# imall

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## **Power MOSFET**

### 30 V, 6 A, Dual N-Channel SOIC-8

#### Features

- Designed for use in low voltage, high speed switching applications
- Ultra Low On-Resistance Provides
- Higher Efficiency and Extends Battery Life
  - $R_{DS(on)} = 0.024 \Omega$ ,  $V_{GS} = 10 V (Typ)$
  - $R_{DS(on)} = 0.030 \Omega$ ,  $V_{GS} = 4.5 V (Typ)$
- Miniature SOIC-8 Surface Mount Package Saves Board Space
- Diode is Characterized for Use in Bridge Circuits
- Diode Exhibits High Speed, with Soft Recovery
- AEC Q101 Qualified NVMD6N03R2
- These Devices are Pb-Free and are RoHS Compliant

#### Applications

- DC-DC Converters
- Computers
- Printers
- Cellular and Cordless Phones
- Disk Drives and Tape Drives

#### MAXIMUM RATINGS (T<sub>J</sub> = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-to-Source Voltage	V <sub>DSS</sub>	30	Volts
Gate-to-Source Voltage - Continuous	V <sub>GS</sub>	±20	Volts
Drain Current - Continuous @ T <sub>A</sub> = 25°C - Single Pulse (tp ≤ 10 μs)	I <sub>D</sub> I <sub>DM</sub>	6.0 30	Adc Apk
Total Power Dissipation @ $T_A = 25^{\circ}C$ (Note 1) @ $T_A = 25^{\circ}C$ (Note 2)	PD	2.0 1.29	Watts
Operating and Storage Temperature Range	T <sub>J</sub> , T <sub>stg</sub>	-55 to +150	°C
Single Pulse Drain-to-Source Avalanche Energy - Starting T <sub>J</sub> = 25°C (V <sub>DD</sub> = 30 Vdc, V <sub>GS</sub> = 5.0 Vdc, V <sub>DS</sub> = 20 Vdc, Peak I <sub>L</sub> = 9.0 Apk, L = 10 mH, R <sub>G</sub> = 25 $\Omega$ )	E <sub>AS</sub>	325	mJ
Thermal Resistance - Junction-to-Ambient (Note 1) - Junction-to-Ambient (Note 2)	R <sub>θJA</sub>	62.5 97	°C/W
Maximum Lead Temperature for Soldering Purposes for 10 seconds	TL	260	°C

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

1. When surface mounted to an FR4 board using 1" pad size, t  $\leq$  10 s

2. When surface mounted to an FR4 board using 1" pad size, t = steady state

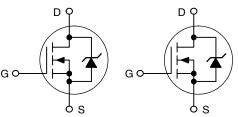


#### **ON Semiconductor®**

#### http://onsemi.com

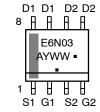
V <sub>DSS</sub>	R <sub>DS(ON)</sub> Typ	I <sub>D</sub> Max
30 V	24 mΩ @ V <sub>GS</sub> = 10 V	6.0 A

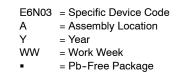
#### N-Channel



#### MARKING DIAGRAM & PIN ASSIGNMENT







(Note: Microdot may be in either location)

#### **ORDERING INFORMATION**

Device	Package	Shipping <sup>†</sup>
NTMD6N03R2G	SOIC-8 (Pb-Free)	2500 / Tape & Reel
NVMD6N03R2G	SOIC-8 (Pb-Free)	2500 / Tape & Reel

+ For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specification Brochure, BRD8011/D.

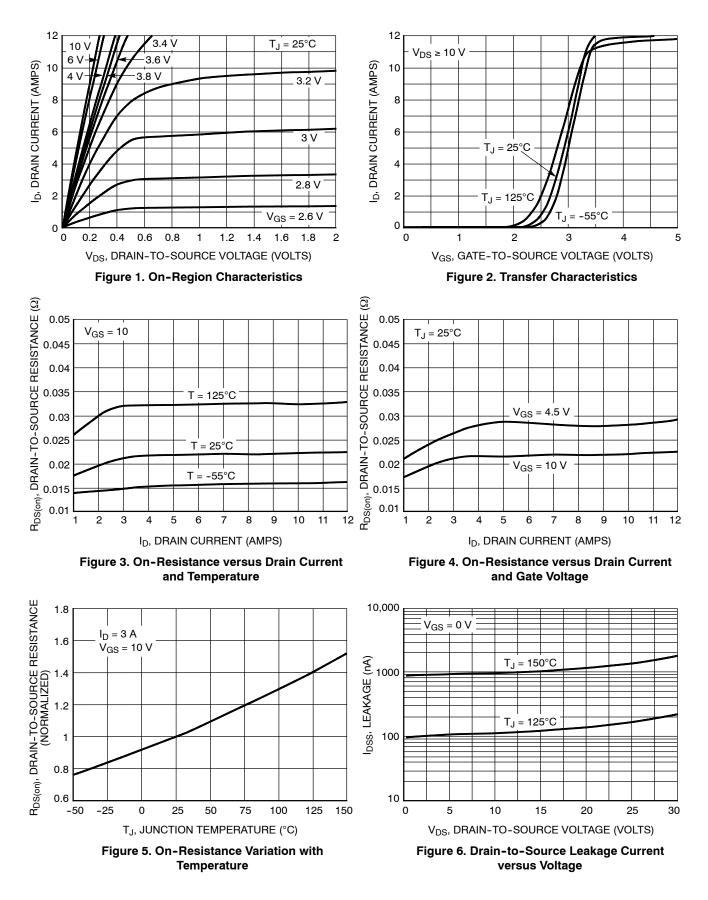
#### **ELECTRICAL CHARACTERISTICS** (T<sub>C</sub> = $25^{\circ}$ C unless otherwise noted)

Characteristic		Symbol	Min	Тур	Max	Unit
OFF CHARACTERISTICS						
Drain-to-Source Breakdown Voltage $(V_{GS} = 0 \text{ Vdc}, I_D = 250 \ \mu\text{A})$ Temperature Coefficient (Positive)		V <sub>(BR)DSS</sub>	30 -	- 30	-	Vdc mV/°C
Zero Gate Voltage Drain Current ( $V_{DS} = 24$ Vdc, $V_{GS} = 0$ Vdc, $T_J = 25^{\circ}$ C) ( $V_{DS} = 24$ Vdc, $V_{GS} = 0$ Vdc, $T_J = 125^{\circ}$ C)		I <sub>DSS</sub>	-		1.0 20	μAdc
Gate-Body Leakage Current (V <sub>GS</sub> = ±20 Vdc, V <sub>DS</sub> = 0 Vdc)		I <sub>GSS</sub>	-	-	100	nAdc
ON CHARACTERISTICS (Note 3)						
Gate Threshold Voltage $(V_{DS} = V_{GS}, I_D = 250 \ \mu Adc)$ Temperature Coefficient (Negative)		V <sub>GS(th)</sub>	1.0 -	1.8 4.6	2.5 -	Vdc mV/°C
Static Drain-to-Source On-State Resistance $(V_{GS} = 10 \text{ Vdc}, I_D = 6 \text{ Adc})$ $(V_{GS} = 4.5 \text{ Vdc}, I_D = 3.9 \text{ Adc})$		R <sub>DS(on)</sub>	-	0.024 0.030	0.032 0.040	Ω
Forward Transconductance $(V_{DS} = 15 \text{ Vdc}, I_D = 5.0 \text{ Adc})$		9fs	-	10	-	Mhos
DYNAMIC CHARACTERISTICS						
Input Capacitance		C <sub>iss</sub>	-	680	950	pF
Output Capacitance	(V <sub>DS</sub> = 24 Vdc, V <sub>GS</sub> = 0 Vdc, f = 1.0 MHz)	C <sub>oss</sub>	-	210	300	
Reverse Transfer Capacitance	· · · · · · · · · · · · · · · · · · ·	C <sub>rss</sub>	-	70	135	
SWITCHING CHARACTERISTICS (N	lotes 3 & 4)					
Turn-On Delay Time		t <sub>d(on)</sub>	-	9	18	ns
Rise Time	$(V_{DD} = 15 \text{ Vdc}, I_D = 1 \text{ A},$	t <sub>r</sub>	ł	22	40	
Turn-Off Delay Time	V <sub>GS</sub> = 10 V, R <sub>G</sub> = 6 Ω)	t <sub>d(off)</sub>	ł	45	80	
Fall Time		t <sub>f</sub>	-	45	80	]
Turn-On Delay Time		t <sub>d(on)</sub>	-	13	30	ns
Rise Time	(V <sub>DD</sub> = 15 Vdc, I <sub>D</sub> = 1 A, V <sub>GS</sub> = 4.5 V,	tr	-	27	50	
Turn-Off Delay Time	$V_{GS} = 4.5 V,$ $R_G = 6 \Omega)$	t <sub>d(off)</sub>	-	22	40	
Fall Time	~ ,	t <sub>f</sub>	-	34	70	
Gate Charge		QT	-	19	30	nC
	(V <sub>DS</sub> = 15 Vdc, V <sub>GS</sub> = 10 Vdc,	Q <sub>1</sub>	-	2.4	-	
	$V_{GS} = 10$ Vac, $I_D = 5$ A)	Q <sub>2</sub>	-	5.0	-	
		Q <sub>3</sub>	-	4.3	-	1
BODY-DRAIN DIODE RATINGS (No	te 3)					
Diode Forward On-Voltage	$(I_{S} = 1.7 \text{ Adc}, V_{GS} = 0 \text{ V})$ $(I_{S} = 1.7 \text{ Adc}, V_{GS} = 0 \text{ V}, T_{J} = 150^{\circ}\text{C})$	V <sub>SD</sub>	-	0.75 0.62	1.0 -	Vdc
Reverse Recovery Time		t <sub>rr</sub>	-	26	-	ns

	$(I_{\rm S} = 1.7 \text{ Adc}, V_{\rm GS} = 0 \text{ V}, T_{\rm J} = 150^{\circ}\text{C})$	- 30	-	0.62	-	
Reverse Recovery Time	<i>"</i>	t <sub>rr</sub>	-	26	-	ns
	(I <sub>S</sub> = 5 A, V <sub>GS</sub> = 0 V, dI <sub>S</sub> /dt = 100 A/μs)	t <sub>a</sub>	-	11	-	
		t <sub>b</sub>	-	15	-	
Reverse Recovery Stored Charge ( $I_S = 5 \text{ A}, \text{ dI}_S/\text{dt} = 100 \text{ A}/\mu\text{s}, \text{ V}_{GS} = 100 \text{ A}/\mu\text{s}$	= 0 V)	Q <sub>RR</sub>	-	0.015	-	μC

Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.
Switching characteristics are independent of operating junction temperature.

#### **TYPICAL MOSFET ELECTRICAL CHARACTERISTICS**



#### **POWER MOSFET SWITCHING**

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals ( $\Delta t$ ) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain-gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ( $I_{G(AV)}$ ) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$ 

During the rise and fall time interval when switching a resistive load,  $V_{GS}$  remains virtually constant at a level known as the plateau voltage,  $V_{SGP}$ . Therefore, rise and fall times may be approximated by the following:

 $t_r = Q_2 x R_G / (V_{GG} - V_{GSP})$ 

 $t_f = Q_2 x R_G / V_{GSP}$ 

where

 $V_{GG}$  = the gate drive voltage, which varies from zero to  $V_{GG}$ 

 $R_G$  = the gate drive resistance

and  $Q_2$  and  $V_{GSP}$  are read from the gate charge curve.

During the turn-on and turn-off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

 $t_{d(on)} = R_G C_{iss} In [V_{GG}/(V_{GG} - V_{GSP})]$  $t_{d(off)} = R_G C_{iss} In (V_{GG}/V_{GSP})$  The capacitance ( $C_{iss}$ ) is read from the capacitance curve at a voltage corresponding to the off-state condition when calculating  $t_{d(on)}$  and is read at a voltage corresponding to the on-state when calculating  $t_{d(off)}$ .

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.

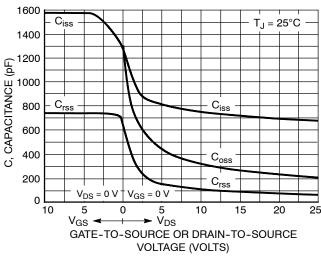
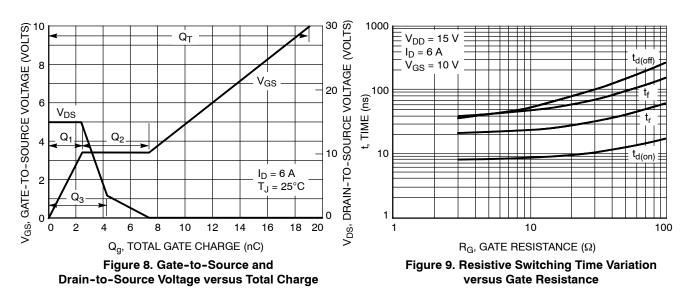


Figure 7. Capacitance Variation





The switching characteristics of a MOSFET body diode are very important in systems using it as a freewheeling or commutating diode. Of particular interest are the reverse recovery characteristics which play a major role in determining switching losses, radiated noise, EMI and RFI.

System switching losses are largely due to the nature of the body diode itself. The body diode is a minority carrier device, therefore it has a finite reverse recovery time,  $t_{rr}$ , due to the storage of minority carrier charge,  $Q_{RR}$ , as shown in the typical reverse recovery wave form of Figure 14. It is this stored charge that, when cleared from the diode, passes through a potential and defines an energy loss. Obviously, repeatedly forcing the diode through reverse recovery further increases switching losses. Therefore, one would like a diode with short  $t_{rr}$  and low  $Q_{RR}$  specifications to minimize these losses.

The abruptness of diode reverse recovery effects the amount of radiated noise, voltage spikes, and current ringing. The mechanisms at work are finite irremovable circuit parasitic inductances and capacitances acted upon by high di/dts. The diode's negative di/dt during  $t_a$  is directly controlled by the device clearing the stored charge. However, the positive di/dt during  $t_b$  is an uncontrollable diode characteristic and is usually the culprit that induces current ringing. Therefore, when comparing diodes, the ratio of  $t_b/t_a$  serves as a good indicator of recovery abruptness and thus gives a comparative estimate of probable noise generated. A ratio of 1 is considered ideal and values less than 0.5 are considered snappy.

Compared to ON Semiconductor standard cell density low voltage MOSFETs, high cell density MOSFET diodes are faster (shorter  $t_{rr}$ ), have less stored charge and a softer reverse recovery characteristic. The softness advantage of the high cell density diode means they can be forced through reverse recovery at a higher di/dt than a standard cell MOSFET diode without increasing the current ringing or the noise generated. In addition, power dissipation incurred from switching the diode will be less due to the shorter recovery time and lower switching losses.

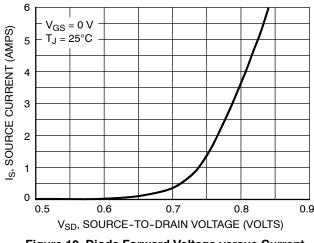


Figure 10. Diode Forward Voltage versus Current

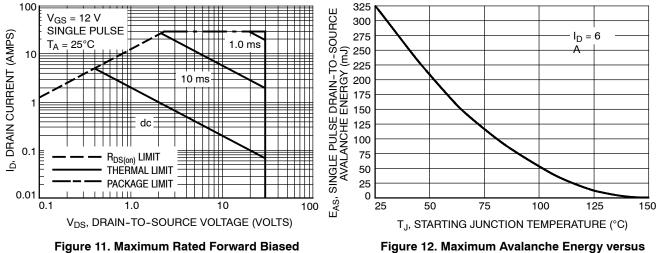
#### SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature ( $T_C$ ) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance – General Data and Its Use."

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current  $(I_{DM})$  nor rated voltage  $(V_{DSS})$  is exceeded, and that the transition time  $(t_r, t_f)$  does not exceed 10  $\mu$ s. In addition the

total power averaged over a complete switching cycle must not exceed  $(T_{J(MAX)} - T_C)/(R_{\mu JC})$ .

A power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and must be adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.



igure 11. Maximum Rated Forward Biase Safe Operating Area

Figure 12. Maximum Avalanche Energy versus Starting Junction Temperature

#### **TYPICAL ELECTRICAL CHARACTERISTICS**

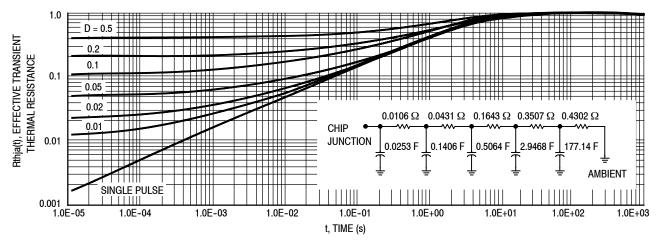


Figure 13. Thermal Response

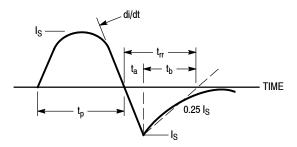
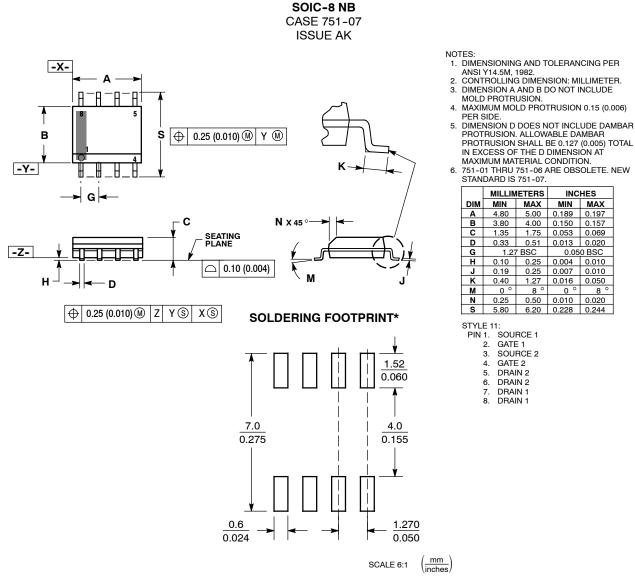


Figure 14. Diode Reverse Recovery Waveform

#### PACKAGE DIMENSIONS



\*For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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