower Protection

To compensate this and have an accurate overpower protection, an offset proportional to the input voltage is added on the CS signal by turning on an internal current source: by adding an external resistor in series between the sense resistor and the CS pin, a voltage offset is created across it by the current. The compensation can be adjusted by changing the value of the resistor.

But this offset is unwanted to appear when the current sense signal is small, i.e. in light load conditions, where it would be in the same order of magnitude. Therefore the compensation current is only added when the FB voltage is higher than  $V_{FB(OPCE)}$ .

However, because the HV pin can be connected to an ac voltage, there is needed an additional circuitry to read or at least closely estimate the actual voltage on the bulk capacitor.

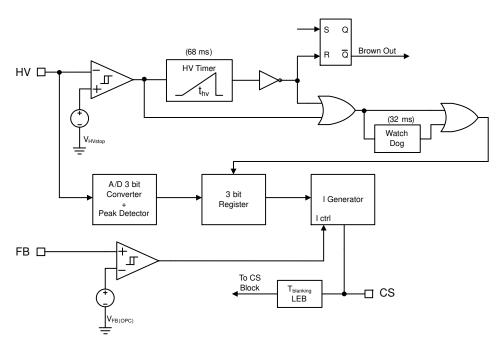


Figure 39. Schematic Overpower Compensation Circuit

A 3 bit A/D converter with the peak detector senses the ac input, and its output is periodically sampled and reset, in order to follow closely the input voltage variations. The sample and reset events are given by the  $V_{HV(stop)}$  comparator used for sampling detection for the AC line

input. If only the DC high voltage input is used, no reset signal is generated by the  $V_{HV(stop)}$  condition and the 32 ms watch dog is used to generate the sampling events for sampling the DC input high voltage line.

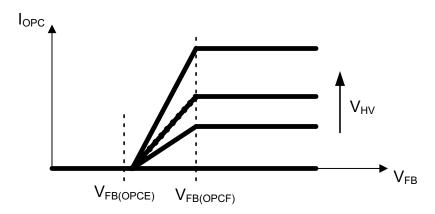


Figure 40. Overpower Compensation Current Relation to Feedback Voltage and Input Voltage

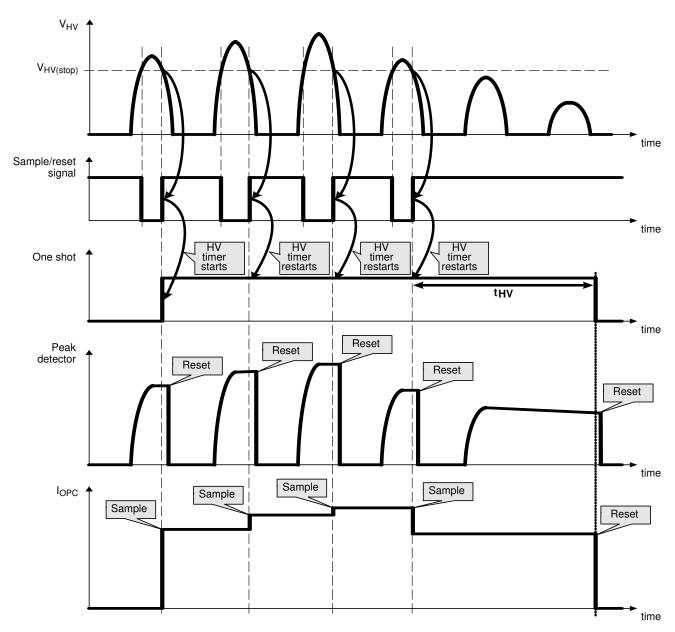


Figure 41. Overpower Compensation

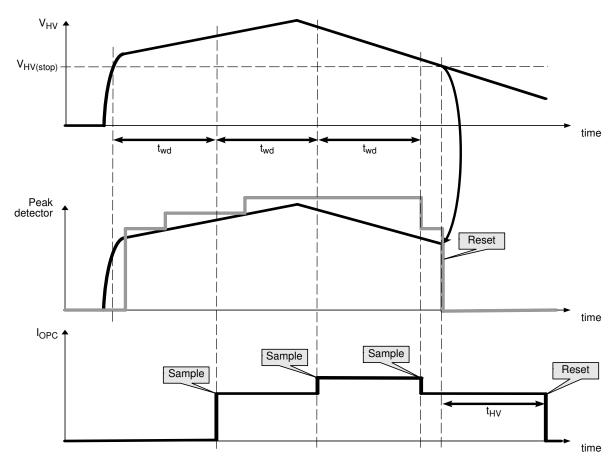


Figure 42. Overpower Compensation

#### Feedback with Slope Compensation

The ratio from the FB voltage to the current sense setpoint is 5, meaning that the FB voltage corresponding to  $V_{ILIM}$  is

3.5 V. There is a pull–up resistor of  $20~k\Omega$  from FB pin to an internal reference.

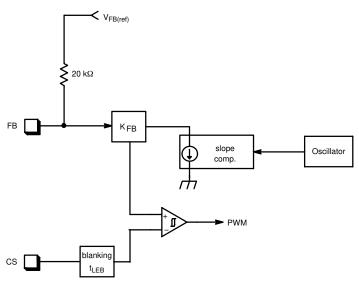


Figure 43. FB Circuitry

In order to allow the NCP1236 to operate in CCM with a duty cycle above 50 %, a fixed slope compensation is internally applied to the current-mode control. The slope

appearing on the internal voltage setpoint for the PWM comparator is -32.5 mV/ $\mu$ s typical for the 65 kHz version, and -50 mV/ $\mu$ s for the 100 kHz version.

#### Overcurrent protection with Fault timer

When an overcurrent occurs on the output of the power supply, the FB loop asks for more power than the controller can deliver, and the CS setpoint reaches  $V_{\rm ILIMIT}$ . When this event occurs, an internal  $t_{fault}$  timer is started: once the timer elapsed, DRV pulses are stopped and the controller is either

latched off (latched protection, version A), or it enters an autorecovery mode (version B). The timer is reset when the CS setpoint goes back below  $V_{ILIM}$  before the timer elapses. The fault timer is also started if the driver signal is reset by the max duty cycle.

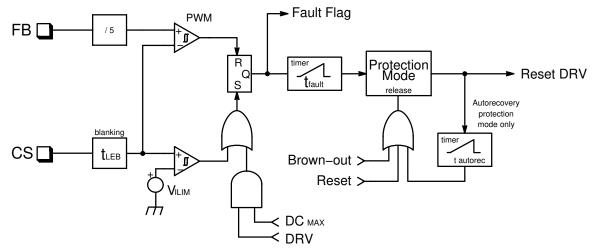
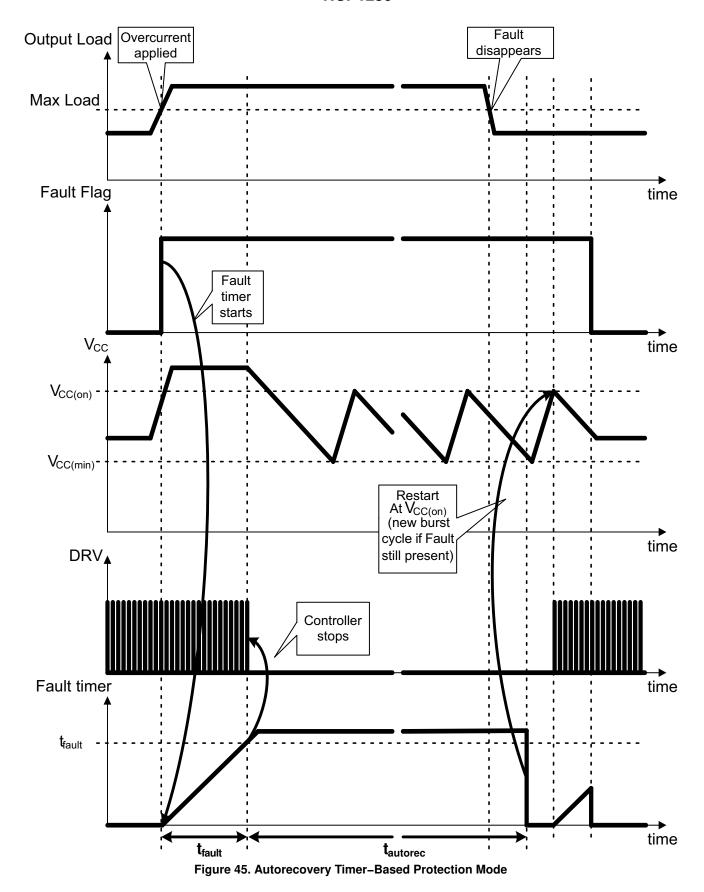


Figure 44. Timer-Based Overcurrent Protection

In autorecovery mode, the controller tries to restart after t<sub>autorec</sub>. If the fault has gone, the supply resumes operation; if not, the system starts a new burst cycle.



In the latched version, the controller can restart only if a brown–out or a  $V_{CC}$  reset occurs, which in a real application

can only happen if the power supply is unplugged from the mains line.