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## Features

- 3V to 6V Operation
- Modulation or Demodulation
- IF From 100 kHz to 250 MHz
- Baseband From DC to 50MHz
- Digital LO Quadrature Divider
- Low Power and Small Size


## Applications

- Digital and Analog Receivers and Transmitters
- High Data Rate Digital Communications
- Spread-Spectrum Communication Systems
- Interactive Cable Systems
- Portable Battery-Powered Equipment


Functional Block Diagram

## Product Description

The RF2713 is a monolithic integrated quadrature modulator/demodulator. The demodulator is used to recover the I and Q baseband signals from the amplified and filtered IF. Likewise, the inputs and outputs can be reconfigured to modulate I/Q signals onto an RF carrier. The RF2713 is intended for IF systems where the IF frequency ranges from 100 kHz to 250 MHz , and the LO frequency is two times the IF. The IC contains all of the required components to implement the modulation/demodulation function and contains a digital divider type $90^{\circ}$ phase shifter, two double balanced mixers, and baseband amplifiers designed to interface with Analog to Digital Converters. The unit operates from a single 3V to 6V power supply.

## Ordering Information

| RF2713 | Quadrature Modulator/Demodulator |
| :--- | :--- |
| RF2713 PCBA-D | Fully Assembled Evaluation Board (Demodulator) |
| RF2713 PCBA-M | Fully Assembled Evaluation Board (Modulator) |

Optimum Technology Matching ${ }^{\circledR}$ Applied

| $\square$ GaAs HBT | $\square$ SiGe BiCMOS | $\square$ GaAs pHEMT | $\square$ GaN HEMT |
| :--- | :--- | :--- | :--- |
| $\square$ GaAs MESFET | $\square$ Si BiCMOS | $\square$ Si CMOS |  |
| $\square$ InGaP HBT | $\square$ SiGe HBT | $\square$ Si BJT |  |

GaAs HBT解

Si BJT

| Absolute Maximum Ratings |  |  |
| :--- | :---: | :---: |
| Parameter | Rating | Unit |
| Supply Voltage | -0.5 to 7.0 | $\mathrm{~V}_{\mathrm{DC}}$ |
| IF Input Level | 500 | $\mathrm{mV}_{\mathrm{PP}}$ |
| Operating Ambient Temperature | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature | -40 to +150 | ${ }^{\circ} \mathrm{C}$ |



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| Parameter | Specification |  |  | Unit | Condition |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Min. | Typ. | Max. |  |  |
| Demodulator Configuration, cont. |  |  |  |  | $\mathrm{IF}_{\text {IN }}=28 \mathrm{mV} \mathrm{VPP}, \mathrm{LO}=200 \mathrm{mV} \mathrm{PP}, \mathrm{Z}_{\text {LOAD }}=10 \mathrm{k} \Omega$ |
| Input 1dB Compression Point | -21 | -18.5 |  | dBm | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, 50 \Omega$ shunt at IF Input |
| I/Q Amplitude Balance |  | 0.1 | 0.5 | dB |  |
| Quadrature Phase Error |  | 1 |  | - |  |
| DC Output |  | 800 |  | mV | $\mathrm{V}_{\text {CC }}=3.0 \mathrm{~V}, \mathrm{I}_{\text {OUT }}$ and $\mathrm{Q}_{\text {OUT }}$ to GND |
|  | 2.0 | 2.4 | 2.8 | V | $\mathrm{V}_{\text {CC }}=5.0 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}$ and $\mathrm{Q}_{\text {OUT }}$ to GND |
| DC Offset |  | <10 | 100 | mV | Iout to Qout |
| Modulator Configuration |  |  |  |  | $\mathrm{IF}_{\text {IN }}=28 \mathrm{mV} \mathrm{PPP}, \mathrm{LO}=200 \mathrm{mV} \mathrm{PP}, \mathrm{Z}_{\text {LOAD }}=1200 \Omega$ |
| Maximum Output |  | -23 |  | dBm | Saturated $\square$ |
| Input Voltage |  | 90 |  | $m V_{P P}$ | Single Sideband, 1dB Gain Compression. |
| Voltage Gain |  | 6 |  | dB | Single Sideband |
| I/Q Amplitude Balance |  | 0.1 |  | dB | $\square)$ |
| Quadrature Phase Error |  | 1 |  | - |  |
| Carrier Suppression |  | 25 |  | $\mathrm{dBC}$ | Unadjusted. Carrier Suppression may be optimized further by adjusting the DC offset level between the $A$ and $B$ inputs. |
| Sideband Suppression |  | 30 |  |  |  |
| Power Supply |  |  |  |  |  |
| Voltage | 3.0 |  | 6.0 | V | Operating limits |
| Current |  | 8 |  | mA | $\mathrm{V}_{\mathrm{CC}}=3.0 \mathrm{~V}$ |
|  | 8 | 10 | 12) | mA | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ |


| Pin | Function | Description (Demodulator Configuration) | Interface Schematic |
| :---: | :---: | :--- | :--- |
| $\mathbf{1}$ | I INPUT A | When the RF2713 is configured as a Quadrature Demodulator, both mixers <br> are driven by the IF. Whether driving the mixers single-endedly (as shown in <br> the application schematic) or differentially, the A Inputs (piss 1 and 3) <br> should be connected to each other. Likewise, both B Inputs (pins 2 and 4) <br> should be connected to each other. This ensures that the IF will reach each <br> mixer with the same amplitude and phase, yielding the best I and Q output <br> amplitude and quadrature balance. Note that connecting the inputs in par- <br> allel changes the input impedance (see the Gilbert Cell mixer equivalent <br> circuit). The single-ended input impedance (as shown in the application cir- <br> cuit) becomes 630 $\Omega$, but in the balanced configuration, the input imped- <br> ance would remain 1260 $\Omega$. |  |
| The mixers are Gilbert Cell designs with balanced inputs. The equivalent |  |  |  |

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| Pin | Function | Description (Demodulator Configuration) | Interface Schematic |
| :---: | :---: | :--- | :--- |
| 13 | LO INPUT | High impedance, single-ended modulator LO input. The LO applied to this <br> pin is frequency divided by a factor of 2 and becomes the "Carrier". For <br> direct demodulation, the Carrier is equal in frequency to the center of the <br> input IF spectrum (except in the case of SSB/SC). The input impedance is <br> determined by an internal $500 \Omega$ bias resistor to $V_{\text {Cc }}$. An external blocking <br> capacitor should be provided if the pin is connected to a device with DC <br> present. Matching the input impedance is typically achieved by adding a <br> 51 $\Omega$ resistor to ground on the source side of the AC coupling capacitor. For <br> the LO input, maximum power transfer is not critical. The internal LO <br> switching circuits are controlled by the voltage, not power, into the part. In <br> cases where the LO source does not have enough available voltage, a reac- <br> tive match (voltage transformer) can be used. The LO circuitry consists of a <br> limiting amplifier followed by a digital divider. The limiting amp ensures <br> that the flip-flop type divider is driven with a square wave over a wide range <br> of input levels. Because the flip-flop uses the rising and falling edges of the <br> limiter output, the quadrature accuracy of the Carrier supplied to the mix- <br> ers is directly related to the duty cycle, or equivalently to the even harmonic <br> content, of the input LO signal. In particular, care should be taken to <br> ensure that the 2xLO level input to this pin is at least 20dB below the LO <br> level. Otherwise, the LO input is not sensitive to the type of input wave <br> form, except for IF frequencies below ~2.5 MHz, in which case the LO input <br> should be a square wave, in order to ensure proper triggering of the flip- <br> flops. IF frequencies below 100 kHz are attainable if the LO is a square <br> wave and sufficiently large DC blocking capacitors are used. |  |
| $\mathbf{1 4}$ | Voltage supply for the entire device. This pin should be well bypassed at all <br> frequencies (IF, LO, Carrier, Baseband) that are present in the part. |  |  |


| Pin | Function | Description (Modulator Configuration) | Interface Schematic |
| :---: | :---: | :---: | :---: |
| 1 | I INPUT A | When the RF2713 is configured as a Quadrature Modulator, each mixer is driven by an independent baseband modulation channel (I and Q). The mixers can be driven single-endedly (as shown in the modulator application circuit) or differentially. When driving single-endedly, the B Inputs (pins 2 and 4) should be connected to each other. This ensures that the baseband signals will reach each mixer with the same DC reference, yielding the best carrier suppression. Note that the input impedance changes according to the drive mode (see the mixer equivalent circuit on the previous page). The single-ended input impedance (as shown in the modulator application circuit) is $1200 \Omega$ for each of the two inputs. In the balanced configuration, the input impedance would be $2400 \Omega$ for each of the two inputs. <br> The mixers are Gilbert Cell designs with balanced inputs. The equivalent schematic for one of the mixers is shown on the previous page. The input impedance of each pin is determined by the $1200 \Omega$ resistor to $V_{C C}$ in parallel with a transistor base. Note from the schematic that all four input pins have an internally set DC bias. For this reason, all four inputs (pins 1 through 4) should be DC blocked. The capacitance values of the blocking capacitors is determined by the baseband frequency. When driving sin-gle-endedly, both the series (pins 1 and 3) and shunt (pins 2 and 4) blocking capacitors should be low impedances, relative to the input impedance. <br> DC bias voltages may be supplied to the inputs pins, if required, in order to increase the amount of carrier suppression. For example, the DC levels on the reference inputs (pins 2 and 4) may be offset from each other by adding different resistor values to ground. These resistors should be larger than $2 \mathrm{k} \Omega$. Note from the mixer schematic that all four input pins have an internally set DC bias. If DC bias is to be supplied, the allowable ranges are limited. For 5 V applications, the DC reference on both I pins or both Q pins must not go below $2.7 \mathrm{~V}_{\mathrm{DC}}$, and in no case should the DC voltage on any of the four pins go below $2.0 \mathrm{~V}_{\mathrm{DC}}$ or above $5.5 \mathrm{~V}_{\mathrm{DC}}$. IF a DC reference is to be supplied, the source must also be capable of sinking current. If optimizing carrier suppression further is not a concern, it is recommended that all four inputs (pins 1 through 4) be DC blocked. |  |
| 2 | I INPUT B | Same as pin 1, except complementary input. | See pin 1. |
| 3 | Q INPUT A | Same as pin 1, except Q Buffer Amplifier. | See pin 1. |
| 4 | Q INPUT B | Same as pin 3, except complementary input. | See pin 1. |
| 5 | BG OUT | Band Gap voltage reference output. This voltage output is held constant over variations in supply voltage and operating temperature and may be used as a reference for other external circuitry. This pin should not be loaded such that the sourced current exceeds 1 mA . This pin should be bypassed with a large $(0.1 \mu \mathrm{~F})$ capacitor. |  |
| 6 | I IF OUT | Connecting pins 6 and 7 to each other accomplishes the summing function of the upconverted I and Q channels. In addition, because these outputs are open collector type, they must be connected to $\mathrm{V}_{\mathrm{CC}}$ in order to properly bias the Gilbert Cell mixers. Maximum gain and output power occur when the load on these two pins is $\sim 1200 \Omega$. In most applications the impedance of the next stage will be lower and a reactive impedance transforming match should be used if maximum gain and output level are of concern. For applications where the gain is not as critical, a $1200 \Omega$ resistor may be added in parallel with a choke inductor. If neither gain nor output level is critical, the inductor may be replaced with a resistor that sets the desired source impedance to drive the next stage. If the next stage is an "open" at DC, the blocking capacitor may be eliminated. |  |

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| Pin | Function | Description (Modulator Configuration) | Interface Schematic |
| :---: | :---: | :---: | :---: |
| 7 | Q IF OUT | Same as pin 6, except complementary input. | Same as pin 6. |
| 8 | Q OUT | Pins 8 and 9 are not used in a normal quadrature modulator application, and are left unconnected. Note, however, that the outputs of each of these pins are independent upconverted $I$ and $Q$ channels. These signals may be useful in other applications where independent IF channels are needed. Also note that these outputs are optimized as baseband outputs for the demodulator configuration. As a result, the gain rolls-off quickly with increasing frequency. This gain roll-off will limit the usefulness of these pins as independent I and Q upconverters. If these outputs are to be used, please refer to the Demodulator pin descriptions regarding load impedances. |  |
| 9 | I OUT | Same as pin 8, except Q Mixer's Output. | Same as pin 8. |
| 10 | GND | Ground connection. Keep traces physically short and connect immediately to ground plane for best performance. |  |
| 11 | GND | Same as pin 10. |  |
| 12 | GND | Same as pin 10. |  |
| 13 | LO INPUT | High impedance, single-ended modulator LO input. The LO applied to this pin is frequency divided by a factor of 2 and becomes the "Carrier". For modulation, the Carrier is the center of the modulated output spectrum (except in the case of SSB/SC). The input impedance is determined by an internal $500 \Omega$ bias resistor to $V_{C C}$. An external blocking capacitor should be provided if the pin is connected to a device with DC present. Matching the input impedance is typically achieved by adding a $51 \Omega$ resistor to ground on the source side of the AC coupling capacitor. For the LO input, maximum power transfer is not critical. The internal LO switching circuits are controlled by the voltage, not power, into the part. In cases where the LO source does not have enough available voltage, a reactive match (voltage transformer) can be used. The LO circuitry consists of a limiting amplifier followed by a digital divider. The limiting amp ensures that the flip-flop type divider is driven with a square wave over a wide range of input levels. Because the flip-flop uses the rising and falling edges of the limiter output, the quadrature accuracy of the Carrier supplied to the mixers is directly related to the duty cycle, or equivalently to the even harmonic content, of the input LO signal. In particular, care should be taken to ensure that the $2 \times L O$ level input to this pin is at least 20 dB below the LO level. Otherwise, the LO input is not sensitive to the type of input wave form, except for IF frequencies below $\sim 2.5 \mathrm{MHz}$, in which case the LO input should be a square wave, in order to ensure proper triggering of the flip-flops. IF frequencies below 100 kHz are attainable if the LO is a square wave and sufficiently large DC blocking capacitors are used. |  |
| 14 | VCC | Voltage supply for the entire device. This pin should be well bypassed at all frequencies (IF, LO, Carrier, Baseband) that are present in the part. |  |

## Gilbert Cell Mixer Equivalent Circuit



Package Drawing


## Application Schematic - Demodulator Configuration



Application Schematic - Modulator Configuration


## Evaluation Board Schematic - Demodulator Configuration

(Download Bill of Materials from www.rfmd.com.)


Evaluation Board Schematic - Modulator Configuration


## Evaluation Board Layout Demodulator Configuration (2713 PCBA-D)

Board Size 2.0" x 2.0"
Board Thickness 0.031", Board Material FR-4


## Evaluation Board Layout Modulator Configuration (2713 PCBA-M)

Board Size 2.0" x 2.0"
Board Thickness 0.031", Board Material FR-4


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## RoHS* Banned Material Content

| RoHS Compliant: | yes |
| :--- | :---: |
| Package total w eight in gran | 0.126 |
| Compliance Date Code: | 0532 |
| Bill of Materials Revision: | Rev - |
| Pb Free Category: | e3 |


| Bill of Materials |  | Parts Per Million (PPM) |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Cd | Hg | Cr VI | PBB | PBDE |  |
| Die | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Molding Compound | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Lead Frame | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Die Attach Epoxy | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Wire | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Solder Plating | 0 | 0 | 0 | 0 | 0 | 0 |  |

This RoHS banned material content declaration was prepared solely on information, including analytical data, provided to RFMD by its suppliers, and applies to the Bill of Materials (BOM) revision noted above.

* DIRECTVE 2002/95/EC OF THE EUROPEAN PARLIAMENT AND OF THE COUNCIL of 27 January 2003 on the restriction of the use of certain hazardous substances in electrical and electronic equipment

