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# **DTC646**

# PWM Fan Speed Controller with Auto-Shutdown and FanSense™ Technology

#### **Features**

- Temperature Proportional Fan Speed for Acoustic Control and Longer Fan Life
- · Efficient PWM Fan Drive
- 3.0V to 5.5V Supply Range:
  - Fan Voltage Independent of TC646 Supply Voltage
  - Supports any Fan Voltage
- FanSense<sup>™</sup> Fault Detection Circuits Protect Against Fan Failure and Aid System Testing
- · Shutdown Mode for "Green" Systems
- Supports Low Cost NTC/PTC Thermistors
- · Space Saving 8-Pin MSOP Package
- · Over-temperature Indication

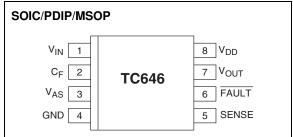
#### **Applications**

- · Power Supplies
- Computers
- File Servers
- · Portable Computers
- · Telecom Equipment
- · UPS, Power Amps
- · General Purpose Fan Speed Control

#### **Available Tools**

- Fan Controller Demonstration Board (TC642DEMO)
- Fan Controller Evaluation Kit (TC642EV)

#### Package Types



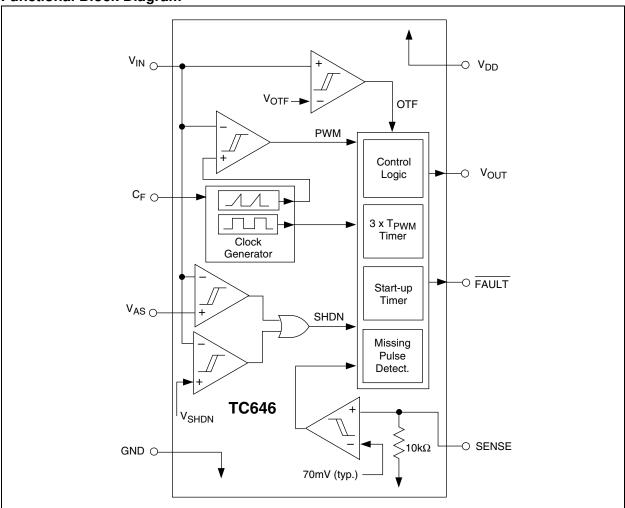
#### **General Description**

The TC646 is a switch mode, fan speed controller for use with brushless DC fans. Temperature proportional speed control is accomplished using pulse width modulation (PWM). A thermistor (or other voltage output temperature sensor) connected to the  $V_{\rm IN}$  input furnishes the required control voltage of 1.25V to 2.65V (typical) for 0% to 100% PWM duty cycle. The TC646 automatically suspends fan operation when measured temperature  $(V_{\rm IN})$  is below a user programmed minimum setting  $(V_{\rm AS})$ . An integrated Start-up Timer ensures reliable motor start-up at turn-on, coming out of shutdown mode, auto-shutdown mode or following a transient fault.

The TC646 features Microchip Technology's proprietary FanSense™ technology for increasing system reliability. In normal fan operation, a pulse train is present at SENSE (Pin 5). A missing-pulse detector monitors this pin during fan operation. A stalled, open, or unconnected fan causes the TC646 to trigger its Start-up Timer once. If the fault persists, the FAULT output goes low and the device is latched in its shutdown mode. FAULT is also asserted if the PWM reaches 100% duty cycle, indicating a possible thermal runaway situation, although the fan continues to run. See Section 5.0, "Typical Applications", for more information and system design guidelines.

The TC646 is available in the 8-pin plastic DIP, SOIC and MSOP packages and is available in the industrial and extended commercial temperature ranges.

## **Functional Block Diagram**



# 1.0 ELECTRICAL CHARACTERISTICS

# **Absolute Maximum Ratings\***

Supply Voltage	6V
Input Voltage, Any Pin (GND - 0.3	$(V_{DD}+0.3V)$
Package Thermal Resistance:	
PDIP (R <sub>0</sub> JA)	125°C/W
SOIC (R <sub>θ,JA</sub> )	155°C/W
MSOP (R <sub>0JA</sub> )	200°C/W
Specified Temperature Range	40°C to +125°C
Storage Temperature Range	-65°C to ±150°C

\*Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operation sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### DC ELECTRICAL SPECIFICATIONS

Symbol	Parameter	Min	Тур	Max	Units	Test Conditions
$V_{DD}$	Supply Voltage	3.0		5.5	V	
I <sub>DD</sub>	Supply Current, Operating	_	0.5	1.0	mA	Pins 6, 7 Open, C <sub>F</sub> = 1 μF, V <sub>IN</sub> = V <sub>C(MAX)</sub>
I <sub>DD(SHDN)</sub>	Supply Current, Shutdown/ Auto-shutdown Mode	_	25	_	μΑ	Pins 6, 7 Open; <b>Note 1</b> C <sub>F</sub> =1 μF, V <sub>IN</sub> = 0.35V
I <sub>IN</sub>	V <sub>IN</sub> , V <sub>AS</sub> Input Leakage	-1.0	_	+1.0	μΑ	Note 1
V <sub>OUT</sub> Output	t .					
t <sub>R</sub>	V <sub>OUT</sub> Rise Time	_	_	50	μsec	I <sub>OH</sub> = 5 mA, <b>Note 1</b>
t <sub>F</sub>	V <sub>OUT</sub> Fall Time	_	_	50	μsec	I <sub>OL</sub> = 1 mA, <b>Note 1</b>
t <sub>SHDN</sub>	Pulse Width(On V <sub>IN</sub> ) to Clear Fault Mode	30	_	_	μsec	V <sub>SHDN</sub> , V <sub>HYST</sub> Specifications, <b>Note 1</b>
I <sub>OL</sub>	Sink Current at V <sub>OUT</sub> Output	1.0	_	_	mA	$V_{OL} = 10\%$ of $V_{DD}$
I <sub>ОН</sub>	Source Current at V <sub>OUT</sub> Output	5.0	_	_	mA	$V_{OH}$ = 80% of $V_{DD}$
SENSE Inpu	t					
V <sub>TH(SENSE)</sub>	SENSE Input Threshold Voltage with Respect to GND	50	70	90	mV	Note 1
FAULT Outp	ut					
V <sub>OL</sub>	Output Low Voltage	_	_	0.3	V	I <sub>OL</sub> = 2.5 mA
t <sub>MP</sub>	Missing Pulse Detector Timer	_	32/F	_	Sec	C <sub>F</sub> = 1.0 μF
<sup>t</sup> STARTUP	Start-up Timer	_	32/F	_	Sec	C <sub>F</sub> = 1.0 μF
t <sub>DIAG</sub>	Diagnostic Timer	_	3/F	_	Sec	C <sub>F</sub> = 1.0 μF

Note 1: Ensured by design, not tested.

# DC ELECTRICAL SPECIFICATIONS (CONTINUED)

<b>Electrical Characteristics:</b> Unless otherwise specified, $T_{MIN} \le T_A \le T_{MAX}$ , $V_{DD} = 3.0V$ to 5.5V							
Symbol	Parameter	Min	Тур	Max	Units	Test Conditions	
V <sub>IN</sub> , V <sub>AS</sub> Input	s						
$V_{C(MAX),}V_{OTF}$	Voltage at V <sub>IN</sub> for 100% Duty Cycle and Overtemp. Fault	2.5	2.65	2.8	V		
V <sub>C(SPAN)</sub>	V <sub>C(MAX)</sub> - V <sub>C(MIN)</sub>	1.3	1.4	1.5	V		
V <sub>AS</sub>	Auto-shutdown Threshold	V <sub>C(MAX)</sub> ~ V <sub>C(SPAN)</sub>	_	V <sub>C(MAX)</sub>	V		
V <sub>SHDN</sub>	Voltage Applied to V <sub>IN</sub> to ensure Reset/Shutdown	_	_	V <sub>DD</sub> x 0.13	V		
$V_{REL}$	Voltage Applied to V <sub>IN</sub> to Release Reset Mode	V <sub>DD</sub> x 0.19	_	_	V	V <sub>DD</sub> = 5V, See Figure 5-11	
V <sub>HYST</sub>	Hysteresis on V <sub>SHDN</sub> , V <sub>REL</sub>	_	0.01 x V <sub>DD</sub>	_	٧		
V <sub>HAS</sub>	Hysteresis on Auto-shutdown Comparator	_	70	_	mV		
Pulse Width N	Modulator						
Fosc	PWM Frequency	26	30	34	Hz	C <sub>F</sub> = 1.0 μF	

Note 1: Ensured by design, not tested.

#### 2.0 PIN DESCRIPTIONS

The descriptions of the pins are listed in Table 2-1.

TABLE 2-1: PIN FUNCTION TABLE

Pin No.	Symbol	Description
1	V <sub>IN</sub>	Analog Input
2	$C_F$	Analog Output
3	$V_{AS}$	Analog Input
4	GND	Ground Terminal
5	SENSE	Analog Input
6	FAULT	Digital (Open Collector) Output
7	V <sub>OUT</sub>	Digital Output
8	$V_{DD}$	Power Supply Input

#### 2.1 Analog Input (V<sub>IN</sub>)

The thermistor network (or other temperature sensor) connects to the  $V_{IN}$  input. A voltage range of 1.25V to 2.65V (typical) on this pin drives an active duty cycle of 0% to 100% on the  $V_{OUT}$  pin. The TC646 enters shutdown mode when  $V_{IN} \leq V_{SHDN}.$  During shutdown, the FAULT output is inactive, and supply current falls to 25  $\mu A$  (typical). The TC646 exits shutdown mode when  $V_{IN} \geq V_{REL}$  (see Section 5.0, "Typical Applications", for details).

#### 2.2 Analog Output (C<sub>F</sub>)

 $C_F$  is the positive terminal for the PWM ramp generator timing capacitor. The recommended  $C_F$  is 1  $\mu F$  for 30 Hz PWM operation.

#### 2.3 Analog Input (V<sub>AS</sub>)

An external resistor divider connected to the  $V_{AS}$  input sets the auto-shutdown threshold. Auto-shutdown occurs when  $V_{IN} \leq V_{AS}$ . The fan is automatically restarted when  $V_{IN} \geq (V_{AS} + V_{HAS})$  (see Section 5.0, "Typical Applications", for more details).

#### 2.4 Ground (GND)

GND denotes the ground terminal.

#### 2.5 Analog Input (SENSE)

Pulses are detected at the SENSE pin as fan rotation chops the current through a sense resistor (R<sub>SENSE</sub>). The absence of pulses indicates a fault (see Section 5.0, "Typical Applications", for more details).

#### 2.6 Digital Output (FAULT)

The FAULT line goes low to indicate a fault condition. When FAULT goes low due to a fan fault condition, the device is latched in shutdown mode until deliberately cleared or until power is cycled. FAULT will also be asserted when the PWM reaches 100% duty cycle, indicating that maximum cooling capability has been reached and a possible over-temperature condition may occur. This is a non-latching state and the FAULT output will go high when the PWM duty cycle goes below 100%.

#### 2.7 Digital Output (V<sub>OUT</sub>)

V<sub>OUT</sub> is an active high complimentary output that drives the base of an external NPN transistor (via an appropriate base resistor) or the gate of an N-channel MOS-FET. This output has asymmetrical drive (see Section 1.0, "Electrical Characteristics").

### 2.8 Power Supply Input (V<sub>DD</sub>)

 $V_{DD}$  may be independent of the fan's power supply (see Section 1.0, "Electrical Characteristics").

#### 3.0 DETAILED DESCRIPTION

#### 3.1 PWM

The PWM circuit consists of a ramp generator and threshold detector. The frequency of the PWM is determined by the value of the capacitor connected to the  $C_F$  input. A frequency of 30 Hz is recommended ( $C_F=1~\mu F$ ). The PWM is also the time base for the Start-up Timer (see Section 3.3, "Start-Up Timer"). The PWM voltage control range is 1.25V to 2.65V (typical) for 0% to 100% output duty cycle.

#### 3.2 V<sub>OUT</sub> Output

The  $V_{OUT}$  pin is designed to drive a low cost transistor or MOSFET as the low side, power switching element in the system. Various examples of driver circuits will be shown throughout this data sheet. This output has asymmetric complementary drive and is optimized for driving NPN transistors or N-channel MOSFETs. Since the system relies on PWM rather than linear control, the power dissipation in the power switch is kept to a minimum. Generally, very small devices (TO-92 or SOT packages) will suffice.

#### 3.3 Start-Up Timer

To ensure reliable fan start-up, the Start-up Timer turns the  $V_{OUT}$  output on for 32 cycles of the PWM whenever the fan is started from the off state. This occurs at power-up and when coming out of shutdown or auto-shutdown mode. If the PWM frequency is 30 Hz ( $C_F=1~\mu F$ ), the resulting start-up time will be approximately one second. If a fan fault is detected, the Diagnostic Timer is triggered once, followed by the Start-up Timer. If the fault persists, the device is shut down (see Section 3.5, "FAULT Output").

# 3.4 SENSE Input (FanSense™ Technology)

The SENSE input (Pin 5) is connected to a low value current sensing resistor in the ground return leg of the fan circuit. During normal fan operation, commutation occurs as each pole of the fan is energized. This causes brief interruptions in the fan current, seen as pulses across the sense resistor. If the device is not in auto-shutdown or shutdown mode, and pulses are not appearing at the SENSE input, a fault exists.

The short, rapid change in fan current (high dl/dt) causes a corresponding dV/dt across the sense resistor,  $R_{SENSE}$ . The waveform on  $R_{SENSE}$  is differentiated and converted to a logic-level pulse-train by  $C_{SENSE}$  and the internal signal processing circuitry. The presence and frequency of this pulse-train is a direct indication of fan operation. See Section 5.0, "Typical Applications", for more details.

### 3.5 FAULT Output

The TC646 detects faults in two ways:

First, pulses appearing at SENSE due to the PWM turning on are blanked, with the remaining pulses being filtered by a missing pulse detector. If consecutive pulses are not detected for thirty-two PWM cycles ( $\cong$ 1 Sec if C<sub>F</sub> = 1 μF), the Diagnostic Timer is activated and VOUT is driven high continuously for three PWM cycles ( $\approx 100$  msec if  $C_F = 1 \mu F$ ). If a pulse is not detected within this window, the Start-up Timer is triggered (see Section 3.3, "Start-up Timer"). This should clear a transient fault condition. If the missing pulse detector times out again, the PWM is stopped and FAULT goes low. When FAULT is activated due to this condition, the device is latched in shutdown mode and will remain off indefinitely. Therefore, the TC646 is prevented from attempting to drive a fan under catastrophic fault conditions.

One of two things will restore operation: Cycling power off and then on again or pulling  $V_{IN}$  below  $V_{SHDN}$  and releasing it to a level above  $V_{REL}$ . When one of these two conditions is satisfied, the normal start-up cycle is triggered and operation will resume if the fault has been cleared.

The second condition by which the TC646 asserts a FAULT is when the PWM control voltage applied to  $V_{\rm IN}$  becomes greater than that needed to drive 100% duty cycle (see Section 1.0, "Electrical Characteristics"). This indicates that the fan is at maximum drive and the potential exists for system overheating. Either heat dissipation in the system has gone beyond the cooling system's design limits or some subtle fault exists (such as fan bearing failure or an airflow obstruction). This output may be treated as a "System Overheat" warning and be used to trigger system shutdown or some other corrective action.

However, in this case, the fan will continue to run even when  $\overline{\text{FAULT}}$  is asserted. If the system is allowed to continue operation, and the temperature (and thus  $V_{IN}$ ) falls, the  $\overline{\text{FAULT}}$  output will become inactive when  $V_{IN}$  <  $V_{OTF}$ 

#### 3.6 Auto-Shutdown Mode

If the voltage on  $V_{IN}$  becomes less than the voltage on  $V_{AS}$ , the fan is automatically shut off (auto-shutdown mode). The TC646 exits auto-shutdown mode when the voltage on  $V_{IN}$  becomes higher than the voltage on  $V_{AS}$  by  $V_{HAS}$  (the auto-shutdown Hysteresis Voltage (see Figure 3-1)). The Start-up Timer is triggered and normal operation is resumed upon exiting auto-shutdown mode. The FAULT output is unconditionally inactive in auto-shutdown mode.

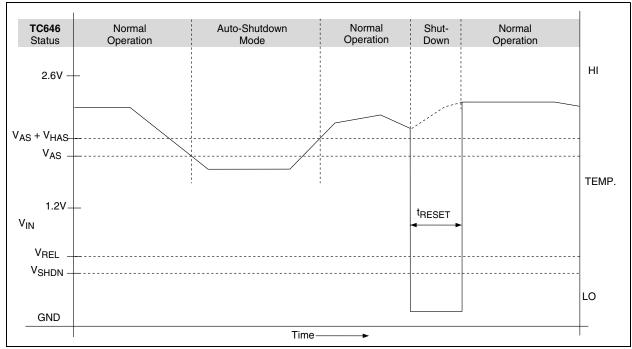


FIGURE 3-1: TC646 Nominal Operation.

#### 3.7 Shutdown Mode (Reset)

If an unconditional shutdown and/or device reset is desired, the TC646 may be placed in shutdown mode by forcing  $V_{\text{IN}}$  to a logic low (i.e.,  $V_{\text{IN}} < V_{\text{SHDN}}$ ) (see Figure 3-1). In this mode, all functions cease and the FAULT output is unconditionally inactive. The TC646 should not be shut down unless all heat producing activity in the system is at a negligible level. The TC646 exits shutdown mode when  $V_{\text{IN}}$  becomes greater than  $V_{\text{REL}}$ , the release voltage.

Entering shutdown mode also performs a complete device reset. Shutdown mode resets the TC646 into its power-up state. The Start-up and Fault Timers, and any current faults, are cleared. FAULT is unconditionally inactive in shutdown mode. Upon exiting shutdown mode (V $_{\rm IN}$  > V $_{\rm REL}$ ), the Start-up Timer will be triggered and normal operation will resume, assuming no fault conditions exist and V $_{\rm IN}$  > V $_{\rm AS}$  + V $_{\rm HAS}$ 

**Note:** If  $V_{\text{IN}} < V_{\text{AS}}$  when the device exits shutdown mode, the fan will not restart as it will be in auto-shutdown mode.

If a fan fault has occurred and the device has latched itself into shutdown mode, performing a reset will not clear the fault unless  $V_{IN}$  >  $(V_{AS} + V_{HAS})$ . If  $V_{IN}$  is not greater than  $(V_{AS} + V_{HAS})$  upon exiting shutdown mode, the fan will not be restarted. Consequently, there is no way to establish that the fan fault has been cleared. To ensure that a complete reset takes place, the user's circuitry must ensure that  $V_{IN} > (V_{AS} + V_{HAS})$ when the device is released from shutdown mode. A recommended algorithm for management of the TC646 by a host microcontroller or other external circuitry is given in Section 5.0, "Typical Applications". A small amount of hysteresis, typically one percent of VDD (50 mV at  $V_{DD} = 5.0V$ ), is designed into the  $V_{SHDN}/$  $V_{\mbox{\scriptsize REL}}$  threshold. The levels specified for  $V_{\mbox{\scriptsize SHDN}}$  and V<sub>REL</sub> in Section 1.0, "Electrical Characteristics", include this hysteresis plus adequate margin to account for normal variations in the absolute value of the threshold and hysteresis.

**CAUTION:** Shutdown mode is unconditional. That is, the fan will remain off as long as the  $V_{IN}$  pin is being held low or  $V_{IN} < V_{AS} + V_{HAS}$ .

#### 4.0 SYSTEM BEHAVIOR

The flowcharts describing the TC646's behavioral algorithm are shown in Figure 4-1. They can be summarized as follows:

#### 4.1 Power-Up

- (1) Assuming the device is not being held in auto-shut-down mode ( $V_{IN} > V_{AS}$ ).......
- (2) Turn V<sub>OUT</sub> output on for 32 cycles of the PWM clock. This ensures that the fan will start from a dead stop.
- (3) During this Start-up Timer, if a fan pulse is detected, branch to Normal Operation; if none are received...
- (4) Activate the 32-cycle Start-up Timer one more time and look for fan pulse; if a fan pulse is detected, proceed to Normal Operation; if none are received...
- (5) Proceed to Fan Fault.
- (6) End.

#### 4.2 Normal Operation

"Normal Operation" is an endless loop which may only be exited by entering shutdown mode, auto-shutdown mode or Fan Fault. The loop can be thought of as executing at the frequency of the oscillator and PWM.

- (1) Reset the missing pulse detector.
- (2) Is the TC646 in shutdown or auto-shutdown mode?

If so...

- a. V<sub>OUT</sub> duty cycle goes to zero.
- b. FAULT is disabled.
- c. Exit the loop and wait for  $V_{IN} > (V_{AS} + V_{HAS})$  to resume operation.
- (3) If an over-temperature fault occurs ( $V_{IN} > V_{OTF}$ ), activate FAULT; release FAULT when  $V_{IN} < V_{OTF}$ .
- (4) Drive V<sub>OUT</sub> to a duty cycle proportional to V<sub>IN</sub> on a cycle by cycle basis.
- (5) If a fan pulse is detected, branch back to the start of the loop (1).
- (6) If the missing pulse detector times out ...
- (7) Activate the 3-cycle Diagnostic Timer and look for pulses; if a fan pulse is detected, branch back to the start of the loop (1); if none are received...
- (8) Activate the 32-cycle Start-up Timer and look for pulses; if a fan pulse is detected, branch back to the start of the loop (1); if none are received...
- (9) Quit Normal Operation and go to Fan Fault.
- (10) End.

#### 4.3 Fan Fault

Fan fault is an infinite loop wherein the TC646 is latched in shutdown mode. This mode can only be released by a reset (i.e.,  $V_{IN}$  being brought below  $V_{SHDN}$ , then above  $(V_{AS} + V_{HAS})$ , or by power-cycling).

- While in this state, FAULT is latched on (low) and the V<sub>OUT</sub> output is disabled.
- A reset sequence applied to the V<sub>IN</sub> pin will exit the loop to Power-up.
- (3) End.

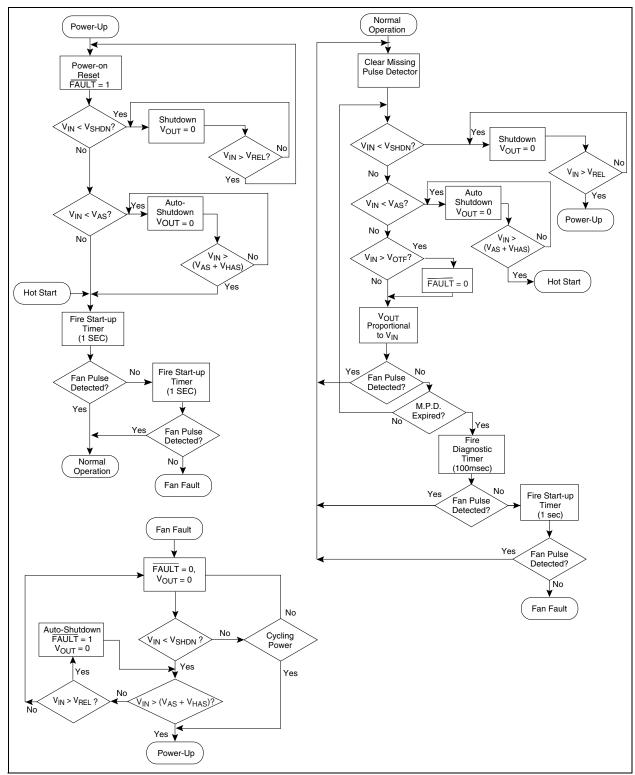


FIGURE 4-1: TC646 Behavioral Algorithm Flowchart.

#### 5.0 TYPICAL APPLICATIONS

Designing with the TC646 involves the following:

- (1) The temperature sensor network must be configured to deliver 1.25V to 2.65V on  $V_{\rm IN}$  for 0% to 100% of the temperature range to be regulated.
- (2) The auto-shutdown temperature must be set with a voltage divider on V<sub>AS</sub>.
- (3) The output drive transistor and associated circuitry must be selected.
- (4) The SENSE network, R<sub>SENSE</sub> and C<sub>SENSE</sub>, must be designed for maximum efficiency while delivering adequate signal amplitude.
- (5) If shutdown capability is desired, the drive requirements of the external signal or circuit must be considered.

The TC642 demonstration and prototyping board (TC642DEMO) and the TC642 Evaluation Kit (TC642EV) provide working examples of TC646 circuits and prototyping aids. The TC642DEMO is a printed circuit board optimized for small size and ease of inclusion into system prototypes. The TC642EV is a larger board intended for benchtop development and analysis. At the very least, anyone contemplating a design using the TC646 should consult the documentation for both TC642EV (DS21403) and TC642DEMO (DS21401). Figure 5-1 shows the base schematic for the TC642DEMO.

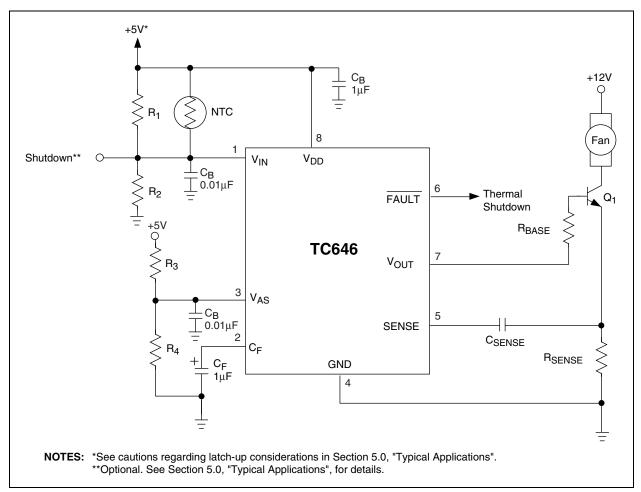
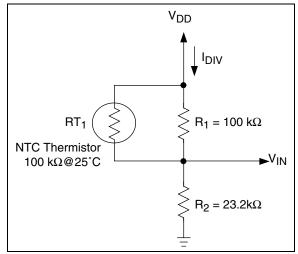


FIGURE 5-1: Typical Application Circuit.

#### 5.1 Temperature Sensor Design

The temperature signal connected to  $V_{IN}$  must output a voltage in the range of 1.25V to 2.65V (typical) for 0% to 100% of the temperature range of interest. The circuit in Figure 5-2 illustrates a convenient way to provide this signal.



**FIGURE 5-2:** Temperature Sensing Circuit.

Figure 5-2 shows a simple temperature dependent voltage divider circuit.  $RT_1$  is a conventional NTC thermistor, while  $R_1$  and  $R_2$  are standard resistors. The supply voltage,  $V_{DD}$ , is divided between  $R_2$  and the parallel combination of  $RT_1$  and  $R_1$ . For convenience, the parallel combination of  $RT_1$  and  $R_1$  will be referred to as  $R_{TEMP}$ . The resistance of the thermistor at various temperatures is obtained from the manufacturer's specifications. Thermistors are often referred to in terms of their resistance at 25°C.

Generally, the thermistor shown in Figure 5-2 is a nonlinear device with a negative temperature coefficient (also called an NTC thermistor). In Figure 5-2,  $R_1$  is used to linearize the thermistor temperature response and  $R_2$  is used to produce a positive temperature coefficient at the  $V_{\text{IN}}$  node. As an added benefit, this configuration produces an output voltage delta of 1.4V, which is well within the range of the  $V_{\text{C(SPAN)}}$  specification of the TC646. A 100 k $\Omega$  NTC thermistor is selected for this application in order to keep  $I_{\text{DIV}}$  at a minimum.

For the voltage range at  $V_{\rm IN}$  to be equal to 1.25V to 2.65V, the temperature range of this configuration is 0°C to 50°C. If a different temperature range is required from this circuit,  $R_1$  should be chosen to equal the resistance value of the thermistor at the center of this new temperature range. It is suggested that a maximum temperature range of 50°C be used with this circuit due to thermistor linearity limitations. With this change,  $R_2$  is adjusted according to the following equations:

#### **EQUATION**

$$\frac{V_{DD} x R_2}{R_{TEMP} (T_I) + R_2} = V(T_I)$$

$$\frac{V_{DD} x R_2}{R_{TEMP} (T_2) + R_2} = V(T_2)$$

Where  $T_1$  and  $T_2$  are the chosen temperatures and  $R_{TEMP}$  is the parallel combination of the thermistor and  $R_1$ .

These two equations facilitate solving for the two unknown variables,  $R_1$  and  $R_2$ . More information about thermistors may be obtained from AN679, "Temperature Sensing Technologies", and AN685, "Thermistors In Single Supply Temperature Sensing Circuits", which can be downloaded from Microchip's web site at www.microchip.com.

# 5.2 Auto-Shutdown Temperature Design

A voltage divider on  $V_{AS}$  sets the temperature where the part is automatically shut down if the sensed temperature at  $V_{IN}$  drops below the set temperature at  $V_{AS}$  (i.e.,  $V_{IN} < V_{AS}$ ). As with the  $V_{IN}$  input, 1.25V to 2.65V corresponds to the temperature range of interest from  $T_1$  to  $T_2$ , respectively. Assuming that the temperature sensor network designed above is linearly related to temperature, the shutdown temperature  $T_{AS}$  is related to  $T_2$  and  $T_1$  by:

#### **EQUATION**

$$\frac{2.65V - 1.25V}{T_2 - T_1} = \frac{V_{AS} - 1.25V}{T_{AS} - T_1}$$

$$V_{AS} = \left(\frac{1.4V}{T_2 - T_1}\right) (T_{AS} - T_1) + 1.25V$$

For example, if 1.25V and 2.65V at  $V_{IN}$  corresponds to a temperature range of  $T_1$  = 0°C to  $T_2$  = 125°C, and the auto-shutdown temperature desired is 25°C, then  $V_{AS}$  voltage is:

#### **EQUATION**

$$V_{AS} = \frac{1.4V}{(125 - 0)} (25 - 0) + 1.25V = 1.53V$$

The V<sub>AS</sub> voltage may be set using a simple resistor divider as shown in Figure 5-3.

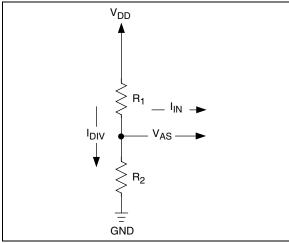


FIGURE 5-3: VAS CIRCUIT

Per Section 1.0, "Electrical Characteristics", the leakage current at the  $V_{AS}$  pin is no more than 1  $\mu A$ . It is conservative to design for a divider current,  $I_{DIV}$ , of 100  $\mu A$ . If  $V_{DD} = 5.0V$  then...

#### **EQUATION**

$$I_{DIV} = 1e^{-4}A = \frac{5.0V}{R_1 + R_2}, therefore$$

$$R_1 + R_2 = \frac{5.0V}{1e^{-4}A} = 50,000\Omega = 50k\Omega$$

We can further specify  $R_1$  and  $R_2$  by the condition that the divider voltage is equal to our desired  $V_{AS}$ . This yields:

#### **EQUATION**

$$V_{AS} = \frac{V_{DD} x R_2}{R_1 + R_2}$$

Solving for the relationship between  $R_1$  and  $R_2$  results in:

#### **EQUATION**

$$R_1 = R_2 x \quad \frac{V_{DD} - V_{AS}}{V_{AS}} = R_2 x \quad \frac{5 - 1.53}{I.53}$$

In the case of this example,  $R_1 = (2.27) R_2$ . Substituting this relationship back into the original equation yields the resistor values:

$$R_2$$
 = 15.3 k $\Omega$ , and  $R_1$  = 34.7 k $\Omega$ 

In this case, the standard values of 34.8 k $\Omega$  and 15.4 k $\Omega$  are very close to the calculated values and would be more than adequate.

#### 5.3 Operations at Low Duty Cycle

One boundary condition which may impact the selection of the minimum fan speed is the irregular activation of the Diagnostic Timer due to the TC646 "missing" fan commutation pulses at low speeds. This is a natural consequence of low PWM duty cycles (typically 25% or less). Recall that the SENSE function detects commutation of the fan as disturbances in the current through  $R_{\mbox{\footnotesize SENSE}}.$  These can only occur when the fan is energized (i.e.,  $V_{\mbox{\footnotesize OUT}}$  is "on"). At very low duty cycles, the  $V_{\mbox{\footnotesize OUT}}$  output is "off" most of the time. The fan may be rotating normally, but the commutation events are occurring during the PWM's off-time.

The phase relationship between the fan's commutation and the PWM edges tends to "walk around" as the system operates. At certain points, the TC646 may fail to capture a pulse within the 32-cycle missing pulse detector window. If this happens, the 3-cycle Diagnostic Timer will be activated, the  $V_{OUT}$  output will be active continuously for three cycles and, if the fan is operating normally, a pulse will be detected. If all is well, the system will return to normal operation. There is no harm in this behavior, but it may be audible to the user as the fan accelerates briefly when the Diagnostic Timer fires. For this reason, it is recommended that  $V_{\rm AS}$  be set no lower than 1.8V.

# 5.4 FanSense™ Network (R<sub>SENSE</sub> and C<sub>SENSE</sub>)

The FanSense network, comprised of R<sub>SENSE</sub> and C<sub>SENSE</sub>, allows the TC646 to detect commutation of the fan motor (FanSense<sup>™</sup> technology). This network can be thought of as a differentiator and threshold detector. The function of R<sub>SENSE</sub> is to convert the fan current into a voltage. C<sub>SENSE</sub> serves to AC-couple this voltage signal and provide a ground-referenced input to the SENSE pin. Designing a proper SENSE network is simply a matter of scaling R<sub>SENSE</sub> to provide the necessary amount of gain (i.e., the current-to-voltage conversion ratio). A 0.1 µF ceramic capacitor is recommended for C<sub>SENSE</sub>. Smaller values require larger sense resistors, and higher value capacitors are bulkier and more expensive. Using a 0.1 µF capacitor results in reasonable values for R<sub>SENSE</sub>. Figure 5-4 illustrates a typical SENSE network. Figure 5-5 shows the waveforms observed using a typical SENSE network.

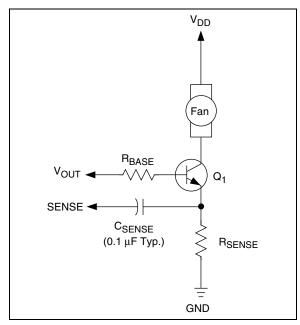


FIGURE 5-4: SENSE Network.

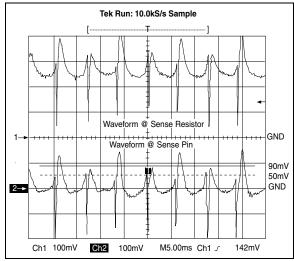


FIGURE 5-5: SENSE Waveforms.

Table 5-1 lists the recommended values of  $R_{SENSE}$  based on the nominal operating current of the fan. Note that the current draw specified by the fan manufacturer may be a worst-case rating for near-stall conditions and not the fan's nominal operating current. The values in Table 5-1 refer to actual average operating current. If the fan current falls between two of the values listed, use the higher resistor value. The end result of employing Table 5-1 is that the signal developed across the sense resistor is approximately 450 mV in amplitude.

TABLE 5-1: R<sub>SENSE</sub> VS. FAN CURRENT

Nominal Fan Current (mA)	$R_{SENSE}(\Omega)$
50	9.1
100	4.7
150	3.0
200	2.4
250	2.0
300	1.8
350	1.5
400	1.3
450	1.2
500	1.0

#### 5.5 Output Drive Transistor Selection

The TC646 is designed to drive an external transistor or MOSFET for modulating power to the fan. This is shown as  $Q_1$  in Figures 5-1, 5-4, 5-6, 5-7, 5-8 and 5-9. The  $V_{OUT}$  pin has a minimum source current of 5 mA and a minimum sink current of 1 mA. Bipolar transistors or MOSFETs may be used as the power switching element, as shown in Figure 5-7. When high current gain is needed to drive larger fans, two transistors may be used in a Darlington configuration. These circuit topologies are shown in Figure 5-7: (a) shows a single NPN transistor used as the switching element; (b) illustrates the Darlington pair; and (c) shows an N-channel MOSFET.

One major advantage of the TC646's PWM control scheme versus linear speed control is that the power dissipation in the pass element is kept very low. Generally, low cost devices in very small packages, such as TO-92 or SOT, can be used effectively. For fans with nominal operating currents of no more than 200 mA, a single transistor usually suffices. Above 200 mA, the Darlington or MOSFET solution is recommended. For the fan sensing function to work correctly, it is imperative that the pass transistor be fully saturated when "on".

Table 5-2 gives examples of some commonly available transistors and MOSFETs. This table should be used as a guide only since there are many transistors and MOSFETs which will work just as well as those listed. The critical issues when choosing a device to use as  $Q_1$  are: (1) the breakdown voltage ( $V_{(BR)CFO}$  or  $V_{DS}$ (MOSFET)) must be large enough to withstand the highest voltage applied to the fan (Note: This will occur when the fan is off); (2) 5 mA of base drive current must be enough to saturate the transistor when conducting the full fan current (transistor must have sufficient gain); (3) the VOLIT voltage must be high enough to sufficiently drive the gate of the MOSFET to minimize the R<sub>DS(on)</sub> of the device; (4) rated fan current draw must be within the transistor's/MOSFET's current handling capability; and (5) power dissipation must be kept within the limits of the chosen device.

A base-current limiting resistor is required with bipolar transistors. This is shown in Figure 5-6.

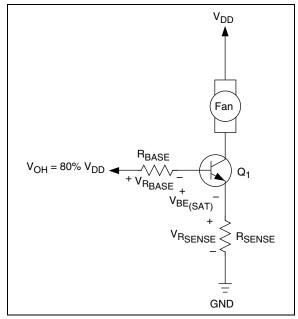


FIGURE 5-6: R<sub>BASE</sub>.

Circuit For Determining

The correct value for this resistor can be determined as follows:

$$\begin{array}{ll} V_{OH} & = V_{RSENSE} + V_{BE(SAT)} + V_{RBASE} \\ V_{RSENSE} & = I_{FAN} \times R_{SENSE} \\ V_{RBASE} & = R_{BASE} \times I_{BASE} \\ I_{BASE} & = I_{FAN} / h_{FE} \end{array}$$

 $V_{OH}$  is specified as 80% of  $V_{DD}$  in Section 1.0, "Electrical Characteristics";  $V_{BE(SAT)}$  is given in the chosen transistor data sheet. It is now possible to solve for R<sub>BASE</sub>.

#### **EQUATION**

$$R_{BASE} = \frac{V_{OH} - V_{BE(SAT)} - V_{RSENSE}}{I_{BASE}}$$

Some applications benefit from the fan being powered from a negative supply to keep motor noise out of the positive supply rails. This can be accomplished as shown in Figure 5-8. Zener diode D<sub>1</sub> offsets the -12V power supply voltage, holding transistor Q1 off when V<sub>OUT</sub> is low. When V<sub>OUT</sub> is high, the voltage at the anode of  $D_1$  increases by  $V_{OUT}$ , causing  $Q_1$  to turn on. Operation is otherwise the same as in the case of fan operation from +12V.

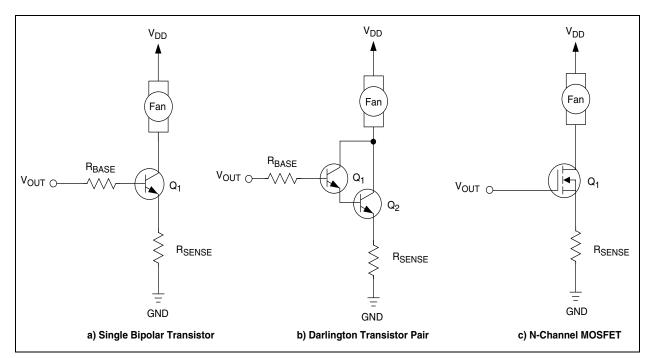


FIGURE 5-7: Output Drive Transistor Circuit Topologies.

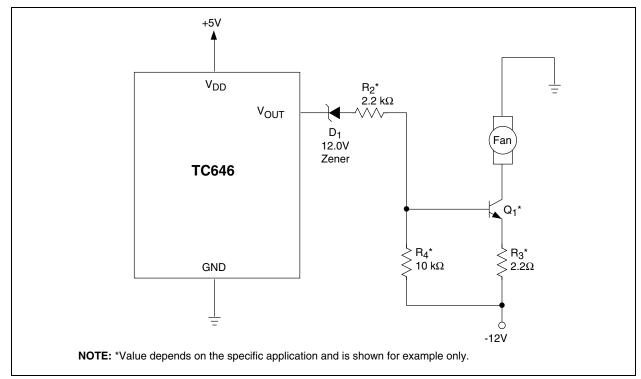


FIGURE 5-8: Power the Fan from a -12V Supply.

TABLE 5-2: TRANSISTORS AND MOSFETS FOR  $Q_1 (V_{DD} = 5V)$ 

	= 0 = 1 = 1 = 1 = 1 = 1 = 1 = 1 = 1 = 1							
Device	Package	Max. V <sub>BE(sat)</sub> /V <sub>GS</sub> (V)	Min. H <sub>FE</sub>	V <sub>CEO</sub> /V <sub>DS</sub> (V)	Fan Current (mA)	Suggested $R_{BASE}(\Omega)$		
MMBT2222A	SOT-23	1.2	50	40	150	800		
MPS2222A	TO-92	1.2	50	40	150	800		
MPS6602	TO-92	1.2	50	40	500	301		
SI2302	SOT-23	2.5	NA	20	500	Note 1		
MGSF1N02E	SOT-23	2.5	NA	20	500	Note 1		
SI4410	SO-8	4.5	NA	30	1000	Note 1		
SI2308	SOT-23	4.5	NA	60	500	Note 1		

Note 1: A series gate resistor may be used in order to control the MOSFET turn-on and turn-off times.

#### 5.6 Latch-up Considerations

As with any CMOS IC, the potential exists for latch-up if signals are applied to the device which are outside the power supply range. This is of particular concern during power-up if the external circuitry (such as the sensor network,  $V_{AS}$  divider or shutdown circuit) is powered by a supply different from that of the TC646. Care should be taken to ensure that the TC646's  $V_{DD}$  supply powers up first. If possible, the networks attached to  $V_{IN}$  and  $V_{AS}$  should connect to the  $V_{DD}$  supply at the same physical location as the IC itself. Even if the IC and any external networks are powered by the same supply, physical separation of the connecting points can result in enough parasitic capacitance and/or inductance in the power supply connections to delay one power supply "routing" versus another.

# 5.7 Power Supply Routing and Bypassing

Noise present on the  $V_{IN}$  and  $V_{AS}$  inputs may cause erroneous operation of the FAULT output. As a result, these inputs should be bypassed with a 0.01  $\mu$ F capacitor mounted as close to the package as possible. This is especially true of  $V_{IN}$ , which is usually driven from a high impedance source (such as a thermistor). In addition, the  $V_{DD}$  input should be bypassed with a 1  $\mu$ F capacitor. Grounds should be kept as short as possible. To keep fan noise off the TC646 ground pin, individual ground returns for the TC646 and the low side of the fan current sense resistor should be used.

#### **Design Example**

Step 1. Calculate  $R_1$  and  $R_2$  based on using an NTC having a resistance of 10 k $\Omega$  at  $T_{MIN}$  (25°C) and 4.65 k $\Omega$  at  $T_{MAX}$  (45°C) (See Figure 5-9).

 $R_1 = 20.5 \text{ k}\Omega$ 

 $R_2 = 3.83 \text{ k}\Omega$ 

Step 2. Set auto-shutdown level V<sub>AS</sub> = 1.8V. Limit the divider current to 100  $\mu$ A from which R<sub>5</sub> = 33 k $\Omega$ 

 $R_6 = 18 \text{ k}\Omega$ 

Step 3. Design the output circuit.

Maximum fan motor current = 250 mA.  $Q_1$  beta is chosen at 50 from which  $R_7$  = 800  $\Omega$ .

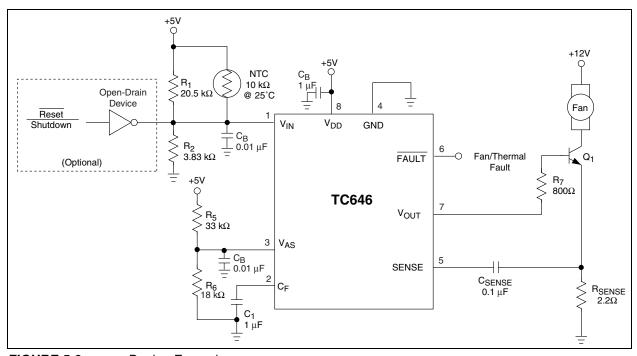


FIGURE 5-9: Design Example.

#### 5.8 TC646 as a Microcontroller Peripheral

In a system containing a microcontroller or other host intelligence, the TC646 can be effectively managed as a CPU peripheral. Routine fan control functions can be performed by the TC646 without controller intervention. The microcontroller receives temperature data from one or more points throughout the system. It calculates a fan operating speed based on an algorithm specifically designed for the application at hand. The processor controls fan speed using complementary port bits I/O1 through I/O3. Resistors  $\rm R_1$  through  $\rm R_6$  (5% tolerance) form a crude 3-bit DAC that translates the 3-bit code from the processor's outputs into a 1.6V DC control signal. A monolithic DAC or digital pot may be used instead of the circuit shown in Figure 5-10.

With V<sub>AS</sub> set at 1.8V, the TC646 enters auto-shutdown when the controller's output code is 000[B]. Output codes 001[B] to 111[B] operate the fan from roughly 40% to 100% of full speed. An open-drain output from the processor (I/O0) can be used to reset the TC646 following detection of a fault condition. The FAULT output can be connected to the controller's interrupt input, or to another I/O pin, for polled operation.

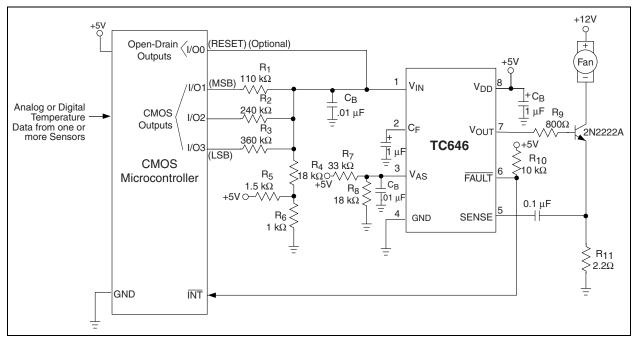


FIGURE 5-10: TC646 as a Microcontroller Peripheral.

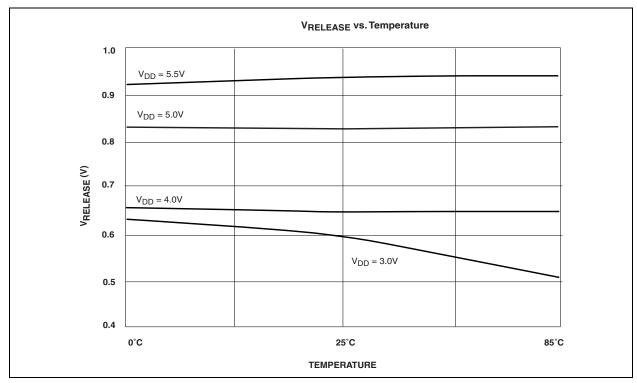


FIGURE 5-11: V<sub>RELEASE</sub> vs. Temperature.

#### 6.0 PACKAGING INFORMATION

#### 6.1 Package Marking Information









8-Lead MSOP



Example:



Example:



Example:



**Legend:** XX...X Customer-specific information

Y Year code (last digit of calendar year)
YY Year code (last 2 digits of calendar year)
WW Week code (week of January 1 is week '01')

NNN Alphanumeric traceability code

(e3) Pb-free JEDEC designator for Matte Tin (Sn)

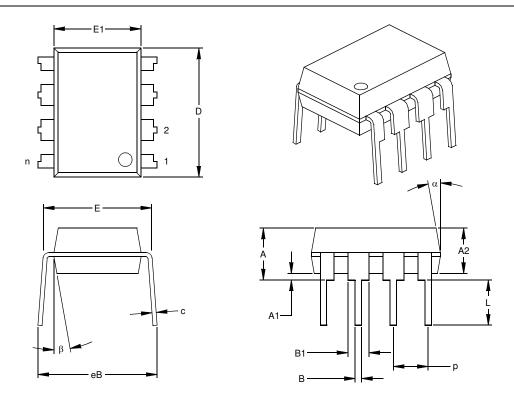
This package is Pb-free. The Pb-free JEDEC designator (e3)

can be found on the outer packaging for this package.

**Note**: In the event the full Microchip part number cannot be marked on one line, it will be carried over to the next line, thus limiting the number of available characters for customer-specific information.

### 8-Lead Plastic Dual In-line (P) – 300 mil (PDIP)

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



	Units		INCHES*		M	IILLIMETERS	3
Dimensi	on Limits	MIN	MOM	MAX	MIN	NOM	MAX
Number of Pins	n		8			8	
Pitch	р		.100			2.54	
Top to Seating Plane	Α	.140	.155	.170	3.56	3.94	4.32
Molded Package Thickness	A2	.115	.130	.145	2.92	3.30	3.68
Base to Seating Plane	A1	.015			0.38		
Shoulder to Shoulder Width	E	.300	.313	.325	7.62	7.94	8.26
Molded Package Width	E1	.240	.250	.260	6.10	6.35	6.60
Overall Length	D	.360	.373	.385	9.14	9.46	9.78
Tip to Seating Plane	L	.125	.130	.135	3.18	3.30	3.43
Lead Thickness	С	.008	.012	.015	0.20	0.29	0.38
Upper Lead Width	B1	.045	.058	.070	1.14	1.46	1.78
Lower Lead Width	В	.014	.018	.022	0.36	0.46	0.56
Overall Row Spacing	§ eB	.310	.370	.430	7.87	9.40	10.92
Mold Draft Angle Top	α	5	10	15	5	10	15
Mold Draft Angle Bottom	β	5	10	15	5	10	15

#### Notes:

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed

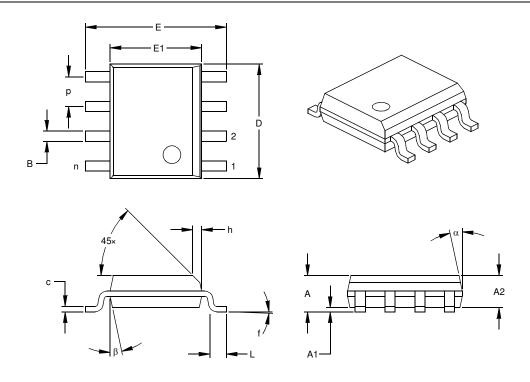
.010" (0.254mm) per side. JEDEC Equivalent: MS-001

Drawing No. C04-018

<sup>\*</sup> Controlling Parameter § Significant Characteristic

## 8-Lead Plastic Small Outline (SN) - Narrow, 150 mil (SOIC)

For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



	Units		INCHES*		N	IILLIMETERS	3
Dimension	Limits	MIN	NOM	MAX	MIN	NOM	MAX
Number of Pins	n		8			8	
Pitch	р		.050			1.27	
Overall Height	Α	.053	.061	.069	1.35	1.55	1.75
Molded Package Thickness	A2	.052	.056	.061	1.32	1.42	1.55
Standoff §	A1	.004	.007	.010	0.10	0.18	0.25
Overall Width	Е	.228	.237	.244	5.79	6.02	6.20
Molded Package Width	E1	.146	.154	.157	3.71	3.91	3.99
Overall Length	D	.189	.193	.197	4.80	4.90	5.00
Chamfer Distance	h	.010	.015	.020	0.25	0.38	0.51
Foot Length	L	.019	.025	.030	0.48	0.62	0.76
Foot Angle	f	0	4	8	0	4	8
Lead Thickness	С	.008	.009	.010	0.20	0.23	0.25
Lead Width	В	.013	.017	.020	0.33	0.42	0.51
Mold Draft Angle Top	α	0	12	15	0	12	15
Mold Draft Angle Bottom	β	0	12	15	0	12	15

#### Notes:

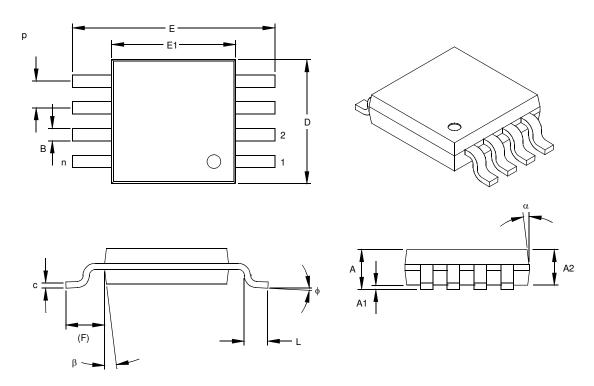
Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side.

JEDEC Equivalent: MS-012 Drawing No. C04-057

<sup>\*</sup> Controlling Parameter § Significant Characteristic

### 8-Lead Plastic Micro Small Outline Package (MS) (MSOP)

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



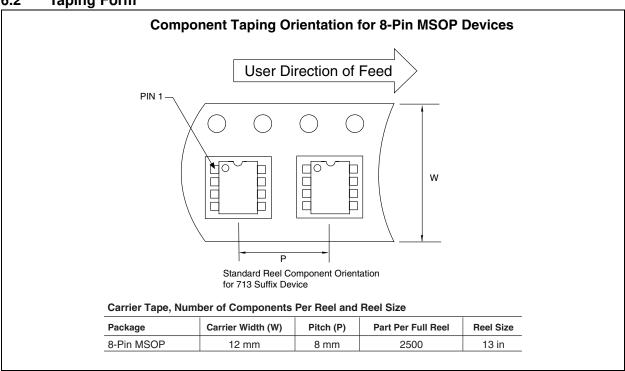
	Units		INCHES		М	LLIMETERS*	
Dimens	sion Limits	MIN	NOM	MAX	MIN	NOM	MAX
Number of Pins	n		8				8
Pitch	р		.026			0.65	
Overall Height	А			.044			1.18
Molded Package Thickness	A2	.030	.034	.038	0.76	0.86	0.97
Standoff §	A1	.002		.006	0.05		0.15
Overall Width	E	.184	.193	.200	4.67	4.90	.5.08
Molded Package Width	E1	.114	.118	.122	2.90	3.00	3.10
Overall Length	D	.114	.118	.122	2.90	3.00	3.10
Foot Length	L	.016	.022	.028	0.40	0.55	0.70
Footprint (Reference)	F	.035	.037	.039	0.90	0.95	1.00
Foot Angle	ф	0		6	0		6
Lead Thickness	С	.004	.006	.008	0.10	0.15	0.20
Lead Width	В	.010	.012	.016	0.25	0.30	0.40
Mold Draft Angle Top	α		7			7	
Mold Draft Angle Bottom	β		7			7	

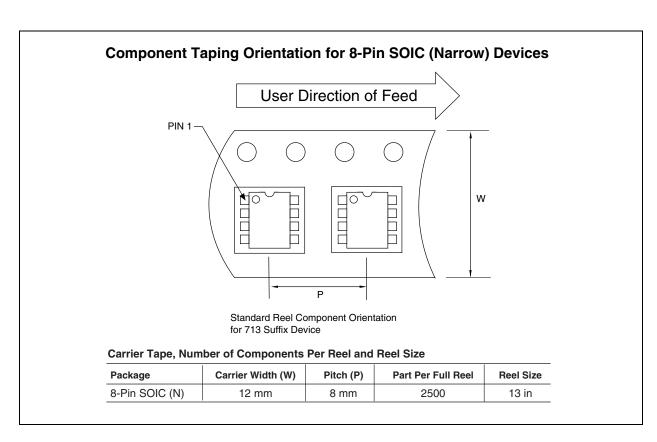
Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed. 010" (0.254mm) per side.

Drawing No. C04-111

<sup>\*</sup>Controlling Parameter § Significant Characteristic

#### 6.2 **Taping Form**





## 7.0 REVISION HISTORY

### **Revision D (December 2012)**

Added a note to each package outline drawing.

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**NOTES:** 

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