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SA58632

2 × 2.2 W BTL audio amplifier

Rev. 02 — 4 March 2010

Product data sheet

1. General description

The SA58632 is a two-channel audio amplifier in an HVQFN20 package. It provides power output of 2.2 W per channel with an 8 Ω load at 9 V supply. The internal circuit is comprised of two BTL (Bridge-Tied Load) amplifiers with a complementary PNP-NPN output stage and standby/mute logic. The SA58632 is housed in a 20-pin HVQFN package, which has an exposed die attach paddle enabling reduced thermal resistance and increased power dissipation.

2. Features

- Low junction-to-ambient thermal resistance using exposed die attach paddle
- Gain can be fixed with external resistors from 6 dB to 30 dB
- Standby mode controlled by CMOS-compatible levels
- Low standby current < 10 μ A
- No switch-on/switch-off plops
- High power supply ripple rejection: 50 dB minimum
- ElectroStatic Discharge (ESD) protection
- Output short-circuit to ground protection
- Thermal shutdown protection

3. Applications

- Professional and amateur mobile radio
- Portable consumer products: toys and games
- Personal computer remote speakers

4. Quick reference data

Table 1. Quick reference data

$V_{CC} = 6\text{ V}$; $T_{amb} = 25\text{ }^{\circ}\text{C}$; $R_L = 8\text{ }\Omega$; $V_{MODE} = 0\text{ V}$; measured in test circuit [Figure 3](#); unless otherwise specified.

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
V_{CC}	supply voltage	operating	2.2	9	18	V
I_q	quiescent current	$R_L = \infty\text{ }\Omega$	[1] -	15	22	mA
I_{stb}	standby current	$V_{MODE} = V_{CC}$	-	-	10	μA
P_o	output power	THD+N = 10 %	1.2	1.5	-	W
		THD+N = 0.5 %	0.9	1.1	-	W
		THD+N = 10 %; $V_{CC} = 9\text{ V}$	-	2.2	-	W
THD+N	total harmonic distortion-plus-noise	$P_o = 0.5\text{ W}$	-	0.15	0.3	%
PSRR	power supply rejection ratio		[2] 50	-	-	dB
			[3] 40	-	-	dB

- [1] With a load connected at the outputs the quiescent current will increase, the maximum of this increase being equal to the DC output offset voltage divided by R_L .
- [2] Supply voltage ripple rejection is measured at the output with a source impedance of $R_s = 0\text{ }\Omega$ at the input. The ripple voltage is a sine wave with a frequency of 1 kHz and an amplitude of 100 mV (RMS), which is applied to the positive supply rail.
- [3] Supply voltage ripple rejection is measured at the output, with a source impedance of $R_s = 0\text{ }\Omega$ at the input. The ripple voltage is a sine wave with a frequency between 100 Hz and 20 kHz and an amplitude of 100 mV (RMS), which is applied to the positive supply rail.

5. Ordering information

Table 2. Ordering information

Type number	Package		
	Name	Description	Version
SA58632BS	HVQFN20	plastic thermal enhanced very thin quad flat package; no leads; 20 terminals; body $6 \times 5 \times 0.85\text{ mm}$	SOT910-1

6. Block diagram

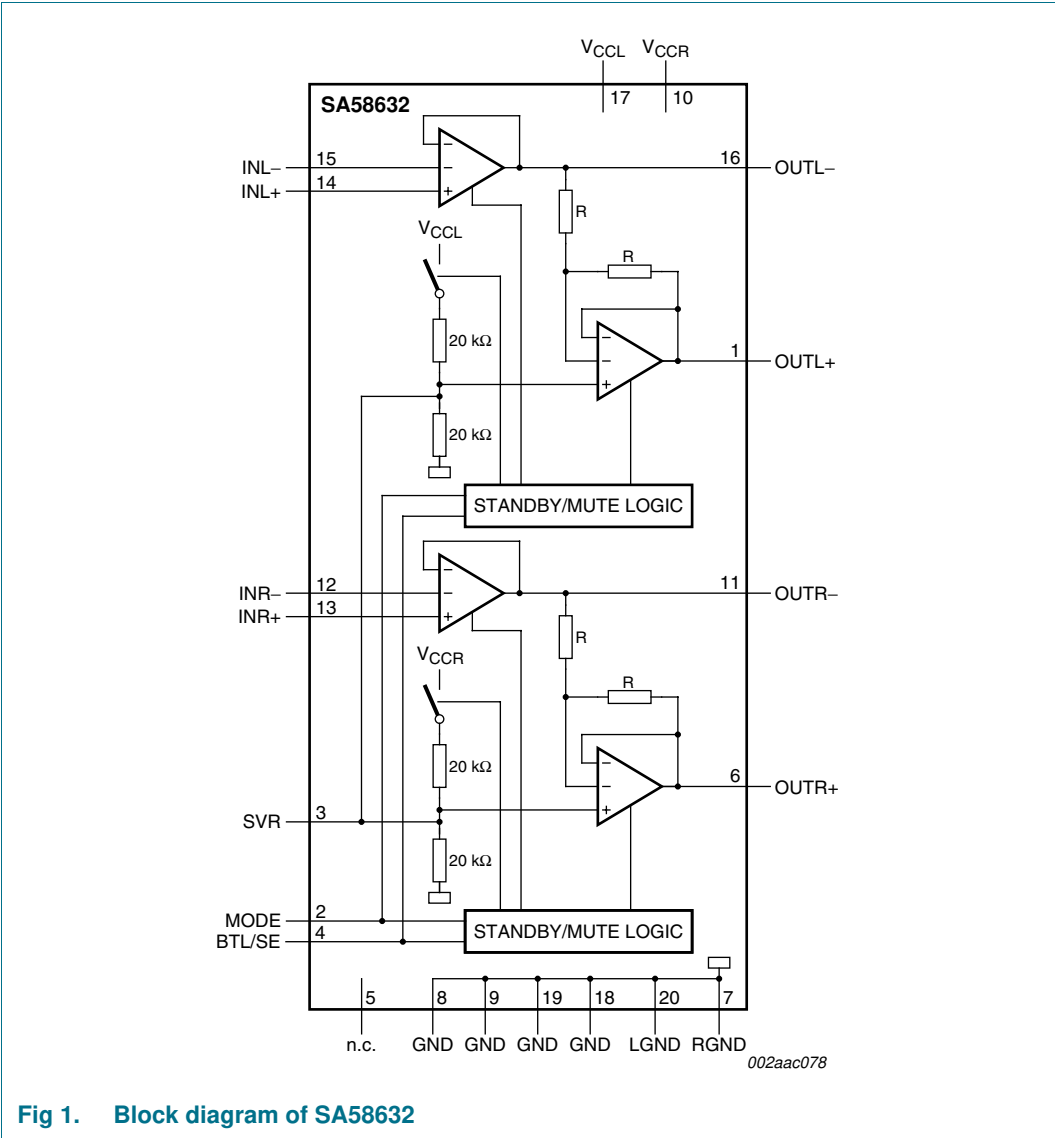
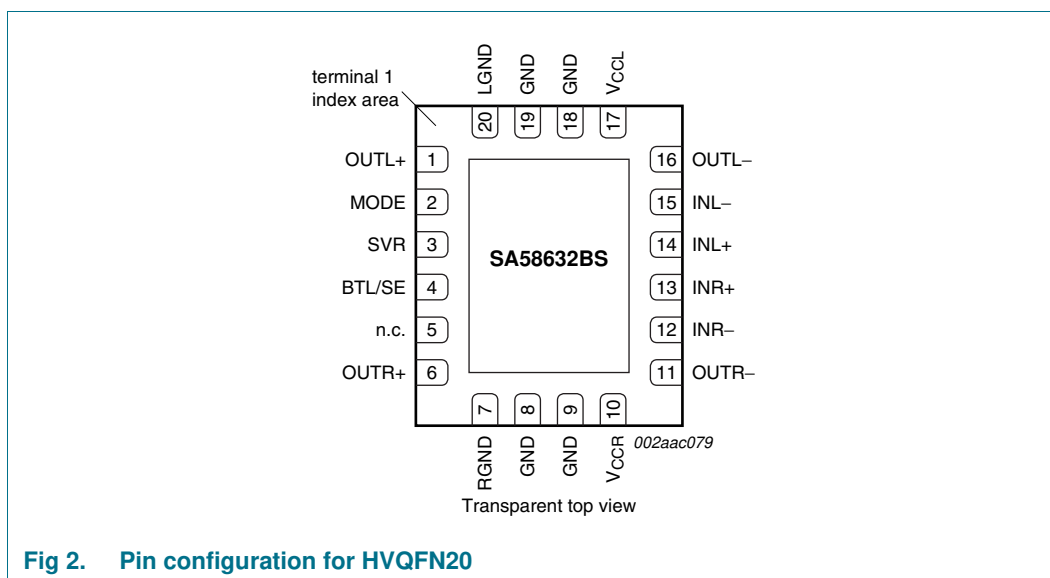


Fig 1. Block diagram of SA58632

7. Pinning information

7.1 Pinning



7.2 Pin description

Table 3. Pin description

Symbol	Pin	Description
OUTL+	1	positive loudspeaker terminal, left channel
MODE	2	operating mode select (standby, mute, operating)
SVR	3	half supply voltage, decoupling ripple rejection
BTL/SE	4	BTL loudspeaker or SE headphone operation
n.c.	5	not connected
OUTR+	6	positive loudspeaker terminal, right channel
RGND	7	ground, right channel
GND	8, 9, 18, 19	ground ^[1]
VCCR	10	supply voltage; right channel
OUTR-	11	negative loudspeaker terminal, right channel
INR-	12	negative input, right channel
INR+	13	positive input, right channel
INL+	14	positive input, left channel
INL-	15	negative input, left channel
OUTL-	16	negative output terminal, left channel
VCCl	17	supply voltage, left channel
LGND	20	ground, left channel

[1] Pins 8, 9, 18 and 19 are connected to the lead frame and also to the substrate. They may be kept floating. When connected to the ground plane, the PCB can be used as heatsink.

8. Functional description

The SA58632 is a two-channel BTL audio amplifier capable of delivering 2×1.5 W output power to an $8\ \Omega$ load at THD+N = 10 % using a 6 V power supply. It is also capable of delivering 2×2.2 W output power to an $8\ \Omega$ load at THD+N = 10 % using a 9 V power supply. Using the MODE pin, the device can be switched to standby and mute condition. The device is protected by an internal thermal shutdown protection mechanism. The gain can be set within a range of 6 dB to 30 dB by external feedback resistors.

8.1 Power amplifier

The power amplifier is a Bridge-Tied Load (BTL) amplifier with a complementary PNP-NPN output stage. The voltage loss on the positive supply line is the saturation voltage of a PNP power transistor, on the negative side the saturation voltage of an NPN power transistor. The total voltage loss is < 1 V. With a supply voltage of 6 V and an $8\ \Omega$ loudspeaker, an output power of 1.5 W can be delivered to the load, and with a 9 V supply voltage and an $8\ \Omega$ loudspeaker an output power of 2.2 W can be delivered.

8.2 Mode select pin (MODE)

The device is in Standby mode (with a very low current consumption) if the voltage at the MODE pin is greater than $V_{CC} - 0.5$ V, or if this pin is floating. At a MODE voltage in the range between 1.5 V and $V_{CC} - 1.5$ V the amplifier is in a mute condition. The mute condition is useful to suppress pop noise at the output, caused by charging of the input capacitor. The device is in Active mode if the MODE pin is grounded or less than 0.5 V (see [Figure 6](#)).

8.3 BTL/SE output configuration

To invoke the BTL configuration (see [Figure 3](#)), the BTL/SE pin is taken to logic HIGH or not connected. The output differentially drives the speakers, so there is no need for coupling capacitors. The headphone can be connected to the amplifier negative outputs using a coupling capacitor for each channel. The headphone common ground is connected to the amplifier ground.

To invoke the Single-Ended (SE) configuration (see [Figure 15](#)), the BTL/SE pin is taken to logic LOW or connected to ground. The positive outputs are muted with a DC level of $0.5V_{CC}$. Using a coupling capacitor for each channel, speakers can be connected to the amplifier negative outputs. The speaker common ground is connected to the amplifier ground. Headphones can be connected to the negative outputs without using output coupling capacitors. The headphone common ground pin is connected to one of the amplifier positive output pins.

9. Limiting values

Table 4. Limiting values

In accordance with the Absolute Maximum Rating System (IEC 60134).

Symbol	Parameter	Conditions	Min	Max	Unit
V _{CC}	supply voltage	operating	−0.3	+18	V
V _I	input voltage		−0.3	V _{CC} + 0.3	V
I _{ORM}	repetitive peak output current		-	1	A
T _{stg}	storage temperature	non-operating	−55	+150	°C
T _{amb}	ambient temperature	operating	−40	+85	°C
V _{P(SC)}	short-circuit supply voltage		-	10	V
P _{tot}	total power dissipation	HVQFN20	-	2.2	W

10. Thermal characteristics

Table 5. Thermal characteristics

Symbol	Parameter	Conditions	Typ	Unit
R _{th(j-a)}	thermal resistance from junction to ambient	in free air	80	K/W
		64.5 mm ² (10 square inch) heat spreader	[1] 22	K/W
R _{th(j-sp)}	thermal resistance from junction to solder point		3	K/W

[1] Thermal resistance is 22 K/W with DAP soldered to 64.5 mm² (10 square inch), 1 ounce copper heat spreader.

11. Static characteristics

Table 6. Static characteristics

V_{CC} = 6 V; T_{amb} = 25 °C; R_L = 8 Ω; V_{MODE} = 0 V; measured in test circuit [Figure 3](#); unless otherwise specified.

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
V _{CC}	supply voltage	operating	2.2	9	18	V
I _q	quiescent current	R _L = ∞ Ω	[1] -	15	22	mA
I _{stb}	standby current	V _{MODE} = V _{CC}	-	-	10	μA
V _O	output voltage		[2] -	2.2	-	V
ΔV _{O(offset)}	differential output voltage offset		-	-	50	mV
I _{IB}	input bias current	pins INL+, INR+	-	-	500	nA
		pins INL-, INR-	-	-	500	nA
V _{MODE}	voltage on pin MODE	operating	0	-	0.5	V
		mute	1.5	-	V _{CC} − 1.5	V
		standby	V _{CC} − 0.5	-	V _{CC}	V
I _{MODE}	current on pin MODE	0 V < V _{MODE} < V _{CC}	-	-	20	μA
V _{I(SE)}	input voltage on pin BTL/SE	single-ended (SE)	0	-	0.6	V
V _{I(BTL)}	input voltage on pin BTL/SE	BTL	0.42 × V _{CC}	-	V _{CC}	V
I _{I(SE)}	input current on pin BTL/SE	V _{I(SE)} = 0 V; pin connected to ground in SE mode	-	-	100	μA

[1] With a load connected at the outputs the quiescent current will increase, the maximum of this increase being equal to the DC output offset voltage divided by R_L.

[2] The DC output voltage with respect to ground is approximately $0.5 \times V_{CC}$.

12. Dynamic characteristics

Table 7. Dynamic characteristics

$V_{CC} = 6\text{ V}$; $T_{amb} = 25\text{ }^{\circ}\text{C}$; $R_L = 8\text{ }\Omega$; $f = 1\text{ kHz}$; $V_{MODE} = 0\text{ V}$; measured in test circuit [Figure 3](#); unless otherwise specified.

Symbol	Parameter	Conditions	Min	Typ	Max	Unit
P_o	output power	THD+N = 10 %	1.2	1.5	-	W
		THD+N = 0.5 %	0.9	1.1	-	W
		THD+N = 10 %; $V_{CC} = 9\text{ V}$; application demo board	-	2.2	-	W
THD+N	total harmonic distortion-plus-noise	$P_o = 0.5\text{ W}$	-	0.15	0.3	%
$G_{v(cl)}$	closed-loop voltage gain		[1] 6	-	30	dB
ΔZ_i	differential input impedance		-	100	-	k Ω
$V_{n(o)}$	output noise voltage		[2] -	-	100	μV
PSRR	power supply rejection ratio		[3] 50	-	-	dB
			[4] 40	-	-	dB
$V_{O(mute)}$	mute output voltage	mute condition	[5] -	-	200	μV
α_{cs}	channel separation		40	-	-	dB

[1] Gain of the amplifier is $2 \times (R_2 / R_1)$ in test circuit of [Figure 3](#).

[2] The output noise voltage is measured at the output in a frequency range from 20 Hz to 20 kHz (unweighted), with a source impedance of $R_s = 0\text{ }\Omega$ at the input.

[3] Supply voltage ripple rejection is measured at the output with a source impedance of $R_s = 0\text{ }\Omega$ at the input. The ripple voltage is a sine wave with a frequency of 1 kHz and an amplitude of 100 mV (RMS), which is applied to the positive supply rail.

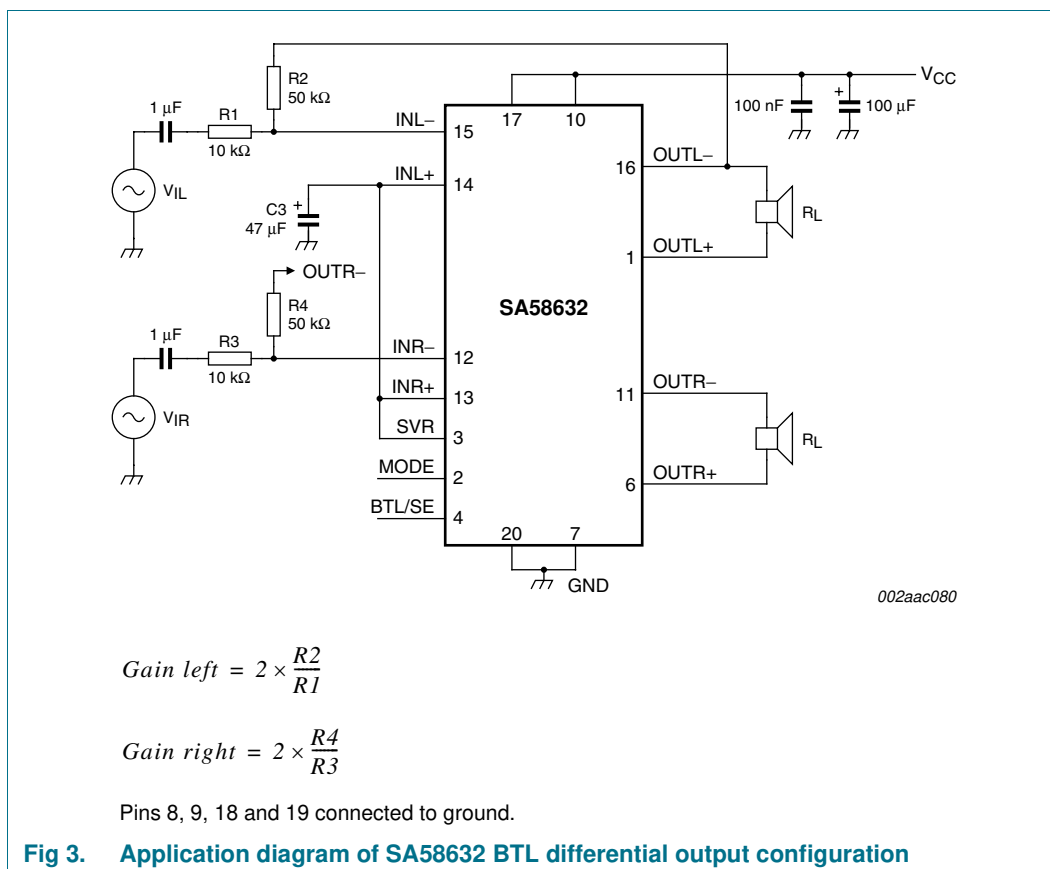
[4] Supply voltage ripple rejection is measured at the output, with a source impedance of $R_s = 0\text{ }\Omega$ at the input. The ripple voltage is a sine wave with a frequency between 100 Hz and 20 kHz and an amplitude of 100 mV (RMS), which is applied to the positive supply rail.

[5] Output voltage in mute position is measured with an input voltage of 1 V (RMS) in a bandwidth of 20 kHz, which includes noise.

13. Application information

13.1 BTL application

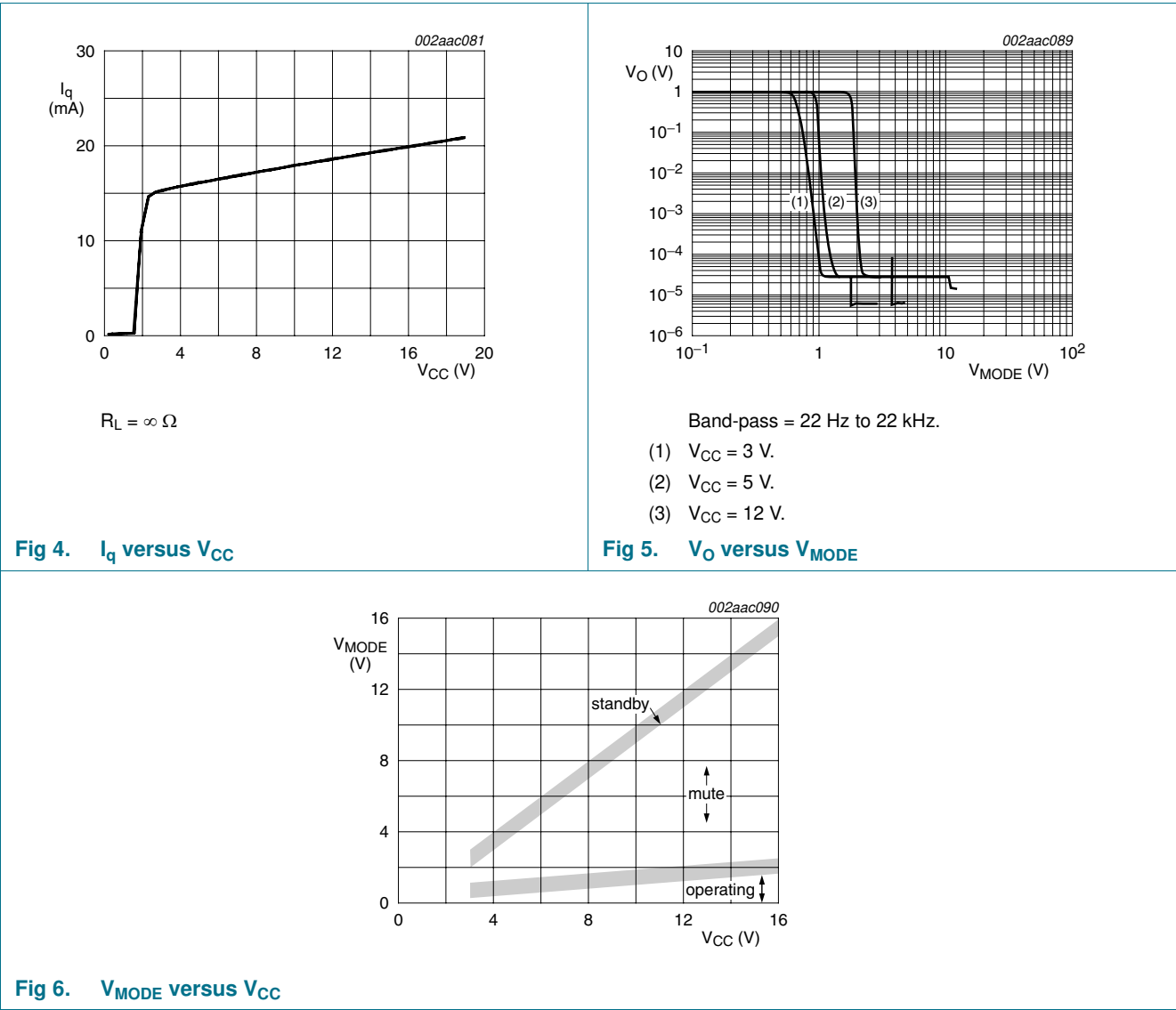
$T_{\text{amb}} = 25\text{ }^{\circ}\text{C}$, $V_{\text{CC}} = 9\text{ V}$, $f = 1\text{ kHz}$, $R_L = 8\text{ }\Omega$, $G_v = 20\text{ dB}$, audio band-pass 22 Hz to 22 kHz. The BTL diagram is shown in [Figure 3](#).



14. Test information

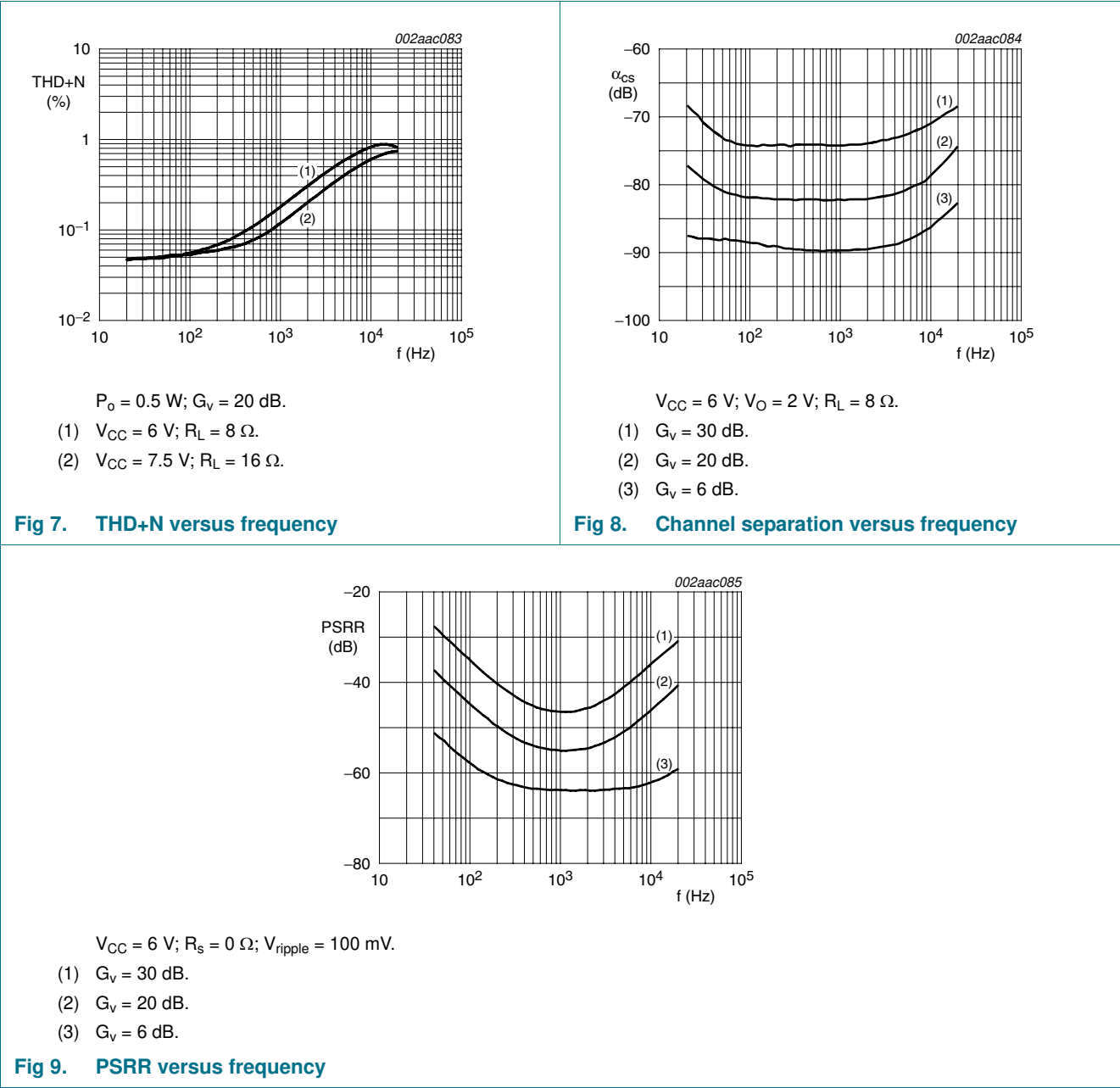
14.1 Static characterization

The quiescent current has been measured without any load impedance (Figure 4). Figure 6 shows three areas: operating, mute and standby. It shows that the DC switching levels of the mute and standby respectively depends on the supply voltage level.



14.2 BTL dynamic characterization

The total harmonic distortion-plus-noise (THD+N) as a function of frequency (Figure 7) was measured with a low-pass filter of 80 kHz. The value of capacitor C2 influences the behavior of PSRR at low frequencies; increasing the value of C2 increases the performance of PSRR.



14.3 Thermal behavior

The measured thermal performance of the HVQFN20 package is highly dependent on the configuration and size of the heat spreader on the application demo board. Data may not be comparable between different semiconductor manufacturers because the application demo boards and test methods are not standardized. Also, the thermal performance of packages for a specific application may be different than presented here, because of the configuration of the copper heat spreader of the application boards may be significantly different.

NXP Semiconductors uses FR-4 type application boards with 1 ounce copper traces with solder coating.

The demo board (see [Figure 23](#)) has a 1 ounce copper heat spreader that runs under the IC and provides a mounting pad to solder to the die attach paddle of the HVQFN20 package. The heat spreader is symmetrical and provides a heat spreader on both top and bottom of the PCB. The heat spreader on top and bottom side of the demo board is connected through 2 mm diameter plated through holes. Directly under the DAP (Die Attach Paddle), the top and bottom side of the PCB are connected by four vias. The total top and bottom heat spreader area is 64.5 mm² (10 in²).

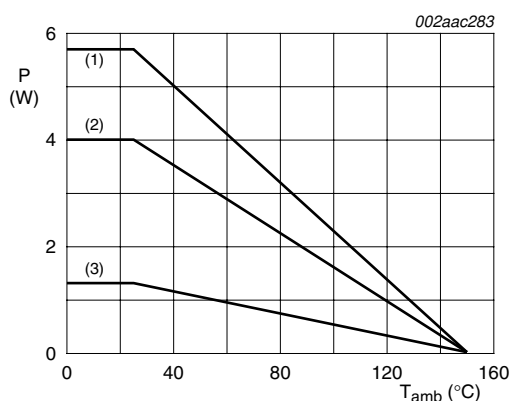
The junction to ambient thermal resistance, $R_{th(j-a)} = 22$ K/W for the HVQFN20 package when the exposed die attach paddle is soldered to 5 square inch area of 1 ounce copper heat spreader on the demo PCB. The maximum sine wave power dissipation for $T_{amb} = 25$ °C is given in [Equation 1](#):

$$\frac{150 - 25}{22} = 5.7 \text{ W} \quad (1)$$

Thus, for $T_{amb} = 60$ °C the maximum total power dissipation is given in [Equation 2](#):

$$\frac{150 - 60}{22} = 4.1 \text{ W} \quad (2)$$

The power dissipation versus ambient temperature curve ([Figure 10](#)) shows the power derating profiles with ambient temperature for three sizes of heat spreaders. For a more modest heat spreader using 5 square inch area on the top or bottom side of the PCB, the $R_{th(j-a)}$ is 31 K/W. When the package is not soldered to a heat spreader, the $R_{th(j-a)}$ increases to 60 K/W.



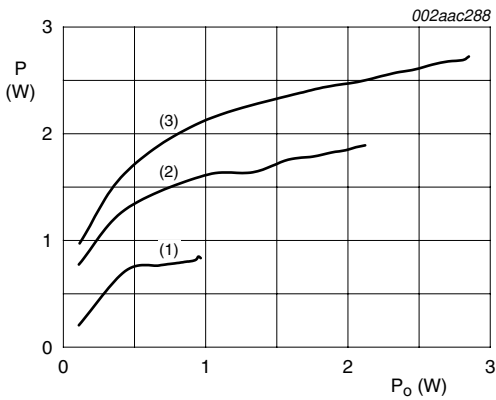
(1) 64.5 mm² heat spreader top and bottom (1 ounce copper).

(2) 32.3 mm² heat spreader top or bottom (1 ounce copper).

(3) No heat spreader.

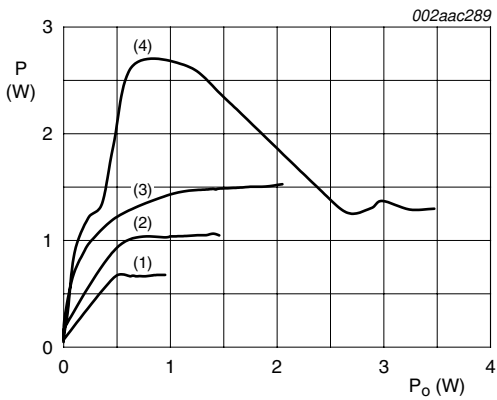
Fig 10. Power dissipation versus ambient temperature

The characteristics curves ([Figure 11a](#) and [Figure 11b](#), [Figure 12](#), [Figure 13a](#) and [Figure 13b](#), and [Figure 14](#)) show the room temperature performance for SA58632 using the demo PCB shown in [Figure 23](#). For example, [Figure 11 “Power dissipation versus output power”](#) (a and b) show the performance as a function of load resistance and supply voltage. Worst case power dissipation is shown in [Figure 12](#). [Figure 13a](#) shows that the part delivers typically 2.8 W per channel for THD+N = 10 % using 8 Ω load at 9 V supply, while [Figure 13b](#) shows that the part delivers 3.3 W per channel at 12 V supply and 16 Ω load, THD+N = 10 %.



- (1) $V_{CC} = 6\text{ V}$.
- (2) $V_{CC} = 7.5\text{ V}$.
- (3) $V_{CC} = 9\text{ V}$.

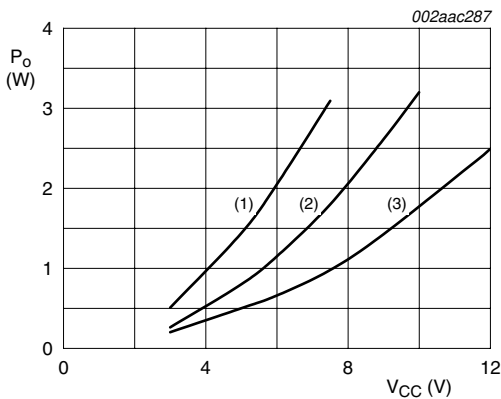
a. $R_L = 8\ \Omega$; $f = 1\text{ kHz}$; $G_v = 20\text{ dB}$



- (1) $V_{CC} = 6\text{ V}$.
- (2) $V_{CC} = 7.5\text{ V}$.
- (3) $V_{CC} = 9\text{ V}$.
- (4) $V_{CC} = 12\text{ V}$.

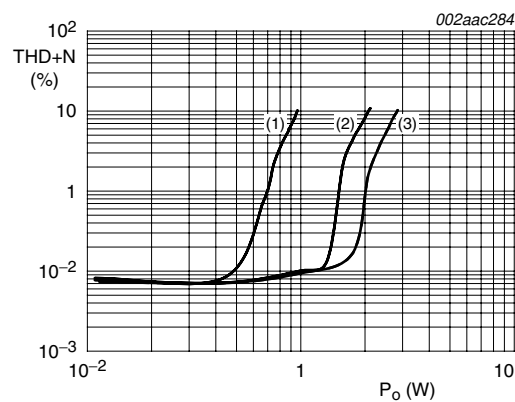
b. $R_L = 16\ \Omega$; $f = 1\text{ kHz}$; $G_v = 20\text{ dB}$

Fig 11. Power dissipation versus output power



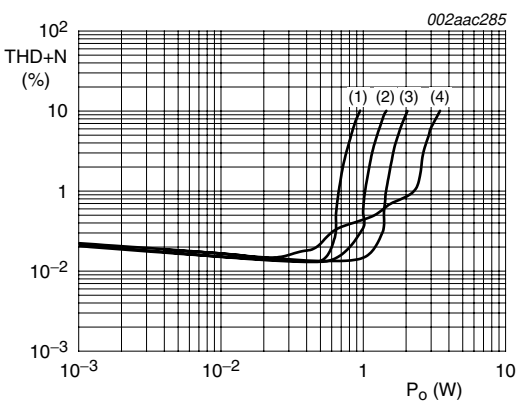
- (1) $R_L = 4\ \Omega$.
- (2) $R_L = 8\ \Omega$.
- (3) $R_L = 16\ \Omega$.

Fig 12. Worst case power dissipation versus V_{CC}



- (1) $V_{CC} = 6$ V.
- (2) $V_{CC} = 7.5$ V.
- (3) $V_{CC} = 9$ V.

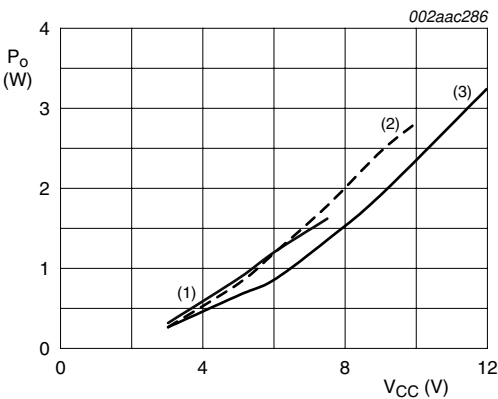
a. $R_L = 8\ \Omega$; $f = 1$ kHz; $G_v = 20$ dB



- (1) $V_{CC} = 6$ V.
- (2) $V_{CC} = 7.5$ V.
- (3) $V_{CC} = 9$ V.
- (4) $V_{CC} = 12$ V.

b. $R_L = 16\ \Omega$; $f = 1$ kHz; $G_v = 20$ dB

Fig 13. THD+N versus output power



THD+N = 10 %; $f = 1$ kHz; $G_v = 20$ dB.

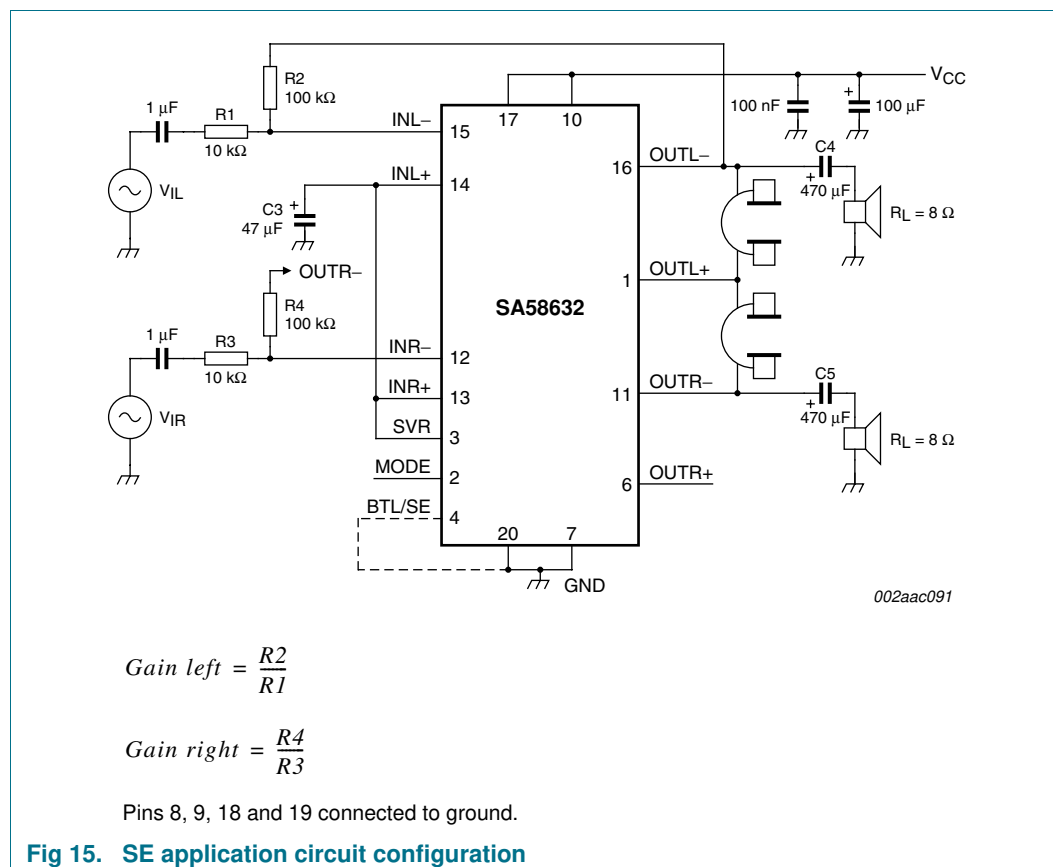
- (1) $R_L = 4\ \Omega$.
- (2) $R_L = 8\ \Omega$.
- (3) $R_L = 16\ \Omega$.

Fig 14. Output power versus V_{CC}

14.4 Single-ended application

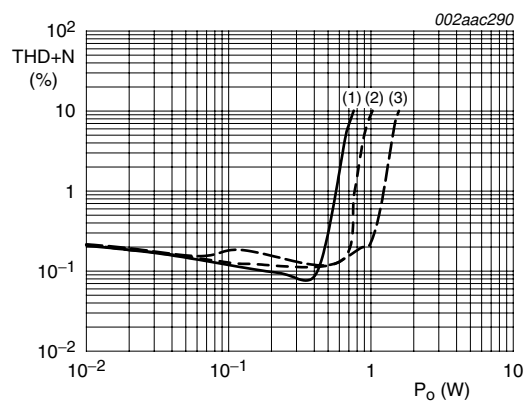
$T_{\text{amb}} = 25\text{ }^{\circ}\text{C}$; $V_{\text{CC}} = 7.5\text{ V}$; $f = 1\text{ kHz}$; $R_{\text{L}} = 8\text{ }\Omega$; $G_{\text{v}} = 20\text{ dB}$; audio band-pass 20 Hz to 20 kHz.

The single-ended application diagram is shown in [Figure 15](#).



If the BTL/SE pin is to ground, the positive outputs (OUTL+, OUTR+) will be in mute condition with a DC level of $0.5V_{\text{CC}}$. When a headphone is used ($R_{\text{L}} > 25\text{ }\Omega$) the SE headphone application can be used without coupling capacitors by placing the load between negative output and one of the positive outputs (for example, pin 1) as the common pin.

Increasing the value of the tantalum or electrolytic capacitor C3 will result in a better channel separation. Because the positive output is not designed for high output current ($2 \times I_{\text{O}}$) at the load impedance ($< 16\text{ }\Omega$), the SE application with output capacitors connected to ground is advised. The capacitor value of C4/C5 in combination with the load impedance determines the low frequency behavior. The total harmonic distortion-plus-noise as a function of frequency was measured with a low-pass filter of 80 kHz. The value of the capacitor C3 influences the behavior of the PSRR at low frequencies; increasing the value of C3 increases the performance of PSRR.

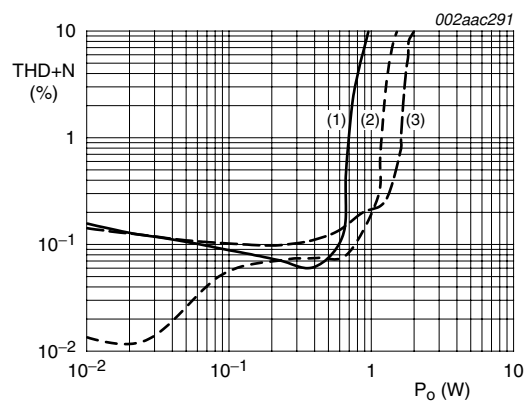


(1) $V_{CC} = 7.5$ V.

(2) $V_{CC} = 9$ V.

(3) $V_{CC} = 12$ V.

a. $R_L = 4 \Omega$; $f = 1$ kHz; $G_v = 10$ dB

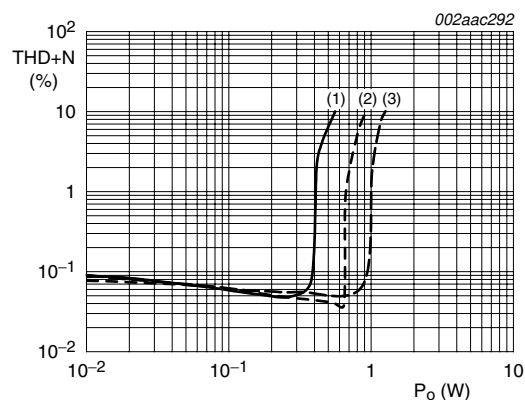


(1) $V_{CC} = 9$ V.

(2) $V_{CC} = 12$ V.

(3) $V_{CC} = 15$ V.

b. $R_L = 8 \Omega$; $f = 1$ kHz; $G_v = 10$ dB



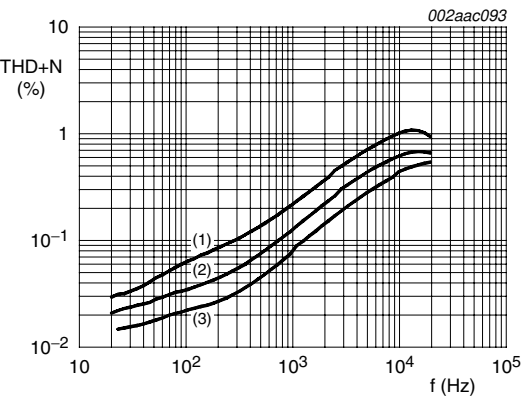
(1) $V_{CC} = 9$ V.

(2) $V_{CC} = 12$ V.

(3) $V_{CC} = 15$ V.

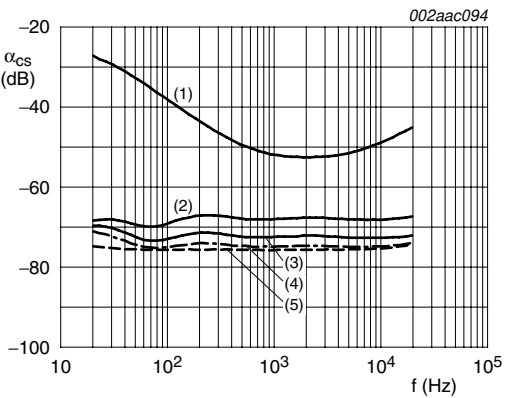
c. $R_L = 16 \Omega$; $f = 1$ kHz; $G_v = 10$ dB

Fig 16. THD+N versus output power



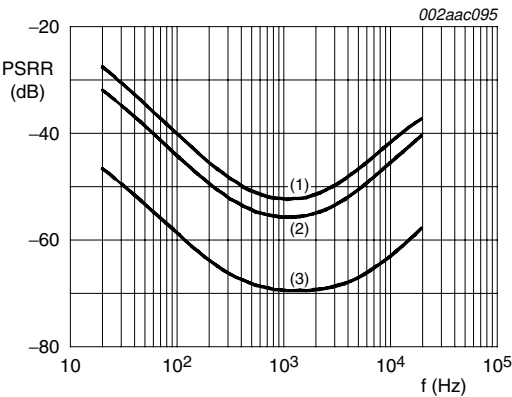
$P_o = 0.5 \text{ W}$; $G_v = 20 \text{ dB}$.
(1) $V_{CC} = 7.5 \text{ V}$; $R_L = 4 \Omega$.
(2) $V_{CC} = 9 \text{ V}$; $R_L = 8 \Omega$.
(3) $V_{CC} = 12 \text{ V}$; $R_L = 16 \Omega$.

Fig 17. THD+N versus frequency



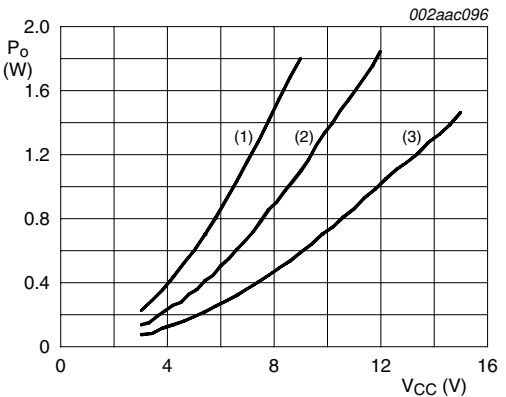
$V_o = 1 \text{ V}$; $G_v = 20 \text{ dB}$.
(1) $V_{CC} = 5 \text{ V}$; $R_L = 32 \Omega$, to buffer.
(2) $V_{CC} = 7.5 \text{ V}$; $R_L = 4 \Omega$.
(3) $V_{CC} = 9 \text{ V}$; $R_L = 8 \Omega$.
(4) $V_{CC} = 12 \text{ V}$; $R_L = 16 \Omega$.
(5) $V_{CC} = 5 \text{ V}$; $R_L = 32 \Omega$.

Fig 18. Channel separation versus frequency



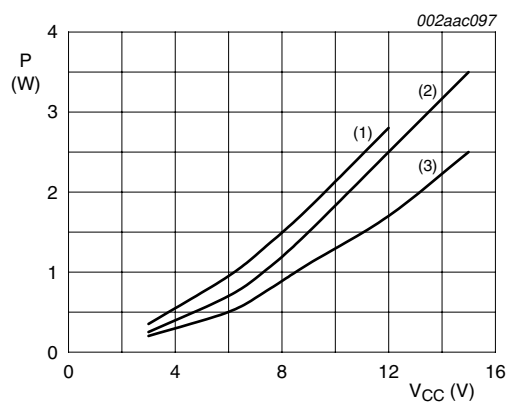
$R_s = 0 \Omega$; $V_{\text{ripple}} = 100 \text{ mV}$.
(1) $G_v = 24 \text{ dB}$.
(2) $G_v = 20 \text{ dB}$.
(3) $G_v = 0 \text{ dB}$.

Fig 19. PSRR versus frequency



$\text{THD+N} = 10 \%$.
(1) $R_L = 4 \Omega$.
(2) $R_L = 8 \Omega$.
(3) $R_L = 16 \Omega$.

Fig 20. P_o versus V_{CC}



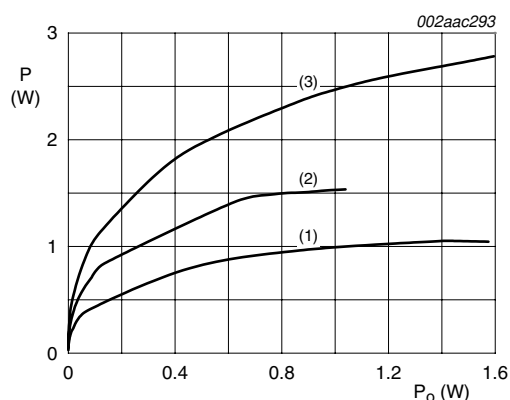
THD+N = 10 %.

(1) $R_L = 4 \Omega$.

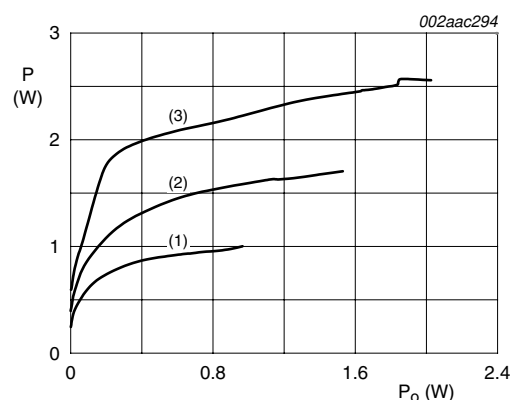
(2) $R_L = 8 \Omega$.

(3) $R_L = 16 \Omega$.

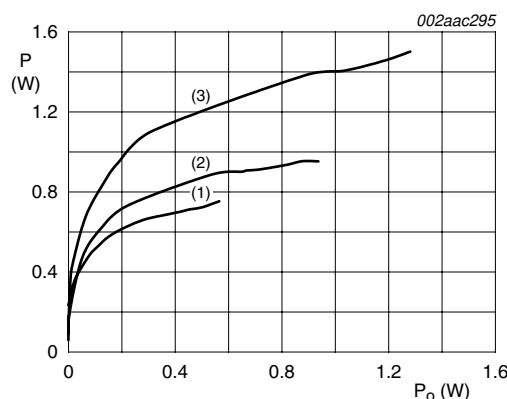
Fig 21. Worst case power dissipation versus V_{CC}



- (1) $V_{CC} = 7.5$ V.
 (2) $V_{CC} = 9$ V.
 (3) $V_{CC} = 12$ V.
 a. $R_L = 4 \Omega$; $f = 1$ kHz; $G_v = 10$ dB



- (1) $V_{CC} = 9$ V.
 (2) $V_{CC} = 12$ V.
 (3) $V_{CC} = 15$ V.
 b. $R_L = 8 \Omega$; $f = 1$ kHz; $G_v = 10$ dB



- (1) $V_{CC} = 9$ V.
 (2) $V_{CC} = 12$ V.
 (3) $V_{CC} = 15$ V.
 c. $R_L = 16 \Omega$; $f = 1$ kHz; $G_v = 10$ dB

Fig 22. Power dissipation versus output power

14.5 General remarks

The frequency characteristics can be adapted by connecting a small capacitor across the feedback resistor. To improve the immunity of HF radiation in radio circuit applications, a small capacitor can be connected in parallel with the feedback resistor ($56 \text{ k}\Omega$); this creates a low-pass filter.

14.6 SA58632BS PCB demo

The application demo board may be used for evaluation in either BTL or SE configuration as shown in the schematics in [Figure 3](#) and [Figure 15](#). The demo PCB is laid out for a 64.5 mm^2 (10 in^2) heat spreader (total of top and bottom heat spreader area).

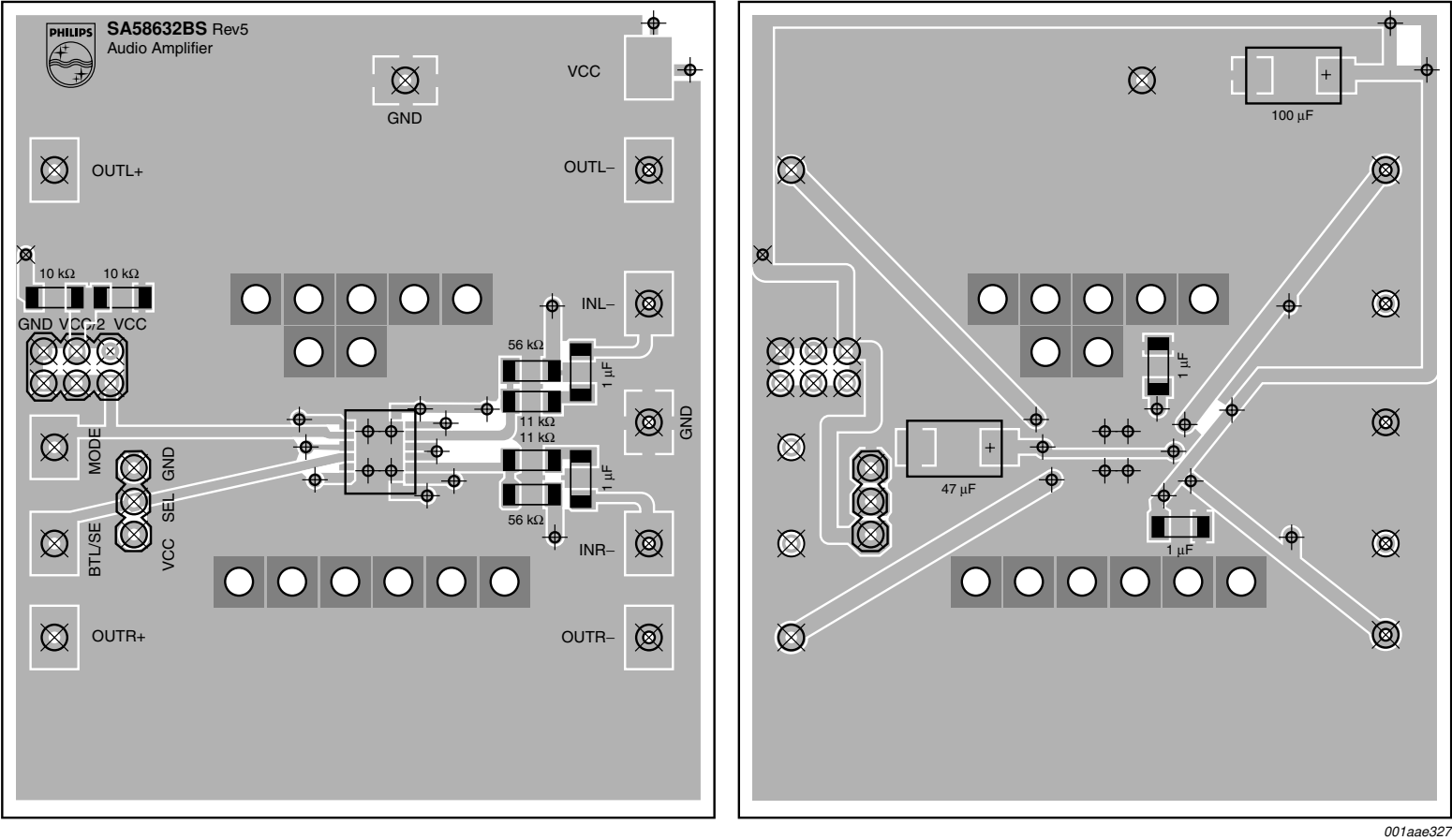


Fig 23. SA58632BS PCB demo

15. Package outline

HVQFN20: plastic thermal enhanced very thin quad flat package; no leads;
20 terminals; body 6 x 5 x 0.85 mm

SOT910-1

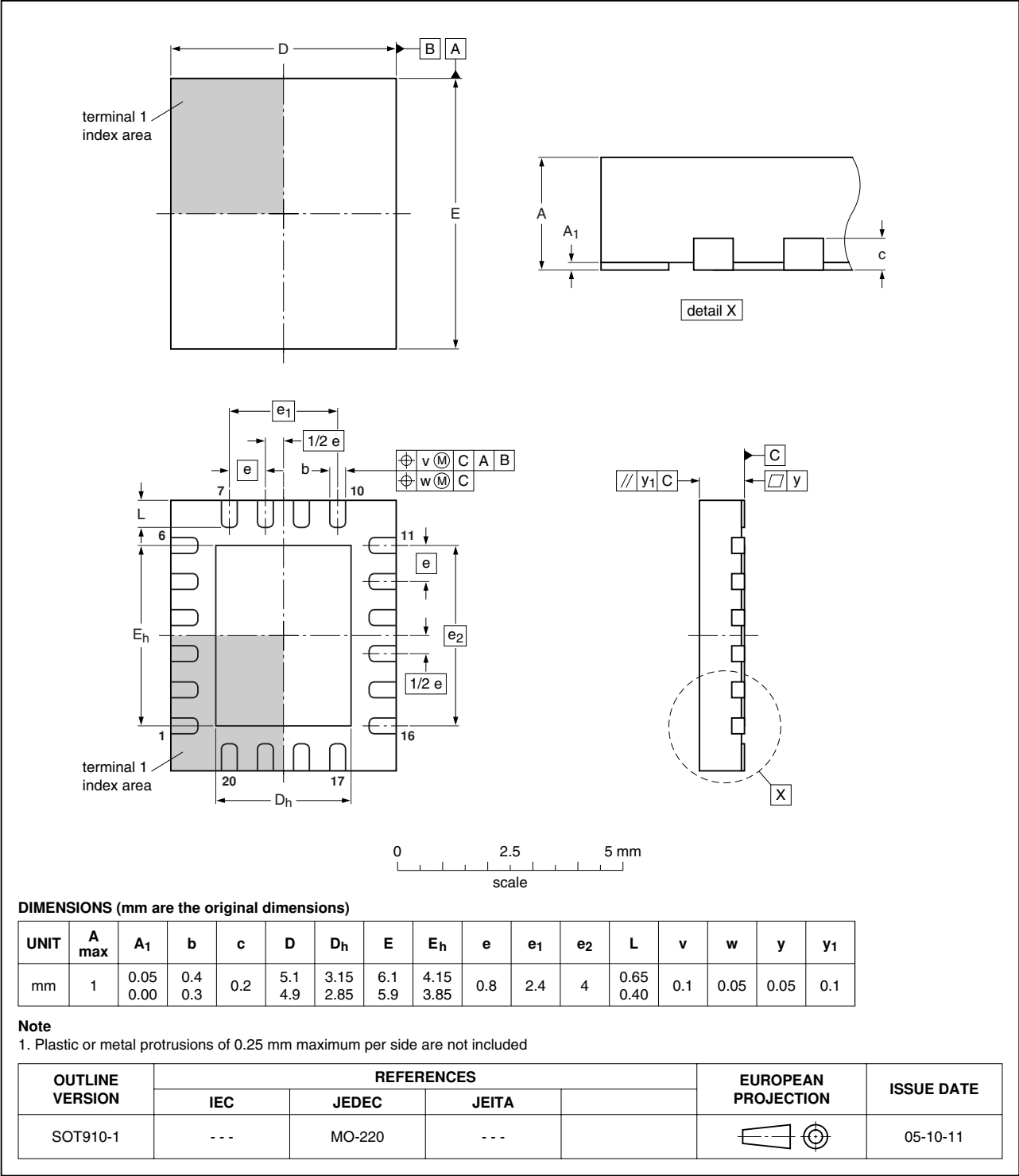


Fig 24. Package outline SOT910-1 (HVQFN20)

16. Soldering of SMD packages

This text provides a very brief insight into a complex technology. A more in-depth account of soldering ICs can be found in Application Note *AN10365 "Surface mount reflow soldering description"*.

16.1 Introduction to soldering

Soldering is one of the most common methods through which packages are attached to Printed Circuit Boards (PCBs), to form electrical circuits. The soldered joint provides both the mechanical and the electrical connection. There is no single soldering method that is ideal for all IC packages. Wave soldering is often preferred when through-hole and Surface Mount Devices (SMDs) are mixed on one printed wiring board; however, it is not suitable for fine pitch SMDs. Reflow soldering is ideal for the small pitches and high densities that come with increased miniaturization.

16.2 Wave and reflow soldering

Wave soldering is a joining technology in which the joints are made by solder coming from a standing wave of liquid solder. The wave soldering process is suitable for the following:

- Through-hole components
- Leadless or leadless SMDs, which are glued to the surface of the printed circuit board

Not all SMDs can be wave soldered. Packages with solder balls, and some leadless packages which have solder lands underneath the body, cannot be wave soldered. Also, leadless SMDs with leads having a pitch smaller than ~0.6 mm cannot be wave soldered, due to an increased probability of bridging.

The reflow soldering process involves applying solder paste to a board, followed by component placement and exposure to a temperature profile. Leadless packages, packages with solder balls, and leadless packages are all reflow solderable.

Key characteristics in both wave and reflow soldering are:

- Board specifications, including the board finish, solder masks and vias
- Package footprints, including solder thieves and orientation
- The moisture sensitivity level of the packages
- Package placement
- Inspection and repair
- Lead-free soldering versus SnPb soldering

16.3 Wave soldering

Key characteristics in wave soldering are:

- Process issues, such as application of adhesive and flux, clinching of leads, board transport, the solder wave parameters, and the time during which components are exposed to the wave
- Solder bath specifications, including temperature and impurities

16.4 Reflow soldering

Key characteristics in reflow soldering are:

- Lead-free versus SnPb soldering; note that a lead-free reflow process usually leads to higher minimum peak temperatures (see [Figure 25](#)) than a SnPb process, thus reducing the process window
- Solder paste printing issues including smearing, release, and adjusting the process window for a mix of large and small components on one board
- Reflow temperature profile; this profile includes preheat, reflow (in which the board is heated to the peak temperature) and cooling down. It is imperative that the peak temperature is high enough for the solder to make reliable solder joints (a solder paste characteristic). In addition, the peak temperature must be low enough that the packages and/or boards are not damaged. The peak temperature of the package depends on package thickness and volume and is classified in accordance with [Table 8](#) and [9](#)

Table 8. SnPb eutectic process (from J-STD-020C)

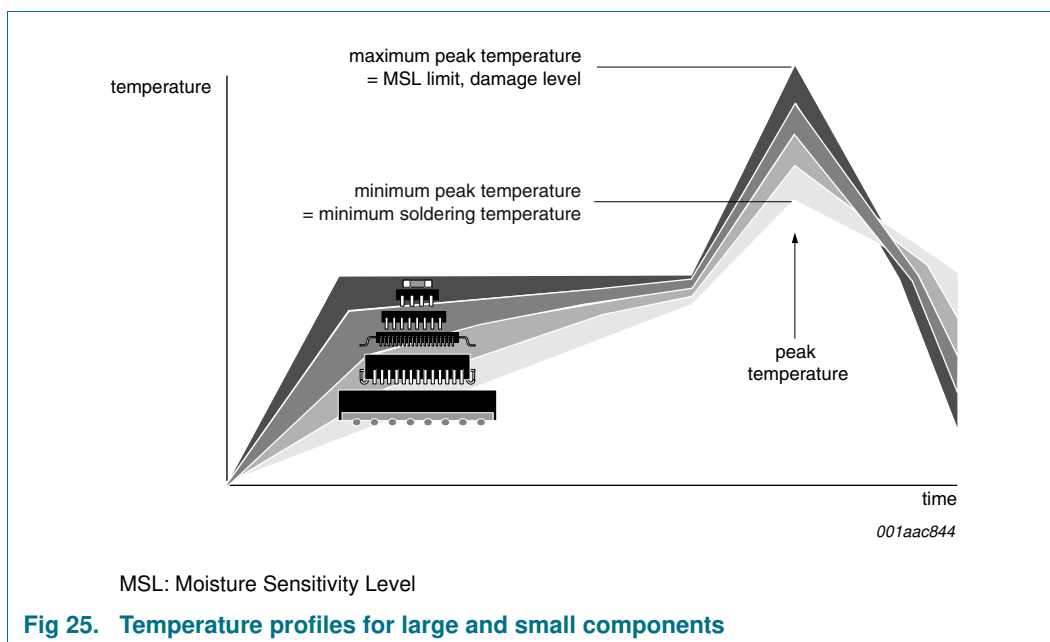
Package thickness (mm)	Package reflow temperature (°C)	
	Volume (mm ³)	
	< 350	≥ 350
< 2.5	235	220
≥ 2.5	220	220

Table 9. Lead-free process (from J-STD-020C)

Package thickness (mm)	Package reflow temperature (°C)		
	Volume (mm ³)		
	< 350	350 to 2000	> 2000
< 1.6	260	260	260
1.6 to 2.5	260	250	245
> 2.5	250	245	245

Moisture sensitivity precautions, as indicated on the packing, must be respected at all times.

Studies have shown that small packages reach higher temperatures during reflow soldering, see [Figure 25](#).



For further information on temperature profiles, refer to Application Note *AN10365* “Surface mount reflow soldering description”.

17. Abbreviations

Table 10. Abbreviations

Acronym	Description
BTL	Bridge-Tied Load
CMOS	Complementary Metal Oxide Semiconductor
DAP	Die Attach Paddle
ESD	ElectroStatic Discharge
NPN	Negative-Positive-Negative
PCB	Printed-Circuit Board
PNP	Positive-Negative-Positive
RMS	Root Mean Squared
SE	Single-Ended
THD	Total Harmonic Distortion

18. Revision history

Table 11. Revision history

Document ID	Release date	Data sheet status	Change notice	Supersedes
SA58632_2	20100304	Product data sheet	-	SA58632_1
Modifications:	<ul style="list-style-type: none">The format of this data sheet has been redesigned to comply with the new identity guidelines of NXP Semiconductors.Legal texts have been adapted to the new company name where appropriate.Table 6 “Static characteristics”: Min. value for $V_{I(BTL)}$ changed from “2 V” to “$0.42 \times V_{CC}$”.			
SA58632_1	20060627	Product data sheet	-	-