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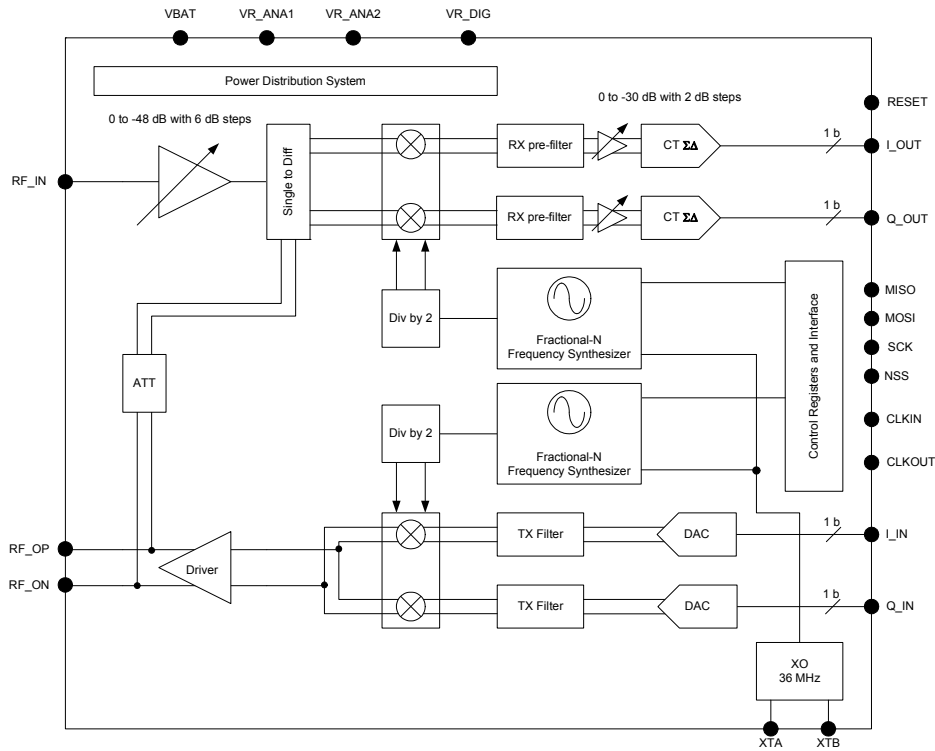


Figure A: SX1257 Block Diagram

### General Description

The SX1257 is a highly integrated RF front-end to digital I and Q modulator/demodulator Multi-PHY mode transceiver capable of supporting multiple constant and non-constant envelope modulation schemes. It is designed to operate over the 862 to 960 MHz European, North American and Japanese ISM (Industrial, Scientific and Medical) license-exempt frequency bands. Its highly integrated architecture allows for a minimum of external components whilst maintaining maximum design flexibility. All major RF communication parameters are programmable and most of them can be dynamically set. The SX1257 offers support for both narrow-band and wide-band communication modes without the need to modify external components. The SX1257 is optimized for low power consumption while offering the provision for high RF output power and channelized operation. TrueRF™ technology enables a low-cost external component count whilst still satisfying ETSI, FCC and ARIB regulations.

### Applications

- IEEE 802.15.4g SUN Multi-PHY Mode Smartgrid
- Cognitive / Software Defined Radio (SDR)

### Key Product Features

- Fully flexible I and Q modulator and demodulator
- Half or full-duplex operation
- Bullet proof RX LNA
- Analog TX and RX pre-filtering
- Programmable tap TX FIR-DAC filter
- Linear TX amplifier for both constant and non-constant envelope modulation schemes

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## Ordering Information

Part Number	Delivery	Minimum Order Quantity
SX1257IWLTRT	MLPQW-32	3'000 pieces

Pb-free, Halogen free, RoHS/WEEE compliant product.

## Document Revision History

Version	ECO	Date	Modifications
1.0	005895	February 2012	First Final datasheet revision
1.1	040837	February 2018	Migration to new data sheet template Correction of Data Hold and Set-Up Time Correction of minor typographical errors
1.2	041328	March 2018	Correction of NSS Hold Time to 50 ns

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# 1. General Description

The SX1257 is a single-chip Zero-IF RF-to-digital front-end transceiver integrated circuit ideally suited for today's high performance multi-PHY mode or SDR ISM band RF applications. The SX1257 has a maximum signal bandwidth of 500 kHz in both transmission and reception and is intended as a high performance, low-cost RF-to-digital converter and provides a generic RF front-end that allows several constant and non-constant envelope modulation schemes to be handled, such as LoRa®, the MR-FSK, MR-OFDM and MR-O-QPSK PHYs of the IEEE 802.15.4g standard for Smart Utility Networks (SUN) and Smartgrid applications in the 862 - 960 MHz license-exempt frequency bands.

The SX1257's advanced features set greatly simplifies system design whilst the high level of integration reduces the external BOM to an optional RF power amplifier, and a handful of passive decoupling and matching components. A simple 4-wire 1-bit digital serial interface is provided for the baseband I and Q data streams to a baseband processor.

The SX1257 can operate in both half and full-duplex mode and is compliant with ETSI, FCC and ARIB regulatory requirements. It is available in a MLPQ-W 5 x 5 mm 32 lead package.

## 1.1 Simplified Block Diagram

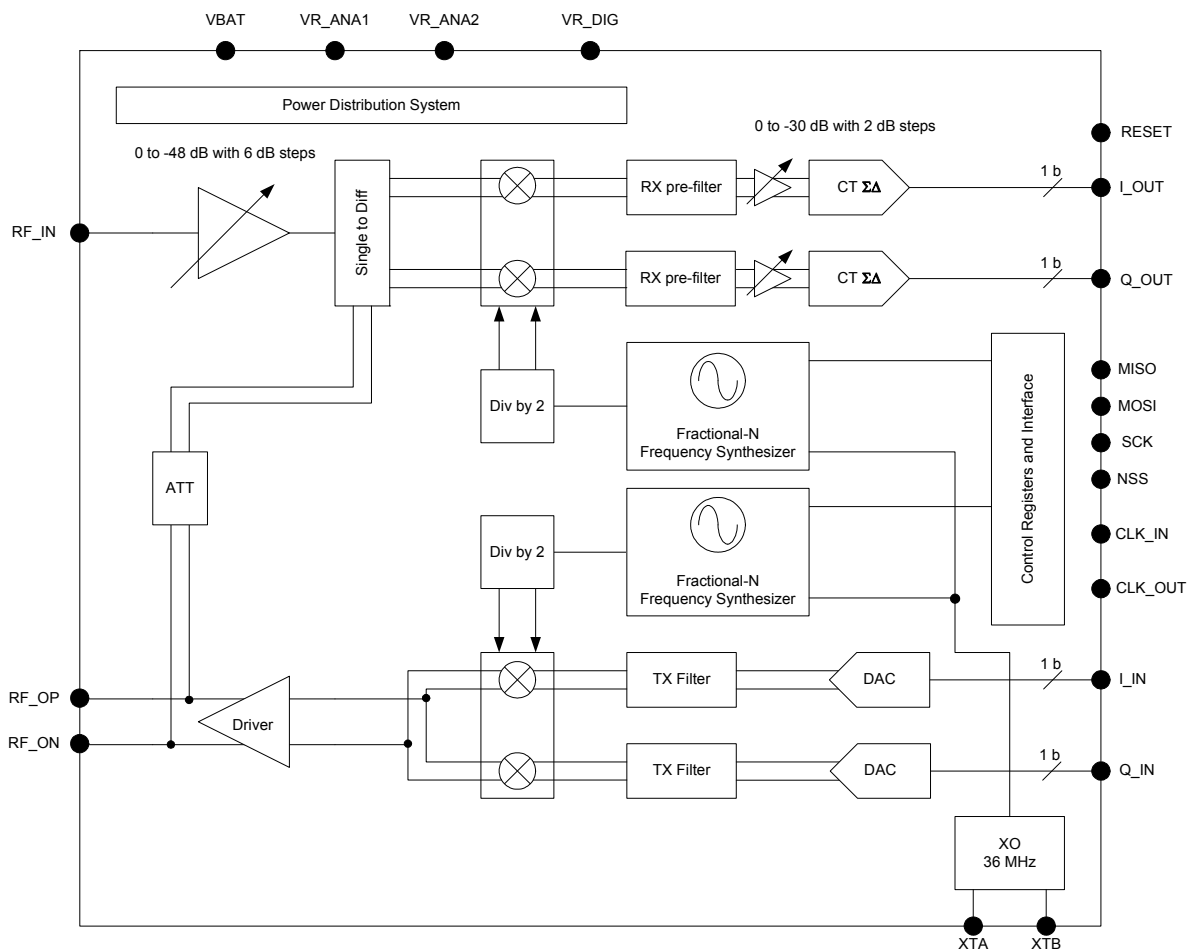


Figure 1-1: SX1257 Block Diagram



## 1.2 I/O Description

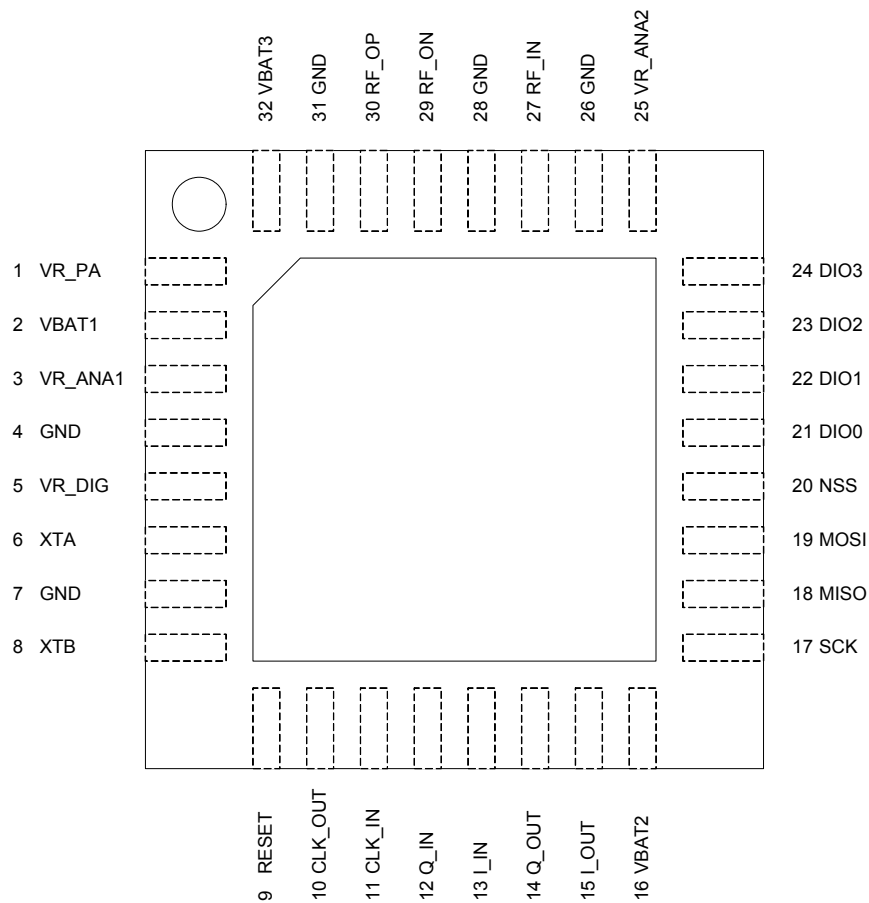
Table 1-1: SX1257 Pinout

Pin Number	Pin Name	Type (I = input O = Output)	Description
0	Ground	-	Exposed Ground pad
1	VR_PA	-	Regulated supply for TX amplifier
2	VBAT1	-	VBAT Supply voltage
3	VR_ANA1	-	Regulated supply for analog TX circuit
4	GND	-	Ground
5	VR_DIG	-	Regulated supply for digital circuit
6	XTA	I/O	Crystal pad
7	GND	-	Ground
8	XTB	I/O	Crystal pad / input for external clock
9	Reset	I/O	Reset
10	CLK_OUT	O	36 MHz digital clock output
11	CLK_IN	I	36 MHz digital clock input
12	Q_IN	I	Digital baseband data input for I (inphase) channel DAC
13	I_IN	I	Digital baseband data input for Q (quadrature) channel DAC
14	Q_OUT	O	Digital baseband data output from I (inphase) channel ADC
15	I_OUT	O	Digital baseband data output from Q (quadrature) channel ADC
16	VBAT2	-	VBAT supply voltage
17	SCK	I	SPI clock
18	MISO	O	Master In Slave Output SPI output
19	MOSI	I	Master Out Slave Input SPI input
20	NSS	I	SPI chip select
21	DIO0	O	Digital I/O, software configured
22	DIO1	O	Digital I/O, software configured
23	DIO2	O	Digital I/O, software configured
24	DIO3	O	Digital I/O, software configured
25	VR_ANA2	-	Regulated supply for analog RX circuit
26	GND	-	Ground
27	RF_IN	I	RX LNA input
28	GND	-	Ground

**Table 1-1: SX1257 Pinout**

Pin Number	Pin Name	Type (I = input O = Output)	Description
29	RF_ON	O	Differential TX Output, negative node
30	RF_OP	O	Differential TX Output, positive node
31	GND	-	Ground
32	VBAT3	-	VBAT supply for TX amplifier

## 1.3 Package View



**Figure 1-2: SX1257 Top View Pin Location**

## 2. Specifications

### 2.1 ESD Notice

The SX1257 is a high performance radio frequency device.

- Class 3A of the JEDEC standard JESD22-A114-C (Human Body Model) on all pins
- Class B of the JEDEC standard JESD22-A115-A (Machine Model) on all pins
- Class III of the JEDEC standard JESD22-C101-C (Charged Device Model) on all pins



The chip should be handled with all the necessary ESD precautions to avoid any permanent damage.

### 2.2 Absolute Maximum Ratings

Stresses above the values listed below may cause permanent device failure.

Exposure to absolute maximum ratings for extended periods may affect device reliability, reducing product life time.

**Table 2-1: Absolute Maximum Ratings**

Symbol	Description	Min	Typ	Max	Unit
VDDmr	Supply voltage	-0.5	-	3.9	V
Tmr	Temperature	-55	-	115	°C
Tj	Junction temperature	-	-	125	°C
Pmr	RF input level	-	-	+6	dBm

### 2.3 Operating Range

Operating ranges define the limits for functional operation and parametric characteristics of the device.

Functionality outside these limits is not guaranteed.

**Table 2-2: Operating Range**

Symbol	Description	Min	Typ	Max	Unit
VDDop	Supply voltage	2.7	-	3.6	V
Top	Temperature under bias	-40	-	85	°C
Clop	Load capacitance on digital ports	-	-	25	pF
ML	RF Input power	-	-	0	dBm

## 2.4 Electrical Specifications

The electrical specifications are given with the following conditions unless otherwise specified:

- VBAT\_IO = VBAT = 3.3 V, all current consumptions are given for VBAT connected to VBAT\_IO
- Temperature = 25 °C
- FXOSC = 36 MHz
- $F_{RF}$  = 915 MHz
- OFDM with 16-QAM
- 3/4 rate coded with 26 active tones (IEEE 802.15.4g MR-OFDM Option 3)
- Output power = -5 dBm (100 ohm differential transmission)
- TXBWANA = 250 kHz
- RXBWANA = 250 kHz
- External baseband RX filter = 150 kHz

### 2.4.1 Power Consumption Specifications

Table 2-3: Power Consumption Specifications

Symbol	Description	Conditions	Min	Typ	Max	Unit
IDDSL	Supply current in sleep mode		-	0.5	1	μA
IDDST	Supply current in standby mode	Crystal oscillator enabled	-	1.15	1.5	mA
IDDRX	Supply current in receive mode	-		20	25	mA
IDDTX	Supply current in transmit mode	RFOutput Power = -5 dBm	-	58	85	mA

### 2.4.2 Frequency Synthesis Specifications

Table 2-4: Frequency Synthesis Specifications

Symbol	Description	Conditions	Min	Typ	Max	Unit
FR	Synthesizer frequency range	Programmable	862	-	1020	MHz
FXOSC	Crystal oscillator frequency	See <a href="#">Section 5. "Configuration and Status Registers" on page 29</a>	32	36	36	MHz
TS_OS	Crystal oscillator wake-up time	from sleep mode	-	300	500	μs
TS_FS	Synthesizer wake-up time	Crystal oscillator enabled	-	100	150	μs
FSTEP	Frequency synthesizer step size	$FSTEP = FXOSC / 2^{19}$	61	68.7	68.7	Hz

## 2.4.3 Transmitter Front-End Specifications

**Table 2-5: Transmitter Front-End Specifications**

Symbol	Description	Conditions	Min	Typ	Max	Unit
FCLK_IN	External clock frequency for TX synthesizer or DAC input clock	SX1257 slave mode	32	-	36	MHz
TXPmax	TX maximum output power	Saturated Power	+5	+8	-	dBm
TXP1dB	TX 1 dB compression point	Peak value	+3	+6	-	dBm
TXOIP3	TX output IP3	-5 dBm average output power	+13	+16	-	dBm
PHN	Transmitter phase noise	100 kHz offset from carrier	-	-98	-	dBc/Hz
PHNF	Transmitter output noise floor	10 MHz offset from carrier	-131	-128	-	dBc/Hz
PHNID	Transmitter integrated DSB phase noise	Integrated bandwidth from 500 Hz to 125 kHz	-	0.6	1.5	°RMS
TXGM	Transmitter IQ gain mismatch	-	-	0.5	1	dB
TXPM	Transmitter IQ phase mismatch	-	-	1	3	°
TXBWANA	Transmitter analog prefilter BW (SSB)	Programmable	210	-	850	kHz
XBWANAPrc	Transmitter analog prefilter BW precision	-	-30	-	+30	%
TXBWDIFG	Transmitter FIR-DAC taps	Programmable	24	-	64	-
TXLO	TX LO leakage (before DC offset calibration)	ADC rms input: -10 dBFS	-	-8	-	dBc
TS_TR	Transmitter wake-up time	Frequency synthesizer enabled	-	120	-	µs

## 2.4.4 Receiver Front-End Specifications

**Table 2-6: Receiver Front-End Specifications**

Symbol	Description	Conditions	Min	Typ	Max	Unit
FCLK_IN	External clock frequency for TX synthesizer or DAC input clock	SX1257 slave mode	32	-	36	MHz
CLK_INJ	External clock jitter specification	External clock, white noise	-	-	0.01	%
RXNF	Receiver noise figure	Maximum LNA gain	-	7	10	dB
RXGR	RX gain range	Adjustable in 2 dB steps	-	70	-	dB
IIP3	3rd order input intercept point Unwanted tones are 2 MHz and 3.8 MHz above the LO	Lowest LNA gain	+10	-	-	dBm
		Highest LNA gain	-28	-25	-	dBm
RXGM	Receiver IQ gain mismatch	-	-	0.5	1	dB
RXPM	Receiver IQ phase mismatch	-	-	1	3	°
RXBWANA	Receiver analog prefilter BW (SSB)	Programmable	250	-	750	kHz

## 2.4.5 SPI Bus Digital Specifications

**Table 2-7: Digital I/O Specifications**

Symbol	Description	Conditions	Min	Typ	Max	Unit
$V_{IH}$	Input high voltage	-	0.8	-	-	VDD
$V_{IL}$	Input low voltage	-	-	-	0.2	VDD
$V_{OH}$	Output high voltage	$I_{max} = 1 \text{ mA}$	0.9	-	-	VDD
$V_{OL}$	Output low voltage	$I_{max} = -1 \text{ mA}$	-	-	0.1	MHz
$F_{SCK}$	SCK frequency	-	-	-	10	ns
$t_{ch}$	SCK high time	-	50	-	-	ns
$t_{cl}$	SCK low time	-	50	-	-	ns
$t_{rise}$	SCK rise time	-	-	5	-	ns
$t_{fall}$	SCK fall time	-	-	5	-	ns
$t_{setup}$	MOSI set-up time	From MOSI change to SCK rising edge	30	-	-	ns
$t_{hold}$	MOSI hold time	From SCK rising edge to MOSI change	60	-	-	ns
$t_{nsetup}$	NSS set-up time	From NSS falling edge to SCK rising edge	30	-	-	ns
$t_{nhold}$	NSS hold time	From SCK falling edge to NSS rising edge	50	-	-	ns
$t_{nhigh}$	NSS high time between SPI access	-	20	-	-	ns
$t_{data}$	Data hold and set-up time	-	25	-	-	ns

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## 3. Circuit Description

### 3.1 Power Supply Strategy

The SX1257 employs an advanced power distribution scheme (PDS), which provides stable operating characteristics over the full temperature and voltage range of operation.

The SX1257 can be powered from any low-noise voltage source via pins VBAT1, VBAT2 and VBAT3. Decoupling capacitors should be connected, as suggested in the reference design, on VR\_PA, VR\_DIG, VR\_ANA1 and VR\_ANA2 pins to ensure a correct operation of the built-in voltage regulators.

### 3.2 Low Battery Detector

A low battery detector is also included allowing the generation of an interrupt signal in response to passing a programmable threshold adjustable through the register RegLowBat. The interrupt signal can be mapped to the DIO0 pin, through the programming of RegDioMapping.

### 3.3 Frequency Synthesizer

The SX1257 incorporates two separate state of the art fractional-N PLLs for the TX and RX circuit blocks.

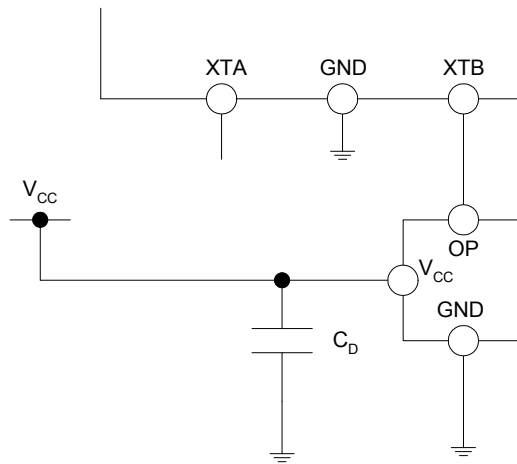
#### 3.3.1 Reference Oscillator

The crystal oscillator is the main timing reference of the SX1257. It provides the reference source for the transmit and receive frequency synthesizers and as a clock for digital processing.

The XO startup time, TS\_OSC, depends on the actual XTAL being connected on pins XTA and XTB. When using the built-in sequencer, the SX1257 optimizes the startup time and automatically triggers the PLL when the XO signal is stable. To manually control the startup time, the user should monitor the signal CLK\_OUT which will only be made available on the output buffer when a stable XO oscillation is achieved.

An external crystal controlled source, such as a clipped-sinewave TCXO, clock can be used to replace the crystal oscillator, This external source should be provided on XTB (pin 8) and XTA (pin 6) should be left open, as illustrated in the following figure.





**Figure 3-1: TCXO Connection**

The peak-peak amplitude of the input signal must never exceed 1.8 V. Please consult your TCXO supplier for an appropriate value of decoupling capacitor, CD. Due to the low jitter requirements required by the receiver digital block it is recommended that only a crystal controlled external frequency source is used.

### 3.3.2 CLK\_OUT Output

For master mode operation the SX1257 provides a system clock output made available at pin CLK\_OUT.

### 3.3.3 PLL Architecture

The SX1257 incorporates two fourth-order type fractional-N sigma-delta PLLs. The PLLs include integrated VCO and programmable bandwidth loop filter, removing the need for any external components. The PLLs are autocalibrating and are capable of fast switching and settling times.

#### 3.3.3.1 VCO

Both TX and RX VCOs operate at twice the RF frequency, with the oscillators centered at 1.9 GHz. This reduces any LO leakage in receive mode, to improve the quadrature precision of the receiver, and to reduce the pulling effects on the VCO during transmission.

The VCO calibration is fully automated, calibration times are fully transparent to the end-user as the processing time is included in the TS\_TR and TS\_RE specifications.

#### 3.3.3.2 PLL Bandwidth

The bandwidth of the PLL loop filters are independently configurable via the configuration registers TxPIIBw and RxPIIBw for the modulation schemes supported, as well as fast channel switching and lock times to support FHSS and frequency agile applications, such as AFA.

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### 3.3.3.3 Carrier Frequency and Resolution

Both the TX and RX embed a 19-bit sigma-delta modulator and the frequency resolution, constant over the entire frequency range, is calculated using the following formula:

$$F_{STEP} = \frac{F_{XOSC}}{2^{19}}$$

The RX and TX carrier frequencies are programmed through registers RegFrFrRx and RegFrFrTx, split across register addresses 0x01 to 0x03 and 0x04 to 0x06, respectively, and are calculated by:

$$F_{RF} = F_{STEP} \times F_{RFXX}^{(23, 0)}$$

where:  $F_{rfxx}$  is the integer value of the RegFrFrRx or RegFrFrTx as defined above.

**Note:**

**As stated above, the  $F_{rfxx}$  settings are split across 3 bytes for both the transmitter and receiver frequency synthesizers. A change in the center frequency will only be taken into account when the least significant byte FrfxxLsb in RegFrFxxLsb is written and when exiting SLEEP mode**

### 3.3.3.4 PLL Lock Time

RX and TX PLL lock times are a function of a number of technical factors, such as synthesized frequency, frequency step, etc. The SX1257 includes an auto-sequencer that manages the start-up sequence of the PLL.

### 3.3.3.5 Lock Detect Indicator

A lock indication signal for both RX and TX PLLs can be accessed via DIO pins, and is toggled high when the PLL reaches its locking range. Please refer to [Table 4-1: "DIO Mapping" on page 28](#) to map this interrupt to the desired DIO pins.

## 3.4 Transmitter Analog Front-End Description

The analog front-end of the SX1257 transmitter stage comprises the TX frequency synthesizer, I and Q channel filters, the I/Q mixer and RF amplifier blocks.

### 3.4.1 Architectural Description

The block diagram of the transmitter front-end block is illustrated below.

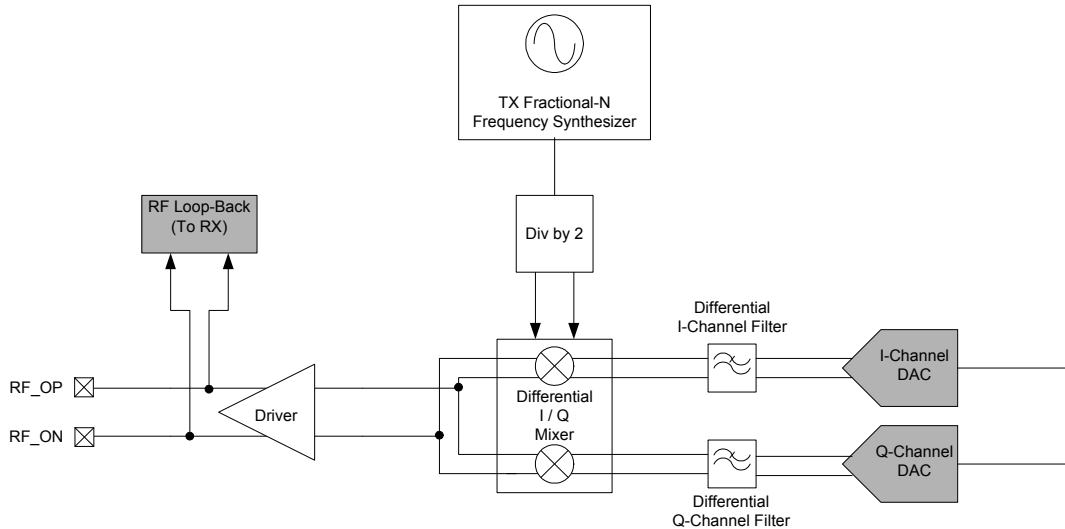


Figure 3-2: SX1257 Transmitter Analog Front-End Block Diagram

### 3.4.2 TX I / Q Channel Filters

Differential analog I and Q signals input to the TX front-end from the TX FIR DAC are filtered by I and Q channel filters. These filters smooth the reconstructed analog waveforms and remove quantization noise generated by the I and Q channel TX FIR DACs. The filters are unity gain third-order low-pass Butterworth types with programmable bandwidth configured via TxAnaBw.

The 3 dB BW of the analog TX filter BW can be calculated from:

$$BW_{3dB} = \frac{17.15}{(41 - \text{RegTxBWAna}(4, 0))}$$

The analog filter bandwidth should be set to greater than the signal bandwidth so as to reduce any group delay variations.

The range of programmable TX analog filter bandwidths is tabulated below.

<b>TxAnaBw [Dec]</b>	<b>TxAnaBw [Bin]</b>	<b>SSB Filter BW [kHz]</b>
0	00000	209
1	00001	214
2	00010	220
3	00011	226
4	00100	232
5	00101	238
6	00110	245
7	00111	252
8	01000	260
9	01001	268
10	01010	277
11	01011	286
12	01100	296
13	01101	306
14	01110	318
15	01111	330
16	10000	343
17	10001	357
18	10010	373
19	10011	390
20	10100	408
21	10101	429
22	10110	451
23	10111	476
24	11000	504
25	11001	536
26	11010	572
27	11011	613
28	11100	660
29	11101	715

TxAnaBw [Dec]	TxAnaBw [Bin]	SSB Filter BW [kHz]
30	11110	780
31	11111	858

### 3.4.3 TX I / Q Up-Conversion Mixers

The TX I / Q mixer block mixes the baseband analog I and Q signals with that from the PLL frequency synthesizer and up converts to the RF carrier frequency. The mixer block includes a highly linear I/ Q mixer stage with programmable gain configurable via configuration register RegTxGain. The modulated RF signal is input to the TX RF amplifier stage.

### 3.4.4 RF Amplifier

The TX amplifier receives the input signal from the TX mixer and provides two differential outputs. The first output provides the RF\_OP and RF\_ON signals in TX mode. The second output is used to provide an internal differential signal to the receiver during RX gain calibration. The amplifier provides good linear performance required to meet the peak to average power level variation of OFDM.

The peak output power is +5 dBm, which allows for an average output power of greater than -5 dBm with 10 dB back-off. The output signal is intended to be amplified through a suitable external RF power amplifier to the maximum permissible level allowed by relevant regulatory standards. The optimum load impedance presented RF amplifier is 100 ohms differential.

## 3.5 Transmitter Digital Baseband Description

The transmitter digital baseband section contains separate I and Q channel digital-to-analog convertors.

### 3.5.1 Digital-to-Analog Converters

The TX DAC is the first block of the SX1257 transmitter. It accepts the 1-bit I and Q noise shaped 32 Msample/second or 36 MSample/second bit-stream from the baseband processor and converts into two analog differential signals. Each TX DAC provides 8-bits of resolution in a 500 kHz bandwidth which corresponds to maximum RF transmitted double-sideband bandwidth of 1 MHz.

A programmable Finite Impulse Response (FIR) filter allows the removal of the digital modulator noise from the external baseband processor. The number of taps implemented by the FIR-DAC and subsequent single-side DAC bandwidth is controlled by the parameter TxDacBw.

TxDacBw [Dec]	TxDacBw [Bin]	No. DAC-FIR Taps	SSB Filter BW [kHz]
0	000	24	
1	001	32	450
2	010	40	
3	011	48	
4	100	56	
5	101	64	290

Examples of the FIR DAC normalized magnitude response are illustrated below.

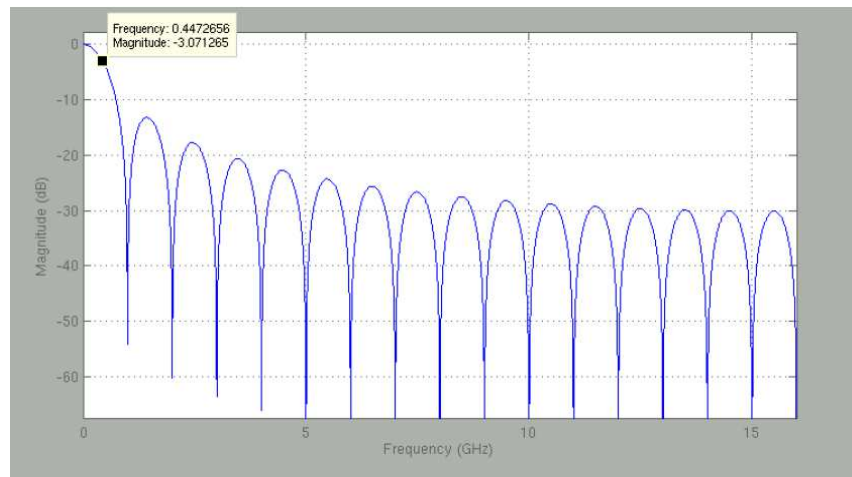
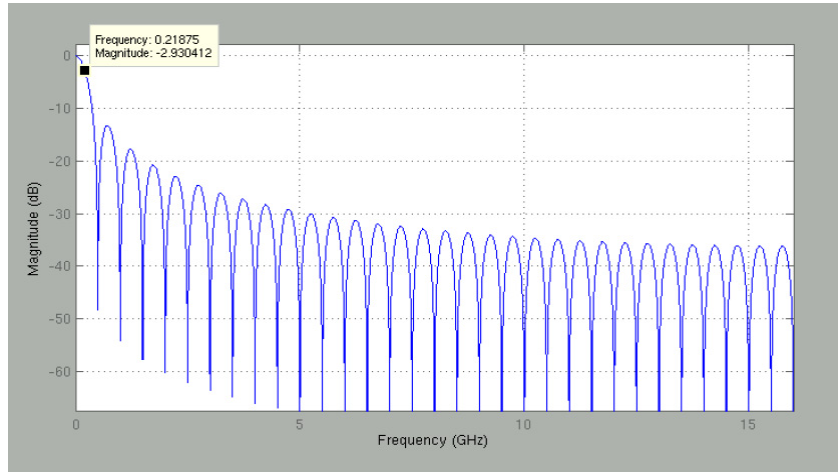


Figure 3-3: FIR-DAC Normalized Magnitude Response with  $f_s = 32$  MHz and  $N = 32$



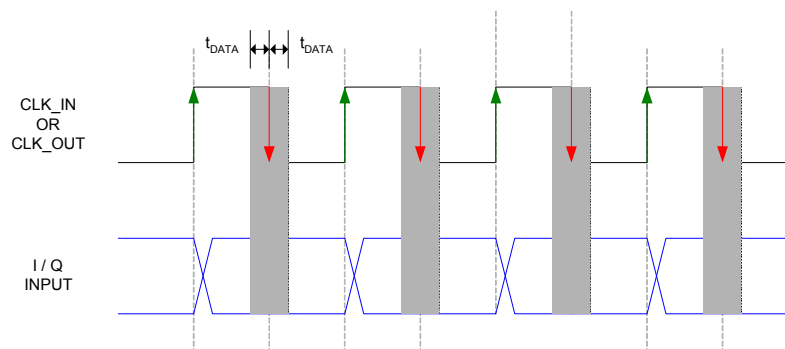
**Figure 3-4: FIR-DAC Normalized Magnitude Response with  $f_s = 32$  MHz and  $N = 64$**

The DAC 3dB bandwidth is proportional to the sampling frequency  $f_s$  and inversely proportional to the number of taps  $N$ . In the case where  $f_s = 32$  MHz with  $N = 32$  the 3 dB bandwidth is typically 450 kHz. Reducing the bandwidth may be useful to reduce the quantisation noise contribution when the signal bandwidth request is lower, as is illustrated in the case where  $N = 64$ , resulting in a 3 dB bandwidth of approximately 290 kHz.

### 3.5.2 I and Q Serial Interface

I and Q data is input to the DACs on the rising edge of the reference sampling clock and is sampled on a falling edge. The TX DAC can be used either with an external clock CLK\_IN or with the internal clock, available on CLK\_OUT for data synchronization (recommended mode).

The I and Q channel bit stream timing diagram is illustrated below.



**Figure 3-5: Transmitter I and Q Channel Bit-Stream Timing Diagram**

## 3.6 Receiver Analog Front-End Description

The SX1257 receiver front-end is based upon a zero-IF architecture, ideally suited to handle multiple complex modulation schemes. The RX chain incorporates a programmable gain LNA and single to differential buffer, I / Q mixer, separate I and Q channel analog low-pass filters and programmable baseband amplifiers. The amplified differential analog I and Q outputs are input to two 5th order continuous-time sigma-delta Analog to Digital Converters (ADC) for further signal processing in the digital domain.

### 3.6.1 Architectural Description

The block diagram of the receiver front-end block is illustrated below.

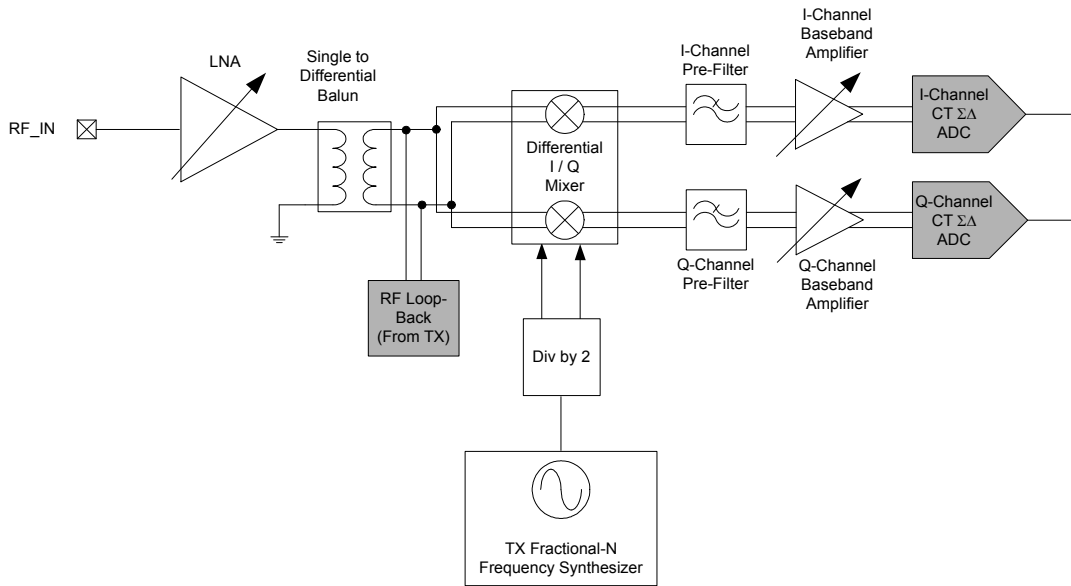


Figure 3-6: SX1257 Receiver Analog Front-End Block Diagram

### 3.6.2 LNA and Single to Differential Buffer

The LNA uses a common-gate topology, which allows for a flat characteristic over the whole frequency range. It is designed to have an input impedance of 50 Ohms or 200 ohms (as selected with bit LnaZin in RegRxAnaGain). A single to differential buffer is implemented to improve the second order linearity of the receiver.

The LNA gain, including the single-to-differential buffer, is programmable over a 48 dB dynamic range, and gain control can be enabled via an external AGC function.

### 3.6.3 I/Q Downconversion Quadrature Mixer

The mixer is inserted between output of the RF buffer stage and the input of the I and Q channel analog low-pass filter stages. This block is designed to downconvert the spectrum of the input RF signal to base-band and offers both high IIP2 and IIP3 responses.



### 3.6.4 Baseband Analog Filters and Amplifiers

The differential I and Q baseband mixer signals are pre-filtered by a programmable 1st order low-pass pre-filter and input to programmable linear baseband amplifiers. The single-sideband 3 dB bandwidth of the pre-filters can be programmed between 250 kHz and 750 kHz. This additional pre-filtering improves the selectivity of the receiver for complex modulation schemes, such as OFDM.

The amplifier stage gain offers 32 dB of programmable gain, in 2 dB steps, from -24 dB to +6 dB via configuration register RegRxAnaGain while the analog filter bandwidth is programmed via the two least significant bits of configuration register RegRxBw.

## 3.7 Receiver Digital Baseband

The receiver digital baseband section contains separate I and Q channel continuous time Sigma-Delta analog-to-digital converters to digitize and filter the analog bit stream.

### 3.7.1 Architectural Block Diagram

The block diagram of the receiver digital baseband is illustrated below.

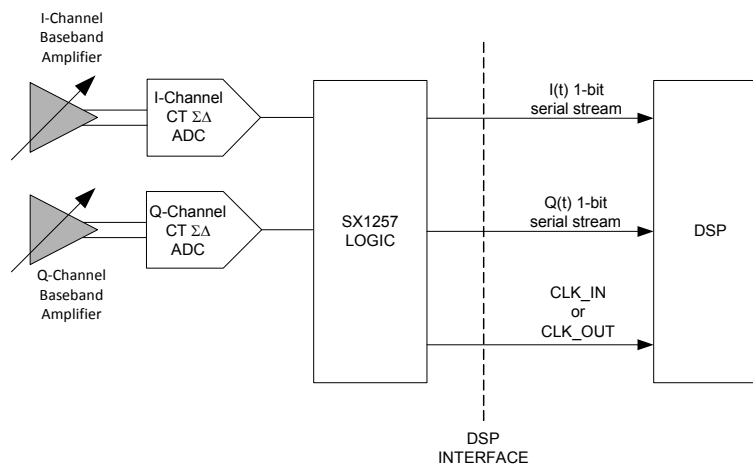


Figure 3-7: SX1257 Digital Receiver Baseband Block Diagram

### 3.7.2 Analog-to-Digital Converters

The receiver digital baseband consists of separate I and Q channel 5th order continuous-time sigma-delta modulator analog-to-digital converters which sample and digitize the analog baseband I and Q signals output at the analog baseband amplifiers.

The ADC output allows for 13 bits of resolution after decimation and filtering by the external baseband processor within a 500 kHz maximum bandwidth, corresponding to a maximum RF received double sideband bandwidth of 1 MHz.

The ADC output is one bit per channel quadrature bit stream at 32 or 36 MSamples/s.

### 3.7.3 Temperature Sensor

The receiver ADC can be used to perform a temperature measurement by digitizing the sensor response. The response of the sensor is  $-1\text{C} / \text{Lsb}$ . Since a CMOS temperature sensor is not accurate by nature, the sensor should be calibrated at ambient temperature for a precise reading.

It takes less than  $100\ \mu\text{s}$  for the SX1257 to evaluate the temperature (from setting  $\text{RxAdcTemp} = "1"$ ). The  $\text{AdcTemp}$  value can be read at  $\text{Q\_OUT}$ . Since there is no on-chip decimation or averaging it is recommended that data on  $\text{Q\_OUT}$  is externally processed, for example using a simple FFT.

The temperature measurement should be performed with the SX1257 in StandbyEnable Mode ( $\text{RegMode} = 0\text{x}01$ )

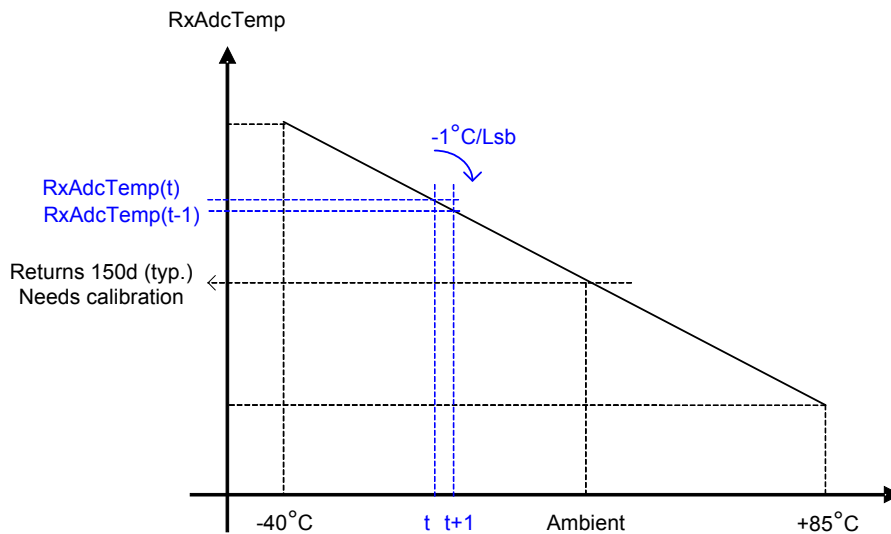


Figure 3-8: Temperature Sensor Response

### 3.7.4 I and Q Serial Interface

I and Q data is input to the ADCs on the rising edge of the reference sampling clock and is sampled on a falling edge. The RX ADC can be used either with an external clock  $\text{CLK\_IN}$  or with the internal clock, available on  $\text{CLK\_OUT}$  (recommended mode) for data synchronization. The I and Q channel bit stream timing diagram is illustrated below.

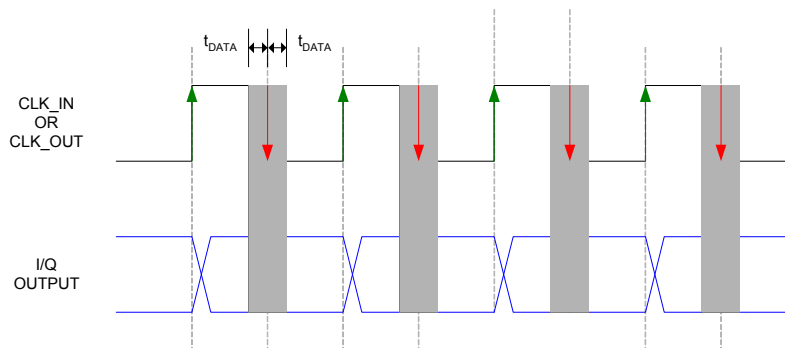


Figure 3-9: Receiver I and Q Channel Bit-Stream Timing Diagram