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# NCP81119

## Multiple-Phase Controller with SVID Interface for Desktop and Notebook CPU Applications

The NCP81119 Multi-Phase buck solution is optimized for Intel® VR12.5 compatible CPUs with user configurations of 4/3/2/1 phases. The controller combines true differential voltage sensing, differential inductor DCR current sensing, input voltage feed-forward, and adaptive voltage positioning to provide accurately regulated power for both Desktop and Notebook applications. The control system is based on Dual-Edge pulse-width modulation (PWM) combined with DCR current sensing providing the fastest initial response to dynamic load events at reduced system cost. It has the capability to shed to single phase during light load operation and can auto frequency scale in light load conditions while maintaining excellent transient performance.

High performance operational error amplifiers are provided to simplify compensation of the system. Patented Dynamic Reference Injection further simplifies loop compensation by eliminating the need to compromise between closed-loop transient response and Dynamic VID performance. Patented Total Current Summing provides highly accurate digital current monitoring.

### Features

- Meets Intel VR12.5 Specifications
- Current Mode Dual Edge Modulation for Fastest Initial Response to Transient Loading
- High Performance Operational Error Amplifier
- Digital Soft Start Ramp
- Dynamic Reference Injection
- Accurate Total Summing Current Amplifier
- Dual High Impedance Differential Voltage and Total Current Sense Amplifiers
- Phase-to-Phase Dynamic Current Balancing
- “Lossless” DCR Current Sensing for Current Balancing
- True Differential Current Balancing Sense Amplifiers for Each Phase
- Adaptive Voltage Positioning (AVP)
- Switching Frequency Range of 280 kHz – 600 kHz
- Startup into Pre-Charged Loads While Avoiding False OVP
- Power Saving Phase Shedding
- Vin Feed Forward Ramp Slope
- Pin Programming for Internal SVID parameters
- Over Voltage Protection (OVP) & Under Voltage Protection (UVP)
- Over Current Protection (OCP)
- VR-RDY Output with Internal Delays
- These are Pb-Free Devices

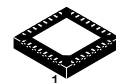
### Applications

- Desktop and Notebook Processors



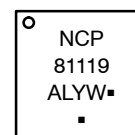
ON Semiconductor®

<http://onsemi.com>



QFN32  
CASE 510AT

### MARKING DIAGRAM



- A = Assembly Location
- L = Wafer Lot
- Y = Year
- W = Work Week
- = Pb-Free Package

(Note: Microdot may be in either location)

### ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page 26 of this data sheet.

# NCP81119

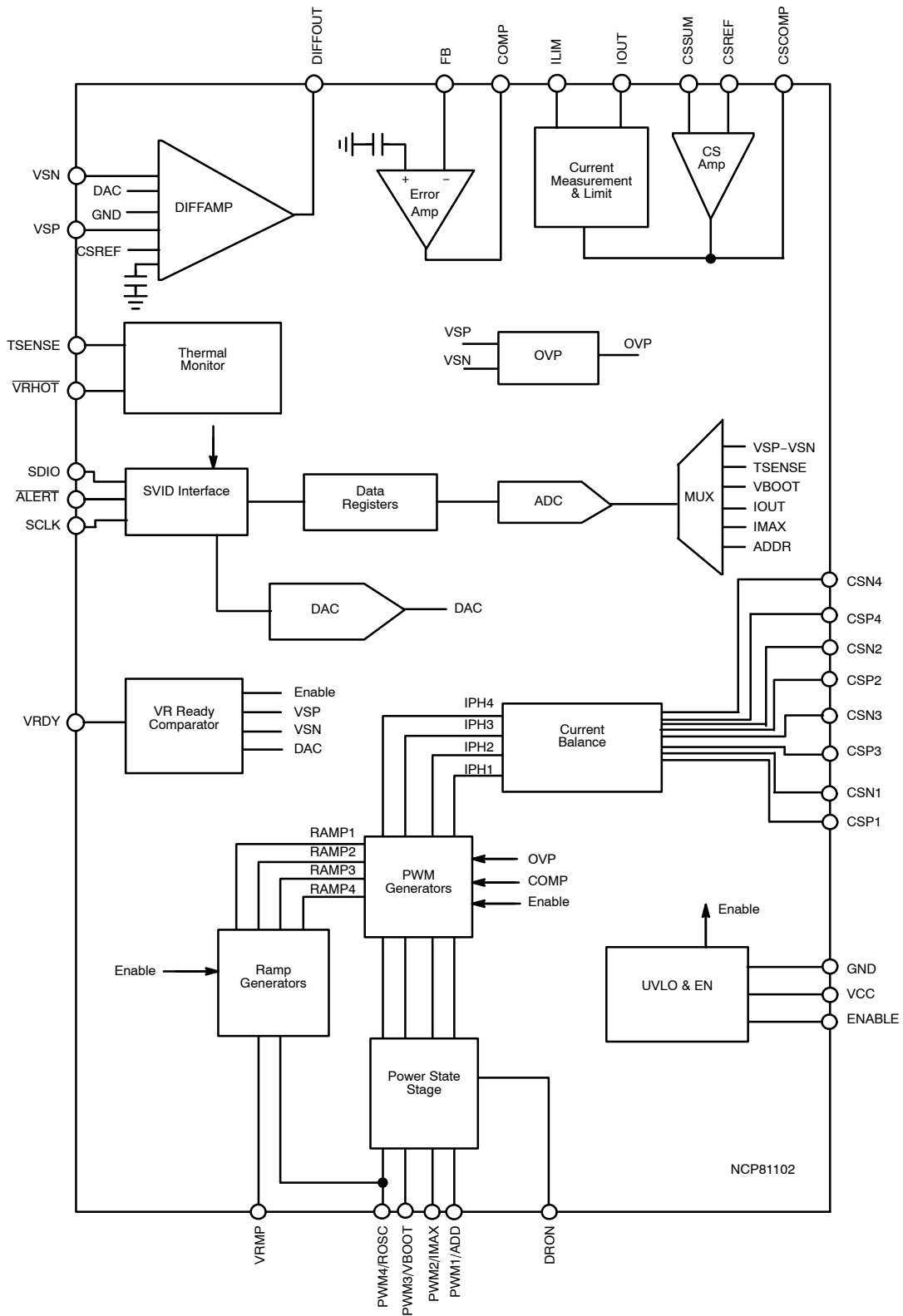
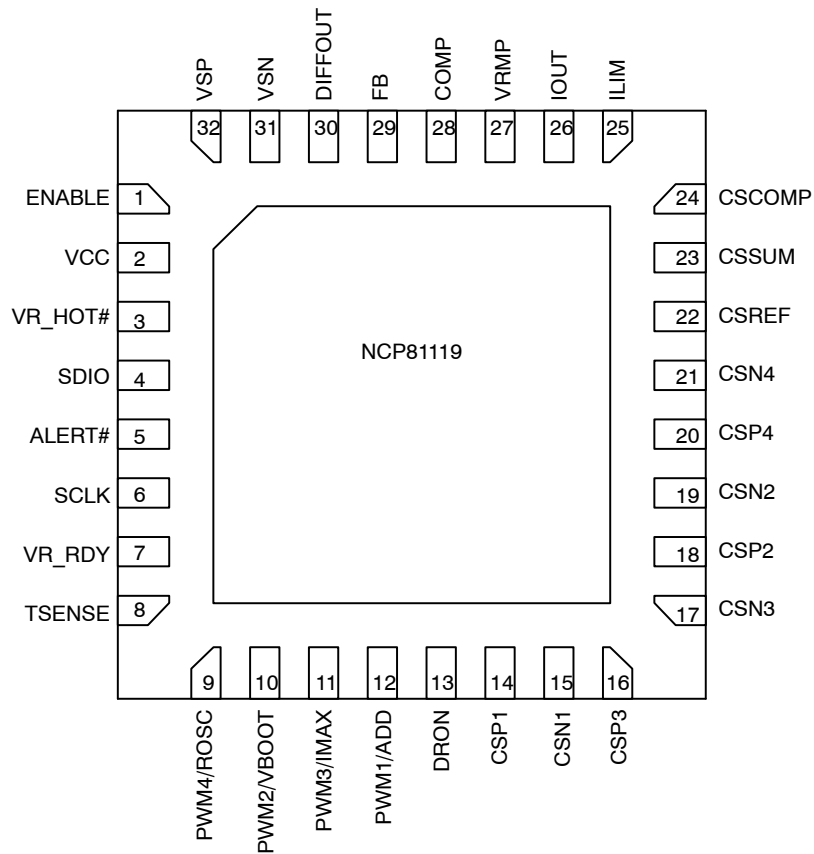


Figure 1. Block Diagram for NCP81119

# NCP81119



**Figure 2. NCP81119 Pin Configurations**

## NCP81119 PIN DESCRIPTIONS

Pin No.	Symbol	Description
1	ENABLE	Logic input. Logic high enables the output and logic low disables the output.
2	VCC	Power for the internal control circuits. A decoupling capacitor is connected from this pin to ground
3	VR_HOT#	Thermal logic output for over temperature
4	SDIO	Serial VID data interface
5	ALERT#	Serial VID ALERT#.
6	SCLK	Serial VID clock
7	VR_RDY	Open drain output. High indicates that the output is regulating
8	TSENSE	Temp Sense input for the multiphase converter
9	PWM4/ROSC	Phase 4 PWM output. A resistance from this pin to ground programs the oscillator frequency
10	PWM2/VBOOT	Phase 2 PWM output. Also as VBOOT input pin to adjust the boot-up voltage. During start up it is used to program VBOOT with a resistor to ground
11	PWM3/IMAX	Phase 3 PWM output. Also as ICC_MAX Input Pin. During start up it is used to program ICC_MAX with a resistor to ground
12	PWM1/ADD	Phase 1 PWM output. Also as Address program pin. A resistor to ground on this pin programs the SVID address of the device
13	DRON	Bidirectional gate drive enable output
14	CSP1	Non-inverting input to current balance sense amplifier for phase 1
15	CSN1	Inverting input to current balance sense amplifier for phase 1
16	CSP3	Non-inverting input to current balance sense amplifier for phase 3

# NCP81119

## NCP81119 PIN DESCRIPTIONS

Pin No.	Symbol	Description
17	CSN3	Inverting input to current balance sense amplifier for phase 3. Pull this Pin to VCC, configure as 1-phase operation
18	CSP2	Non-inverting input to current balance sense amplifier for phase 2
19	CSN2	Inverting input to current balance sense amplifier for phase 2. Pull this Pin to VCC, configure as 2-phase operation
20	CSP4	Non-inverting input to current balance sense amplifier for phase 4
21	CSN4	Inverting input to current balance sense amplifier. Pull this Pin to VCC, configure as 3-phase operation
22	CSREF	Total output current sense amplifier reference voltage input, a capacitor on this pin is used to ensure CSREF voltage signal integrity
23	CSSUM	Inverting input of total current sense amplifier
24	CSCOMP	Output of total current sense amplifier
25	ILIM	Over current shutdown threshold setting. Resistor to CSCOMP to set threshold
26	IOUT	Total output current monitor.
27	VRMP	Feed-forward input of $V_{in}$ for the ramp slope compensation. The current fed into this pin is used to control the ramp of PWM slope
28	COMP	Output of the error amplifier and the inverting inputs of the PWM comparators
29	FB	Error amplifier voltage feedback
30	DIFFOUT	Output of the differential remote sense amplifier
31	VSN	Inverting input to differential remote sense amplifier
32	VSP	Non-inverting input to the differential remote sense amplifier
33	FLAG / GND	Power supply return (QFN Flag)

# NCP81119

## ABSOLUTE MAXIMUM RATINGS

### ELECTRICAL INFORMATION

Pin Symbol	V <sub>MAX</sub>	V <sub>MIN</sub>
COMP	VCC + 0.3 V	-0.3 V
CSCOMP	VCC + 0.3 V	-0.3 V
VSN	GND + 300 mV	GND - 300 mV
DIFFOUT	VCC + 0.3 V	-0.3 V
VR_RDY	VCC + 0.3 V	-0.3 V
VCC	6.5 V	-0.3 V
IOUT	2.0 V	-0.3 V
VRMP	+25 V	-0.3 V
All Other Pins	VCC + 0.3 V	-0.3 V

\*All signals referenced to GND unless noted otherwise.

### THERMAL INFORMATION

Description	Symbol	Typ	Unit
Thermal Characteristic QFN Package (Note 1)	R <sub>θJA</sub>	68	°C/W
Operating Junction Temperature Range (Note 2)	T <sub>J</sub>	-10 to 125	°C
Operating Ambient Temperature Range		-10 to 100	°C
Maximum Storage Temperature Range	T <sub>STG</sub>	-40 to +150	°C
Max Power Dissipation	P <sub>d</sub>	110 to 131	mW
Moisture Sensitivity Level QFN Package	MSL	1	

\*The maximum package power dissipation must be observed.

1. JESD 51-5 (1S2P Direct-Attach Method) with 0 LFM
2. JESD 51-7 (1S2P Direct-Attach Method) with 0 LFM

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## ELECTRICAL CHARACTERISTICS

Unless otherwise stated:  $-10^{\circ}\text{C} < T_A < 100^{\circ}\text{C}$ ;  $V_{CC} = 5\text{ V}$ ;  $C_{VCC} = 0.1\ \mu\text{F}$

Parameter	Test Conditions	Min	Typ	Max	Unit
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### ERROR AMPLIFIER

Input Bias Current	@ 1.3 V	-25		25	$\mu\text{A}$
Open Loop DC Gain	CL = 20 pF to GND, RL = 10 k $\Omega$ to GND		80		dB
Open Loop Unity Gain Bandwidth	CL = 20 pF to GND, RL = 10 k $\Omega$ to GND		20		MHz
Slew Rate	$\Delta V_{in} = 100\text{ mV}$ , $G = -10\text{ V/V}$ , $\Delta V_{out} = 1.5\text{ V} - 2.5\text{ V}$ , CL = 20 pF to GND, DC Load = 10k to GND		20		V/ $\mu\text{s}$
Maximum Output Voltage	I <sub>SOURCE</sub> = 2.0 mA	3.5			V
Minimum Output Voltage	I <sub>SINK</sub> = 2.0 mA			1	V

### DIFFERENTIAL SUMMING AMPLIFIER

Input Bias Current	VSP, VSN = 1.3 V	-15		15	$\mu\text{A}$
VSP Input Voltage Range		-0.3		3.0	V
VSN Input Voltage Range		-0.3		0.3	V
-3dB Bandwidth	CL = 20 pF to GND, RL = 10 k $\Omega$ to GND		10		MHz
Closed Loop DC gain	VS+ to VS- = 0.5 to 1.3 V		1.0		V/V

### CURRENT SUMMING AMPLIFIER

Offset Voltage (Vos)		-300		300	$\mu\text{V}$
Input Bias Current	CSSUM = CSREF = 1 V	-10		10	$\mu\text{A}$
Open Loop Gain			80		dB
Current Sense Unity Gain Bandwidth	C <sub>L</sub> = 20 pF to GND, R <sub>L</sub> = 10 k $\Omega$ to GND		10		MHz

### CURRENT BALANCE AMPLIFIER

Maximum CSCOMP Output Voltage	I <sub>source</sub> = 2 mA	3.5			V
Minimum CSCOMP Output Voltage	I <sub>sink</sub> = 500 $\mu\text{A}$			0.1	V
Input Bias Current	CSP <sub>1-4</sub> = CSN <sub>1-4</sub> = 1.2	-50		50	nA
Common Mode Input Voltage Range	CSPx = CSNx	0		2.3	V
Differential Mode Input Voltage Range	CSNx = 1.2 V	-100		100	mV
Input Offset Voltage Matching	CSPx = CSNx = 1.2 V, Measured from the average	-1.5		1.5	mV
Current Sense Amplifier Gain	0 V < CSPx - CSNx < 0.1 V,	5.7	6.0	6.3	V/V
Multiphase Current Sense Gain Matching	CSP - CSN = 10 mV to 30 mV	-3		3	%
-3dB Bandwidth			8		MHz

### INPUT SUPPLY

Supply Voltage Range		4.75		5.25	V
VCC Quiescent Current	EN = high, PS0,1,2 Mode		25		mA
	EN = high, PS3 Mode		15		mA
	EN = low		30		$\mu\text{A}$

3. Guaranteed by design or characterization data, not in production test.

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## ELECTRICAL CHARACTERISTICS

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Parameter	Test Conditions	Min	Typ	Max	Unit
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### INPUT SUPPLY

UVLO Threshold	VCC rising			4.5	V
	VCC falling	4			V
VCC UVLO Hysteresis			160		mV
UVLO Threshold	VRMP rising			4.2	V
	VRMP failing	3			V

### DAC SLEW RATE

Soft Start Slew Rate			5		mv/ $\mu\text{s}$
Slew Rate Slow			5		mv/ $\mu\text{s}$
Slew Rate Fast			20		mv/ $\mu\text{s}$

### ENABLE INPUT

Enable High Input Leakage Current	External 1k pull-up to 3.3 V			1.0	$\mu\text{A}$
Upper Threshold	$V_{\text{UPPER}}$	0.8			V
Lower Threshold	$V_{\text{LOWER}}$			0.3	V
Total Hysteresis	$V_{\text{UPPER}} - V_{\text{LOWER}}$		90		mV
Enable Delay Time	Measure time from Enable transitioning HI to when DRON goes high			5	ms

### DRON

Output High Voltage	Sourcing 500 $\mu\text{A}$	3.0			V
Output Low Voltage	Sinking 500 $\mu\text{A}$			0.1	V
Rise Time	CL (PCB) = 20 pF, $\Delta V_o = 10\%$ to 90%		156		ns
Fall Time			55		ns
Internal Pull Down Resistance	EN = Low		70		k $\Omega$

### IOUT OUTPUT

Input Referred Offset Voltage	Ilimit to CSREF	-1.75		1.75	mV
Output Source Current	Ilimit sink current = 80 $\mu\text{A}$			850	$\mu\text{A}$
Current Gain	$(I_{\text{OUT CURRENT}}) / (I_{\text{LIMIT CURRENT}})$ , $R_{\text{LIM}} = 20\text{k}$ , $R_{\text{IOUT}} = 5.0\text{k}$ , DAC = 0.8 V, 1.25 V, 1.52 V	9.5	10	10.5	

### OSCILLATOR

Switching Frequency Range		280		600	KHz
4 Phase Operation				600	kHz

### OUTPUT OVER VOLTAGE & UNDER VOLTAGE PROTECTION (OVP & UVP)

Absolute Over Voltage Threshold During Soft Start	CSREF	2.8	2.9	3	V
Over Voltage Threshold Above DAC	VSP rising	350	400	425	mV
Over Voltage Delay	VSP rising to PWMx low		50		ns
Under Voltage	Ckt in development		300		mV
Under-voltage Delay	Ckt in development		5		$\mu\text{s}$

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## ELECTRICAL CHARACTERISTICS

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Parameter	Test Conditions	Min	Typ	Max	Unit
<b>VR12.5 DAC</b>					
System Voltage Accuracy	$(-10^{\circ}\text{C} - +85^{\circ}\text{C})$ $1.5\text{ V} \leq \text{DAC} < 2.3\text{ V}$ $1.0\text{ V} < \text{DAC} < 1.49\text{ V}$ $0.5\text{ V} < \text{DAC} < 0.99\text{ V}$	-0.5 -8 -10		0.5 8 +10	% mV mV

## OVERCURRENT PROTECTION

ILIM Threshold Current (OCP shutdown after 50 $\mu\text{s}$ delay)	(PS0) $R_{lim} = 20\text{k}$	9.0	10	11.0	$\mu\text{A}$
ILIM Threshold Current (immediate OCP shutdown)	(PS0) $R_{lim} = 20\text{k}$	13.5	15	16.5	$\mu\text{A}$
ILIM Threshold Current (OCP shutdown after 50 $\mu\text{s}$ delay)	(PS1, PS2, PS3) $R_{lim} = 20\text{k}$ , N = number of phases in PS0 mode		10/N		$\mu\text{A}$
ILIM Threshold Current (immediate OCP shutdown)	(PS1, PS2, PS3) $R_{lim} = 20\text{k}$ , N = number of phases in PS0 mode		15/N		$\mu\text{A}$

## MODULATORS (PWM Comparators)

0% Duty Cycle	COMP voltage when the PWM outputs remain LO		1.3		V
100% Duty Cycle	COMP voltage when the PWM outputs remain HI $VRMP = 12.0\text{ V}$		2.5		V
PWM Ramp Duty Cycle Matching	COMP = 2 V, PWM Ton matching		1		%
PWM Phase Angle Error	Between adjacent phases at $25^{\circ}$		5		deg
Ramp Feed-forward Voltage range		5		20	V

## VR\_HOT#

Output Low Voltage	$I_{VRHOT} = -4\text{ mA}$			0.3	V
Output Leakage Current	High Impedance State	-1.0		1.0	$\mu\text{A}$

## TSENSE

Alert# Assert Threshold			491		mV
Alert# De-assert Threshold			513		mV
VRHOT Assert Threshold			472		mV
VRHOT Rising Threshold			494		mV
TSENSE Bias Current		115	120	125	$\mu\text{A}$

## ADC

Voltage Range		0		2	V
Total Unadjusted Error (TUE)		-1		+1	%
Differential Nonlinearity (DNL)	8-bit			1	LSB
Power Supply Sensitivity			$\pm 1$		%
Conversion Time			30		$\mu\text{s}$
Round Robin			90		$\mu\text{s}$

## VR\_RDY, (Power Good) OUTPUT

Output Low Saturation Voltage	$I_{VR_RDY} = 4\text{ mA}$			0.3	V
Rise Time	External pull-up of 1 k $\Omega$ to 3.3 V, $C_{TOT} = 45\text{ pF}$ , $\Delta V_o = 10\%$ to 90%		100		ns
Fall Time	External pull-up of 1 k $\Omega$ to 3.3 V, $C_{TOT} = 45\text{ pF}$ , $\Delta V_o = 90\%$ to 10%		10		ns
Output Voltage at Power-up	VR_RDY pulled up to 5 V via 2 k $\Omega$		1.0		V

3. Guaranteed by design or characterization data, not in production test.

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## ELECTRICAL CHARACTERISTICS

Unless otherwise stated:  $-10^{\circ}\text{C} < T_A < 100^{\circ}\text{C}$ ;  $V_{CC} = 5\text{ V}$ ;  $C_{VCC} = 0.1\ \mu\text{F}$

Parameter	Test Conditions	Min	Typ	Max	Unit
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### VR\_RDY, (Power Good) OUTPUT

Output Leakage Current When High	VR_RDY = 5.0 V	-1.0		1.0	$\mu\text{A}$
VR_RDY Delay (rising)	DAC=TARGET to VR_RDY		5		$\mu\text{s}$
VR_RDY Delay (falling)	From OCP or OVP		5		$\mu\text{s}$

### PWM OUTPUTS

Output High Voltage	Sourcing 500 $\mu\text{A}$	$V_{CC} - 0.2\text{V}$	-	-	V
Output Mid Voltage	No Load, SetPS = 02	1.9	2.0	2.1	V
Output Low Voltage	Sinking 500 $\mu\text{A}$			0.7	V
Rise and Fall Time	CL (PCB) = 50 pF, $\Delta V_o = \text{GND to } V_{CC}$		10		ns

### PHASE DETECTION

CSN Pin Threshold Voltage			4.5		V
Phase Detect Timer			50		$\mu\text{s}$

### SCLK, SDIO

$V_{IL}$	Input Low Voltage			0.45	V
$V_{IH}$	Input Voltage High including hysteresis	0.72			V
$V_{OH}$	Output High Voltage		1.05		V
$V_{OL}$	SDA, ALERT# and VRHOT			0.3	$\Omega$
Leakage Current		-100		100	$\mu\text{A}$
Pad Capacitance (Note 3)				4.0	pF
VR clock to data delay (Tco) (Note 3)		4		8.3	ns
Setup time (Tsu) (Note 3)		7			ns
Hold time (Thld) (Note 3)		14			ns

3. Guaranteed by design or characterization data, not in production test.

**Table 1. VR12.5 VID CODES**

VID7	VID6	VID5	VID4	VID3	VID2	VID1	VID0	Voltage (V)	HEX
0	0	0	0	0	0	0	0	OFF	00
0	0	0	0	0	0	0	1	0.5	01
0	0	0	0	0	0	1	0	0.51	02
0	0	0	0	0	0	1	1	0.52	03
0	0	0	0	0	1	0	0	0.53	04
0	0	0	0	0	1	0	1	0.54	05
0	0	0	0	0	1	1	0	0.55	06
0	0	0	0	0	1	1	1	0.56	07
0	0	0	0	1	0	0	0	0.57	08
0	0	0	0	1	0	0	1	0.58	09
0	0	0	0	1	0	1	0	0.59	0A
0	0	0	0	1	0	1	1	0.60	0B

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**Table 1. VR12.5 VID CODES**

VID7	VID6	VID5	VID4	VID3	VID2	VID1	VID0	Voltage (V)	HEX
0	0	0	0	1	1	0	0	0.61	0C
0	0	0	0	1	1	0	1	0.62	0D
0	0	0	0	1	1	1	0	0.63	0E
0	0	0	0	1	1	1	1	0.64	0F
0	0	0	1	0	0	0	0	0.65	10
0	0	0	1	0	0	0	1	0.66	11
0	0	0	1	0	0	1	0	0.67	12
0	0	0	1	0	0	1	1	0.68	13
0	0	0	1	0	1	0	0	0.69	14
0	0	0	1	0	1	0	1	0.70	15
0	0	0	1	0	1	1	0	0.71	16
0	0	0	1	0	1	1	1	0.72	17
0	0	0	1	1	0	0	0	0.73	18
0	0	0	1	1	0	0	1	0.74	19
0	0	0	1	1	0	1	0	0.75	1A
0	0	0	1	1	0	1	1	0.76	1B
0	0	0	1	1	1	0	0	0.77	1C
0	0	0	1	1	1	0	1	0.78	1D
0	0	0	1	1	1	1	0	0.79	1E
0	0	0	1	1	1	1	1	0.80	1F
0	0	1	0	0	0	0	0	0.81	20
0	0	1	0	0	0	0	1	0.82	21
0	0	1	0	0	0	1	0	0.83	22
0	0	1	0	0	0	1	1	0.84	23
0	0	1	0	0	1	0	0	0.85	24
0	0	1	0	0	1	0	1	0.86	25
0	0	1	0	0	1	1	0	0.87	26
0	0	1	0	0	1	1	1	0.88	27
0	0	1	0	1	0	0	0	0.89	28
0	0	1	0	1	0	0	1	0.9	29
0	0	1	0	1	0	1	0	0.91	2A
0	0	1	0	1	0	1	1	0.92	2B
0	0	1	0	1	1	0	0	0.93	2C
0	0	1	0	1	1	0	1	0.94	2D
0	0	1	0	1	1	1	0	0.95	2E
0	0	1	0	1	1	1	1	0.96	2F
0	0	1	1	0	0	0	0	0.97	30
0	0	1	1	0	0	0	1	0.98	31
0	0	1	1	0	0	1	0	0.99	32
0	0	1	1	0	0	1	1	1	33
0	0	1	1	0	1	0	0	1.01	34

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**Table 1. VR12.5 VID CODES**

VID7	VID6	VID5	VID4	VID3	VID2	VID1	VID0	Voltage (V)	HEX
0	0	1	1	0	1	0	1	1.02	35
0	0	1	1	0	1	1	0	1.03	36
0	0	1	1	0	1	1	1	1.04	37
0	0	1	1	1	0	0	0	1.05	38
0	0	1	1	1	0	0	1	1.06	39
0	0	1	1	1	0	1	0	1.07	3A
0	0	1	1	1	0	1	1	1.08	3B
0	0	1	1	1	1	0	0	1.09	3C
0	0	1	1	1	1	0	1	1.1	3D
0	0	1	1	1	1	1	0	1.11	3E
0	0	1	1	1	1	1	1	1.12	3F
0	1	0	0	0	0	0	0	1.13	40
0	1	0	0	0	0	0	1	1.14	41
0	1	0	0	0	0	1	0	1.15	42
0	1	0	0	0	0	1	1	1.16	43
0	1	0	0	0	1	0	0	1.17	44
0	1	0	0	0	1	0	1	1.18	45
0	1	0	0	0	1	1	0	1.19	46
0	1	0	0	0	1	1	1	1.2	47
0	1	0	0	1	0	0	0	1.21	48
0	1	0	0	1	0	0	1	1.22	49
0	1	0	0	1	0	1	0	1.23	4A
0	1	0	0	1	0	1	1	1.24	4B
0	1	0	0	1	1	0	0	1.25	4C
0	1	0	0	1	1	0	1	1.26	4D
0	1	0	0	1	1	1	0	1.27	4E
0	1	0	0	1	1	1	1	1.28	4F
0	1	0	1	0	0	0	0	1.29	50
0	1	0	1	0	0	0	1	1.3	51
0	1	0	1	0	0	1	0	1.31	52
0	1	0	1	0	0	1	1	1.32	53
0	1	0	1	0	1	0	0	1.33	54
0	1	0	1	0	1	0	1	1.34	55
0	1	0	1	0	1	1	0	1.35	56
0	1	0	1	0	1	1	1	1.36	57
0	1	0	1	1	0	0	0	1.37	58
0	1	0	1	1	0	0	1	1.38	59
0	1	0	1	1	0	1	0	1.39	5A
0	1	0	1	1	0	1	1	1.4	5B
0	1	0	1	1	1	0	0	1.41	5C
0	1	0	1	1	1	0	1	1.42	5D

# NCP81119

**Table 1. VR12.5 VID CODES**

VID7	VID6	VID5	VID4	VID3	VID2	VID1	VID0	Voltage (V)	HEX
0	1	0	1	1	1	1	0	1.43	5E
0	1	0	1	1	1	1	1	1.44	5F
0	1	1	0	0	0	0	0	1.45	60
0	1	1	0	0	0	0	1	1.46	61
0	1	1	0	0	0	1	0	1.47	62
0	1	1	0	0	0	1	1	1.48	63
0	1	1	0	0	1	0	0	1.49	64
0	1	1	0	0	1	0	1	1.5	65
0	1	1	0	0	1	1	0	1.51	66
0	1	1	0	0	1	1	1	1.52	67
0	1	1	0	1	0	0	0	1.53	68
0	1	1	0	1	0	0	1	1.54	69
0	1	1	0	1	0	1	0	1.55	6A
0	1	1	0	1	0	1	1	1.56	6B
0	1	1	0	1	1	0	0	1.57	6C
0	1	1	0	1	1	0	1	1.58	6D
0	1	1	0	1	1	1	0	1.59	6E
0	1	1	0	1	1	1	1	1.6	6F
0	1	1	1	0	0	0	0	1.61	70
0	1	1	1	0	0	0	1	1.62	71
0	1	1	1	0	0	1	0	1.63	72
0	1	1	1	0	0	1	1	1.64	73
0	1	1	1	0	1	0	0	1.65	74
0	1	1	1	0	1	0	1	1.66	75
0	1	1	1	0	1	1	0	1.67	76
0	1	1	1	0	1	1	1	1.68	77
0	1	1	1	1	0	0	0	1.69	78
0	1	1	1	1	0	0	1	1.7	79
0	1	1	1	1	0	1	0	1.71	7A
0	1	1	1	1	0	1	1	1.72	7B
0	1	1	1	1	1	0	0	1.73	7C
0	1	1	1	1	1	0	1	1.74	7D
0	1	1	1	1	1	1	0	1.75	7E
0	1	1	1	1	1	1	1	1.76	7F
1	0	0	0	0	0	0	0	1.77	80
1	0	0	0	0	0	0	1	1.78	81
1	0	0	0	0	0	1	0	1.79	82
1	0	0	0	0	0	1	1	1.8	83
1	0	0	0	0	1	0	0	1.81	84
1	0	0	0	0	1	0	1	1.82	85
1	0	0	0	0	1	1	0	1.83	86

# NCP81119

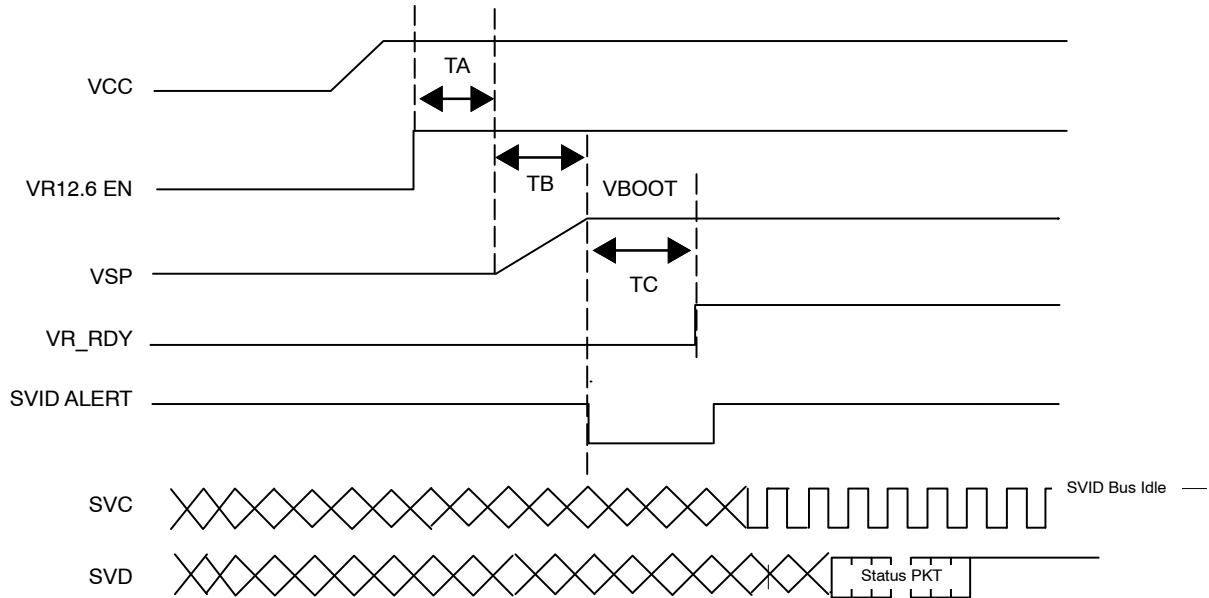
**Table 1. VR12.5 VID CODES**

VID7	VID6	VID5	VID4	VID3	VID2	VID1	VID0	Voltage (V)	HEX
1	0	0	0	0	1	1	1	1.84	87
1	0	0	0	1	0	0	0	1.85	88
1	0	0	0	1	0	0	1	1.86	89
1	0	0	0	1	0	1	0	1.87	8A
1	0	0	0	1	0	1	1	1.88	8B
1	0	0	0	1	1	0	0	1.89	8C
1	0	0	0	1	1	0	1	1.9	8D
1	0	0	0	1	1	1	0	1.91	8E
1	0	0	0	1	1	1	1	1.92	8F
1	0	0	1	0	0	0	0	1.93	90
1	0	0	1	0	0	0	1	1.94	91
1	0	0	1	0	0	1	0	1.95	92
1	0	0	1	0	0	1	1	1.96	93
1	0	0	1	0	1	0	0	1.97	94
1	0	0	1	0	1	0	1	1.98	95
1	0	0	1	0	1	1	0	1.99	96
1	0	0	1	0	1	1	1	2	97
1	0	0	1	1	0	0	0	2.01	98
1	0	0	1	1	0	0	1	2.02	99
1	0	0	1	1	0	1	0	2.03	9A
1	0	0	1	1	0	1	1	2.04	9B
1	0	0	1	1	1	0	0	2.05	9C
1	0	0	1	1	1	0	1	2.06	9D
1	0	0	1	1	1	1	0	2.07	9E
1	0	0	1	1	1	1	1	2.08	9F
1	0	1	0	0	0	0	0	2.09	A0
1	0	1	0	0	0	0	1	2.1	A1
1	0	1	0	0	0	1	0	2.11	A2
1	0	1	0	0	0	1	1	2.12	A3
1	0	1	0	0	1	0	0	2.13	A4
1	0	1	0	0	1	0	1	2.14	A5
1	0	1	0	0	1	1	0	2.15	A6
1	0	1	0	0	1	1	1	2.16	A7
1	0	1	0	1	0	0	0	2.17	A8
1	0	1	0	1	0	0	1	2.18	A9
1	0	1	0	1	0	1	0	2.19	AA
1	0	1	0	1	0	1	1	2.2	AB
1	0	1	0	1	1	0	0	2.21	AC
1	0	1	0	1	1	0	1	2.22	AD
1	0	1	0	1	1	1	0	2.23	AE
1	0	1	0	1	1	1	1	2.24	AF

# NCP81119

**Table 1. VR12.5 VID CODES**

VID7	VID6	VID5	VID4	VID3	VID2	VID1	VID0	Voltage (V)	HEX
1	0	1	1	0	0	0	0	2.25	B0
1	0	1	1	0	0	0	1	2.26	B1
1	0	1	1	0	0	1	0	2.27	B2
1	0	1	1	0	0	1	1	2.28	B3
1	0	1	1	0	1	0	0	2.29	B4
1	0	1	1	0	1	0	1	2.3	B5



**Figure 3. SVID Timing Diagram**

Description	Min	Typ	Max	Unit
$T_A^1$			5	mS
$T_B^1$			10	mV/ $\mu$ S
$T_C^1$	0		6	$\mu$ S
$T_D^1$ External Enable de-assert to recognition of de-assert	0		1	$\mu$ S
$T_E^1$ Internal Enable de-assert to VR_RDY de-assert			500	nS

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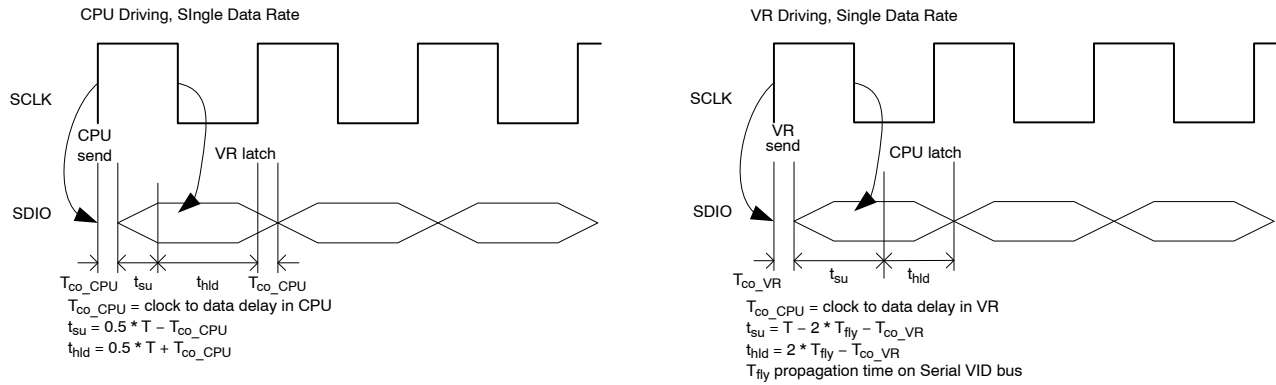


Figure 4.

## STATE TRUTH TABLE

STATE	VR_RDY Pin	Error AMP Comp Pin	OVP & UVP	DRON Pin	Method of Reset
POR $0 < VCC < UVLO$	N/A	N/A	N/A	Resistive pull down	
Disabled $EN < \text{threshold}$ $UVLO > \text{threshold}$	Low	Low	Disabled	Low	
Start up Delay & Calibration $EN > \text{threshold}$ $UVLO > \text{threshold}$	Low	Low	Disabled	Low	
DRON Fault $EN > \text{threshold}$ $UVLO > \text{threshold}$ $DRON < \text{threshold}$	Low	Low	Disabled	Resistive pull up	Driver must release DRON to high
Soft Start $EN > \text{threshold}$ $UVLO > \text{threshold}$ $DRON > \text{High}$	Low	Operational	Active / No latch	High	
Normal Operation $EN > \text{threshold}$ $UVLO > \text{threshold}$ $DRON > \text{High}$	High	Operational	Active / Latching	High	N/A
Over Voltage	Low	N/A	DAC + 150 mV	High	
Over Current	Low	Operational	Last DAC Code	Low	
VID Code = 00h	Low: if Reg34h:bit0 = 0; High: if Reg34h:bit0 = 1	Clamped at 0.9 V	Disabled	High, PWM outputs in low state	



# NCP81119

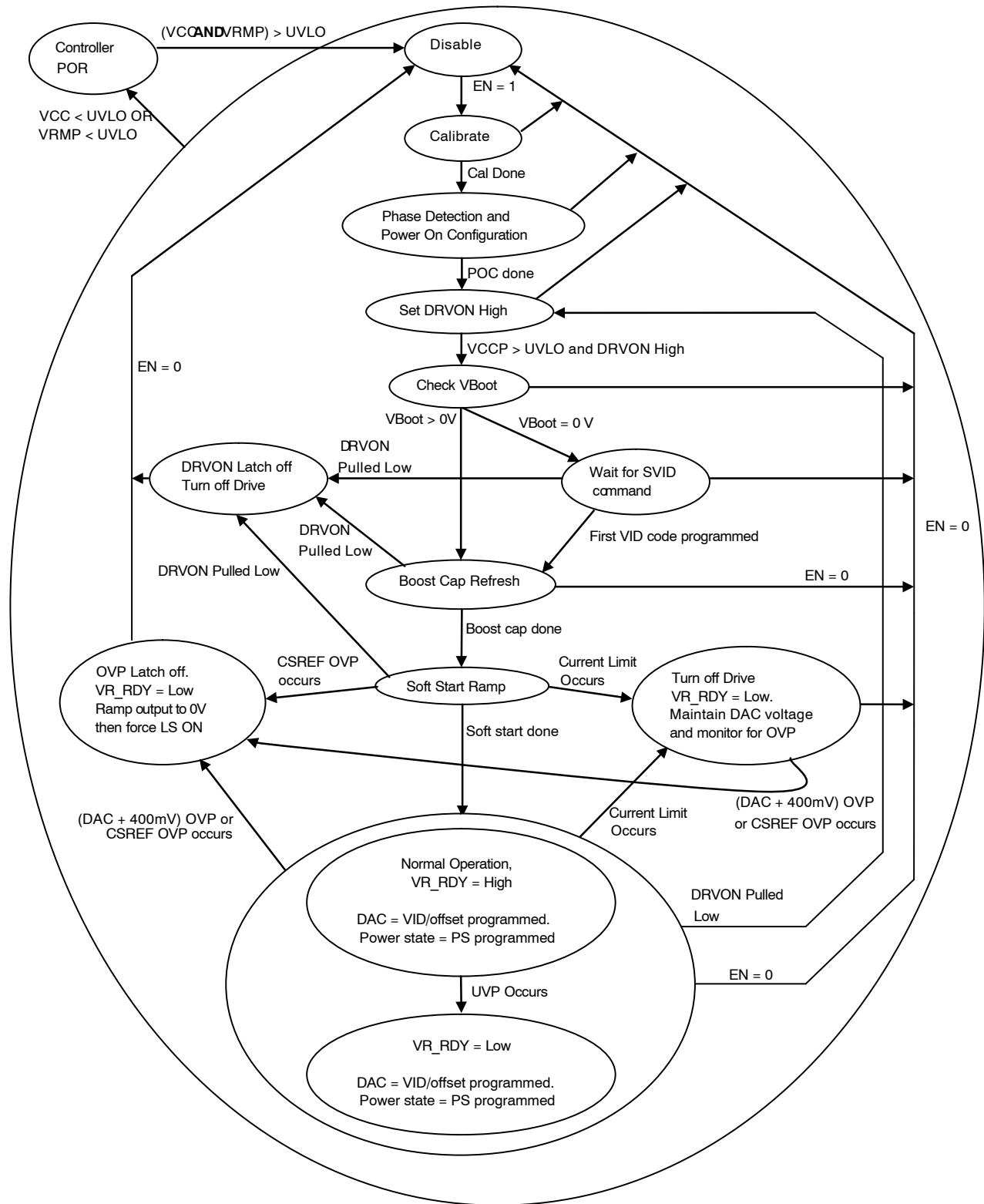


Figure 5.

# NCP81119

## General

The NCP81119 is a four phase dual edge modulated multiphase PWM controller, designed to meet the Intel VR12.5 specifications with a serial SVID control interface. The NCP81119 implements PS0, PS1, PS2 and PS3 power saving states. It is designed to work in notebook, desktop, and server applications.

Power Status	PWM Output Operating Mode
PS0	Multi-phase PWM interleaving output
PS1	Single-phase RPM CCM mode (PWM1 or PWM3, PWM2~4 stay in Mid)
PS2	Single-phase RPM DCM mode (PWM1 only, PWM2~4 stay in Mid)
PS3	Single-phase RPM DCM mode (PWM1 only, PWM2~4 stay in Mid)

## Serial VID interface (SVID)

The Serial VID Interface (SVID Interface) is a 3 wire digital interface used to transfer power management information between the CPU (Master) and the NCP81119 (Slave). The 3 wires are clock (SCLK), data (SDIO) and ALERT#. The SCLK is unidirectional and generated by the master. The SDIO is bi-directional, used for transferring data from the CPU to the NCP81119 and from the NCP81119 to the CPU. The ALERT# is an open drain output from the NCP81119 to signal to the master that the Status Register should be read.

SCLK, SDIO and ALERT# should be pulled high to CPU I/O voltage VTT (which is typically 1.0 to 1.1 V) using 55  $\Omega$  Resistors. The SVID bus will operate at a max frequency of 43 MHz.

VID code change is supported by SVID interface with three options as below:

Option	SVID Command Code	Feature	Register Address (Indicating the slew rate of VID code change)
SetVID_Fast	01h	>10 mV/ $\mu$ s VID code change slew rate	24h
SetVID_Slow	02h	=1/4 of SetVID_Fast VID code change slew rate	25h
SetVID_Decay	03h	No control, VID code down	N/A

## Serial VID

The NCP81119 supports the Intel serial VID interface. It communicates with the microprocessor through three wires (SCLK, SDIO, ALERT#). The table of supported registers is shown below.

Index	Name	Description	Access	Default
00h	Vendor ID	Uniquely identifies the VR vendor. The vendor ID assigned by Intel to ON Semiconductor is 0x1Ah	R	0x1Ah
01h	Product ID	Uniquely identifies the VR product. The VR vendor assigns this number.	R	0x12
02h	Product Revision	Uniquely identifies the revision or stepping of the VR control IC. The VR vendor assigns this data.	R	0x04
03h	Product date code ID		R	00
05h	Protocol ID	Identifies the SVID Protocol the controller supports	R	0x02
06h	Capability	<p>Informs the Master of the controller's Capabilities, 1 = supported, 0 = not supported</p> <p>Bit 7 = iout_format. Bit 7 = 0 when 1A = 1LSB of Reg 15h. Bit 7 = 1 when Reg 15 FFh = lcc_Max. Default = 1</p> <p>Bit 6 = ADC Measurement of Temp Supported = 1</p> <p>Bit 5 = ADC Measurement of Pin Supported = 0</p> <p>Bit 4 = ADC Measurement of Vin Supported = 1</p> <p>Bit 3 = ADC Measurement of Iin Supported = 0</p> <p>Bit 2 = ADC Measurement of Pout Supported = 1</p> <p>Bit 1 = ADC Measurement of Vout Supported = 1</p> <p>Bit 0 = ADC Measurement of Iout Supported = 1</p>	R	0xD7
10h	Status_1	Data register read after the ALERT# signal is asserted. Conveying the status of the VR.	R	00h

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Index	Name	Description	Access	Default
11h	Status_2	Data register showing optional status_2 data.	R	00h
12h	Temp zone	Data register showing temperature zones the system is operating in	R	00h
15h	I_out	8 bit binary word ADC of current. This register reads 0xFF when the output current is at Icc_Max	R	01h
16h	V_out	8 bit binary word ADC of output voltage, measured between VSP and VSN. LSB size is 15.5 mV	R	01h
17h	VR_Temp	8 bit binary word ADC of voltage. Binary format in deg C, IE 100C = 64h. A value of 00h indicates this function is not supported	R	01h
18h	P_out	8 bit binary word representative of output power. The output voltage is multiplied by the output current value and the result is stored in this register. A value of 00h indicates this function is not supported	R	01h
1Ah	V_in	8 bit binary word ADC of input voltage. LSB size = 110 mV.		
1Ch	Status 2 Last read	When the status 2 register is read its contents are copied into this register. The format is the same as the Status 2 Register.	R	00h
21h	Icc_Max	Data register containing the Icc_Max the platform supports. The value is measured on the ICCMAX pin on power up and placed in this register. From that point on the register is read only.	R	00h
22h	Temp_Max	Data register containing the max temperature the platform supports and the level VR_hot asserts. This value defaults to 100°C and programmable over the SVID Interface	R/W	64h
24h	SR_fast	Slew Rate for SetVID_fast commands. Binary format in mV/us.	R	0Ah
25h	SR_slow	Slew Rate for SetVID_slow commands. It is 4 times slower than the SR_fast rate. Binary format in mV/us	R	02h
26h	Vboot	The Vboot is programmed using resistors on the Vboot pin which is sensed on power up. The controller will ramp to Vboot and hold at Vboot until it receives a new SVID SetVID command to move to a different voltage.	R	00h
30h	Vout_Max	Programmed by master and sets the maximum VID the VR will support. If a higher VID code is received, the VR should respond with "not supported" acknowledge. VR 12.5 VID format.	RW	B5h
31h	VID setting	Data register containing currently programmed VID voltage. VID data format.	RW	00h
32h	Pwr State	Register containing the current programmed power state.	RW	00h
33h	Offset	Sets offset in VID steps added to the VID setting for voltage margining. Bit 7 is sign bit, 0=positive margin, 1= negative margin. Remaining 7 BITS are # VID steps for margin 2s complement. 00h = no margin 01h = +1 VID step 02h = +2 VID steps FFh = -1 VID step FEh = -2 VID steps.	RW	00h
34h	MultiVR Config			

### BOOT VOLTAGE PROGRAMMING

The NCP81119 has a Vboot voltage register that can be externally programmed. The Boot voltage for the NCP81119 is set using VBOOT pin on power up. A 10uA current is sourced from the VBoot pin and the resulting voltage is measured. This is compared with the thresholds in Table below and the corresponding value is placed in the VBoot registers (0x26). This value is set on power up and cannot be changed after the initial power up sequence is complete.

### BOOT VOLTAGE TABLE

R	VBoot	Phase Number in PS1
30.1k	0 V	1
49.9k	1.65 V	1

# NCP81119

## BOOT VOLTAGE TABLE

R	VBoot	Phase Number in PS1
69.8k	1.70 V	1
90.9k	1.75 V	1
130k	0 V	2
150k	1.65 V	2
169k	1.70 V	2
Open	1.75 V	2

## Remote Sense Amplifier

A high performance high input impedance true differential amplifier is provided to accurately sense the output voltage of the regulator. The VSP and VSN inputs should be connected to the regulator's output voltage sense points. The remote sense amplifier takes the difference of the output voltage with the DAC voltage and adds the droop voltage to

$$V_{DIFOUT} = (V_{VSP} - V_{VSN}) + (1.3 \text{ V} - V_{DAC}) + (V_{DROOP} - V_{CSREF})$$

This signal then goes through a standard error compensation network and into the inverting input of the error amplifier. The non-inverting input of the error amplifier is connected to the same 1.3 V reference used for the differential sense amplifier output bias.

## Addressing Programming

The NCP81119 supports 9 possible SVID device addresses. Pin 12 (PWM1/ADDR) is used to set the SVID address. On power up a 10uA current is sourced from this pin through a resistor connected to this pin and the resulting voltage is measured. Table below provides the resistor values for each corresponding SVID address. The address value is latched at startup.

## SVID Address Table

Missing SVID Table

Resistor Value	SVID Address
10 k	0000
22 k	0001
36 k	0010
51 k	0011
68 k	0100
91 k	0101
120 k	0110
160 k	0111
220 k	1000

## Differential Current Feedback Amplifiers

Each phase has a low offset differential amplifier to sense that phase current for current balance. The inputs to the CSN<sub>x</sub> and CSP<sub>x</sub> pins are high impedance inputs. It is recommended that any external filter resistor RCSN does not exceed 10 kΩ to avoid offset issues with leakage current. It is also recommended that the voltage sense element be no less than 0.5 mΩ for accurate current balance. Fine tuning of this time constant is generally not required. The individual phase current is summed into the PWM comparator feedback this way current is balanced via a current mode control approach.

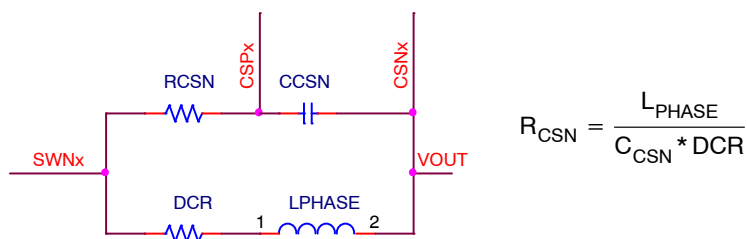


Figure 6.

**Total Current Sense Amplifier**

The NCP81119 uses a patented approach to sum the phase currents into a single temperature compensated total current signal. This signal is then used to generate the output voltage droop, total current limit, and the output current monitoring functions. The total current signal is floating with respect to CSREF. The current signal is the difference between CSCOMP and CSREF. The Ref(n) resistors sum the signals from the output side of the inductors to create a low impedance virtual ground, the capacitor is used to ensure that the CSREF voltage signal integrity. The amplifier actively filters and gains up the voltage applied across the inductors to recover the voltage drop across the inductor series resistance (DCR). Rth is placed near an inductor to sense the temperature of the inductor. This allows the filter time constant and gain to be a function of the Rth NTC resistor and compensate for the change in the DCR with temperature.

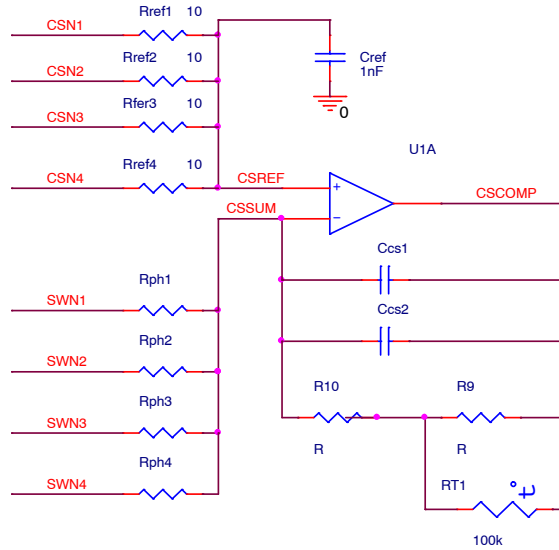


Figure 7.

The DC gain equation for the current sensing:

$$V_{CSCOMP-CSREF} = \frac{Rcs2 + \frac{Rcs1 \cdot Rth}{Rcs1 + Rth}}{Rph} * (I_{out\_Total} * DCR)$$

Set the gain by adjusting the value of the Rph resistors. The DC gain should be set to the output voltage droop. If the voltage from CSCOMP to CSREF is less than 100 mV at ICCMAX then it is recommend increasing the gain of the CSCOMP amp. This is required to provide a good current signal to offset voltage ratio for the ILIMIT pin. When no droop is needed, the gain of the amplifier should be set to provide ~100mV across the current limit programming resistor at full load. The values of Rcs1 and Rcs2 are set based on the 100k NTC and the temperature effect of the inductor and should not need to be changed. The NTC should be placed near the closest inductor. The output voltage droop should be set with the droop filter divider.

The pole frequency in the CSCOMP filter should be set equal to the zero from the output inductor. This allows the circuit to recover the inductor DCR voltage drop current signal. Ccs1 and Ccs2 are in parallel to allow for fine tuning of the time constant using commonly available values. It is best to fine tune this filter during transient testing.

$$F_z = \frac{DCR@25^{\circ}C}{2 * \pi * L_{Phase}}$$

**Programming the Current Limit**

The current limit thresholds are programmed with a resistor between the ILIMIT and CSCOMP pins. The ILIMIT pin mirrors the voltage at the CSREF pin and mirrors the sink current internally to IOUT (reduced by the IOUT Current Gain) and the current limit comparators. The 100% current limit trips if the ILIMIT sink current exceeds 10 μA for 50 μs. The 150% current limit trips with minimal delay if the ILIMIT sink current exceeds 15 μA. Set the value of the current limit resistor based on the CSCOMP–CSREF voltage as shown below.

$$R_{LIMIT} = \frac{\frac{Rcs2 + \frac{Rcs1 \cdot Rth}{Rcs1 + Rth}}{Rph} * (I_{out\_LIMIT} * DCR)}{10\mu} \quad \text{or} \quad R_{LIMIT} = \frac{IV_{CSCOMP-CSREF@ILIMIT}}{10\mu}$$

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## Programming IOOUT

The IOOUT pin sources a current in proportion to the ILIMIT sink current. The voltage on the IOOUT pin is monitored by the internal A/D converter and should be scaled with an external resistor to ground such that a load equal to ICCMAX generates a 2 V signal on IOOUT. A pull-up resistor from 5 V V<sub>CC</sub> can be used to offset the IOOUT signal positive if needed.

$$R_{IOOUT} = \frac{2.0 \text{ V} * R_{LIMIT}}{10 * \frac{R_{cs2} + \frac{R_{cs1} * R_{th}}{R_{cs1} + R_{th}}}{R_{ph}} * (I_{out_{ICCMAX}} * DCR)}$$

## Programming ICC\_MAX

The SVID interface provides the platform ICC\_MAX value at register 21h for. A resistor to ground on the IMAX pin programs these registers at the time the part is enabled. 10 µA is sourced from these pins to generate a voltage on the program resistor. The value of the register is 1 A per LSB and is set by the equation below. The resistor value should be no less than 10k.

$$ICC\_MAX_{21h} = \frac{R * 10 \mu\text{A} * 256 \text{ A}}{2 \text{ V}}$$

## Programming TSENSE

A temperature sense inputs are provided. A precision current is sourced out the output of the TSENSE pin to generate a voltage on the temperature sense network. The voltage on the temperature sense input is sampled by the internal A/D converter. A 100k NTC similar to the VISHAY ERT-J1VS104JA should be used. Rcomp1 is mainly used for noise. See the specification table for the thermal sensing voltage thresholds and source current.

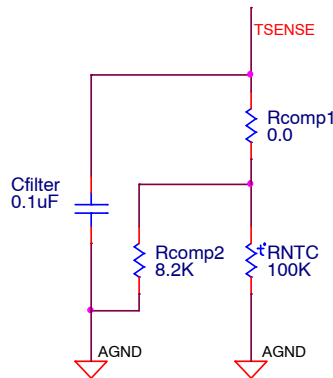


Figure 8.

## Precision Oscillator

A programmable precision oscillator is provided. The clock oscillator serves as the master clock to the ramp generator circuit. This oscillator is programmed by a resistor to ground on the ROSC pin. The oscillator frequency range is between 280 kHz to 650 kHz on the NCP81119 The graph below lists the resistor options and associated frequency setting.

# NCP81119

## NCP81119 Operating Frequency vs. $R_{osc}$

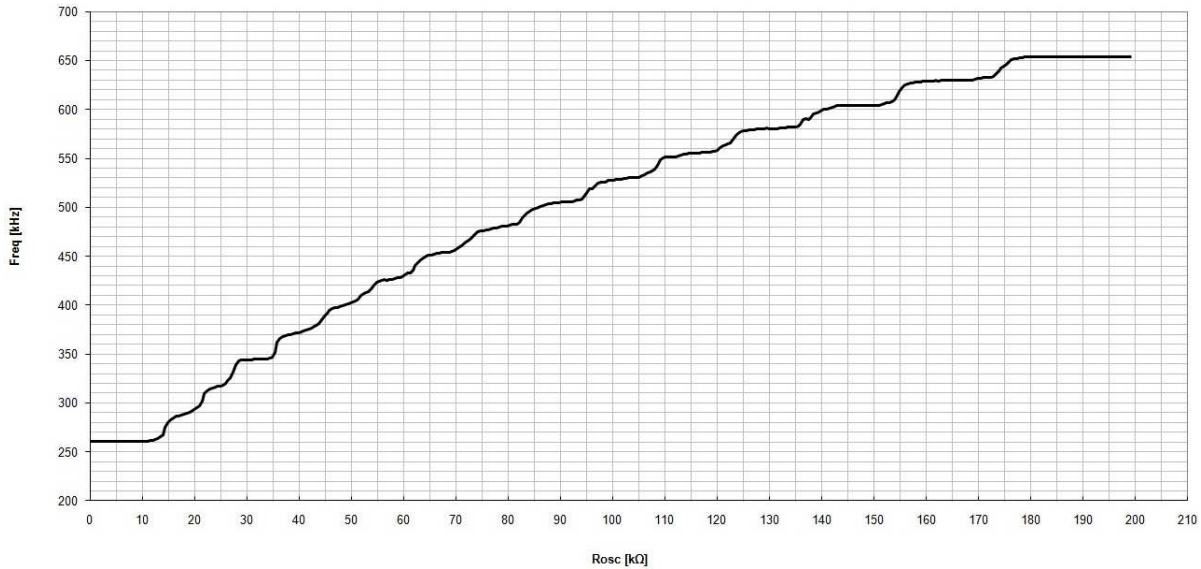


Figure 9. NCP81119  $R_{osc}$  vs. Frequency

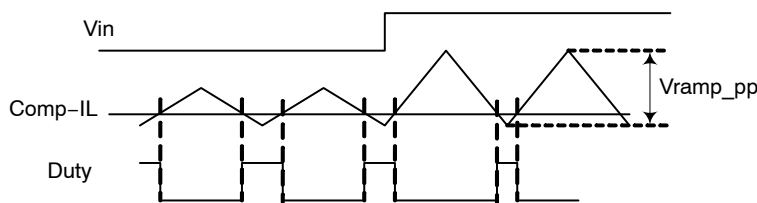
The oscillator generates triangle ramps that are 0.5~2.5 V in amplitude depending on the VRMP pin voltage to provide input voltage feed forward compensation. The ramps are equally spaced out of phase with respect to each other.

### Programming the Ramp Feed-Forward Circuit

The ramp generator circuit provides the ramp used by the PWM comparators. The ramp generator provides voltage feed-forward control by varying the ramp magnitude with respect to the VRMP pin voltage. The VRMP pin also has a 4 V UVLO function. The VRMP UVLO is only active after the controller is enabled. The VRMP pin is high impedance input when the controller is disabled.

The PWM ramp time is changed according to the following,

$$V_{RAMPpk\leftarrow pkPP} = 0.1 * V_{VRMP}$$



### PWM Comparators

The noninverting input of the comparator for each phase is connected to the summed output of the error amplifier (COMP) and each phase current ( $I_L * DCR * \text{Phase Balance Gain Factor}$ ). The inverting input is connected to the oscillator ramp voltage with a 1.3 V offset. The operating input voltage range of the comparators is from 0 V to 3.0 V and the output of the comparator generates the PWM output.

During steady state operation, the duty cycle is centered on the valley of the sawtooth ramp waveform. The steady state duty cycle is still calculated by approximately  $V_{out}/V_{in}$ . During a transient event, the controller will operate in a hysteretic mode with the duty cycles pull in for all phases as the error amp signal increases with respect to all the ramps.

### PHASE DETECTION SEQUENCE

During start-up, the number of operational phases and their phase relationship is determined by the internal circuitry monitoring the CSN Pins. Normally, NCP81119 operates as a 4-phase  $V_{core}$  PWM controller. Connecting CSN4 pin to  $V_{CC}$  programs 3-phase operation, connecting CSN2 and CSN4 pin to  $V_{CC}$  programs 2-phase operation, connecting CSN2, CSN3 and CSN4 pin to  $V_{CC}$  programs 1-phase operation. Prior to soft start, while ENABLE is high, CSN4 to CSN2 pins sink approximately 50  $\mu A$ . An internal comparator checks the voltage of each pin versus a threshold of 4.5 V. If the pin is tied to

## NCP81119

$V_{CC}$ , its voltage is above the threshold. Otherwise, an internal current sink pulls the pin to GND, which is below the threshold. PWM1 is low during the phase detection interval, which takes 30  $\mu$ s. After this time, if the remaining CSN outputs are not pulled to  $V_{CC}$ , the 50  $\mu$ A current sink is removed, and NCP81119 functions as normal 4 phase controller. If the CSNs are pulled to  $V_{CC}$ , the 50  $\mu$ A current source is removed, and the outputs are driven into a high impedance state.

The PWM outputs are logic-level devices intended for driving fast response external gate drivers such as the NCP5901 and NCP5911. Because each phase is monitored independently, operation approaching 100% duty cycle is possible. In addition, more than one PWM output can be on at the same time to allow overlapping phases.

### PROTECTION FEATURES

#### Under voltage Lockouts

There are several under voltage monitors in the system. Hysteresis is incorporated within the comparators. NCP81119 monitors the VCC Shunt supply. The gate driver monitors both the gate driver  $V_{CC}$  and the BST voltage. When the voltage on the gate driver is insufficient it will pull DRON low and prevents the controller from being enabled. The gate driver will hold DRON low for a minimum period of time to allow the controller to hold off its startup sequence. In this case the PWM is set to the MID state to begin soft start.

#### Gate Driver UVLO Restart

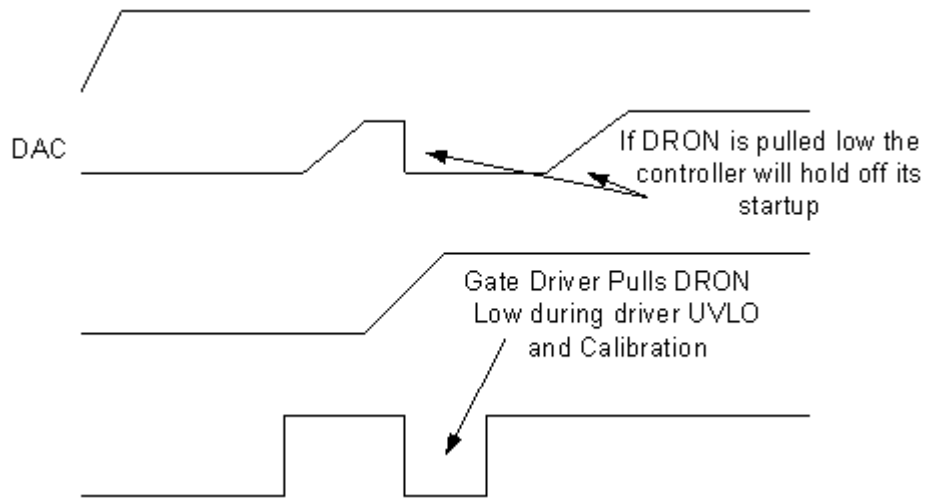


Figure 10.

#### Soft Start

Soft start is implemented internally. A digital counter steps the DAC up from zero to the target voltage based on the predetermined rate in the spec table. The PWM signals will start out open with a test current to collect data on phase count and for setting internal registers. After the configuration data is collected, if the controller is enabled the PWMs will be set to 2.0 V MID state to indicate that the drivers should be in diode mode. DRON will then be asserted. As the DAC ramps the PWM outputs will begin to fire. Each phase will move out of the MID state when the first PWM pulse is produced. When the controller is disabled the PWM signal will return to the MID state.



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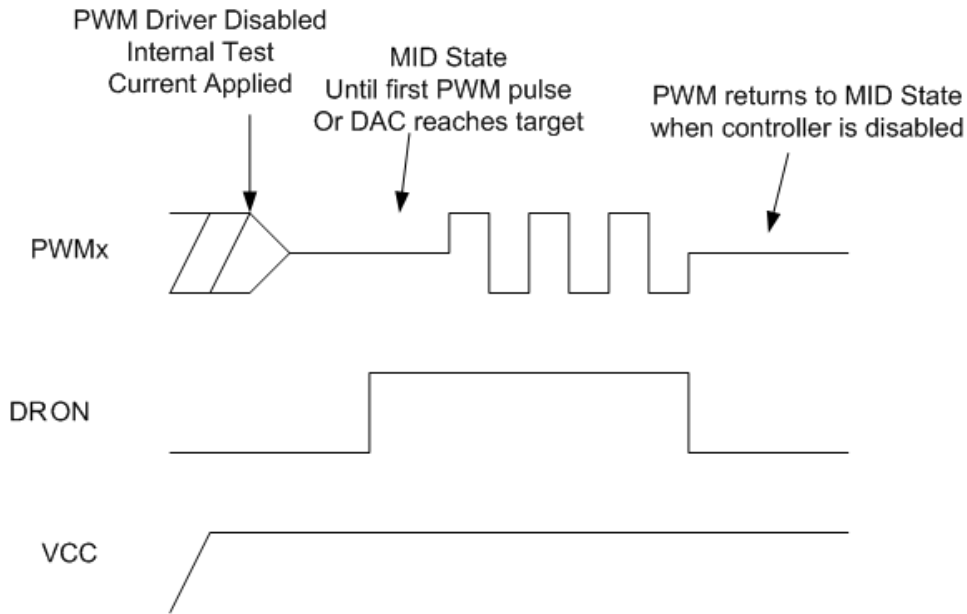


Figure 11.

## Over Current Latch– Off Protection

The NCP81119 compares a programmable current–limit set point to the voltage from the output of the current–summing amplifier. The level of current limit is set with the resistor from the ILIM pin to CSCOMP. The current through the external resistor connected between ILIM and CSCOMP is then compared to the internal current limit current  $I_{CL}$ . If the current generated through this resistor into the ILIM pin ( $I_{lim}$ ) exceeds the internal current–limit threshold current ( $I_{CL}$ ), an internal latch–off counter starts, and the controller shuts down if the fault is not removed after 50  $\mu s$  (shut down immediately for 150% load current) after which the outputs will remain disabled until the  $V_{CC}$  voltage or EN is toggled.

On startup a  $clim1/clim2$  current limit protection is enabled once the output voltage has exceeded 250 mV or if the internal DAC voltage has increased above 300 mV, this allow for protection again a  $V_{out}$  short to ground. This is necessary because the voltage swing of CSCOMP cannot go below ground. This limits the voltage drop across the DCR through the current balance circuitry.

The over–current limit is programmed by a resistor on the ILIM pin. The resistor value can be calculated by the following equation:

$$R_{ILIM} = \frac{I_{LIM} * DCR * R_{CS} / R_{PH}}{I_{CL}}$$

Where  $I_{CL} = 10 \mu A$

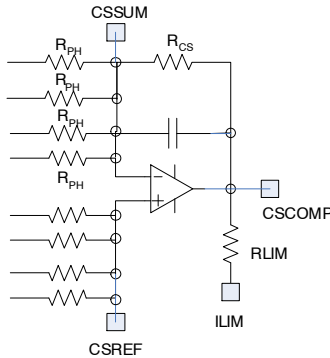


Figure 12.

**Under Voltage Monitor**

The output voltage is monitored at the output of the differential amplifier for UVLO. If the output falls more than 300mV below the DAC-DROOP voltage the UVLO comparator will trip sending the VR\_RDY signal low.

**Over Voltage Protection**

The output voltage is also monitored at the output of the differential amplifier for OVP. During normal operation, if the output voltage exceeds the DAC voltage by 400 mV, the VR\_RDY flag goes low, and the DAC will be ramped down to 0 V. At the same time, the high side gate drivers are all turned off and the low side gate drivers are all turned on until the voltage falls to new DAC voltage 0.2 V. The part will stay in this mode until the V<sub>CC</sub> voltage or EN is toggled.

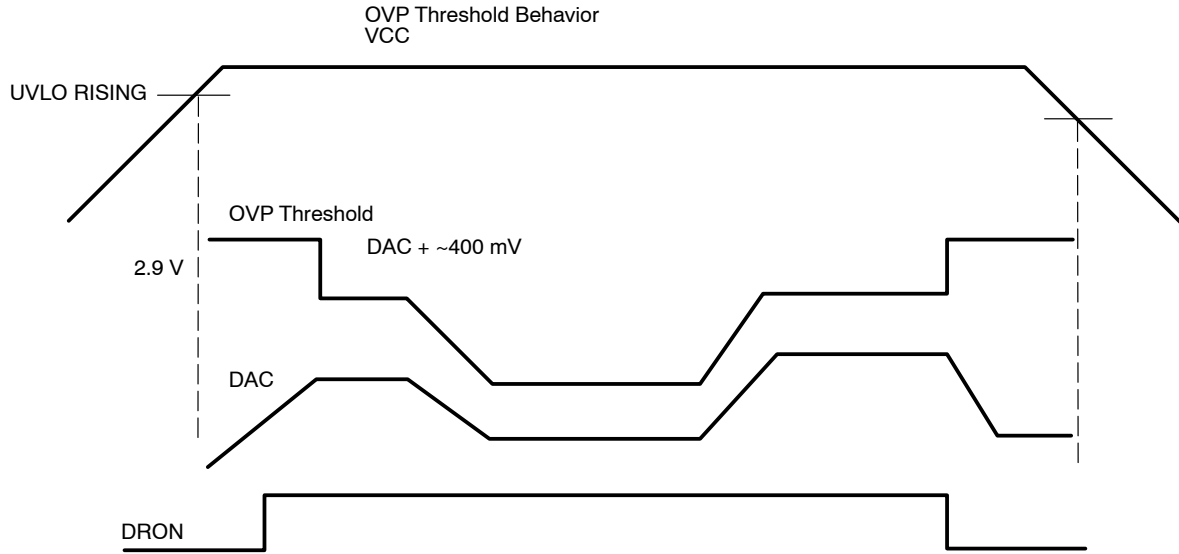


Figure 13. OVP Threshold Behavior

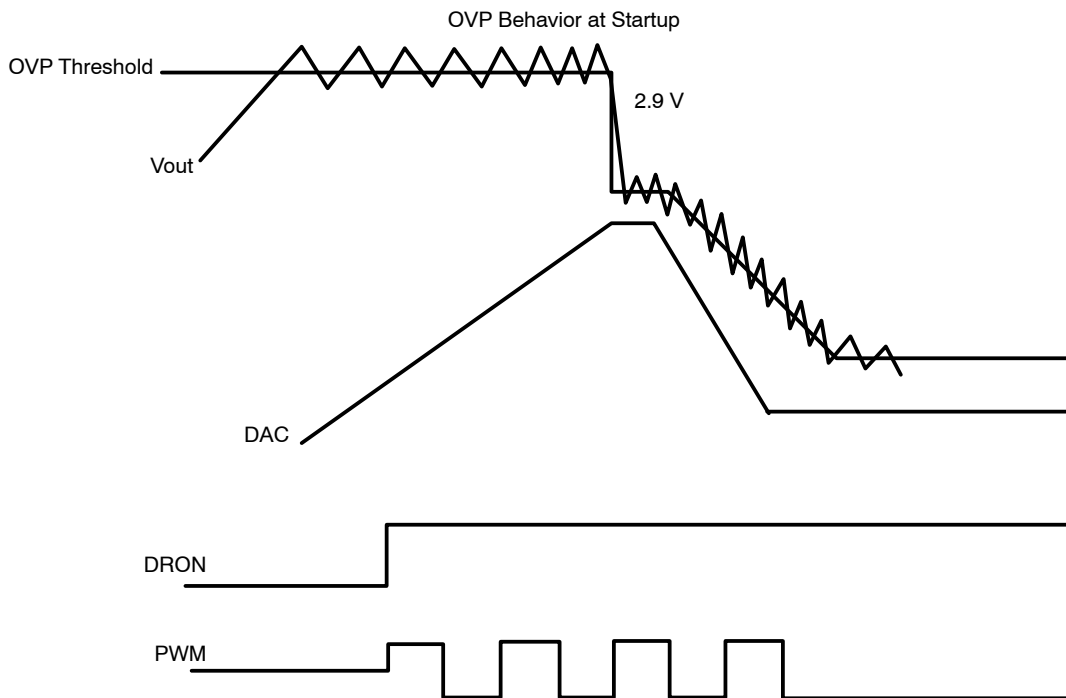


Figure 14. OVP Behavior at Startup