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The S-8365/8366 Series is a CMOS step-up switching regulator controller which mainly consists of a reference voltage source, an oscillation circuit, an error amplifier, a phase compensation circuit, a timer latch short-circuit protection circuit, a PWM control circuit (S-8365 Series) and a PWM / PFM switching control circuit (S-8366 Series).
With an external low-ON-resistance Nch Power MOS FET, this product is ideal for applications requiring high efficiency and a high output current.
The S-8365 Series efficiently works on voltage's condition of large I/O difference due to the PWM control circuit linearly varies the duty ratio to $90 \%$.
During light-load, the S-8366 Series switches its operation to the PFM control by the PWM / PFM switching control circuit in order to prevent efficiency decline due to the IC operating current.
Ceramic capacitors can be used for output capacitor. Small packages SNT-6A, SOT-23-5 and SOT-23-6 enable high-density mounting.

## Features

- Low operation voltage
- Input voltage range
- Oscillation frequency
- Reference voltage
- Soft start function
- Low current consumption
- Duty ratio
- Shutdown function
- External parts
- Timer latch short-circuit protection circuit
- UVLO (under-voltage lockout) function
- Lead-free, Sn 100\%, halogen-free* ${ }^{* 1}$
: Start at $1.1 \mathrm{~V}(1 \mathrm{~mA})$ guaranteed (in the product without UVLO function)
: 1.8 V to 5.5 V
: $1.2 \mathrm{MHz}, 600 \mathrm{kHz}$
: $0.6 \mathrm{~V} \pm 2.0 \%$
: 7 ms typ.
: $70 \mu \mathrm{~A}$ typ. at switching off
: Built-in PWM / PFM switching control circuit (S-8366 Series) 28\% to $85 \%$ (1.2 MHz product)
$28 \%$ to $90 \%$ ( 600 kHz product)
: Current consumption $1.0 \mu \mathrm{~A}$ max. at shutdown
: Inductor, diode, capacitor, transistor
: Selectable with / without short-circuit protection circuit for each product Settable delay time by external capacitor (in the product with short-circuit protection)
: Selectable with / without UVLO for each product
*1. Refer to "■ Product Name Structure" for details.


## Applications

- MP3 players, digital audio players
- Digital cameras, GPS, wireless transceiver
- Portable devices


## ■ Packages

- SNT-6A
- SOT-23-5
- SOT-23-6


## ■ Block Diagram

1. With UVLO function and short-circuit protection


Figure 1
2. With UVLO function, without short-circuit protection


Figure 2
3. Without UVLO and short-circuit protection


Figure 3
Caution To stabilize the output voltage and oscillation frequency of the S-8365/8366 Series, the input voltage of $1.8 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD}} \leq 5.5 \mathrm{~V}$ is necessary. When connecting the VOUT output to the VDD pin, set the input voltage (Vоит) as to satisfy the above range, including the spike voltage generated in VOUT.

## ■ Product Name Structure

Users can select the control system, oscillation frequency, short-circuit protection, UVLO function, packages for the S-8365/8366 Series. Refer to "1. Product name" regarding the contents of product name, "2. Packages" regarding the package drawings and "3. Product list" regarding the product type.

1. Product name
(1) SNT-6A


[^0](2) SOT-23-5, SOT-23-6

*1. Refer to the tape drawing.
2. Packages

| Package name | Drawing code |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Package | Tape | Reel | Land |
| SNT-6A | PG006-A-P-SD | PG006-A-C-SD | PG006-A-R-SD | PG006-A-L-SD |
| SOT-23-5 | MP005-A-P-SD | MP005-A-C-SD | MP005-A-R-SD | - |
| SOT-23-6 | MP006-A-P-SD | MP006-A-C-SD | MP006-A-R-SD | - |

## 3. Product list

(1) S-8365 Series (PWM control)

Table 1

| SOT-23-5 | SOT-23-6 | SNT-6A | Oscillation <br> frequency | Short-circuit <br> protection | UVLO <br> function | ON/ <br> pin <br> pull-down |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | S-8365AABBA-M6T1y2 | S-8365AABBA-I6T1U2 | 1.2 MHz | Available | Available | Unavailable |
| S-8365AAABA-M5T1y2 | - | S-8365AAABA-I6T1U2 | 1.2 MHz | Unavailable | Available | Unavailable |
| S-8365AAAAA-M5T1y2 | - | S-8365AAAAA-I6T1U2 | 1.2 MHz | Unavailable | Unavailable | Unavailable |
| - | S-8365ABBBA-M6T1y2 | S-8365ABBBA-I6T1U2 | 600 kHz | Available | Available | Unavailable |
| S-8365ABABA-M5T1y2 | - | S-8365ABABA-I6T1U2 | 600 kHz | Unavailable | Available | Unavailable |
| S-8365ABAAA-M5T1y2 | - | S-8365ABAAA-I6T1U2 | 600 kHz | Unavailable | Unavailable | Unavailable |

Remark 1. Contact our sales office for S-8365AxBAA (without UVLO function, with short-circuit protection).
2. Contact our sales office for S-8365AxxxB (ON/ $\overline{\text { OFF }}$ pin pull-down).
3. $\mathrm{y}: \mathrm{S}$ or U
4. Please select products of environmental code $=U$ for $\mathrm{Sn} 100 \%$, halogen-free products.
(2) S-8366 Series (PWM / PFM switching control)

Table 2

| SOT-23-5 | SOT-23-6 | SNT-6A | Oscillation <br> frequency | Short-circuit <br> protection | UVLO <br> function | ON/OFF <br> pin <br> pull-down |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | S-8366AABBA-M6T1y2 | S-8366AABBA-I6T1U2 | 1.2 MHz | Available | Available | Unavailable |
| S-8366AAABA-M5T1y2 | - | S-8366AAABA-I6T1U2 | 1.2 MHz | Unavailable | Available | Unavailable |
| S-8366AAAAA-M5T1y2 | - | S-8366AAAAA-I6T1U2 | 1.2 MHz | Unavailable | Unavailable | Unavailable |
| - | S-8366ABBBA-M6T1y2 | S-8366ABBBA-I6T1U2 | 600 kHz | Available | Available | Unavailable |
| S-8366ABABA-M5T1y2 | - | S-8366ABABA-I6T1U2 | 600 kHz | Unavailable | Available | Unavailable |
| S-8366ABAAA-M5T1y2 | - | S-8366ABAAA-I6T1U2 | 600 kHz | Unavailable | Unavailable | Unavailable |

Remark 1. Contact our sales office for S-8366AxBAA (without UVLO function, with short-circuit protection).
2. Contact our sales office for S-8366AxxxB (ON/OFF pin pull-down).
3. $\mathrm{y}: \mathrm{S}$ or U
4. Please select products of environmental code $=U$ for $\mathrm{Sn} 100 \%$, halogen-free products.

## ■ Pin Configurations

1. SNT-6A


Figure 4

Table 3 With Short-Circuit Protection

| Pin No. | Symbol | Description |
| :---: | :--- | :--- |
| 1 | EXT | External transistor connection pin |
| 2 | VSS | GND pin |
| 3 | ON/OFF | Power-off pin <br> "H" : Power-on (normal operation) <br> "L" Power-off (standby) |
| 4 | FB | Output voltage feedback pin |
| 5 | CSP | Delay time setting pin for short-circuit <br> protection |
| 6 | VDD | IC power supply pin |

Table 4 Without Short-Circuit Protection

| Pin No. | Symbol | Description |
| :---: | :--- | :--- |
| 1 | EXT | External transistor connection pin |
| 2 | VSS | GND pin |
| 3 | ON $/ \overline{\text { OFF }}$ | Power-off pin <br> "H" : Power-on (normal operation) <br> "L" Power-off (standby) |
| 4 | FB | Output voltage feedback pin |
| 5 | NC"1 | No connection |
| 6 | VDD | IC power supply pin |

*1. The NC pin indicates electrically open.
The NC pin can be connected to VDD or VSS.
2. SOT-23-5

Table 5 Without Short-Circuit Protection
Top view


Figure 5

| Pin No. | Symbol | Description |
| :---: | :--- | :--- |
| 1 | ON/ OFF | Power-off pin <br> "H" : Power-on (normal operation) <br> "L" : Power-off (standby) |
| 2 | VSS | GND pin |
| 3 | EXT | External transistor connection pin |
| 4 | VDD | IC power supply pin |
| 5 | FB | Output voltage feedback pin |

## 3. SOT-23-6

Top view
654


Figure 6
Table 6 With Short-Circuit Protection

| Pin No. | Symbol | Description |
| :---: | :--- | :--- |
| 1 | VDD | IC power supply pin |
| 2 | CSP | Delay time setting pin for <br> short-circuit protection |
| 3 | FB | Output voltage feedback pin |
| 4 | ON/ $\overline{\text { OFF }}$ | Power-off pin <br> "H" : Power-on (normal operation) <br> "L" Power-off (standby) |
| 5 | VSS | GND pin |
| 6 | EXT | External transistor connection pin |

## Absolute Maximum Ratings

Table 7 Absolute Maximum Ratings
( $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{ss}}=0 \mathrm{~V}$ unless otherwise specified)

| Item |  | Symbol | Absolute Maximum Ratings | Unit |
| :---: | :---: | :---: | :---: | :---: |
| VDD pin voltage |  | $V_{D D}$ | $\mathrm{V}_{\mathrm{ss}}-0.3$ to $\mathrm{V}_{\mathrm{ss}}+6.0$ | V |
| FB pin voltage |  | $\mathrm{V}_{\text {Fb }}$ | Vss-0.3 to VdD+0.3 | V |
| EXT pin voltage |  | $\mathrm{V}_{\text {EXT }}$ | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\mathrm{DD}}+0.3$ | V |
| ON/OFF pin voltage |  | Von/OFF | $\mathrm{V}_{\text {ss }}-0.3$ to $\mathrm{V}_{\mathrm{DD}}+0.3$ | V |
| CSP pin voltage |  | Vcsp | $\mathrm{V}_{\text {ss }}-0.3$ to $\mathrm{V}_{\mathrm{DD}}+0.3$ | V |
| Power dissipation | SNT-6A | Pd | $400^{* 1}$ | mW |
|  | SOT-23-5 |  | $600^{* 1}$ | mW |
|  | SOT-23-6 |  | $650{ }^{* 1}$ | mW |
| Operating ambient temperature |  | Topr | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature |  | $\mathrm{T}_{\text {stg }}$ | -40 to +125 | ${ }^{\circ} \mathrm{C}$ |

*1. When mounted on board
[Mounted board]
(1) Board size : $114.3 \mathrm{~mm} \times 76.2 \mathrm{~mm} \times \mathrm{t} 1.6 \mathrm{~mm}$
(2) Name : JEDEC STANDARD51-7

Caution The absolute maximum ratings are rated values exceeding which the product could suffer physical damage. These values must therefore not be exceeded under any conditions.


Figure 7 Package Power Dissipation (When Mounted on Board)

## ■ Electrical Characteristics

1. $\mathbf{1 . 2} \mathrm{MHz}$ product

Table 8 Electrical Characteristics
( $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}, \mathrm{Ta}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| Item | Symbol | Conditions | Min. | Typ. | Max. | Unit | Test Circuit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input voltage*1 | $V_{D D}$ | - | 1.8 | - | 5.5 | V | 2 |
| Operating start voltage*2 | VSt1 | Product without UVLO function, $\text { lout }=1 \mathrm{~mA}$ | - | - | 1.1 | V | 3 |
| Oscillation start voltage | $V_{\text {ST2 }}$ | No external parts for product without UVLO function, | - | - | 1.0 | V | 1 |
| Operation holding voltage | Vhld | Product without UVLO function, lout $=1 \mathrm{~mA}$, Determined by decreasing $V_{D D}$ gradually | 0.8 | - | - | V | 3 |
| FB voltage | $\mathrm{V}_{\text {FB }}$ | - | 0.588 | 0.6 | 0.612 | V | 1 |
| FB voltage temperature coefficient | $\begin{aligned} & \frac{\Delta \mathrm{V}_{\mathrm{FB}}}{\Delta \mathrm{Ta}} \\ & \hline \end{aligned}$ | $\mathrm{Ta}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | - | $\pm 100$ | - | ppm $/{ }^{\circ} \mathrm{C}$ | 1 |
| FB pin input current | IfB | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , FB pin | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
| Current consumption at operation*3 | Iss1 | At switching operation, no load $V_{F B}=V_{F B(S)} \times 0.95$ | - | 500 | - | $\mu \mathrm{A}$ | 1 |
| Current consumption at switching off | Iss2 | At switching stop, $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 1.5$ | - | 70 | 120 | $\mu \mathrm{A}$ | 1 |
| Current consumption at shutdown | Isss | Von/ $/ \overline{\text { FF }}=0 \mathrm{~V}$ | - | - | 1.0 | $\mu \mathrm{A}$ | 1 |
| EXT pin output current | IExTH | $\mathrm{V}_{\text {EXT }}=\mathrm{V}_{\text {DD }}-0.4 \mathrm{~V}$ | - | -130 | -60 | mA | 1 |
|  | lextl | $\mathrm{V}_{\text {EXT }}=0.4 \mathrm{~V}$ | 100 | 200 | - | mA | 1 |
| Oscillation frequency | fosc | - | 1.0 | 1.2 | 1.4 | MHz | 1 |
| Maximum duty ratio | $\begin{array}{\|l} \hline \text { Max } \\ \text { Duty } \\ \hline \end{array}$ | $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 0.95$ | 80 | 85 | 90 | \% | 1 |
| PWM / PFM switching Duty ratio*4 | $\begin{array}{\|l} \hline \text { PFM } \\ \text { Duty } \\ \hline \end{array}$ | $\mathrm{V}_{\text {DD }}=\mathrm{V}_{\text {out }}(\mathrm{s})-0.1 \mathrm{~V}$, no load | 20 | 28 | 36 | \% | 2 |
| Short-circuit protection delay time*5 | tpro | Product with short-circuit protection, $\text { At CSP }=0.1 \mu \mathrm{~F}$ | 37.5 | 50 | 75 | ms | 1 |
| UVLO release voltage | Vuvlo+ | Product with UVLO function | 1.60 | 1.70 | 1.78 | V | 1 |
| UVLO hysteresis width | Vuvlohys | Product with UVLO function | 0.05 | 0.10 | 0.15 | V | 1 |
| High level input voltage | VSH | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\text { OFF }}$ pin | 0.75 | - | - | V | 1 |
| Low level input voltage | $\mathrm{V}_{\text {SL }}$ | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\mathrm{OFF}}$ pin | - | - | 0.3 | V | 1 |
| High level input current | Ish | Product without ON/OFF pin pull-down, $V_{D D}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\mathrm{OFF}} \mathrm{pin}$ | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
|  |  | Product with ON/OFF pin pull-down, $V_{D D}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\mathrm{OFF}} \mathrm{pin}$ | 0.2 | 1.0 | 2.5 | $\mu \mathrm{A}$ | 1 |
| Low level input current | ISL | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , ON/OFF pin | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
| Soft-start time | tss | - | 5 | 7 | 10 | ms | 2 |

*1. The $\mathrm{S}-8365 / 8366$ Series steps up from $\mathrm{V}_{\mathrm{DD}}=1.1 \mathrm{~V}$, but set the input voltage as to $1.8 \mathrm{~V} \leq \mathrm{VDD} \leq 5.5 \mathrm{~V}$ for stabilizing the output voltage and oscillation frequency.
*2. This is the guaranteed value measured with external parts shown in "Table 10 External Parts List" and with test circuits shown in Figure 10. The operating start voltage varies largely depending on diode's forward voltage. Evaluate sufficiently with actual device.
*3. $V_{F B(S)}$ is a setting value for $F B$ voltage.
*4. Vout(s) is a setting value for output voltage. Vout is the typical value of actual output voltage.
$V_{\text {Vout(s) }}$ can be set by using the rate of $\mathrm{V}_{\mathrm{FB}}$ and the output voltage setting resistors ( $\mathrm{R}_{\text {FB1 }}, \mathrm{R}_{\text {FB2 }}$ ).
For details, refer to " $\square$ External Parts Selection".
*5. The short-circuit protection time can be set by the external capacitor, and the maximum set value by the external capacitor is unlimited when an ideal case is assumed. But use CSP = approximately $0.47 \mu \mathrm{~F}$ as a target maximum value due to the need to consider the discharge time of the capacitor.
For details, refer to " $■$ External Parts Selection".

## 2. 600 kHz product

Table 9 Electrical Characteristics
( $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}, \mathrm{Ta}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| Item | Symbol | Conditions | Min. | Typ. | Max. | Unit | Test Circuit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Input voltage*1 | VDD | - | 1.8 | - | 5.5 | V | 2 |
| Operating start voltage*2 | VSt1 | Product without UVLO function, $\text { lout }=1 \mathrm{~mA}$ | - | - | 1.0 | V | 3 |
| Oscillation start voltage | $V_{\text {ST2 }}$ | No external parts for product without UVLO function, | - | - | 0.9 | V | 1 |
| Operation holding voltage | Vhlo | Product without UVLO function, lout $=1 \mathrm{~mA}$, Determined by decreasing VDD gradually | 0.8 | - | - | V | 3 |
| FB voltage | $\mathrm{V}_{\text {FB }}$ | - | 0.588 | 0.6 | 0.612 | V | 1 |
| FB voltage temperature coefficient | $\frac{\Delta \mathrm{V}_{\mathrm{FB}}}{\Delta \mathrm{Ta}}$ | $\mathrm{Ta}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | - | $\pm 100$ | - | ppm $/{ }^{\circ} \mathrm{C}$ | 1 |
| FB pin input current | $\mathrm{I}_{\text {FB }}$ | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , FB pin | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
| Current consumption at operation*3 | Iss1 | At switching operation, no load $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 0.95$ | - | 300 | - | $\mu \mathrm{A}$ | 1 |
| Current consumption at switching off | Iss2 | At switching stop, $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 1.5$ | - | 70 | 120 | $\mu \mathrm{A}$ | 1 |
| Current consumption at shutdown | Isss | Von/ $/ \overline{\text { FF }}=0 \mathrm{~V}$ | - | - | 1.0 | $\mu \mathrm{A}$ | 1 |
| EXT pin output current | Іехтн | $\mathrm{V}_{\text {EXT }}=\mathrm{V}_{\mathrm{DD}}-0.4 \mathrm{~V}$ | - | -130 | -60 | mA | 1 |
|  | IExtL | $\mathrm{V}_{\text {EXT }}=0.4 \mathrm{~V}$ | 100 | 200 | - | mA | 1 |
| Oscillation frequency | fosc | - | 510 | 600 | 690 | kHz | 1 |
| Maximum duty ratio | Max <br> Duty | $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 0.95$ | 85 | 90 | 95 | \% | 1 |
| PWM / PFM switching Duty ratio ${ }^{*}$ | $\begin{array}{\|l} \hline \text { PFM } \\ \text { Duty } \\ \hline \end{array}$ | $\mathrm{V}_{\text {DD }}=\mathrm{V}_{\text {Out }}(\mathrm{s})-0.1 \mathrm{~V}$, no load | 20 | 28 | 36 | \% | 2 |
| Short-circuit protection delay time*5 | tpro | Product with short-circuit protection, $\text { At CSP }=0.1 \mu \mathrm{~F}$ | 37.5 | 50 | 75 | ms | 1 |
| UVLO release voltage | Vuvlo+ | Product with UVLO function | 1.60 | 1.70 | 1.78 | V | 1 |
| UVLO hysteresis width | Vuvlohys | Product with UVLO function | 0.05 | 0.10 | 0.15 | V | 1 |
| High level input voltage | $\mathrm{V}_{\text {SH }}$ | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\mathrm{OFF}}$ pin | 0.75 | - | - | V | 1 |
| Low level input voltage | VsL | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , ON/OFF pin | - | - | 0.3 | V | 1 |
| High level input current | Ish | Product without ON/OFF pin pull-down, $V_{D D}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\mathrm{OFF}} \mathrm{pin}$ | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
|  |  | Product with ON/ $\overline{\text { OFF }}$ pin pull-down, $V_{D D}=1.8 \mathrm{~V}$ to 5.5 V , ON/ $\overline{\text { OFF }}$ pin | 0.2 | 1.0 | 2.5 | $\mu \mathrm{A}$ | 1 |
| Low level input current | ISL | $\mathrm{V}_{\mathrm{DD}}=1.8 \mathrm{~V}$ to 5.5 V , ON/OFF pin | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
| Soft-start time | tss | - | 5 | 7 | 10 | ms | 2 |

*1. The $\mathrm{S}-8365 / 8366$ Series steps up from $\mathrm{V}_{\mathrm{DD}}=1.0 \mathrm{~V}$, but set the input voltage as to $1.8 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD}} \leq 5.5 \mathrm{~V}$ for stabilizing the output voltage and oscillation frequency.
*2. This is the guaranteed value measured with external parts shown in "Table 10 External Parts List" and with test circuits shown in Figure 10. The operating start voltage varies largely depending on diode's forward voltage. Evaluate sufficiently with actual device.
*3. $\quad \mathrm{V}_{\mathrm{FB}(\mathrm{S})}$ is a setting value for FB voltage.
*4. Vout(s) is a setting value for output voltage. Vout is the typical value of actual output voltage. $V_{\text {Out(S) }}$ can be set by using the rate of $\mathrm{V}_{\mathrm{FB}}$ and the output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}, \mathrm{R}_{\mathrm{FB}}$ ).
For details, refer to " $\square$ External Parts Selection".
*5. The short-circuit protection time can be set by the external capacitor, and the maximum set value by the external capacitor is unlimited when an ideal case is assumed. But use CSP = approximately $0.47 \mu \mathrm{~F}$ as a target maximum value due to the need to consider the discharge time of the capacitor.
For details, refer to " $■$ External Parts Selection".

## ■ External Parts List When Measuring Electrical Characteristics

Table 10 External Parts List

| Element Name | Symbol | Consonants | Manufacturer | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| Inductor | L | $2.2 \mu \mathrm{H}$ (1.2 MHz product) | TAIYO YUDEN Co., Ltd. | NR6028T |
|  |  | $3.3 \mu \mathrm{H}$ ( 600 kHz product) | TDK Corporation | LTF5022 |
| Transistor | M1 | - | Vishay Intertechnology, Inc. | Si3460BDV |
|  | Q1 | - | TOSHIBA CORPORATION | 2SD2652 |
| Diode | SD | - | SHINDENGEN ELECTRIC MANUFACTURING CO.,LTD | D1FH3 |
| Input capacitor | $\mathrm{C}_{\text {IN }}$ | $10 \mu \mathrm{~F}$ | TDK Corporation | C3225X7R1E106MB |
| Output capacitor | Cout | $22 \mu \mathrm{~F}$ | TDK Corporation | C4532X7R1E226MB |
| FB pin capacitor | Cfb | 47 pF | Murata Manufacturing Co., Ltd. | GRM1882C1H series |
| CSP pin capacitor | CSP | $0.1 \mu \mathrm{~F}$ | TDK Corporation | C1220X7R1E104MB |
| Speed-up capacitor | $\mathrm{C}_{\mathrm{b}}$ | 2200 pF | TDK Corporation | C1005X7R1H222K |
| Base resistor | $\mathrm{R}_{\mathrm{b}}$ | $1 \mathrm{k} \Omega$ | ROHM Co., Ltd. | MCR03 series |
| Output voltage setting resistor 1 | $\mathrm{R}_{\text {FB1 }}$ | $220 \mathrm{k} \Omega$ | ROHM Co., Ltd. | MCR03 series |
| Output voltage setting resistor 2 | R $\mathrm{FB}^{2}$ | $30 \mathrm{k} \Omega$ | ROHM Co., Ltd. | MCR03 series |

## ■ Test Circuits

1. 



Figure 8
2.


Figure 9
3.


Figure 10

## ■ Operation

## 1. Switching control method

### 1.1 PWM control (S-8365 Series)

The S-8365 Series is a switching regulator controller that uses a pulse width modulation method (PWM). In conventional PFM control switching regulators, pulses are skipped when the output load current is small, causing a fluctuation in the ripple frequency of the output voltage, resulting in increased ripple voltage.
For the S-8365 Series, although the pulse width changes from $0 \%$ to $90 \%$ in accordance with each load current (or $0 \%$ to $85 \%$ for 1.2 MHz products), since the switching frequency does not change, the ripple voltage generated due to switching can be eliminated by filtering. The ripple voltage can thus be lowered in the wide input voltage and load current ranges.

### 1.2 PWM / PFM switching control (S-8366 Series)

The S-8366 Series switching regulator controller automatically switches between the pulse width modulation method (PWM) and pulse frequency modulation method (PFM) according to the load current.
A low ripple power can be supplied by operating on PWM control for which the pulse width changes from $28 \%$ to $90 \%$ (or $28 \%$ to $85 \%$ for 1.2 MHz products) in the range where the output load current is large.
The S-8366 Series operates on PFM control when the output load current is small and the fixed pulses which have the width of $28 \%$ are skipped according to the load current amount. Therefore, the oscillation circuit intermittently oscillates, reducing the self-current consumption. This avoids decreased efficiency when the output load current is small. The point at which PWM control switches to PFM control varies depending on the external element (inductor, diode, etc.), input voltage value, and output voltage value, and this method achieves high efficiency in the output load current of about $100 \mu \mathrm{~A}$.

## 2. Soft-start function

The S-8365/8366 Series has a soft-start circuit. The output voltage (Vout) gradually rises after power-on or startup when the ON/ $\overline{\mathrm{OFF}}$ pin is set to high, suppressing rush current and overshooting the output voltage. The soft-start time (tss) for the S-8365/8366 Series is defined as the time from startup until Vout reaches $90 \%$ of the output set voltage value (Vout(s)). A reference voltage adjustment method is used as the soft-start method and the reference voltage gradually rises from 0 V after soft-start.
A soft-start performs by controlling the FB pin voltage so that it follows the rise of the reference voltage. After the reference voltage rises once, it is reset to 0 if the ON/OFF pin voltage drops to low, the power supply voltage drops to the UVLO detection voltage, or the S-8365/8366 Series enters the short-circuit protection latch status. A soft-start is performed regardless of conditions when resuming step-up operation.

## 3. Shutdown pin

This pin stops or starts step-up operations.

### 3.1 Without ON/OFF pin pull-down

When this pin is set to the low level, the voltage of the EXT pin is fixed to 0 V , and the external transistor and all internal circuits stop, substantially reducing the current consumption.
Do not use the ON/ $\overline{\text { OFF }}$ pin in a floating state because it is set up as shown in Figure 11 and is not internally pulled up or down. Do not apply a voltage of between 0.3 V and 0.75 V to the ON/OFF pin because applying such a voltage increases the current consumption. If the ON/OFF pin is not used, connect it to the VDD pin.

Table 11

| ON/OFF pin | CR Oscillation <br> Circuit | Output Voltage |
| :---: | :---: | :---: |
| "H" | Operates | Set value |
| "L" | Stops | $\cong V_{\text {IN }}{ }^{* 1}$ |

*1. Voltage obtained by subtracting the voltage drop due to the DC resistance of the inductor and the diode forward voltage from $\mathrm{V}_{\mathrm{IN}}$.


Figure 11

### 3.2 With ON/ $\overline{\text { OFF }}$ pin pull-down

When the ON/ $\overline{O F F}$ pin is set to the low level, the voltage of the EXT pin is fixed to 0 V , and the external transistor and all internal circuits stop substantially reducing the current consumption.
The ON/ $\overline{\mathrm{OFF}}$ pin is set up as shown in Figure 12 and is internally pulled down by using the depression transistor, so all circuits stop even if this pin is floating. Do not apply a voltage of between 0.3 V and 0.75 V to the ON/ $\overline{\mathrm{OFF}}$ pin because applying such a voltage increases the current consumption. If the ON/ $\overline{\mathrm{OFF}}$ pin is not used, connect it to the VDD pin.

Table 12

| ON/OFF Pin | CR Oscillation <br> Circuit | Output Voltage |
| :---: | :---: | :---: |
| "H" | Operates | Set value |
| "L" | Stops | $\cong V_{I N}{ }^{* 1}$ |
| High-Z | Stops | $\cong V_{I N}{ }^{* 1}$ |

*1. Voltage obtained by subtracting the voltage drop due to the DC resistance of the inductor and the diode forward voltage from Vin.


Figure 12

## 4. Timer latch type short-circuit protection (products with short-circuit protection function)

The S-8365/8366 Series incorporates a timer latch type short-circuit protection circuit that stops switching operation if the output short circuits for a certain time or more. Connect a capacitor (CSP) to the CSP pin to set the delay time of this circuit.
The S-8365/8366 Series operates on the maximum duty if the output voltage drops due to output short-circuiting or other factors. When it enters the maximum duty status, charging the constant current to CSP is started. If this status is held for the short-circuit protection delay time or more, the voltage of the CSP pin exceeds the reference voltage and the IC enters the latch mode.
Note that switching operation stops in latch mode but the internal circuits normally operate, which differs from the power-off status. The constant current is continuously charged to CSP even in latch mode, so the voltage of the CSP pin rises to the Vdo level.
To reset the latch mode of short-circuit protection, lower $V_{D D}$ to the UVLO detection voltage or lower or set the ON/ $\overline{\mathrm{OFF}}$ pin to the low level.


Figure 13

## 5. UVLO function (products with UVLO function)

The S-8365/8366 Series has a UVLO (undervoltage lockout) circuit for avoiding IC malfunctions due to power supply voltage drops. The S-8365/8366 Series stops switching operation upon UVLO detection and retains the external transistor in the off state. After entering the UVLO detection status once, the soft-start function is reset. Note, however, that the other internal circuits operate normally and that the status differs from the power-off status.

## Operation Principles

The S-8365/8366 Series is a step-up switching regulator controller. Figure 14 shows the basic circuit diagram.
Step-up switching regulators start current supply by the input voltage $(\mathrm{V} / \mathrm{N})$ when the Nch power MOS FET is turned on and holds energy in the inductor at the same time. When the Nch power MOS FET is turned off, the CONT pin voltage is stepped up to discharge the energy held in the inductor and the current is discharged to Vout through the diode. When the discharged current is stored in CL, a voltage is generated, and the potential of Vout increases until the voltage of the FB pin reaches the same potential as the internal reference voltage.
For the PWM control method, the switching frequency (fosc) is fixed and the Vout voltage is held constant according to the ratio of the ON time and OFF time (ON duty) of the Nch power MOS FET in each period.
For the PWM control method, the Vout voltage is held constant by controlling the ON time.
In the S-8366 Series, the Nch power MOS FET is turned on when the fixed duty cycle is $28 \%$ for the PFM control method. When energy is discharged to Vout once and the Vout potential exceeds the set value, the Nch power MOS FET stays in the off status until Vout decreases to the set value or less due to the load discharge. Time Vout decreases to the set value or less depends on the amount of load current, so, the switching frequency varies depending on this current.


Figure 14 Basic Circuit of Step-up Switching Regulator
The ON duty in the current continuous mode can be calculated by using the equation below. Use the S-8365/8366 Series in the range where the ON duty is less than the maximum duty. Note that the products with short-circuit protection is set in the timer-latch status if the maximum duty lasts the short-circuit protection delay time (tpro) or more.
The maximum duty is $85 \%$ typ. for 1.2 MHz products and $90 \%$ for 600 kHz products.

$$
\text { ON duty }=\left(1-\frac{V_{\text {IN }}}{V_{\text {OUT }}+V_{D^{* 1}}}\right) \times 100[\%]
$$

The ON time (ton) can be calculated by using the following equation :

$$
\begin{align*}
\text { ton } & =\frac{1}{f_{\text {OSC }}} \times \text { ON duty } \\
& =\frac{1}{f_{\text {OSC }}} \times\left(1-\frac{V_{\text {IN }}}{V_{\text {OUT }}+V_{D}^{* 1}}\right) \tag{1}
\end{align*}
$$

*1. $V_{D}$ : Forward voltage of diode

## 1. Continuous current mode

The following explains the current that flows into the inductor when the step-up operation stabilizes in a certain status and lout is sufficiently large.
When the Nch power MOS FET is turned on, current ( $I_{1}$ ) flows in the direction shown in Figure 14. The inductor current (IL) at this time gradually increases in proportion with the ON time (ton) of the Nch power MOS FET.

Current change of inductor within ton :
$\Delta \mathrm{I}_{\mathrm{L}(\mathrm{ON})}=\mathrm{I} \mathrm{L}$ max. $-\mathrm{I}_{\mathrm{L}}$ min.

$$
=\frac{V_{\mathbb{I N}}}{L} \times \text { toN }
$$

When the Nch power MOS FET is turned off, the voltage of the CONT pin is stepped up to Vout $+\mathrm{V}_{\mathrm{D}}$ and the voltage on both ends of the inductor becomes $V_{\text {out }}+V_{D}-V_{\text {In }}$. However, it is assumed here that $V_{\text {out }} \gg V_{D}$ and $V_{D}$ is ignored.

Current change of inductor within toff:

$$
\Delta L_{\text {LOFF })}=\frac{V_{\text {OUT }}-V_{\text {IN }}}{L} \times \text { toFF }
$$

The input power equals the output power in an ideal situation where there is no loss by components.
lin(AV):

$$
\begin{align*}
& P_{\text {IN }}=P_{\text {OUT }} \\
& \mathrm{I}_{\text {IN }(\mathrm{AV})} \times \mathrm{V}_{\text {IN }}=\text { IoUT } \times \mathrm{V}_{\text {OUT }} \\
& \therefore \operatorname{IIN(AV)}=\frac{\mathrm{VOUT}^{\mathrm{VIN}_{\text {IN }}} \times \operatorname{IOUT} \ldots .}{} \tag{2}
\end{align*}
$$

The current that flows in the inductor consists of a ripple current that changes due to variation over time and a direct current.

From Figure 15 :
$\operatorname{lin}(A V):$

$$
\begin{align*}
\operatorname{IIN(AV)} & =\operatorname{IIN(DC)}+\frac{\Delta \operatorname{l}_{\mathrm{L}}}{2} \\
& =\operatorname{IIN(DC)}+\frac{\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}}{2 \times \mathrm{L}} \times \text { toFF } \\
& =\operatorname{IIN(DC)}+\frac{\mathrm{V}_{\text {IN }}}{2 \times \mathrm{L}} \times \text { ton.......... } \tag{3}
\end{align*}
$$

Above, the continuous mode is the operation mode when $\operatorname{lin(DC)}>0$ as shown in Figure 15 and the inductor current continuously flows.
While the output current (lout) continues to decrease, $\operatorname{liN(DC)}$ reaches 0 as shown in Figure 16. This point is the critical point of the continuous mode.
As shown in equations (2) and (3), the direct current component (lin(DC)) depends on lout.
Iout(0) when $\operatorname{lin(DC)}$ reaches 0 (critical point):

$$
\operatorname{loUT}(0)=\frac{\mathrm{ton} \times \mathrm{V}_{\text {IN }}{ }^{2}}{2 \times \mathrm{L} \times \mathrm{V}_{\text {OUT }}}
$$

ton can be calculated using equation (1).
When the output current decreases below lout(0), the current flowing in the inductor stops flowing in the toff period as shown in Figure 17. This is the discontinuous mode.


Figure 15 Continuous Mode (Current Cycle of Inductor Current IL)


Figure 16 Critical Point (Current Cycle of Inductor Current IL)


Figure 17 Discontinuous Mode (Current Cycle of Inductor Current IL)

## ■ External Parts Selection

## 1. Inductor

The recommended $L$ value of the $\mathrm{S}-8365 / 8366$ Series is $2.2 \mu \mathrm{H}$ for 1.2 MHz products and $3.3 \mu \mathrm{H}$ for 600 kHz products.
Note the following when changing the inductance.
The inductance ( L ) has a strong influence on the maximum output current (lout) and efficiency ( $\eta$ ).
The inductor peak current (IPK) increases when $L$ is decreased, which improves the circuit stability and increases the lout users can obtain. If $L$ is decreased further, the ability of the external transistor to drive the current becomes insufficient, reducing the efficiency and decreasing lout.
The loss due to the lpk of the switching transistor is decreased by increasing $L$ and the efficiency maximizes at a certain $L$ value. If $L$ is increased further, the loss due to the serial resistance of the inductor increases, lowering the efficiency.

Caution When selecting an inductor, be careful about its allowable current. If a current exceeding the allowable current flows through the inductor, magnetic saturation occurs, substantially lowering the efficiency and destroying ICs due to large current. Therefore, select an inductor such that lpk does not exceed the allowable current. The following equations express IPK in the ideal statuses in the discontinuous and continuous modes :

$$
\begin{array}{ll}
I_{\text {PK }}=\sqrt{\frac{2 \times \text { IOUT } \times\left(V_{\text {OUT }}+V_{D}^{* 2}-V_{\text {IN }}\right)}{f o s c^{* 1} \times L}} & \text { (Discontinuous mode) } \\
I_{\text {PK }}=\frac{V_{\text {OUT }}+V_{D}{ }^{* 2}}{V_{\text {IN }}} \times \text { IoUT }+\frac{\left(V_{\text {OUT }}+V_{D}{ }^{* 2}-V_{\text {IN }}\right) \times V_{\text {IN }}}{2 \times\left(V_{\text {OUT }}+V_{D}{ }^{* 2}\right) \times f_{\text {Oscc }} \times \mathrm{L}} \times & \text { (Continuous mode) }
\end{array}
$$

*1. fosc : oscillation frequency
*2. $V_{D}$ is the forward voltage of a diode. The reference value is 0.4 V .
However, current exceeding the above equation flows because conditions are practically not ideal. Perform sufficient evaluation with actual application.

Table 13 Typical Inductors (for Small Low-Profile Devices)

| Manufacture | Product Name | L Value | DC Resistance | Rated Current | Dimensions $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ [mm] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TDK Corporation | VLF3010ST-2R2M | $2.2 \mu \mathrm{H}$ | $0.092 \Omega$ max. | 1.1 A max. | $2.8 \times 3.0 \times 1.0$ |
|  | VLF3010ST-3R3M | $3.3 \mu \mathrm{H}$ | $0.130 \Omega$ max. | 0.88 A max. | $2.8 \times 3.0 \times 1.0$ |
|  | VLS252010-2R2M | $2.2 \mu \mathrm{H}$ | $0.190 \Omega$ max. | 1.2 A max. | $2.5 \times 2.0 \times 1.0$ |
|  | VLS252010-3R3M | $3.3 \mu \mathrm{H}$ | $0.304 \Omega$ max. | 1.0 A max. | $2.5 \times 2.0 \times 1.0$ |
| Coilcraft, Inc. | LPS3008-222ML | $2.2 \mu \mathrm{H}$ | $0.175 \Omega$ max. | 1.1 A max. | $3.0 \times 3.0 \times 0.8$ |
|  | LPS3008-332ML | $3.3 \mu \mathrm{H}$ | $0.285 \Omega$ max. | 0.88 A max. | $3.0 \times 3.0 \times 0.8$ |
| Taiyo Yuden Co., Ltd. | NR3010T2R2M | $2.2 \mu \mathrm{H}$ | $0.114 \Omega$ max. | 1.1 A max. | $3.0 \times 3.0 \times 1.0$ |
|  | NR3010T3R3M | $3.3 \mu \mathrm{H}$ | $0.168 \Omega$ max. | 0.87 A max. | $3.0 \times 3.0 \times 1.0$ |
| Sumida Corporation | CDRH2D11BNP-2R2N | $2.2 \mu \mathrm{H}$ | $0.0955 \Omega$ max. | 1.4 A max. | $3.0 \times 3.0 \times 1.2$ |
|  | CDRH2D11BNP-3R3N | $3.3 \mu \mathrm{H}$ | $0.154 \Omega$ max. | 1.0 A max. | $3.0 \times 3.0 \times 1.2$ |

Table 14 Typical Inductors (for Large Current, High Step-up Rate)

| Manufacture | Product Name | L Value | DC Resistance | Rated <br> Current | Dimensions $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ <br> $[\mathrm{mm}]$ |
| :--- | :--- | :---: | :---: | :---: | :---: |
| TDK Corporation | LTF5022T-2R2M | $2.2 \mu \mathrm{H}$ | $0.040 \Omega$ max. | $3.4 \mathrm{~A} \mathrm{max}$. | $5.0 \times 5.2 \times 2.2$ |
|  | LTF5022T-3R3M | $3.3 \mu \mathrm{H}$ | $0.060 \Omega$ max. | $2.7 \mathrm{~A} \mathrm{max}$. | $5.0 \times 5.2 \times 2.2$ |
| Coilcraft, Inc. | LPS6225-222ML | $2.2 \mu \mathrm{H}$ | $0.045 \Omega$ max. | $4.1 \mathrm{~A} \mathrm{max}$. | $6.0 \times 6.0 \times 2.4$ |
|  | LPS6225-332ML | $3.3 \mu \mathrm{H}$ | $0.055 \Omega$ max. | $3.6 \mathrm{~A} \mathrm{max}$. | $6.0 \times 6.0 \times 2.4$ |
| Taiyo Yuden Co., Ltd. | NR6028T2R2M | $2.2 \mu \mathrm{H}$ | $0.020 \Omega$ max. | $4.2 \mathrm{~A} \mathrm{max}$. | $6.0 \times 6.0 \times 2.8$ |

## 2. Diode

Use an externally mounted that meets the following conditions.

- Low forward voltage (Schottky barrier diode or similar type)
- High switching speed
- Reverse withstand voltage of Vout + spike voltage or more
- Rated current of Ipk or more


## 3. Input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) and output capacitor ( $\mathrm{C}_{\text {оut }}$ )

To improve efficiency, an input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) lowers the power supply impedance and averages the input current. Select $\mathrm{C}_{\mathrm{IN}}$ according to the impedance of the power supply used. The recommended capacitance is $10 \mu \mathrm{~F}$ for the S-8365/8366 Series.
An output capacitor (Cout), which is used to smooth the output voltage, requires a capacitance larger than that of the step-down type because the current is intermittently supplied from the input to the output side in the step-up type. A $22 \mu \mathrm{~F}$ ceramic capacitor is recommended for the S-8365/8366 Series. However, a higher capacitance is recommended if the output voltage is high or the load current is large. If the output voltage or load current is low, about $10 \mu \mathrm{~F}$ can be used without problems.
Select Cout after sufficient evaluation with actual application.
A ceramic capacitor can be used for both the input and output.

## 4. Capacitor for setting short-circuit protection delay time (CSP) (products with short-circuit protection)

For the S-8365/8366 Series, the short-circuit protection delay time can be set to any value by using an external capacitor. Connect the capacitor between the CSP and VSS pins. Select the capacitor value according to the equation below and Figure 18.
Note, however, that the equation and figure show a theoretical value assuming an ideal capacitor value and typ. IC conditions. Variations of the capacitor and IC are not considered.
For the IC variations, see the short-circuit protection delay time (tpRo) in "■ Electrical Characteristics".

$$
\operatorname{CSP}[\mu \mathrm{F}] \cong \frac{\mathrm{tpRO}[\mathrm{~ms}] \times 1.2 \times 10^{-3}}{0.6}
$$



Figure 18 CSP vs. tPRo

## 5. External transistor

A bipolar (NPN) or enhanced (Nch) MOS FET transistor can be used as an external transistor.

### 5.1 Bipolar NPN type

The driving ability to increase output current by using a bipolar transistor is determined based on the hfe value and $R_{b}$ value of the bipolar transistor. Figure 19 shows the peripheral circuit.


Figure 19 External Transistor Peripheral Circuit
The recommended $R_{b}$ value is around $1 \mathrm{k} \Omega$. Calculate the required base current ( $l_{b}$ ) based on the $h_{F E}$ value of the bipolar transistor by using $\mathrm{I}_{\mathrm{b}}=\frac{\mathrm{I}_{\mathrm{PK}}}{\mathrm{h}_{\mathrm{FE}}}$, and then select an $\mathrm{R}_{\mathrm{b}}$ value smaller than that determined using:
$R_{b}=\frac{V_{D D}-0.7}{\mathrm{I}_{\mathrm{b}}}-\frac{0.4}{\left|\mathrm{I}_{\text {EXTH }}\right|}$
Smaller $\mathrm{R}_{\mathrm{b}}$ values increase the output current, but decrease the efficiency. Actually, the current might flow on pulses or the $V_{D D}$ or $V_{S S}$ voltage might drop due to wiring resistance, so determine the optimum value based on experimentation.
Inserting a speed-up capacitor $\left(\mathrm{C}_{b}\right)$ in parallel with the $\mathrm{R}_{\mathrm{b}}$ resistor as shown in Figure 19 reduces switching loss and increases efficiency.
Select a speed-up capacitor for which the $C_{b}$ value satisfies $C_{b} \leq \frac{1}{2 \times \pi \times R_{b} \times \text { fosc } \times 0.7}$.
Actually, however, the optimum $C_{b}$ value varies depending on the characteristics of the bipolar transistor used, so determine the optimum value based on experimentation.

### 5.2 Enhanced MOS FET type

Use an Nch power MOS FET. A MOS FET that has low ON-resistance (Ron) and input capacitance (CIss) is ideal for gaining efficiency. The ON-resistance and input capacitance generally have a tradeoff relationship. ON-resistance is efficient in the range where the output current is high with relatively low frequency switching, and input capacitance is efficient in the range where the output current is medium to low with high frequency switching. Therefore, select a MOS FET for which the ON-resistance and input capacitance are optimum under your usage conditions.
The input voltage ( $V_{D D}$ ) is supplied as the gate voltage of a MOS FET, so select a MOS FET for which the gate withstand voltage is higher than the maximum value used for the input voltage, and for which the drain withstand voltage is greater than or equal to the output voltage ( $\mathrm{V}_{\text {OUT }}$ ) + the forward voltage of the diode ( $\mathrm{V}_{\mathrm{D}}$ ).
If a MOS FET for which the threshold value is near the UVLO detection voltage is used, a high current flows upon power-on, and, in the worst case, the output voltage might not increase and the timer latch type short-circuit protection circuit might operate. Therefore, select a MOS FET for which the threshold value is sufficiently lower than the UVLO detection voltage.

## 6. Output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}, \mathrm{R}_{\mathrm{FB} 2}$ ), capacitor for phase compensation ( $\mathrm{C}_{\mathrm{FB}}$ )

For the S-8365/8366 Series, Vоut can be set to any value by using external divider resistors. Connect the divider resistors between the VOUT and VSS pins.
Because $\mathrm{V}_{\mathrm{FB}}=0.6 \mathrm{~V}$ typ., $\mathrm{V}_{\text {out }}$ can be calculated by using the following equation :

$$
V_{\text {OUT }}=\frac{R_{F B 1}+R_{F B 2}}{R_{F B 2}} \times 0.6
$$

Connect divider resistors $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\mathrm{FB} 2}$ as close to the IC as possible to minimize the effects of noise. If noise has an effect, adjust the values of $R_{F B 1}$ and $R_{F B 2}$ so that $R_{F B 1}+R_{F B 2}<100 \mathrm{k} \Omega$.
$C_{F B}$, which is connected in parallel with $R_{F B 1}$, is a capacitor for phase compensation.
By setting the zero point (the phase feedback) by adding capacitor $C_{\text {FB }}$ to output voltage setting resistor RFB1 in parallel, the phase margin increases, improving the stability of the feedback loop. To effectively use the feedback portion of the phase based on the zero point, define $\mathrm{C}_{\text {FB }}$ by using the following equation :

$$
C_{F B} \cong \frac{\sqrt{L \times C_{O U T}}}{3 \times R_{F B 1}} \times \frac{V_{O U T}}{V_{D D}}
$$

This equation is only a guide.
The following explains the optimum setting.
To efficiently use the feedback portion of the phase based on the zero point, specify settings so that the phase feeds back at the zero point frequency ( $f_{z e r o}$ ) of $R_{F B 1}$ and $C_{F B}$ according to the phase delay at the pole frequency (fpole) of $L$ and Cout. The zero point frequency is generally set slightly higher than the pole frequency.
The following equations are used to determine the pole frequency of $L$ and Cout and the zero point frequency set using $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{C}_{\mathrm{Fb}}$.

$$
\begin{aligned}
& \mathrm{f}_{\text {pole }} \cong \frac{1}{2 \times \pi \times \sqrt{L \times C_{\text {OUT }}}} \times \frac{V_{D D}}{V_{\text {OUT }}} \\
& \mathrm{f}_{\text {zero }} \cong \frac{1}{2 \times \pi \times R_{F B 1} \times \mathrm{C}_{F B}}
\end{aligned}
$$

The transient response can be improved by setting the zero point frequency in a lower frequency range. If, however, the zero point frequency is set in a significantly lower range, the gain increases in the range of high frequency and the phase margin decreases. This might result in unstable operation. Determine the proper value after sufficient evaluation with actual application.

The typical constants based on our evaluation are shown in Table 15.
Table 15 Example of Constant for External Parts

| $V_{\text {Out }(S)}[\mathrm{V}]$ | $\mathrm{V}_{\mathrm{DD}}[\mathrm{V}]$ | $\mathrm{R}_{\mathrm{FB} 1}[\mathrm{k} \Omega]$ | $\mathrm{R}_{\mathrm{FB} 2}[\mathrm{k} \Omega]$ | $\mathrm{C}_{\text {FB }}[\mathrm{pF}]$ | $\mathrm{L}[\mu \mathrm{H}]$ | Cout $[\mu \mathrm{F}]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.8 | 1.2 | 30 | 15 | 100 | 3.3 | 10 |
| 1.8 | 1.2 | 30 | 15 | 82 | 2.2 | 10 |
| 3.32 | 1.2 | 68 | 15 | 82 | 3.3 | 10 |
| 3.32 | 1.2 | 68 | 15 | 68 | 2.2 | 10 |
| 5.0 | 1.8 | 110 | 15 | 68 | 3.3 | 22 |
| 5.0 | 1.8 | 110 | 15 | 56 | 2.2 | 22 |
| 9.0 | 3.3 | 210 | 15 | 39 | 3.3 | 22 |
| 9.0 | 3.3 | 210 | 15 | 33 | 2.2 | 22 |
| 15.0 | 3.3 | 360 | 15 | 39 | 3.3 | 22 |
| 15.0 | 3.3 | 360 | 15 | 33 | 2.2 | 22 |

## ■ Standard Circuit

(1) With short-circuit protection (SNT-6A, SOT-23-6)


Figure 20
(2) Without short-circuit protection (SOT-23-5)


Figure 21
(3) Low input voltage (SOT-23-5)


Figure 22
Caution The above connection diagram and constant will not guarantee successful operation. Perform thorough evaluation using an actual application to set the constants.

## Precaution

- Mount external capacitors and inductor as close as possible to the IC. Set single point ground.
- Characteristics ripple voltage and spike noise occur in IC containing switching regulators. Moreover rush current flows at the time of a power supply injection. Because these largely depend on the inductor, the capacitor and impedance of power supply used, fully check them using an actually mounted model.
- The $0.1 \mu \mathrm{~F}$ capacitor connected between the VDD and VSS pins is a bypass capacitor. It stabilizes the power supply in the IC when application is used with a heavy load, and thus effectively works for stable switching regulator operation. Allocate the bypass capacitor as close to the IC as possible, prioritized over other parts.
- Although the IC contains a static electricity protection circuit, static electricity or voltage that exceeds the limit of the protection circuit should not be applied.
- The power dissipation of the IC greatly varies depending on the size and material of the board to be connected. Perform sufficient evaluation using an actual application before designing.
- SII Semiconductor Corporation claims no responsibility for any disputes arising out of or in connection with any infringement by products including this IC of patents owned by a third party.


[^0]:    *1. Refer to the tape drawing.

