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Zero-voltage-switching resonant converter controller

Rev. 03 — 26 March 2007

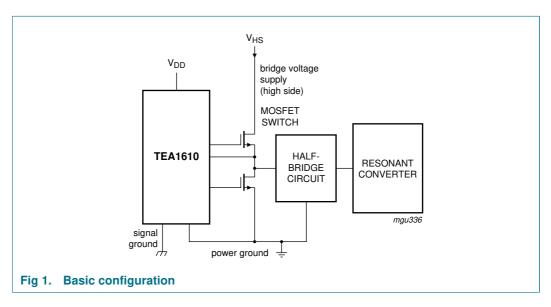
**Product data sheet** 

### 1. General description

The TEA1610 is a monolithic integrated circuit implemented in a high-voltage Diffusion Metal Oxide Semiconductor (DMOS) process. The circuit is a high voltage controller for a zero-voltage switching resonant converter. The IC provides the drive function for two discrete power MOSFETs in a half-bridge configuration. It also includes a level-shift circuit, an oscillator with accurately-programmable frequency range, a latched shut-down function and a transconductance error amplifier.

To guarantee an accurate 50 % switching duty factor, the oscillator signal passes through a divide-by-two flip-flop before being fed to the output drivers.

The circuit is very flexible and enables a broad range of applications for different mains voltages.



### 2. Features

- Integrated high voltage level-shift function
- Integrated high voltage bootstrap diode
- Low start-up current (green function)
- Adjustable dead time

- Transconductance error amplifier for ultra high-ohmic regulation feedback
- Latched shut-down circuit for overcurrent and overvoltage protection
- Adjustable minimum and maximum frequencies
- Undervoltage lockout



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### 3. Applications

TV and monitor power supplies

High voltage power supplies

### 4. Quick reference data

Table 1.	Quick reference data					
Symbol	Parameter	Conditions	Min	Тур	Max	Unit
V <sub>HS</sub>	high side driver voltage		0	-	600	V
I <sub>GH(source)</sub>	high side output source current	$V_{DD(F)} = 13 V;$ $V_{SH} = 0 V;$ $V_{GH} = 0 V$	-135	-180	-225	mA
I <sub>GL(source)</sub>	low side output source current	$V_{GL} = 0 V$	-135	-180	-225	mA
$I_{GH(sink)}$	high side output sink current		-	300	-	mA
I <sub>GL(sink)</sub>	low side output sink current	$V_{GL} = 14 V$	-	300	-	mA
f <sub>bridge(max)</sub>	maximum bridge frequency	$C_{F} = 100 \text{ pF};$ $I_{IFS} = 1 \text{ mA};$ $I_{IRS} = 200 \mu\text{A};$ $f_{bridge} = \frac{f_{OSC}}{2}$	[1] 450	500	550	kHz
V <sub>I(CM)</sub>	common mode input voltage		[2] _	-	2.5	V

[2] This parameter applies specifically to the error amplifier.

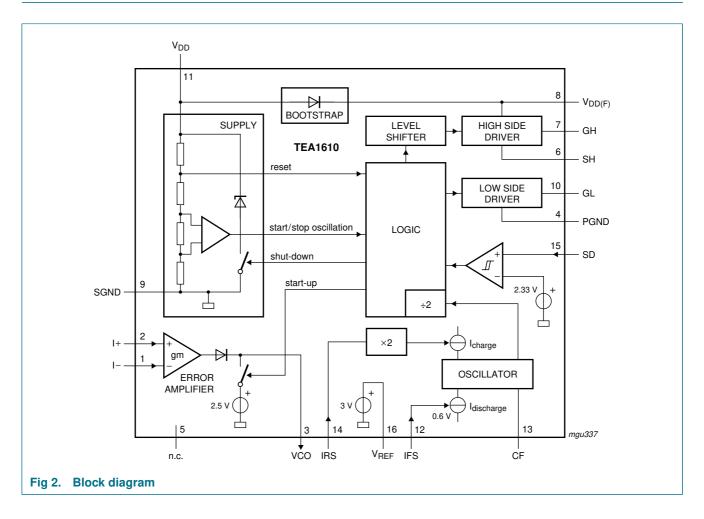
## 5. Ordering information

#### Table 2. Ordering information

Type number	Package	Package				
	Name	Description	Version			
TEA1610P	DIP16	plastic dual in-line package; 16 leads (300 mil); long body	SOT38-1			
TEA1610T	SO16	plastic small outline package; 16 leads; body width 3.9 mm; low stand-off height	SOT109-2			

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## 6. Block diagram



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## 7. Pinning information

### 7.1 Pinning

	]			_
	16 V <sub>REF</sub>	I- 1		16 V <sub>REF</sub>
I+ 2	15 SD	l+ 2		15 SD
VCO 3	14 IRS	VCO 3		14 IRS
PGND 4 TEA1610P	13 CF	PGND 4		13 CF
n.c. 5	12 IFS	n.c. 5	TEA1610T	12 IFS
SH 6	11 V <sub>DD</sub>	SH 6		11 V <sub>DD</sub>
GH 7	10 GL	GH 7		10 GL
V <sub>DD(F)</sub> 8	9 SGND	V <sub>DD(F)</sub> 8		9 SGND
001aaf866	1	L	001aaf867	7
Fig 3. Pin configuration for TEA1610P		Fig 4. Pin confi	guration for	TEA1610T

### 7.2 Pin description

Table 3.	Pin description	
Symbol	Pin	Description
I-	1	error amplifier inverting input
l+	2	error amplifier non-inverting input
VCO	3	error amplifier output
PGND	4	power ground
n.c.	5	not connected (high voltage spacer)
SH	6	high side switch source
GH	7	gate of the high side switch
$V_{\text{DD}(F)}$	8	floating supply voltage for the high side driver
SGND	9	signal ground
GL	10	gate of the low side switch
$V_{DD}$	11	supply voltage
IFS	12	oscillator discharge current input
CF	13	oscillator capacitor
IRS	14	oscillator charge current input
SD	15	shut-down input
V <sub>REF</sub>	16	reference voltage

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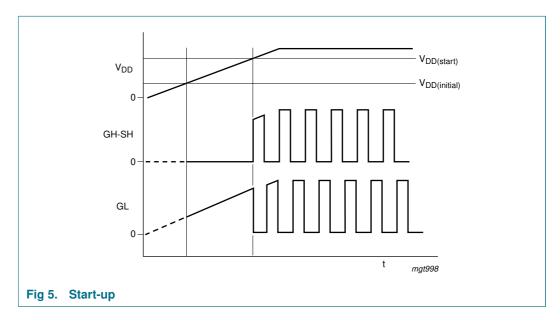
### 8. Functional description

#### 8.1 Start-up

When the applied voltage at  $V_{DD}$  reaches  $V_{DD(initial)}$  (see Figure 5), the low side power switch is turned-on while the high side power switch remains in the non-conducting state. This start-up output state guarantees the initial charging of the bootstrap capacitor ( $C_{boot}$ ) used for the floating supply of the high side driver.

During start-up, the voltage on the frequency capacitor (C<sub>f</sub>) is zero and defines the start-up state. The output voltage of the error amplifier is kept constant (typ. 2.5 V) and switching starts at about 80 % of the maximum frequency at the moment pin V<sub>DD</sub> reaches the start level.

The start-up state is maintained until  $V_{DD}$  reaches the start level (13.5 V), the oscillator is activated and the converter starts operating.

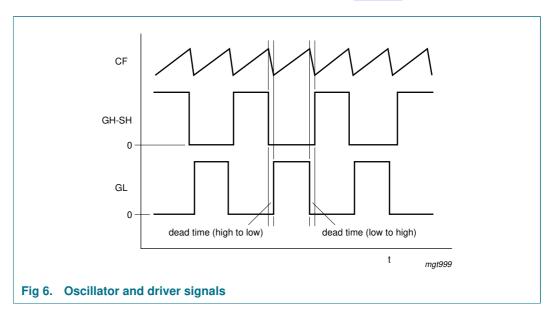


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#### 8.2 Oscillator

The internal oscillator is a current-controlled oscillator that generates a sawtooth output. The frequency of the sawtooth is determined by the external capacitor  $C_f$  and the currents flowing into the IFS and IRS pins.

The minimum frequency and the dead time are set by the capacitor  $C_f$  and resistors  $R_{f(min)}$  and  $R_{dt}$ . The maximum frequency is set by resistor  $R_{\Delta f}$  (see Figure 10). The oscillator frequency is exactly twice the bridge frequency to achieve an accurate 50 % duty factor. An overview of the oscillator and driver signals is given in Figure 6.



### 8.3 Dead time resistor

The dead time resistor  $R_{dt}$  is connected between the 3 V reference pin (V<sub>REF</sub>) and the IFS current input pin (see Figure 10). The voltage on the IFS pin is kept constant at a temperature independent value of 0.6 V. The current that flows into the IFS pin is determined by the value of resistor  $R_{dt}$  and the 2.4 V voltage drop across this resistor. The IFS input current equals the discharge current of capacitor  $C_f$  and determines the falling slope of the oscillator.

The falling slope time is used to create a dead time  $(t_{dt})$  between two successive switching actions of the half-bridge switches:

$$I_{IFS} = \frac{2.4V}{R_{dt}}$$
$$t_{dt} = \frac{C_f \times \Delta V_{Cf}}{I_{IFS}}$$
$$t_{IFS} = t_{dt}$$

#### 8.4 Minimum frequency resistor

The  $R_{f(min)}$  resistor is connected between the  $V_{REF}$  pin (3 V reference voltage) and the IRS current input (held at a temperature independent voltage level of 0.6 V). The charge current of the capacitor  $C_f$  is twice the current flowing into the IRS pin.

The  $R_{f(min)}$  resistor has a voltage drop of 2.4 V and its resistance defines the minimum charge current (rising slope) of the  $C_f$  capacitor if the control current is zero. The minimum frequency is defined by this minimum charge current ( $I_{IRS1}$ ) and the discharge current:

$$I_{IRS1} = \frac{2.4V}{R_{f(min)}}$$
$$t_{IRS1} = \frac{C_f \times \Delta V_{Cf}}{2 \times I_{IRS1}}$$
$$f_{osc(min)} = \frac{1}{t_{dt} + t_{IRS1}}$$

$$f_{bridge(min)} = \frac{f_{osc(min)}}{2}$$

#### 8.5 Maximum frequency resistor

The output voltage is regulated by changing the frequency of the half-bridge converter. The maximum frequency is determined by the  $R_{\Delta f}$  resistor which is connected between the error amplifier output VCO and the oscillator current input pin IRS. The current that flows through the  $R_{\Delta f}$  resistor ( $I_{IRS2}$ ) is added to the current flowing through the  $R_{f(min)}$  resistor. As a result, the charge current  $I_{CF}$  increases and the oscillation frequency increases. As the falling slope of the oscillator is constant, the relationship between the output frequency and the charge current is not a linear function (see Figure 7 and Figure 9):

$$I_{IRS2} = \frac{V_{VCO} - 0.6}{R_{\Delta f}}$$
$$t_{IRS2} = \frac{C_f \times \Delta V_{Cf}}{2 \times (I_{IRS1} + I_{IRS2})}$$

The maximum output voltage of the error amplifier and the value of  $R_{\Delta f}$  determine the maximum frequency:

$$I_{IRS2(max)} = \frac{V_{VCO(max)} - 0.6}{R_{\Delta f}}$$
$$t_{IRS(min)} = \frac{C_f \times \Delta V_{Cf}}{2 \times (I_{IRS2} + I_{IRS2(max)})}$$
$$f_{osc(max)} = \frac{1}{T_{OSC}}$$

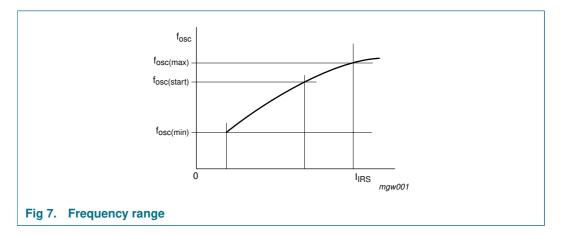
Zero-voltage-switching resonant converter controller

$$f_{bridge(max)} = \frac{f_{osc(max)}}{2}$$

$$T_{OSC} = t_{IRS(min)} + t_{IFS}$$

Bridge frequency accuracy is optimum in the low frequency region. At higher frequencies both the dead time and the oscillator frequency show a decay.

The frequency of the oscillator depends on the value of capacitor  $C_f$ , the peak-to-peak voltage swing  $V_{Cf}$  and the charge and discharge currents. However, at higher frequencies the accuracy decreases due to delays in the circuit.



### 8.6 Error amplifier

The error amplifier is a transconductance amplifier. Thus the output current at pin VCO is determined by the amplifier transconductance and the differential voltage on input pins I+ and I-. The output current  $I_{VCO}$  is fed to the IRS input of the current-controlled oscillator.

The source capability of the error amplifier increases current in the IRS pin when the differential input voltage is positive. Therefore the minimum current is determined by resistor  $R_{f(min)}$  and the minimum frequency setting is independent of the characteristics of the error amplifier.

The error amplifier has a maximum output current of 0.5 mA for an output voltage up to 2.5 V. If the source current decreases, the oscillator frequency also decreases resulting in a higher regulated output voltage.

During start-up, the output voltage of the amplifier is held at a constant value of 2.5 V. This voltage level defines, together with resistor  $R_{\Delta f}$ , the initial switching frequency of the TEA1610 after start-up.

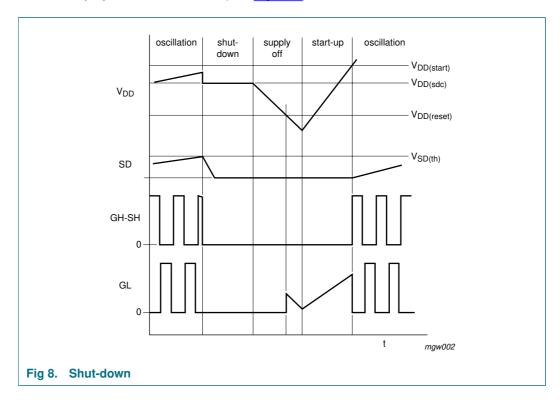
### 8.7 Shut-down

The shut-down input (SD) has an accurate threshold level of 2.33 V. When the voltage on input SD reaches 2.33 V, both power switches immediately switch off and the TEA1610 enters shut-down mode.

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During shut-down mode, pin  $V_{DD}$  is clamped by an internal Zener diode at 12.0 V with 1 mA input current. This clamp prevents  $V_{DD}$  rising above the rating of 14 V due to low supply current to the TEA1610 in shut-down mode.

When the TEA1610 is in the shut-down mode, it can be activated again only by lowering  $V_{DD}$  below the  $V_{DD(reset)}$  level (typically 5.3 V). The shut-down latch is then reset and a new start-up cycle can commence (see Figure 8).



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### 9. Limiting values

<b>Table 4.</b> In accordar	Limiting values ace with the Absolute Maximum Ra	ating System (IE	C 6(	)134).		
Symbol	Parameter	Conditions		Min	Max	Unit
Voltages						
V <sub>HS</sub>	high side driver voltage			0	600	V
V <sub>DD</sub>	supply voltage		<u>[1]</u>	0	15	V
$V_{I+}$	amplifier non-inverting input voltage			0	5	V
V <sub>I-</sub>	amplifier inverting input voltage			0	5	V
V <sub>SD</sub>	shut-down input voltage			0	5	V
Currents						
I <sub>IFS</sub>	oscillator falling slope input current			-	1	mA
I <sub>IRS</sub>	oscillator rising slope input current			-	1	mA
I <sub>REF</sub>	V <sub>REF</sub> source current			-	-2	mA
Power and	temperature					
P <sub>tot</sub>	total power dissipation	T <sub>amb</sub> < 70 °C		-	0.8	W
T <sub>amb</sub>	ambient temperature	operating		-25	+70	°C
T <sub>stg</sub>	storage temperature			-25	+150	°C
Handling						
V <sub>ESD</sub>	electrostatic discharge voltage		[2]	-	2000	V
			[3]	-	200	V

 It is recommended that a 100 nF capacitor be placed as close as possible to the V<sub>DD</sub> pin (as indicated in Figure 10, and in the application note).

[2] Human body model class 2: equivalent to discharging a 100 pF capacitor through a 1.5 k $\Omega$  series resistor.

[3] Machine model class 2: equivalent to discharging a 200 pF capacitor through a 0.75  $\mu H$  coil and 10  $\Omega$  resistor.

### **10. Thermal characteristics**

Table 5.	Thermal characteristics			
Symbol	Parameter	Conditions	Тур	Unit
R <sub>th(j-a)</sub>	thermal resistance from junction to ambient	in free air	100	K/W
$R_{th(j\text{-}pin)}$	thermal resistance from junction to pin		50	K/W

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## **11. Characteristics**

#### Table 6. Characteristics

All voltages are referred to the ground pins which must be connected externally; positive currents flow into the IC;  $V_{DD} = 13 V$  and  $T_{amb} = 25 \circ C$ ; tested using the circuit shown in Figure 10, unless otherwise specified.

Symbol	Parameter	Conditions	Min	Тур	Max	Unit
High voltag	ge pins V <sub>DD(F)</sub> , GH and	SH				
lL	leakage current	$V_{DD(F)}$ , $V_{GH}$ and $V_{SH}$ = 600 V	-	-	30	μA
Supply pin	V <sub>DD</sub>					
V <sub>DD(initial)</sub>	supply voltage for defined driver output	low side on; high side off	-	4	5	V
V <sub>DD(start)</sub>	start oscillator voltage		12.9	13.4	13.9	V
V <sub>DD(stop)</sub>	stop oscillator voltage		9.0	9.4	9.8	V
V <sub>DD(hys)</sub>	start-stop hysteresis voltage		3.8	4.0	4.2	V
V <sub>DD(sdc)</sub>	shut-down clamp voltage	low side off; high side off; I <sub>DD</sub> = 1 mA	11.0	12.0	13.0	V
V <sub>DD(reset)</sub>	reset voltage		4.5	5.3	6.0	V
I <sub>DD</sub>	supply current:	low side on; high side off $C_f = 100 \text{ pF}; I_{IFS} = 0.5 \text{ mA};$ $I_{IRS} = 50 \mu\text{A}; C_o = 200 \text{ pF}$ low side off; high side off; $V_{DD} = 9 \text{ V}$	<u>(1)</u>			
	start-up		130	180	220	μA
	operating		-	2.4	-	mA
	shut-down		-	130	180	μA
Reference	voltage on pin V <sub>REF</sub>					
V <sub>REF</sub>	reference voltage	I <sub>REF</sub> = 0 mA	2.9	3.0	3.1	V
REF	current capability	source only	-1.0	-	-	mA
Z <sub>o(VREF)</sub>	output impedance	I <sub>REF</sub> = –1 mA	-	5.0	-	Ω
$\frac{\Delta V_{REF}}{\Delta T}$	temperature coefficient	$I_{REF} = 0 \text{ mA}; T_j = 25 \text{ to } 150 ^\circ\text{C}$	-	-0.3	-	mV/K
Current co	ntrolled oscillator pins	IRS, IFS, CF				
CF(ch)(min)	minimum CF charge current	$I_{IRS}$ = 15 $\mu$ A; $V_{CF}$ = 2 V	28	30	32	μA
CF(ch)(max)	maximum CF charge current	$I_{IRS} = 200 \ \mu\text{A}; \ V_{CF} = 2 \ V$	340	380	420	μA
V <sub>IRS</sub>	voltage on pin IRS	$I_{IRS} = 200 \ \mu A$	570	600	630	mV
CF(dis)(min)	minimum CF discharge current	$I_{IRS}$ = 50 $\mu$ A; $V_{CF}$ = 2 V	47	50	53	μA
CF(dis)(max)	maximum CF discharge current	$I_{IFS} = 1 \text{ mA}; V_{CF} = 2 \text{ V}$	0.93	0.98	1.03	mA
V <sub>IFS</sub>	voltage on pin IFS	I <sub>IFS</sub> = 1 mA	570	600	630	mV
f <sub>bridge(min)</sub>	minimum bridge frequency (for stable operation)	$C_{F} = 100 \text{ pF}; I_{IFS} = 0.5 \text{ mA};$ $I_{IRS} = 50 \mu\text{A}; f_{bridge} = \frac{f_{OSC}}{2}$	188	200	212	kHz

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#### Table 6. Characteristics ...continued

All voltages are referred to the ground pins which must be connected externally; positive currents flow into the IC;  $V_{DD} = 13 V$  and  $T_{amb} = 25 \degree C$ ; tested using the circuit shown in Figure 10, unless otherwise specified.

Symbol	Parameter	Conditions	Min	Тур	Max	Unit
fbridge(max)	maximum bridge frequency	$C_{F} = 100 \text{ pF}; \text{ I}_{IFS} = 1 \text{ mA};$ $\text{I}_{IRS} = 200  \mu\text{A}; \text{ f}_{bridge} = \frac{f_{OSC}}{2}$	<u>[2]</u> 450	500	550	kHz
V <sub>CF(L)</sub>	CF trip level LOW	DC level	-	1.27	-	V
V <sub>CF(H)</sub>	CF trip level HIGH	DC level	-	3.0	-	V
V <sub>Cf(p-p)</sub>	C <sub>f</sub> voltage (peak-to-peak value)		1.63	1.73	1.83	V
t <sub>dt</sub>	dead time	$\label{eq:cf} \begin{split} C_f &= 100 \text{ pF}; \text{ I}_{IFS} = 0.5 \text{ mA}; \\ \text{ I}_{IRS} &= 50  \mu\text{A} \end{split}$	0.37	0.40	0.43	μs
Output dri	vers					
I <sub>GH(source)</sub>	high side output source current	$\label{eq:VDD(F)} \begin{array}{l} V_{DD(F)} = 13 \ V; \ V_{SH} = 0 \ V; \\ V_{GH} = 0 \ V \end{array}$	–135	-180	-225	mA
I <sub>GH(sink)</sub>	high side output sink current	$V_{DD(F)} = 13 \text{ V}; \text{ V}_{SH} = 0 \text{ V};$ $V_{GH} = 13 \text{ V}$	-	300	-	mA
I <sub>GL(source)</sub>	low side output source current	$V_{GL} = 0 V$	–135	-180	-225	mA
$I_{GL(sink)}$	low side output sink current	V <sub>GL</sub> = 14 V	-	300	-	mA
V <sub>GH(H)</sub>	high side output voltage HIGH	$\label{eq:VDD(F)} \begin{array}{l} V_{DD(F)} = 13 \text{ V};  V_{SH} = 0 \text{ V}; \\ I_{GH} = 10 \text{ mA} \end{array}$	10.8	12	-	V
V <sub>GH(L)</sub>	high side output voltage LOW	$\label{eq:VDD(F)} \begin{array}{l} V_{DD(F)} = 13 \ \text{V}; \ \text{V}_{SH} = 0 \ \text{V}; \\ I_{GH} = 10 \ \text{mA} \end{array}$	-	0.2	0.5	V
V <sub>GL(H)</sub>	low side output voltage HIGH	I <sub>GL</sub> = 10 mA	10.8	12	-	V
V <sub>GL(L)</sub>	low side output voltage LOW	I <sub>GL</sub> = 10 mA	-	0.2	0.5	V
V <sub>d(boot)</sub>	bootstrap diode voltage drop	I = 5 mA	1.5	1.8	2.1	V
Shut-dowr	input pin SD					
I <sub>SD</sub>	input current	V <sub>SD</sub> = 2.33 V	0	0.2	0.5	μA
V <sub>SD(th)</sub>	threshold level		2.26	2.33	2.40	V
Error ampl	ifier pins I+, I-, VCO					
I <sub>I(CM)</sub>	common mode input current	$V_{I(CM)} = 1 V$	-	-0.1	-0.5	μA
V <sub>I(CM)</sub>	common mode input voltage		-	-	2.5	V
V <sub>I(offset)</sub>	input offset voltage	$V_{I(CM)} = 1 V; I_{VCO} = -10 mA$	-2	0	+2	mV
9 <sub>m</sub>	transconductance	$V_{I(CM)} = 1$ V; source only	-	330	-	μ <b>A</b> /mV
A <sub>o</sub>	open loop gain	$V_{I(CM)} = 1 V$	<u>[3]</u> _	70	-	dB
GB	gain bandwidth product	$V_{I(CM)} = 1 V$	<u>[3]</u> _	5	-	MHz

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#### Table 6. Characteristics ...continued

All voltages are referred to the ground pins which must be connected externally; positive currents flow into the IC;  $V_{DD} = 13 V$  and  $T_{amb} = 25 °C$ ; tested using the circuit shown in Figure 10, unless otherwise specified.

Symbol	Parameter	Conditions	Min	Тур	Max	Unit
V <sub>VCO(max)</sub>	maximum VCO voltage	operating	<u>3</u> 3.2	3.6	4.0	V
I <sub>VCO(max)</sub>	maximum output current	operating; $V_{VCO} = 1 V$	-0.4	-0.5	-0.6	mA
V <sub>VCO(start)</sub>	start VCO voltage	$I_{VCO} = 0.3 \text{ mA}$	2.3	2.5	2.7	V

[1] The supply current I<sub>DD</sub> increases with increasing bridge frequency to drive the capacitive load of two MOSFETs. Typical MOSFETs for the TEA1610 application are 8N50 (NXP type PHX80N50E, Q<sub>g(tot)</sub> = 55 nC typ.) and these will increase the supply current at 150 kHz according to the following formula:

 $\Delta I_{DD} = 2 \times Q_{g(tot)} \times f_{bridge} = 2 \times 55nC \times 150kHz = 16.5mA$ 

[2] The frequency of the oscillator depends on the value of capacitor C<sub>f</sub>, the peak-to-peak voltage swing V<sub>CF</sub>, and the charge/discharge currents I<sub>CF(ch)</sub> and I<sub>CF(dis)</sub>.

[3] This parameter is tested with a resistor of 10 k $\Omega$  connected from pin VCO to GND.

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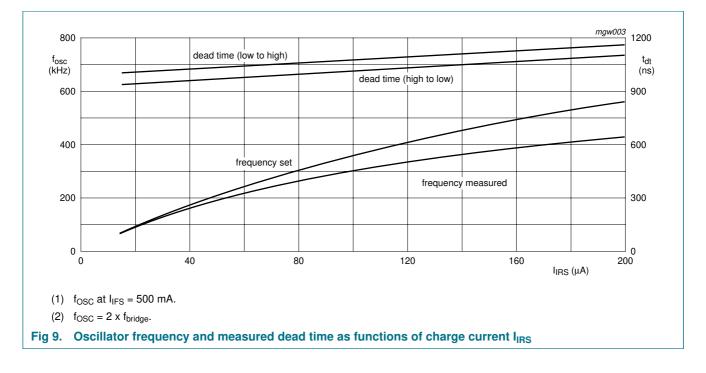
### **12. Application information**

An application example of a zero-voltage switching resonant converter application using TEA1610 is shown in Figure 10. In the off-mode the V<sub>DD</sub> voltage is pulled below the stop level of 9.4 V by the 7.5 V Zener diode and the half-bridge is not driven. In the on-mode the TEA1610 starts-up with a high-ohmic bleeder resistor. After passing the level for start of oscillation, the TEA1610 is in normal operating mode and consumes the normal supply current delivered by the 12 V supply. The dead time is set by R<sub>dt</sub> and C<sub>f</sub>. The minimum frequency is adjusted by R<sub>f(min)</sub> and the frequency range is set by R<sub> $\Delta f$ </sub>. The output voltage is adjusted with a potentiometer connected to the inverting input of the error amplifier and is regulated via a feedback circuit. The shut-down input is used for overvoltage protection. To prevent interference, filter capacitors can be added on pins IFS, IRS and V<sub>REF</sub>. The maximum value of each filter capacitor is 100 pF.

Practical values of the application example are given in Figure 9, in which the measured oscillator frequency with capacitor  $C_f = 220 \text{ pF}$  is shown as a function of the charge current  $I_{IRS}$ . Note that the slope of the measured frequency differs from the theoretical frequency (frequency set) calculated as described in <u>Section 8.5 "Maximum frequency resistor"</u>.

The measured dead time is directly related to the charge current (total current flowing into pin IRS) and therefore to the oscillator frequency.

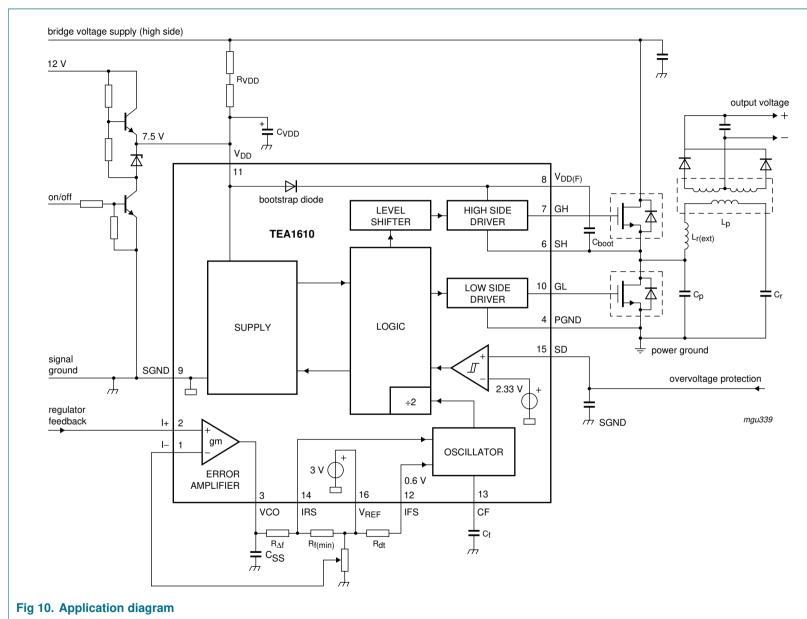
The measured frequency graph can be used to determine the required  $R_{\Delta f}$  resistor for a certain maximum frequency in an application with the same value of capacitor  $C_f$ .



More application information can be found in application note AN99011.



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### **13. Test information**

### 13.1 Quality information

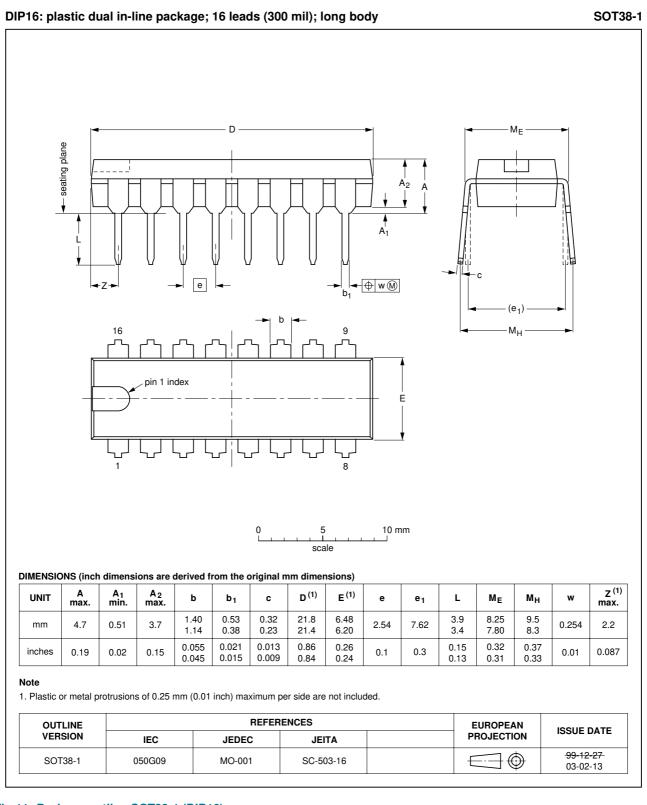
The General Quality Specification for Integrated Circuits, SNW-FQ-611 is applicable.

#### **NXP Semiconductors**

## **TEA1610P; TEA1610T**

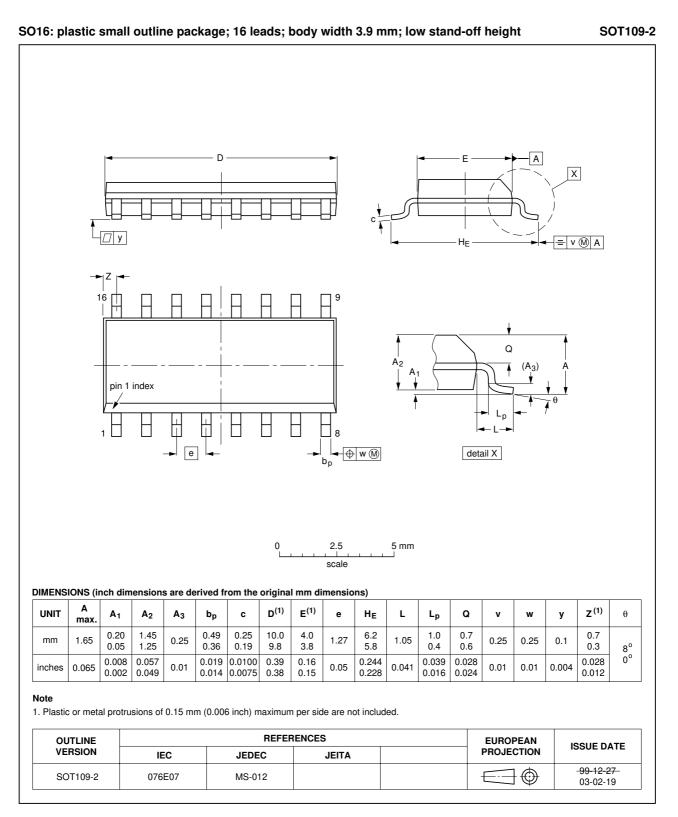
Zero-voltage-switching resonant converter controller

### 14. Package outline



#### Fig 11. Package outline SOT38-1 (DIP16)

Zero-voltage-switching resonant converter controller



#### Fig 12. Package outline SOT109-2 (SO16)

Zero-voltage-switching resonant converter controller

## 15. Revision history

Table 7. Revision	history			
Document ID	Release date	Data sheet status	Change notice	Supersedes
TEA1610T_P_3	20070326	Product data sheet	-	TEA1610T_P_2
Modifications:	<ul> <li>In Table 4 "L</li> </ul>	<u>imiting values"</u> , maximum	value for V <sub>DD</sub> changed f	rom 14 V to 15 V.
TEA1610T_P_2	20070206	Product data sheet	-	TEA1610T_P_1
Modifications:		of this data sheet has beer f NXP Semiconductors.	redesigned to comply v	vith the new identity
	<ul> <li>Legal texts</li> </ul>	have been adapted to the r	new company name whe	ere appropriate.
	<ul> <li>Equations n frequency re</li> </ul>		imum frequency resistor	and <u>Section 8.5 "Maximum</u>
TEA1610T_P_1	20010425	Product specification	-	-

Zero-voltage-switching resonant converter controller

## 16. Legal information

### 16.1 Data sheet status

Document status <sup>[1][2]</sup>	Product status <sup>[3]</sup>	Definition
Objective [short] data sheet	Development	This document contains data from the objective specification for product development.
Preliminary [short] data sheet	Qualification	This document contains data from the preliminary specification.
Product [short] data sheet	Production	This document contains the product specification.

[1] Please consult the most recently issued document before initiating or completing a design.

[2] The term 'short data sheet' is explained in section "Definitions".

[3] The product status of device(s) described in this document may have changed since this document was published and may differ in case of multiple devices. The latest product status information is available on the Internet at URL http://www.nxp.com.

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Zero-voltage-switching resonant converter controller

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