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TLD5190

H-Bridge DC/DC Controller
Infineon® LITIX™ Power



| | | |
|-------------------|---------------|--------------|
| Package | PG-VQFN-48-31 | PG-TQFP-48-9 |
| Marking | TLD5190QV | TLD5190QU |
| Sales Name | TLD5190QV | TLD5190QU |

1 Overview

Features

- Single Inductor high power Buck-Boost controller
- Wide LED forward voltage Range (2 V up to 55 V)
- Wide VIN Range (IC 4.5 V to 40 V, Power 4.5 V to 55 V)
- Switching Frequency Range from 200 kHz to 700 kHz
- Maximum Efficiency in every condition (up to 96%)
- Constant Current (LED) and Constant Voltage Regulation
- EMC optimized device: Features an auto Spread Spectrum
- Open Load, Overvoltages, Shorted LED fault and Overtemperature Diagnostic Outputs
- LED and Input current sense with dedicated monitor Outputs
- Advanced protection features for device and load
- Enhanced Dimming features: Analog and PWM dimming
- LED current accuracy +/- 3%
- Available in a small thermally enhanced PG-VQFN-48-31 or PG-TQFP-48-9 package
- Automotive AEC Qualified

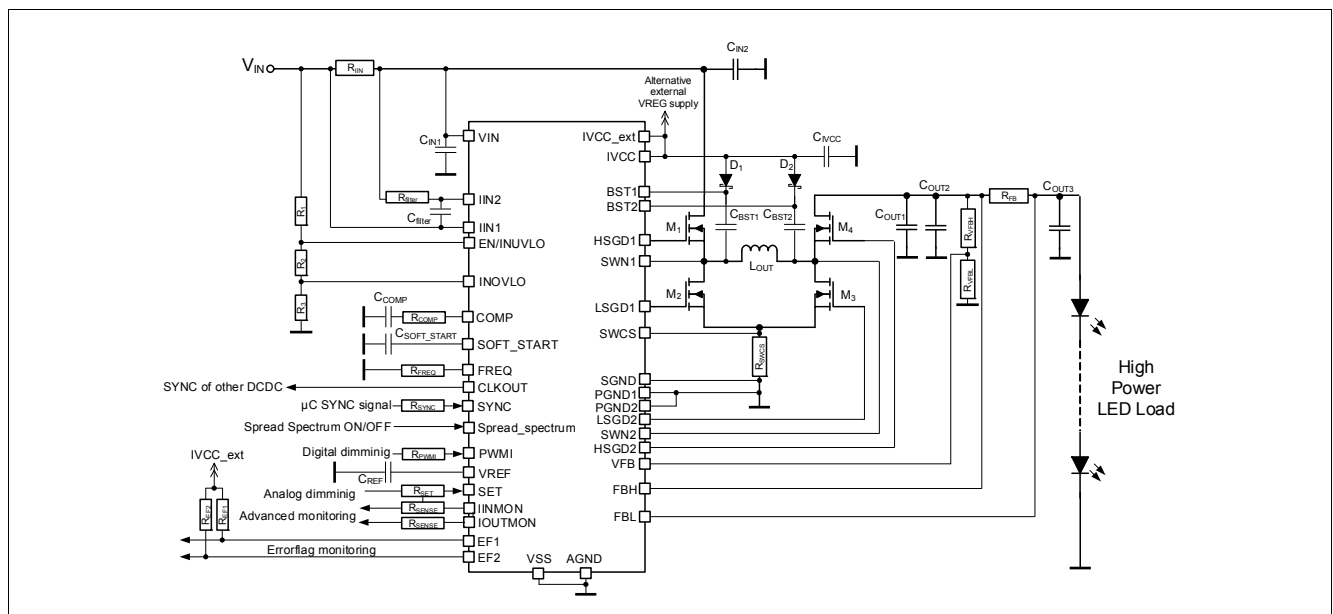
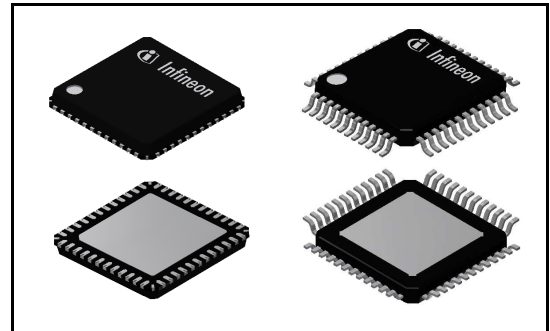


Figure 1 Application Drawing - TLD5190 as current regulator

Overview

Description

The TLD5190 is a synchronous MOSFET H-Bridge DC/DC controller with built in protection features. This concept is beneficial for driving high power LEDs with maximum system efficiency and minimum number of external components. The TLD5190 offers both analog and digital (PWM) dimming. The switching frequency is adjustable in the range of 200 kHz to 700 kHz. It can be synchronized to an external clock source. A built in Spread Spectrum switching frequency modulation and the forced continuous current regulation mode improve the overall EMC behavior. Furthermore the current mode regulation scheme provides a stable regulation loop maintained by small external compensation components. The adjustable soft start feature limits the current peak as well as voltage overshoot at start-up. The TLD5190 is suitable for use in the harsh automotive environment.

Table 1 Product Summary

| | | |
|--|------------------|--|
| Power Stage input voltage range | V_{POW} | 4.5 V ... 55 V |
| Device Input supply voltage range | V_{VIN} | 4.5 V ... 40 V |
| Maximum output voltage (depending by the application conditions) | $V_{OUT(max)}$ | 55 V as LED Driver Boost Mode 50 V as LED Driver Buck Mode 50 V as Voltage regulator |
| Switching Frequency range | f_{SW} | 200 kHz... 700 kHz |
| Typical NMOS driver on-state resistance at $T_j = 25^\circ\text{C}$ (Gate Pull Up) | $R_{DS(ON_PU)}$ | 2.3 Ω |
| Typical NMOS driver on-state resistance at $T_j = 25^\circ\text{C}$ (Gate Pull Down) | $R_{DS(ON_PD)}$ | 1.2 Ω |

Protective Functions

- Over load protection of external MOSFETs
- Shorted load, open load, output overvoltage protection
- Input overvoltage and undervoltage protection
- Thermal shutdown of device with autorestart behavior
- Electrostatic discharge protection (ESD)

Diagnostic Functions

- Diagnostic information via Error Flags
- Open load detection in ON-state
- Device Overtemperature shutdown
- Advanced diagnostic functions provide I_{LED} and I_{IN} information

Applications

- Especially designed for driving high power LEDs in automotive applications
- Automotive Exterior Lighting: full LED headlamp assemblies (Low Beam, High Beam, Matrix Beam, Pixel Light)
- General purpose current/voltage controlled DC/DC LED driver

Block Diagram

2 Block Diagram

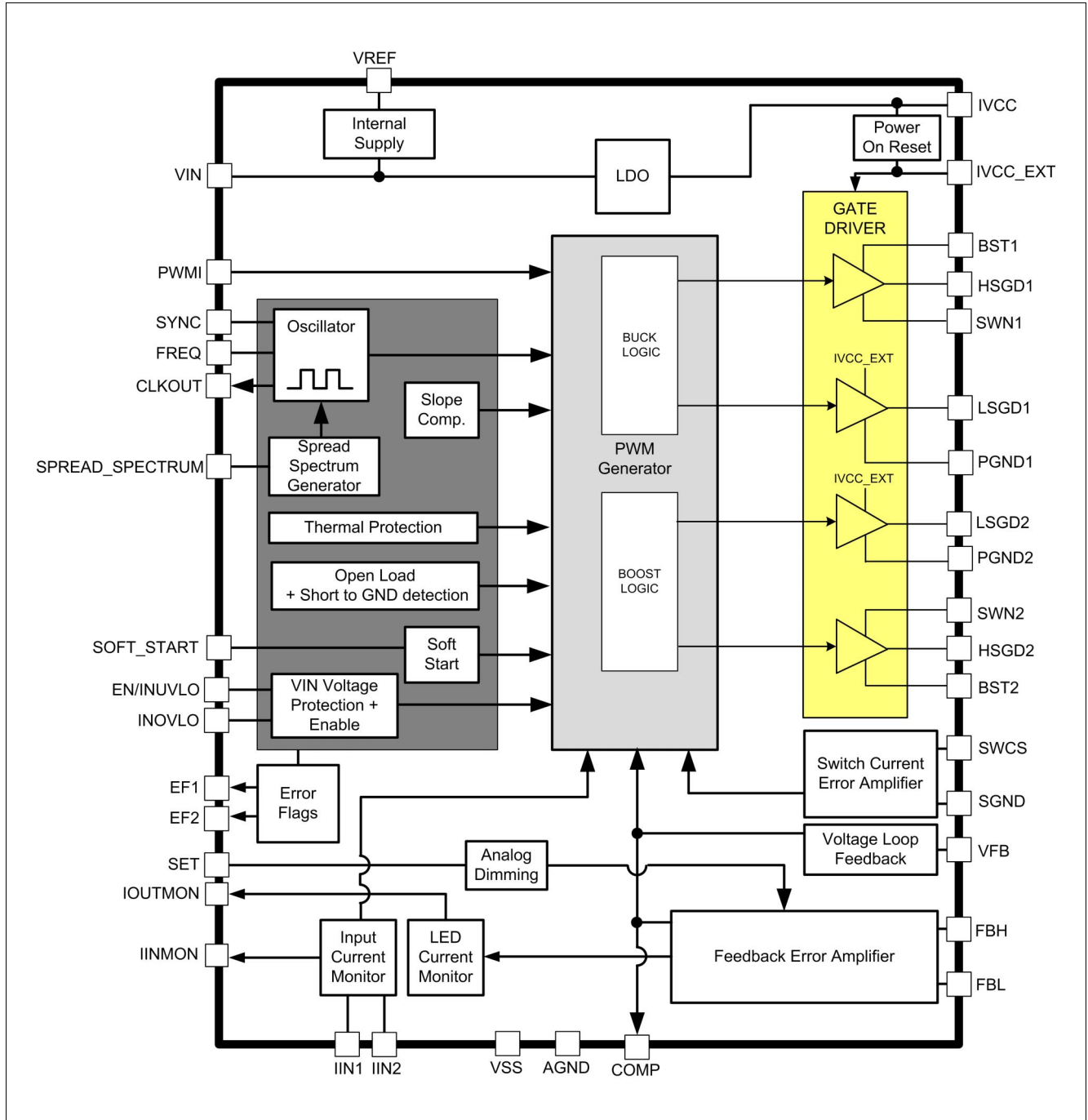


Figure 2 Block Diagram - TLD5190

Pin Configuration

3 Pin Configuration

3.1 Pin Assignment

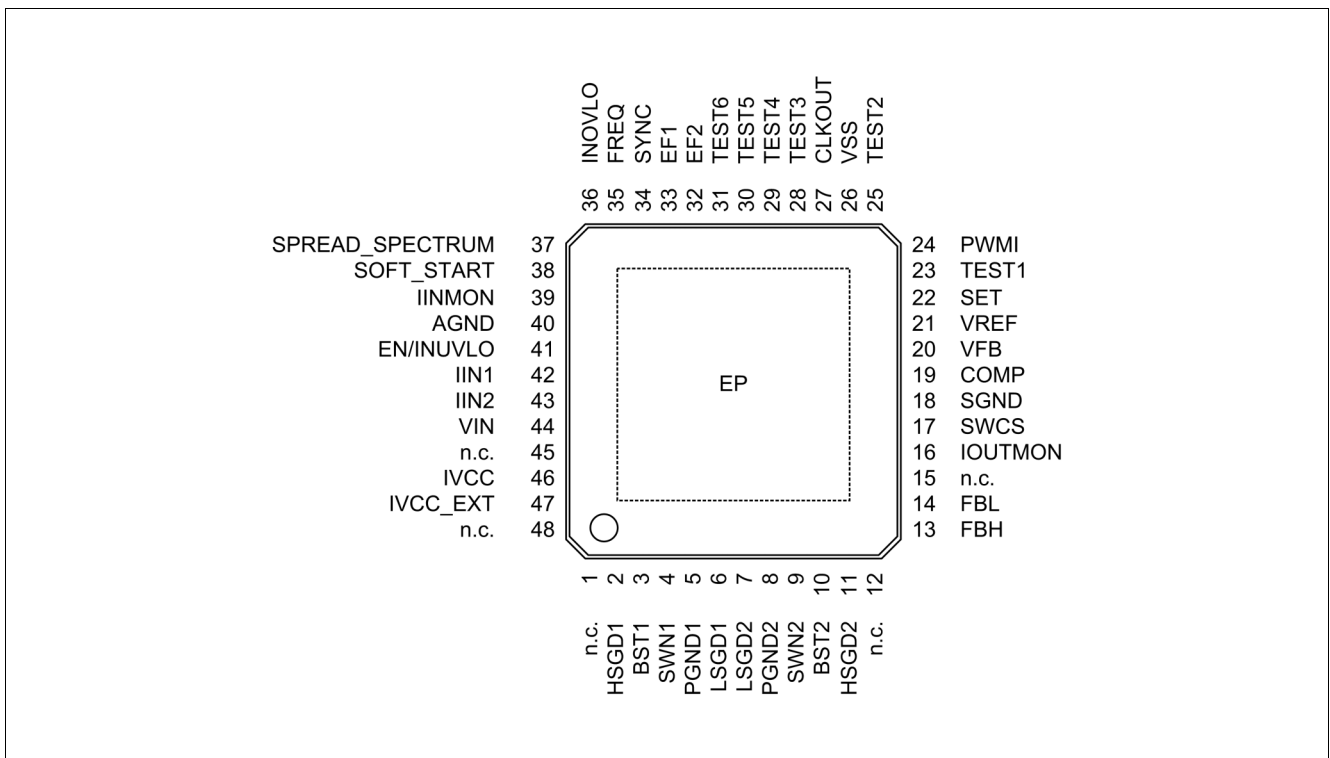


Figure 3 Pin Configuration - TLD5190

Pin Configuration

3.2 Pin Definitions and Functions

| Pin | Symbol | I/O ¹⁾ | | Function |
|---------------------------|----------|-------------------|----|--|
| Power Supply | | | | |
| 1, 12, 15, 45, 48 | n.c. | - | | Not connected, tie to AGND on the Layout; |
| 44 | VIN | - | | Power Supply Voltage; Supply for internal biasing. |
| 47 | IVCC_EXT | I | PD | External LDO input; Input to alternatively supply internal Gate Drivers via an external LDO. Connect to IVCC pin to use internal LDO to supply gate drivers. Must not be left open. |
| 5, 8 | PGND1, 2 | - | | Power Ground; Ground for power potential. Connect externally close to the chip. |
| 26 | VSS | - | | Digital GPIO Ground; Ground for GPIO pins. |
| 40 | AGND | - | | Analog Ground; Ground Reference |
| - | EP | - | | Exposed Pad; Connect to external heatspreading Cu area (e.g. inner GND layer of multilayer PCB with thermal vias). |
| Gate Driver Stages | | | | |
| 2 | HSGD1 | O | | Highside Gate Driver Output 1; Drives the top n-channel MOSFET with a voltage equal to V_{IVCC_EXT} superimposed on the switch node voltage SWN1. Connect to gate of external switching MOSFET. |
| 11 | HSGD2 | O | | Highside Gate Driver Output 2; Drives the top n-channel MOSFET with a voltage equal to V_{IVCC_EXT} superimposed on the switch node voltage SWN2. Connect to gate of external switching MOSFET. |
| 6 | LSGD1 | O | | Lowside Gate Driver Output 1; Drives the lowside n-channel MOSFET between GND and V_{IVCC_EXT} . Connect to gate of external switching MOSFET. |
| 7 | LSGD2 | O | | Lowside Gate Driver Output 2; Drives the lowside n-channel MOSFET between GND and V_{IVCC_EXT} . Connect to gate of external switching MOSFET. |
| 4 | SWN1 | IO | | Switch Node 1; SWN1 pin swings from a diode voltage drop below ground up to V_{IN} . |
| 9 | SWN2 | IO | | Switch Node 2; SWN2 pin swings from ground up to a diode voltage drop above V_{OUT} . |
| 46 | IVCC | O | | Internal LDO output; Used for internal biasing and gate driver supply. Bypass with external capacitor close to the pin. Pin must not be left open. |

Pin Configuration

| Pin | Symbol | I/O ¹⁾ | | Function |
|---------------------------|-----------|-------------------|----|--|
| Inputs and Outputs | | | | |
| 23 | TEST1 | - | | Test Pin; Used for Infineon end of line test, connect to GND in application. |
| 25 | TEST2 | - | | Test Pin; Used for Infineon end of line test, connect to GND in application. |
| 28 | TEST3 | - | | Test Pin; Used for Infineon end of line test, connect to GND in application. |
| 29 | TEST4 | - | | Test Pin; Used for Infineon end of line test, connect to GND in application. |
| 30 | TEST5 | - | | Test Pin; Used for Infineon end of line test, connect to GND in application. |
| 31 | TEST6 | - | | Test Pin; Used for Infineon end of line test, connect to GND in application. |
| 41 | EN/INUVLO | I | PD | Enable/Input Under Voltage Lock Out; Used to put the device in a low current consumption mode, with additional capability to fix an undervoltage threshold via external components. Pin must not be left open. |
| 35 | FREQ | I | | Frequency Select Input; Connect external resistor to GND to set frequency. |
| 34 | SYNC | I | PD | Synchronization Input; Apply external clock signal for synchronization. |
| 24 | PWMI | I | PD | Control Input; Digital input 5 V or 3.3 V. |
| 13 | FBH | I | | Output current Feedback Positive; Non inverting Input (+). |
| 14 | FBL | I | | Output current Feedback Negative; Inverting Input (-). |
| 3 | BST1 | IO | | Bootstrap capacitor; Used for internal biasing and to drive the Highside Switch HSGD1. Bypass to SWN1 with external capacitor close to the pin. Pin must not be left open. |
| 10 | BST2 | IO | | Bootstrap capacitor; Used for internal biasing and to drive the Highside Switch HSGD2. Bypass to SWN2 with external capacitor close to the pin. Pin must not be left open. |
| 17 | SWCS | I | | Current Sense Input; Inductor current measurement - Non Inverting Input (+). |
| 18 | SGND | I | | Current Sense Ground; Inductor current sense - Inverting Input (-). Route as Differential net with SWCS on the Layout. |
| 42 | IIN1 | I | | Input Current Monitor Positive; Non Inverting Input (+), connect to VIN if input current monitor is not needed. |
| 43 | IIN2 | I | | Input Current Monitor Negative; Inverting Input (-), connect to VIN if input current monitor is not needed. |

Pin Configuration

| Pin | Symbol | I/O ¹⁾ | | Function |
|-----|-----------------|-------------------|----|---|
| 19 | COMP | O | | Compensation Network Pin; Connect R and C network to pin for stability phase margin adjustment. |
| 38 | SOFT_START | O | | Softstart configuration Pin; Connect a capacitor C_{SOFT_START} to GND to fix a soft start ramp default time. |
| 36 | INOVLO | I | | Input Overvoltage Protection Pin; Define an upper voltage threshold and switches OFF the device in case of overvoltages on the VIN supply. Must not be left open. |
| 20 | VFB | I | | Voltage Loop Feedback Pin; VFB is intended to set output protection functions. |
| 22 | SET | I | | Analog current sense adjustment Pin; A voltage V_{SET} between 0.2 V and 1.5 V will adjust the I_{LED} or V_{OUT} in a linear relation. |
| 37 | SPREAD_SPECTRUM | I | PD | Spread Spectrum Pin; This pin is enabling and disabling the SPREAD SPECTRUM function. This feature is beneficial to improve the EMC performance. |
| 39 | IINMON | O | | Input current monitor output; Monitor pin that produces a voltage that is 20 times the voltage $V_{IN1-IN2}$. IINMON will be equal 1 V when $V_{IN1}-V_{IN2} = 50$ mV. |
| 16 | IOUTMON | O | | Output current monitor output; Monitor pin that produces a voltage that is 200 mV + 8 times the voltage $V_{FBH-FBL}$. IOUTMON will be equal 1.4 V when $V_{FBH-FBL} = 150$ mV. |
| 21 | VREF | O | PD | Voltage Reference Output Pin; Supplies an accurate 2 V output voltage for standalone analog dimming and LED temperature compensation via external resistors. Bypass with an external 100nF capacitor close to the pin. Pin must not be left open. |

Logic Outputs

| | | | | |
|----|--------|---|--|---|
| 27 | CLKOUT | O | | Clock Output Pin; Switching Oscillator output signal to supply additional SYNC Inputs of other DCDC devices (beneficial for standalone operations without μ C). |
| 33 | EF1 | O | | Error Flag 1; An open drain output which is pulled to LOW when an output Short to GND or Overtemperature occurs. |
| 32 | EF2 | O | | Error Flag 2; An open drain output which is pulled to LOW when an OPEN load, Overvoltages or Overtemperature occurs. |

1) O: Output, I: Input,
PD: pull-down circuit integrated,
PU: pull-up circuit integrated

General Product Characteristics

4 General Product Characteristics

4.1 Absolute Maximum Ratings

Table 2 Absolute Maximum Ratings¹⁾
 $T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$; all voltages with respect to AGND, (unless otherwise specified)

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|--|---------------------------|--------|------|------|------|------------------------|----------|
| | | Min. | Typ. | Max. | | | |
| Supply Voltages | | | | | | | |
| VIN Supply Input | V_{VIN} | -0.3 | - | 60 | V | - | P_4.1.1 |
| IVCC Internal Linear Voltage Regulator Output voltage | V_{IVCC} | -0.3 | - | 6 | V | - | P_4.1.3 |
| IVCC_EXT External Linear Voltage Regulator Input voltage | V_{IVCC_EXT} | -0.3 | - | 6 | V | - | P_4.1.4 |
| VREF Voltage reference output | V_{REF} | -0.3 | - | 3.6 | V | - | P_4.1.5 |
| Gate Driver Stages | | | | | | | |
| LSGD1,2 - PGND1,2 Lowside Gatedriver voltage | $V_{LSGD1,2-}$ PGND1,2 | -0.3 | - | 5.5 | V | - | P_4.1.54 |
| HSGD1,2 - SWN1,2 Highside Gatedriver voltage | $V_{HSGD1,2-}$ SWN1,2 | -0.3 | - | 5.5 | V | - | P_4.1.55 |
| SWN1, SWN2 switching node voltage | $V_{SWN1,2}$ | -1 | - | 60 | V | - | P_4.1.6 |
| (BST1-SWN1), (BST2-SWN2) Bootstrap voltage | $V_{BST1,2-}$ SWN1,2 | -0.3 | - | 6 | V | - | P_4.1.7 |
| BST1, BST2 Bootstrap voltage related to GND | $V_{BST1,2}$ | -0.3 | - | 65 | V | - | P_4.1.8 |
| SWCS Switch Current Sense Input voltage | V_{SWCS} | -0.3 | - | 0.3 | V | - | P_4.1.9 |
| SGND Switch Current Sense GND voltage | V_{SGND} | -0.3 | - | 0.3 | V | - | P_4.1.10 |
| SWCS-SGND Switch Current Sense differential voltage | V_{SWCS-} SGND | -0.5 | - | 0.5 | V | - | P_4.1.11 |
| PGND1,2 Power GND voltage | $V_{PGND1,2}$ | -0.3 | - | 0.3 | V | - | P_4.1.28 |
| High voltage Pins | | | | | | | |
| IIN1, IIN2 Input Current monitor voltage | $V_{IIN1,2}$ | -0.3 | - | 60 | V | - | P_4.1.12 |

General Product Characteristics

Table 2 Absolute Maximum Ratings¹⁾ (cont'd)
 $T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$; all voltages with respect to AGND, (unless otherwise specified)

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|--|-----------------|--------|------|------|------|------------------------|----------|
| | | Min. | Typ. | Max. | | | |
| IIN1-IIN2 Input Current monitor differential voltage | $V_{IIN1-IIN2}$ | -0.5 | - | 0.5 | V | - | P_4.1.13 |
| FBH, FBL Feedback Error Amplifier voltage | $V_{FBH, FBL}$ | -0.3 | - | 60 | V | - | P_4.1.14 |
| FBH-FBL Feedback Error Amplifier differential voltage | $V_{FBH-FBL}$ | -0.5 | - | 0.5 | V | - | P_4.1.15 |
| EN/INUVLO Device enable/input undervoltage lockout | $V_{EN/INUVLO}$ | -0.3 | - | 60 | V | - | P_4.1.16 |

Digital (I/O) Pins

| | | | | | | | |
|--|------------------------|------|---|-----|---|---|----------|
| PWMI Digital Input voltage | V_{PWMI} | -0.3 | - | 5.5 | V | - | P_4.1.17 |
| SYNC Synchronization Input voltage | V_{SYNC} | -0.3 | - | 5.5 | V | - | P_4.1.22 |
| CLKOUT Clock Output voltage | V_{CLKOUT} | -0.3 | - | 5.5 | V | - | P_4.1.23 |
| SPREAD_SPECTRUM Spread Spectrum Input voltage | $V_{SPREAD_SPECTRUM}$ | -0.3 | - | 5.5 | V | - | P_4.1.24 |

Analog Pins

| | | | | | | | |
|--|-------------------|------|---|-----|---|---|----------|
| VFB Loop Input voltage | V_{VFB} | -0.3 | - | 5.5 | V | - | P_4.1.25 |
| INOVLO Input overvoltage lockout | V_{INOVLO} | -0.3 | - | 5.5 | V | - | P_4.1.26 |
| EF1, 2 Error Flags output voltage | $V_{EF1,2}$ | -0.3 | - | 5.5 | V | - | P_4.1.27 |
| SET Analog dimming Input voltage | V_{SET} | -0.3 | - | 5.5 | V | - | P_4.1.29 |
| COMP Compensation Input voltage | V_{COMP} | -0.3 | - | 3.6 | V | - | P_4.1.30 |
| SOFT_START Softstart Voltage | V_{SOFT_START} | -0.3 | - | 3.6 | V | - | P_4.1.31 |
| FREQ Voltage at frequency selection pin | V_{FREQ} | -0.3 | - | 3.6 | V | - | P_4.1.32 |
| IINMON Voltage at input monitor pin | V_{IINMON} | -0.3 | - | 3.6 | V | - | P_4.1.33 |
| IOUTMON Voltage at output monitor pin | $V_{IOUTMON}$ | -0.3 | - | 5.5 | V | - | P_4.1.34 |

Temperatures

General Product Characteristics

Table 2 Absolute Maximum Ratings¹⁾ (cont'd)
 $T_j = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$; all voltages with respect to AGND, (unless otherwise specified)

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|---------------------------------------|------------------------------|--------|------|------|--------------------|------------------------|----------|
| | | Min. | Typ. | Max. | | | |
| Junction Temperature | T_j | -40 | – | 150 | $^{\circ}\text{C}$ | – | P_4.1.35 |
| Storage Temperature | T_{stg} | -55 | – | 150 | $^{\circ}\text{C}$ | – | P_4.1.36 |
| ESD Susceptibility | | | | | | | |
| ESD Resistivity of all Pins | $V_{\text{ESD,HBM}}$ | -2 | – | 2 | kV | HBM ²⁾ | P_4.1.37 |
| ESD Resistivity to GND | $V_{\text{ESD,CDM}}$ | -500 | – | 500 | V | CDM ³⁾ | P_4.1.38 |
| ESD Resistivity of corner Pins to GND | $V_{\text{ESD,CDM_corner}}$ | -750 | – | 750 | V | CDM ³⁾ | P_4.1.39 |

- 1) Not subject to production test, specified by design.
- 2) ESD susceptibility, HBM according to ANSI/ESDA/JEDEC JS001 (1.5 kV, 100 pF)
- 3) ESD susceptibility, Charged Device Model “CDM” ESDA STM5.3.1 or ANSI/ESD S.5.3.1

Note: Stresses above the ones listed here may cause permanent damage to the device. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Integrated protection functions are designed to prevent IC destruction under fault conditions described in the datasheet. Fault conditions are considered as “outside” normal operating range. Protection functions are not designed for continuous repetitive operation.

4.2 Functional Range

Table 3 Functional Range

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|--------------------------------------|------------------|--------|------|------|--------------------|------------------------|---------|
| | | Min. | Typ. | Max. | | | |
| Device Extended Supply Voltage Range | V_{VIN} | 4.5 | – | 40 | V | 1) | P_4.2.1 |
| Device Nominal Supply Voltage Range | V_{VIN} | 8 | – | 36 | V | – | P_4.2.2 |
| Power Stage Voltage Range | V_{POW} | 4.5 | – | 55 | V | 1) | P_4.2.5 |
| Junction Temperature | T_j | -40 | – | 150 | $^{\circ}\text{C}$ | – | P_4.2.4 |

- 1) Not subject to production test, specified by design.

Note: Within the functional range the IC operates as described in the circuit description. The electrical characteristics are specified within the conditions given in the related electrical characteristics table.

4.3 Thermal Resistance

Note: This thermal data was generated in accordance with JEDEC JESD51 standards. For more information, go to www.jedec.org.

General Product Characteristics

Table 4

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|---------------------|------------|--------|------|------|------|------------------------|---------|
| | | Min. | Typ. | Max. | | | |
| Junction to Case | R_{thJC} | – | 0.9 | – | K/W | ^{1) 2)} | P_4.3.1 |
| Junction to Ambient | R_{thJA} | – | 25 | – | K/W | ³⁾ 2s2p | P_4.3.2 |

- 1) Not subject to production test, specified by design.
- 2) Specified R_{thJC} value is simulated at natural convection on a cold plate setup (all pins and the exposed pad are fixed to ambient temperature). $T_a = 25^\circ\text{C}$; The IC is dissipating 1 W.
- 3) Specified R_{thJA} value is according to JEDEC 2s2p (JESD 51-7) + (JESD 51-5) and JEDEC 1s0p (JESD 51-3) + heatsink area at natural convection on FR4 board; The device was simulated on a 76.2 x 114.3 x 1.5 mm board. The 2s2p board has 2 outer copper layers (2 x 70 μm Cu) and 2 inner copper layers (2 x 35 μm Cu). A thermal via (diameter = 0.3 mm and 25 μm plating) array was applied under the exposed pad and connected the first outer layer (top) to the first inner layer and second outer layer (bottom) of the JEDEC PCB. $T_a = 25^\circ\text{C}$; The IC is dissipating 1 W.

5 Power Supply

The TLD5190 is supplied by the following pins:

- VIN (main supply voltage)
- IVCC_EXT (supply for internal gate driver stages)

The VIN supply provides internal supply voltages for the analog and digital blocks.

IVCC_EXT is the supply for the low side driver stages. This supply is used also to charge, through external Schottky diodes, the bootstrap capacitors which provide supply voltages to the high side driver stages. If no external voltage is available this pin must be shorted to IVCC, which is the output of an internal 5 V LDO.

The supply pins VIN and IVCC_EXT have undervoltage detections.

Undervoltage on IVCC_EXT or IVCC voltages forces a deactivation of the driver stages, thus stopping the switching activity.

Moreover the double function pin EN/INUVLO can be used as an input undervoltage protection by placing a resistor divider from VIN to GND (refer to [Chapter 10.3](#)).

If EN/INUVLO undervoltage is detected, it will turn-off the IVCC voltage regulator and stop switching.

[Figure 4](#) shows a basic concept drawing of the supply domains and interactions among pins VIN and IVCC/IVCC_EXT.

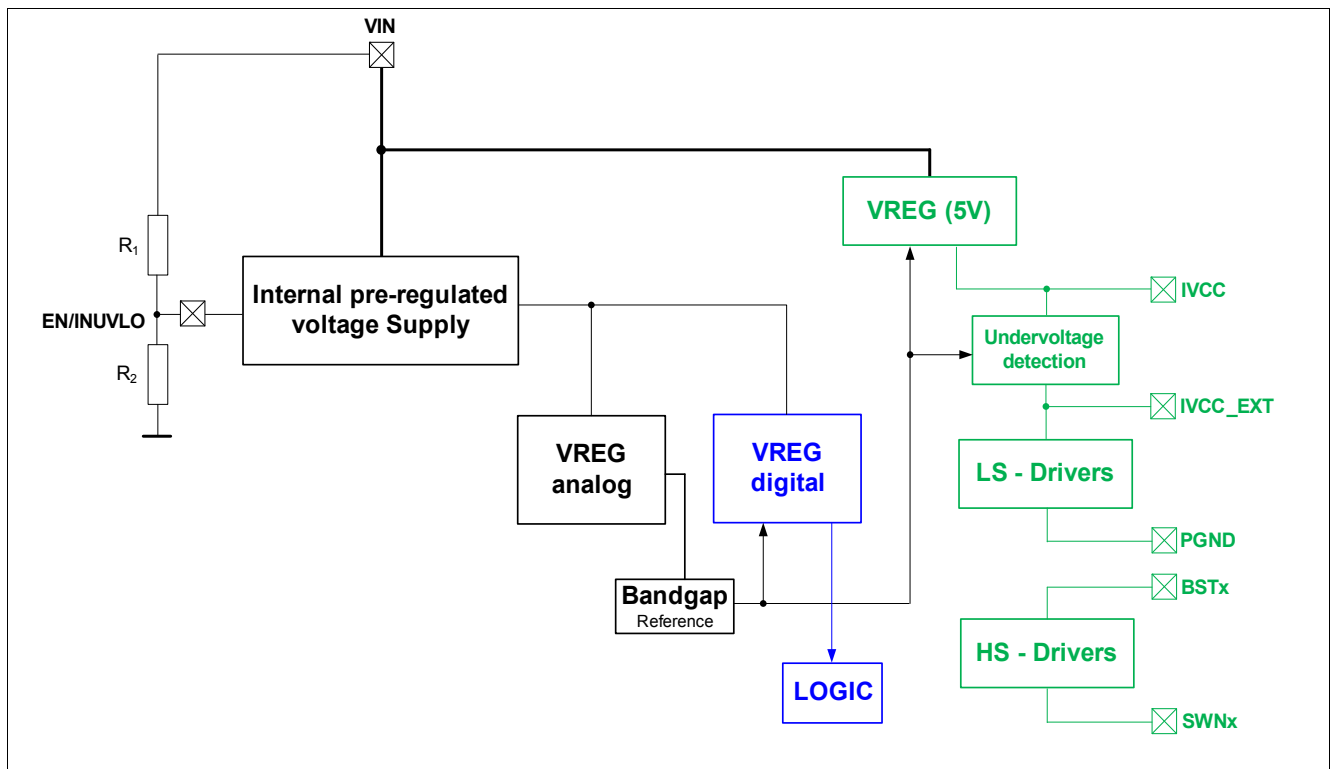


Figure 4 Power Supply Concept Drawing

Power Supply

Usage of EN/INUVLO pin in different applications

The pin EN/INUVLO is a double function pin and can be used to put the device into a low current consumption mode. An undervoltage threshold should be fixed by placing an external resistor divider (A) in order to avoid low voltage operating conditions. This pin can be driven by a μC -port as shown in (B).

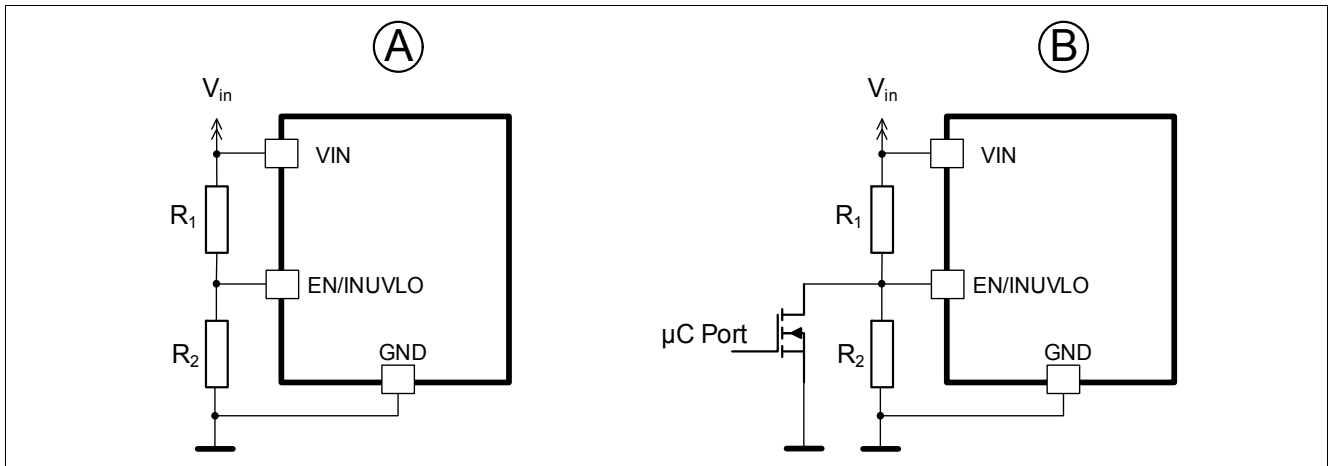


Figure 5 Usage of EN/INUVLO pin in different applications

Power Supply

5.1 Different Power States

TLD5190 has the following power states:

- SLEEP state
- IDLE state
- ACTIVE state

The transition between the power states is determined according to these variables after a filter time of max. 3 clock cycles:

- VIN level
- EN/INUVLO level
- IVCC level
- IVCC_EXT level

The state diagram including the possible transitions is shown in [Figure 6](#).

The Power-up condition is entered when the supply voltage V_{VIN} exceeds its minimum supply voltage threshold $V_{VIN(ON)}$.

SLEEP

When the TLD5190 is in the SLEEP state, all outputs are OFF, independently from the supply voltages V_{IN} , IVCC and IVCC_EXT. The current consumption is low. Refer to parameter: $I_{VIN(SLEEP)}$.

The transition from SLEEP to ACTIVE state requires a specified time: t_{ACTIVE} .

IDLE

In IDLE state the internal voltage regulator is working. Diagnosis functions are not available. The output drivers are switched OFF, independently from the supply voltages V_{IN} , IVCC and IVCC_EXT.

ACTIVE

In active state the device will start switching activity to provide power at the output only when PWMI = HIGH. To start the Highside gate drivers HSGD1,2 the voltage level $V_{BST1,2} - V_{SWN1,2}$ needs to be above the threshold $V_{BST1,2} - V_{SWN1,2_UVth}$. In ACTIVE state the device current consumption via V_{IN} is dependent on the external MOSFET used and the switching frequency f_{SW} .

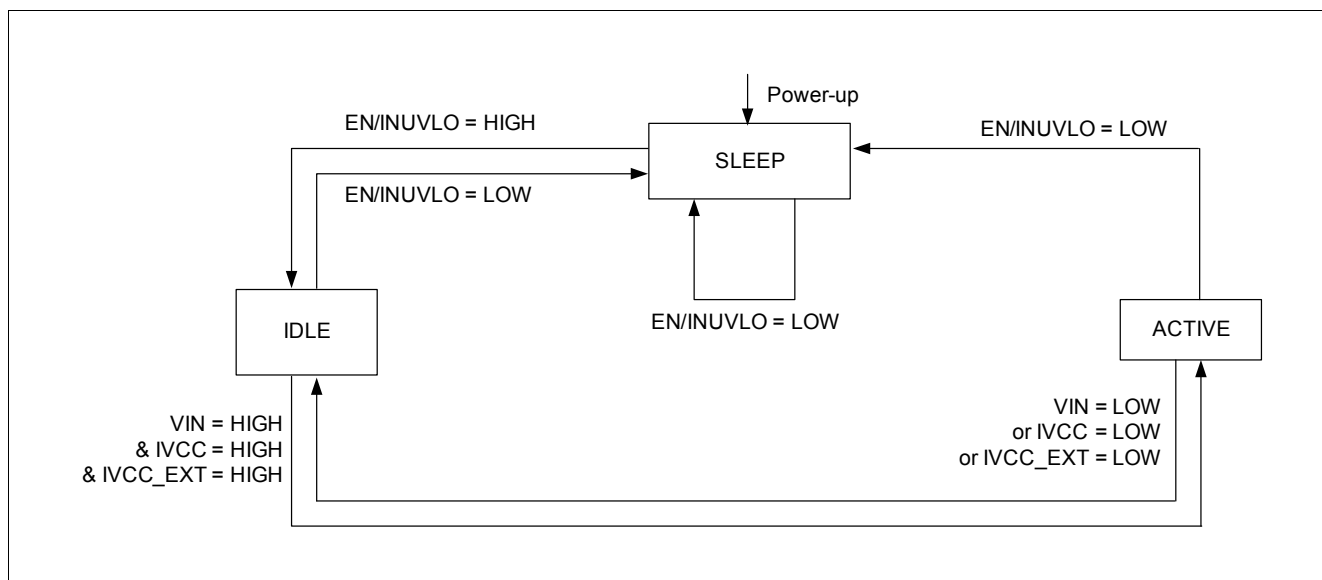


Figure 6 Simplified State Diagram

Power Supply

5.2 Electrical Characteristics

Table 5 EC Power Supply

$V_{IN} = 8\text{ V to }36\text{ V}$, $T_J = -40^\circ\text{C to }+150^\circ\text{C}$, all voltages with respect to AGND; (unless otherwise specified)

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|---|-----------------------|--------|------|------|---------------|---|----------|
| | | Min. | Typ. | Max. | | | |
| Power Supply V_{IN} | | | | | | | |
| Input Voltage Startup | $V_{VIN(ON)}$ | – | – | 4.7 | V | V_{IN} increasing; $V_{EN/INUVLO} = \text{HIGH}$; $IVCC = IVCC_EXT = 10\text{ mA}$; | P_5.3.1 |
| Input Undervoltage switch OFF | $V_{VIN(OFF)}$ | – | – | 4.5 | V | V_{IN} decreasing; $V_{EN/INUVLO} = \text{HIGH}$; $IVCC = IVCC_EXT = 10\text{ mA}$; | P_5.3.14 |
| Device operating current | $I_{VIN(ACTIVE)}$ | – | 4.4 | 6 | mA | ¹⁾ ACTIVE mode; CLKOUT freq. 300 KHz; $V_{PWMI} = 0\text{ V}$; | P_5.3.2 |
| V_{IN} Sleep mode supply current | $I_{VIN(SLEEP)}$ | – | – | 1.5 | μA | $V_{EN/INUVLO} = 0\text{ V}$; $V_{IN} = 13.5\text{ V}$; $V_{IVCC} = V_{IVCC_EXT} = 0\text{ V}$; | P_5.3.3 |
| EN/INUVLO Pin characteristics | | | | | | | |
| Input Undervoltage falling Threshold | $V_{EN/INUVLOth}$ | 1.6 | 1.75 | 1.9 | V | – | P_5.3.7 |
| EN/INUVLO Rising Hysteresis | $V_{EN/INUVLO(hyst)}$ | – | 90 | – | mV | ¹⁾ | P_5.3.8 |
| EN/INUVLO input Current LOW | $I_{EN/INUVLO(LOW)}$ | 0.45 | 0.89 | 1.34 | μA | $V_{EN/INUVLO} = 0.8\text{ V}$; | P_5.3.9 |
| EN/INUVLO input Current HIGH | $I_{EN/INUVLO(HIGH)}$ | 1.1 | 2.2 | 3.3 | μA | $V_{EN/INUVLO} = 2\text{ V}$; | P_5.3.10 |
| Timings | | | | | | | |
| SLEEP mode to ACTIVE time | t_{ACTIVE} | – | – | 0.7 | ms | ¹⁾ $V_{IVCC} = V_{IVCC_EXT}$; $C_{IVCC} = 10\text{ }\mu\text{F}$; $V_{IN} = 13.5\text{ V}$; | P_5.3.11 |

1) Not subject to production test, specified by design.

6 Regulator Description

The TLD5190 includes all of the functions necessary to provide constant current to the output as usually required to drive LEDs. A voltage mode regulation can also be implemented (Refer to [Chapter 6.6](#)).

It is designed to control 4 gate driver outputs in a H-Bridge topology by using only one inductor and 4 external MOSFETs. This topology is able to operate in high power BOOST, BUCK-BOOST and BUCK mode applications with maximum efficiency.

The transition between the different regulation modes is done automatically by the device itself, with respect to the application boundary conditions.

The transition phase between modes is seamless.

6.1 Regulator Diagram Description

The TLD5190 includes two analog current control inputs (IIN1, IIN2) to limit the maximum Input current (Block A1 and A7 in [Figure 7](#)).

A second analog current control loop (A5, A6 with compressive gain = $IFBx_{gm}$) connected to the sensing pins FBL, FBH regulates the output current.

The regulator function is implemented by a pulse width modulated (PWM) current mode controller. The error in the output current loop is used to determine the appropriate duty cycle to get a constant output current.

An external compensation network (R_{COMP} , C_{COMP}) is used to adjust the control loop to various application boundary conditions.

The inductor current for the current mode loop is sensed by the R_{SWCS} resistor.

R_{SWCS} is used also to limit the maximum external switches / inductor current.

If the Voltage across R_{SWCS} exceeds its overcurrent threshold (V_{SWCS_buck} or V_{SWCS_boost} for buck or boost operation respectively) the device reduces the duty cycle in order to bring the switches current below the imposed limit.

The current mode controller has a built-in slope compensation as well to prevent sub-harmonic oscillations.

The control loop logic block (LOGIC) provides a PWM signal to four internal gate drivers. The gate drivers (HSGD1,2 and LSGD1,2) are used to drive external MOSFETs in an H-Bridge setup . Once the soft start expires a forced CCM regulation mode is performed.

The control loop block diagram displayed in [Figure 7](#) shows a typical constant current application. The voltage across R_{FB} sets the output current. R_{IN} is used to fix the maximum input current.

Regulator Description

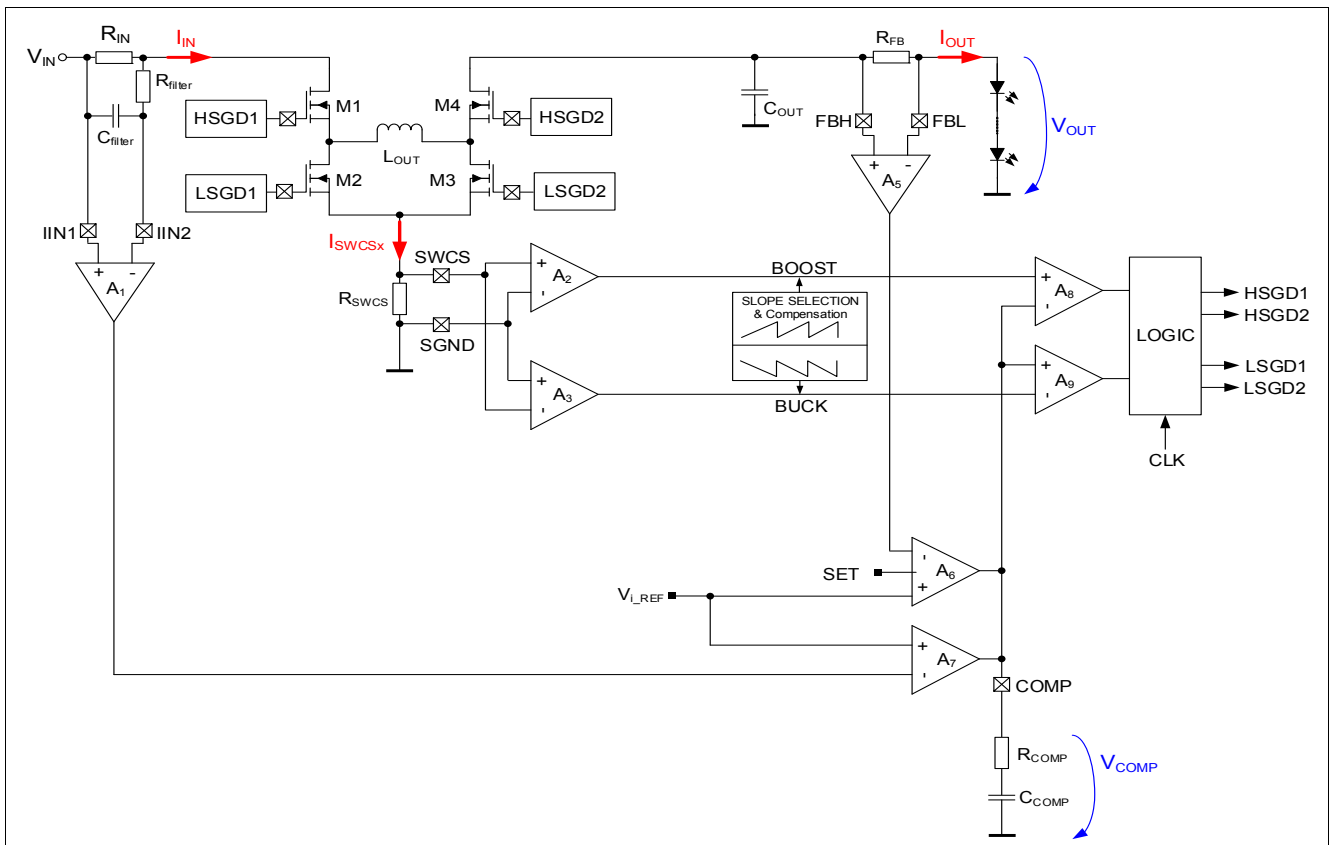


Figure 7 Regulator Block Diagram - TLD5190

Regulator Description

6.2 Adjustable Soft Start Ramp

The soft start routine limits the current through the inductor and the external MOSFET switches during initialization to minimize potential overshoots at the output.

The soft start routine is applied:

- At first turn on (first PWM rise after EN = High)
- After Output Short to GND or Open Load detection
- After Input Overvoltage detection

The soft start rising edge gradually increases the current of the inductor (L_{OUT}) over t_{SOFT_START} by clamping the COMP voltage. The soft start ramp is defined by a capacitor placed at the SOFT_START pin.

Selection of the SOFT_START capacitor (C_{SOFT_START}) can be done according to the approximate formula described in [Equation \(6.1\)](#):

$$t_{SOFT_START} = \frac{V_{ss_th_eff}}{I_{SOFT_START(PU)}} \cdot C_{SOFT_START} \quad (6.1)$$

Note: $V_{ss_th_eff}$ is the soft start effectiveness threshold, that depends on load condition. Its value is about 0.7 V for the buck mode and 1.4 V for the boost mode

The SOFT START pin is also used to implement a fault mask and wait-before-retry time, on rising and falling edge respectively, see and chapter [Chapter 10.2](#) for details.

If an open load or a short on the output is detected, a pull-down current source $I_{SOFT_START_PD}$ (P_6.4.20) is activated. Through a pull-up resistor connected from VREF to the SOFT START pin it is possible to source a current higher than $I_{SOFT_START_PD}$, the TLD5190 will latch OFF until the EN/INUVLO pin is toggled. Without any resistor to VREF the pull-down current decreases until $V_{SOFT_START_RESET}$ (P_6.4.22) is reached (the pull-up current source turns on again). If the fault condition hasn't been removed until $V_{SOFT_START_LOFF}$ (P_6.4.21) is reached, the pull-down current source $I_{SOFT_START_PD}$ turns on again initiating a new cycle. This will continue until the fault is removed.

If an input overvoltage is detected the soft start is kept low as long as the overvoltage remains.

At first PWM rise after EN = High, the internal PWM is extended till one of the 2 following condition is reached:

- Until V_{SOFT_START} exceeds $V_{Soft_Start1,2_LOFF}$
- Until $V_{FBH-FBL}$ exceeds $V_{FBH-FBL_OL}$

Regulator Description

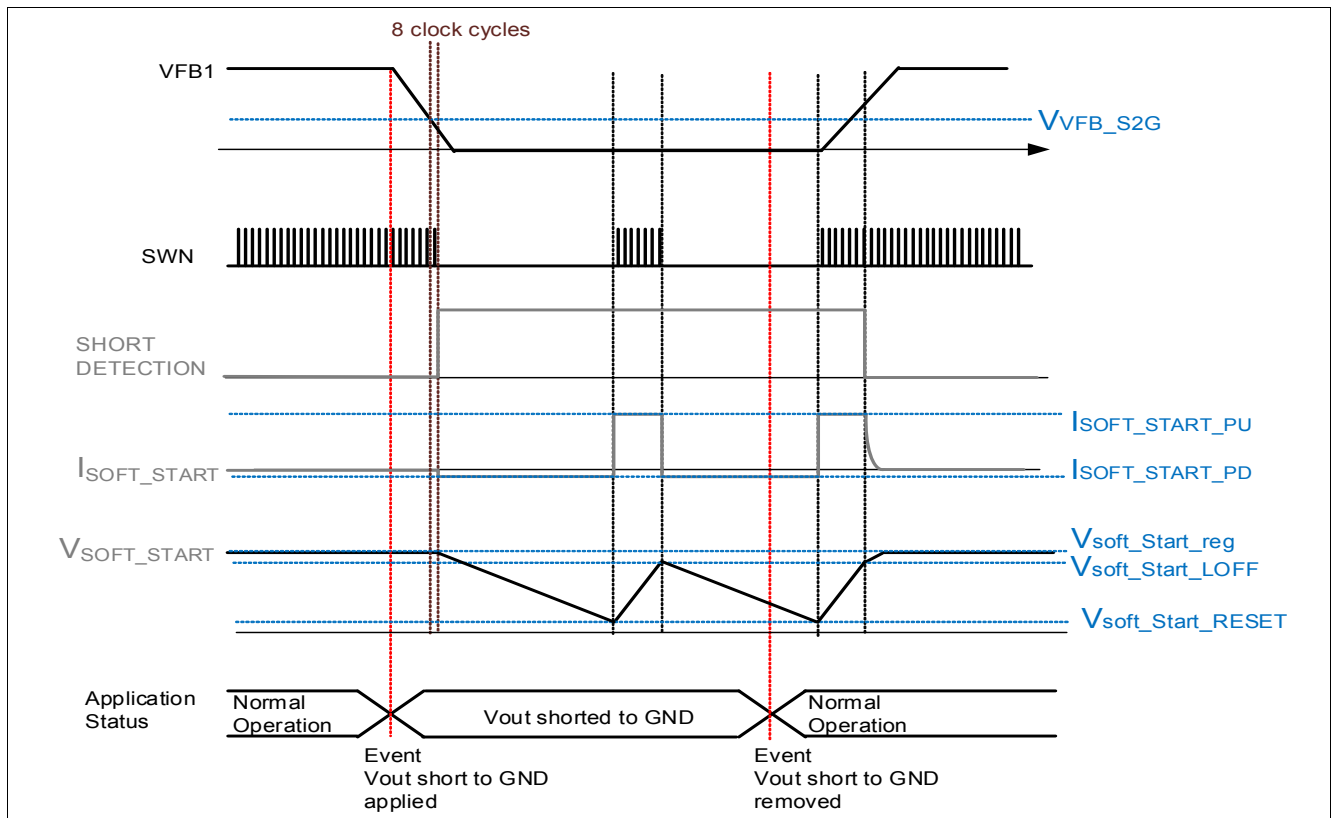


Figure 8 Soft Start timing diagram on a short to ground detected by the VFB pin

6.3 Switching Frequency setup

The switching frequency can be set from 200 kHz to 700 kHz by an external resistor connected from the FREQ pin to GND or by supplying a sync signal as specified in chapter [Chapter 11.2](#). Select the switching frequency with an external resistor according to the graph in [Figure 9](#) or the following approximate formulas.

$$f_{SW} [kHz] = 5375 * (R_{FREQ} [k\Omega])^{-0.8} \tag{6.2}$$

$$R_{FREQ} [k\Omega] = 46023 * (f_{SW} [kHz])^{-1.25} \tag{6.3}$$

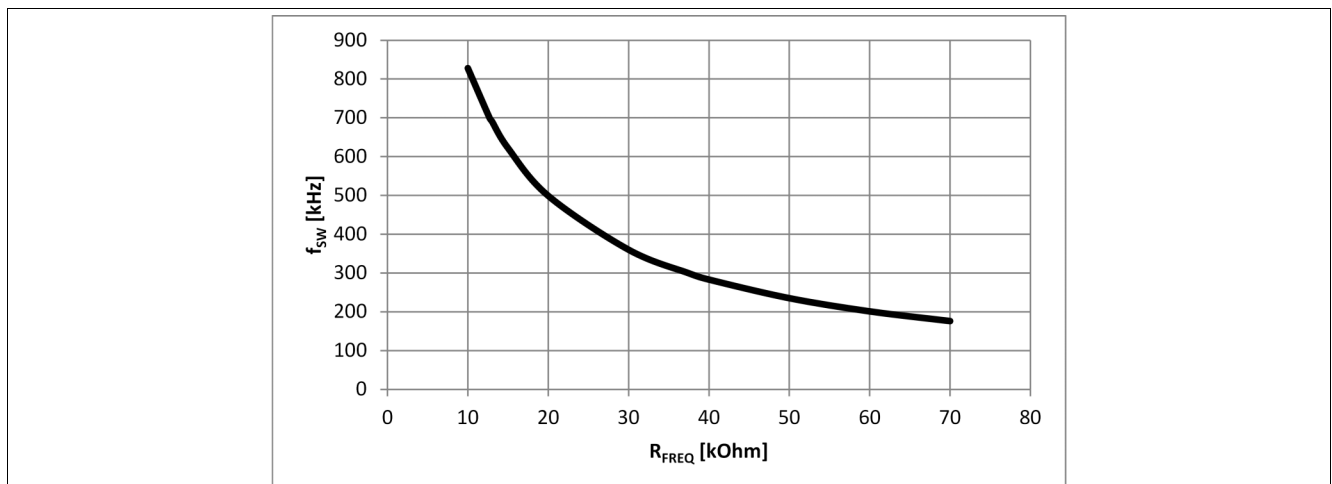


Figure 9 Switching Frequency f_{sw} versus Frequency Select Resistor to GND R_{FREQ}

Regulator Description

6.4 Operation of 4 switches H-Bridge architecture

Inductor L_{OUT} connects in an H-Bridge configuration with 4 external N channel MOSFETs (M1, M2, M3 & M4)

- Transistor M1 and M3 provides a path between V_{IN} and ground through L_{OUT} in one direction (Driven by top and bottom gate drivers HSGD1 and LSGD2)
- Transistor M2 and M4 provides a path between V_{OUT} and ground through L_{OUT} in the other direction (Driven by top and bottom gate drivers HSGD2 and LSGD1)
- Nodes SWN1, SWN2, voltage across R_{SWCS} , input and load currents are also monitored by the TLD5190

| | BOOST MODE | BUCK-BOOST MODE | BUCK MODE |
|----|------------|-----------------|-----------|
| M1 | ON | PWM | PWM |
| M2 | OFF | PWM | PWM |
| M3 | PWM | PWM | OFF |
| M4 | PWM | PWM | ON |

Figure 10 4 switches H-Bridge architecture Transistor Status summary

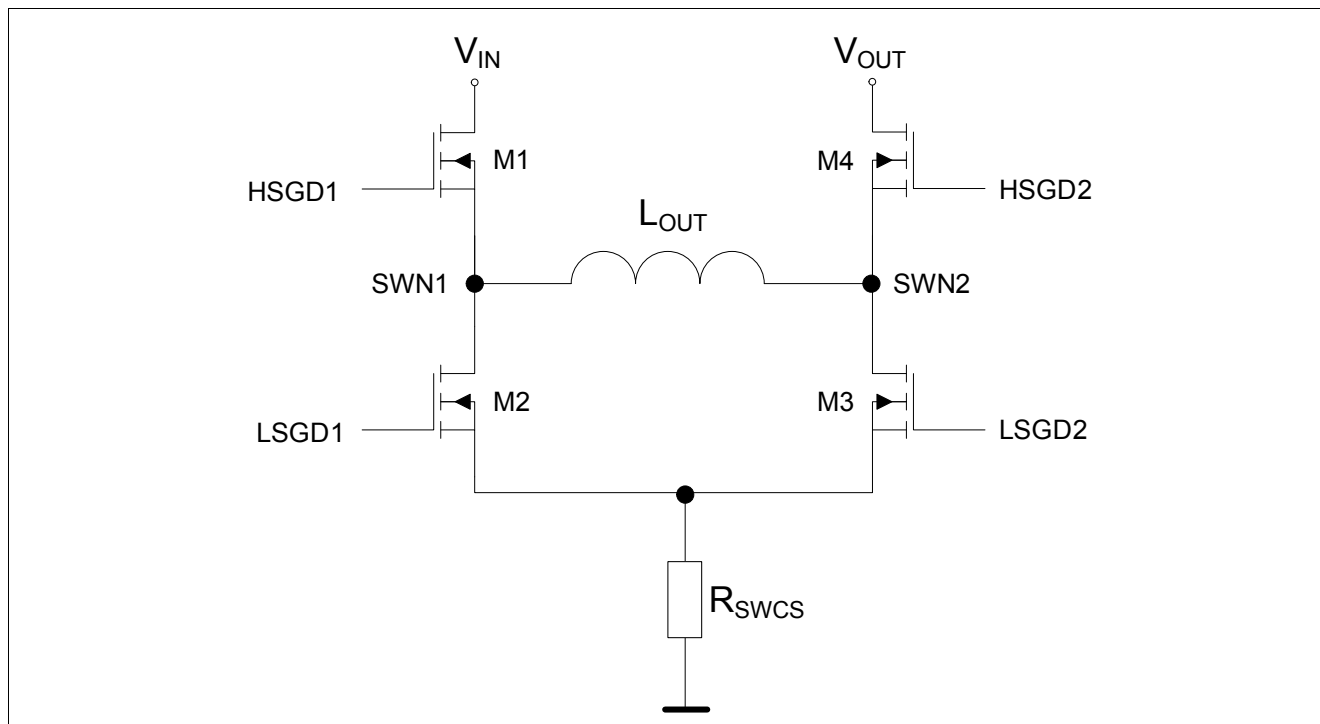


Figure 11 4 switches H-Bridge architecture overview

6.4.1 Boost mode ($V_{IN} < V_{OUT}$)

- M1 is always ON, M2 is always OFF
- Every cycle M3 turns ON first and inductor current is sensed (peak current control)
- M3 stays ON until the upper reference threshold is reached across R_{SWCS} (Energizing)

Regulator Description

- M2 turns OFF, M1 turns ON until the end of the cycle (Energizing)
- Switches M1 and M2 alternate, behaving like a typical synchronous BUCK Regulator (see [Figure 14](#))

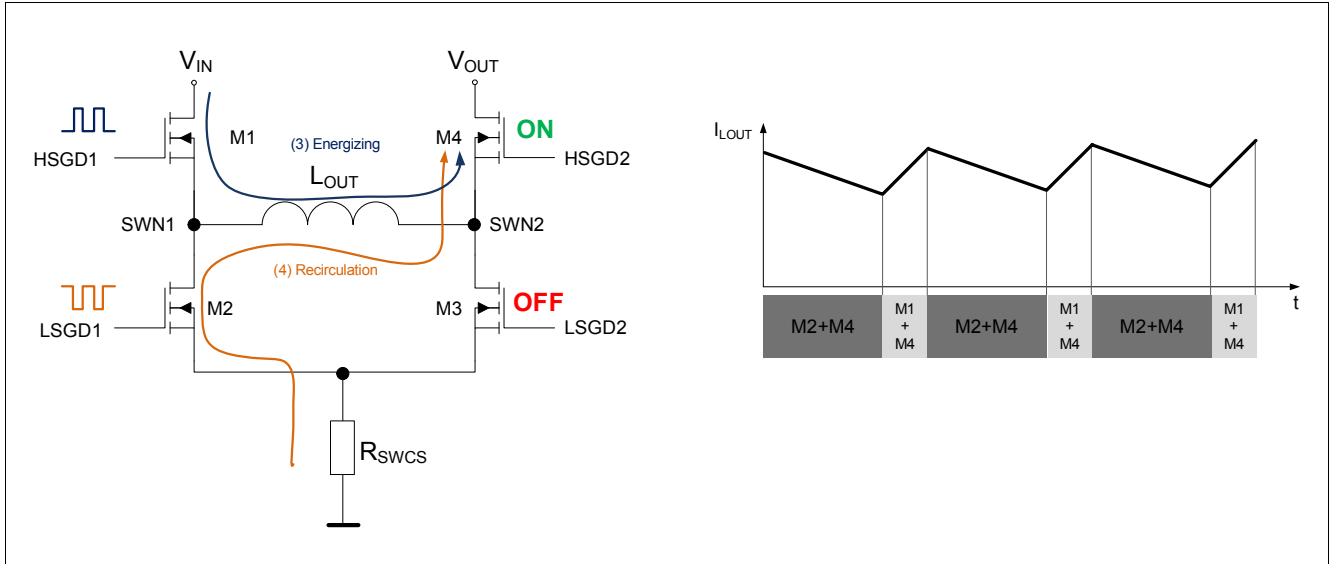


Figure 14 4 switches H-Bridge architecture in BUCK mode

Simplified comparison of 4 switches architecture to traditional asynchronous Buck approach.

- M3 is always OFF in this mode (open).
- M4 is always ON in this mode (closed connection inductor to V_{OUT}).
- M2 acts as a synchronous diode, with significantly lower conduction losses ($I^2 \times R_{DS(ON)}$ vs. $0.7 V \times I$)

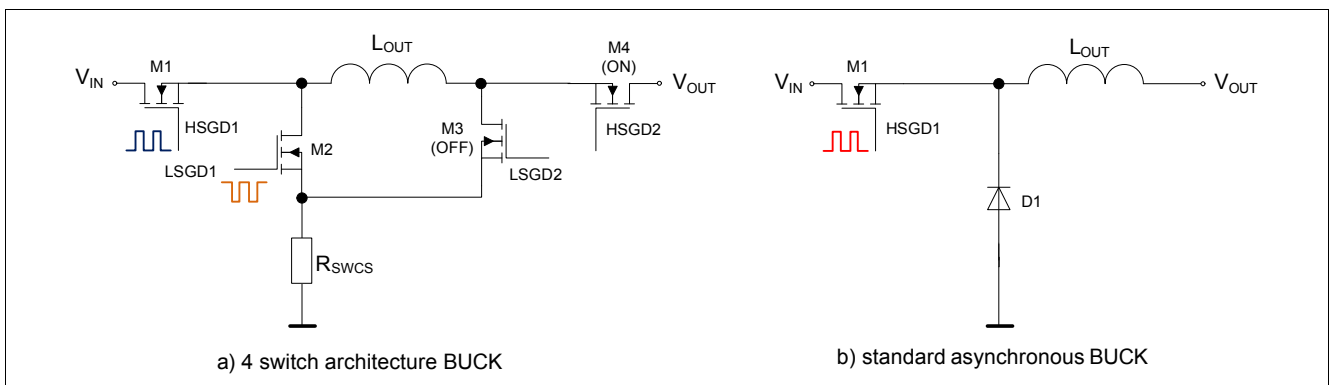


Figure 15 4 switches H-Bridge architecture in BUCK mode compared to standard async BUCK

6.4.3 Buck-Boost mode ($V_{IN} \sim V_{OUT}$)

- When V_{IN} is close to V_{OUT} the controller is in Buck-Boost operation
- All switches are switching in buck-boost operation. The direct energy transfer from the Input to the output ($M1+M4 = ON$) is beneficial to reduce ripple current and improves the energy efficiency of the Buck-Boost control scheme
- The two buck boost waveforms and switching behaviors are displayed in [Figure 16](#) below

Regulator Description

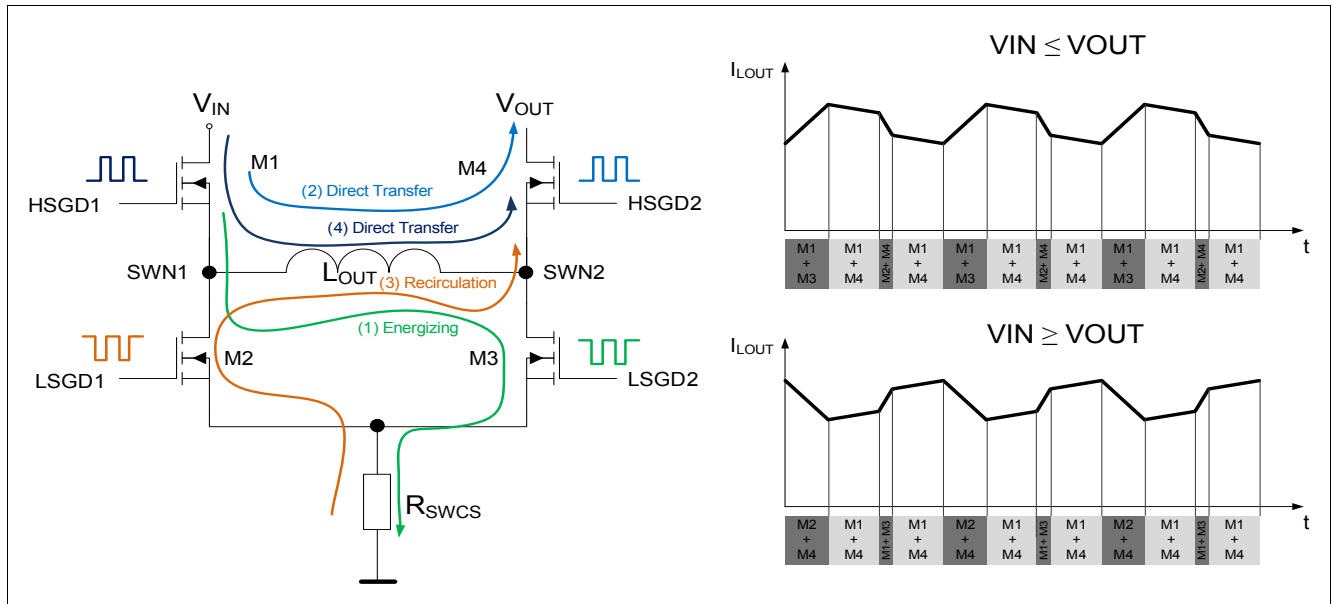


Figure 16 4 switches H-Bridge architecture in BUCK-BOOST mode

6.5 Flexible current sense

The flexible current sense implementation enables highside and lowside current sensing.

The [Figure 17](#) displays the application examples for the highside and lowside current sense concept.

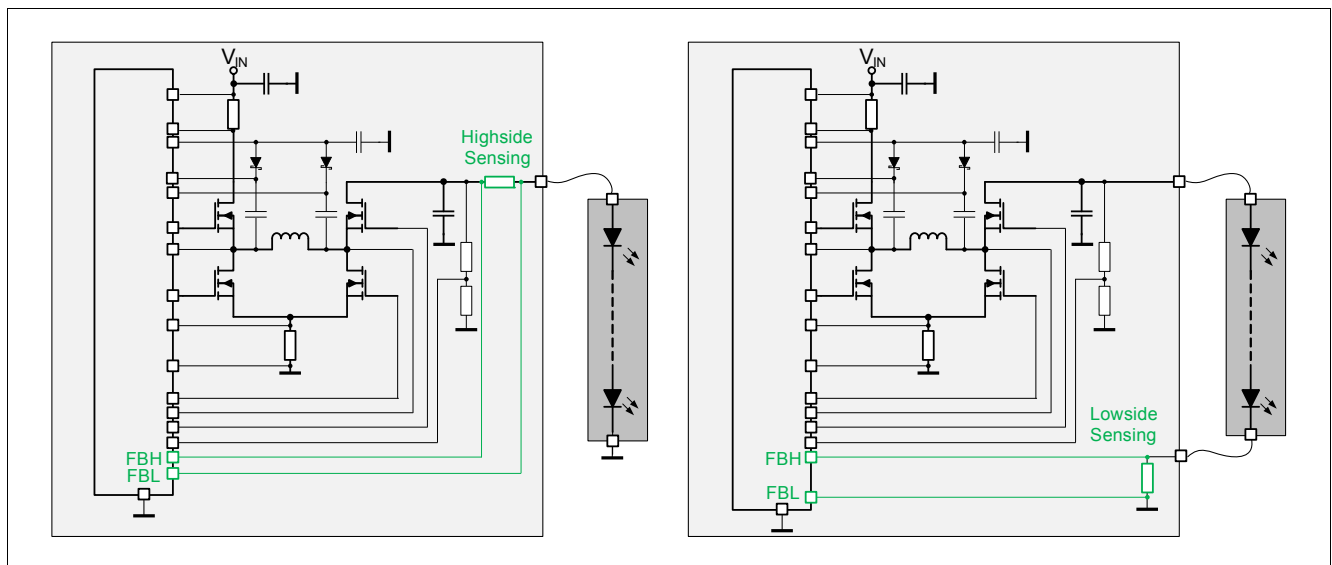


Figure 17 Highside and lowside current sensing - TLD5190

Regulator Description

6.6 Programming Output Voltage (Constant Voltage Regulation)

For a voltage regulator, the output voltage can be set by selecting the values R_{FB1} , R_{FB2} and R_{FB3} according to the following Equation (6.4):

$$V_{OUT} = \left(I_{FBH} + \frac{V_{FBH-FBL}}{R_{FB2}} \right) \cdot R_{FB1} + \left(\frac{V_{FBH-FBL}}{R_{FB2}} - I_{FBL} \right) \cdot R_{FB3} + V_{FBH-FBL} \quad (6.4)$$

If Analog dimming is performed, due to the variations on the I_{FBL} (I_{FBL_HSS} (P_6.4.9) and I_{FBL_LSS} (P_6.4.40)) current on the entire voltage spanning, a non linearity on the output voltage may be observed. To minimize this effect RFBx resistors should be properly dimensioned.

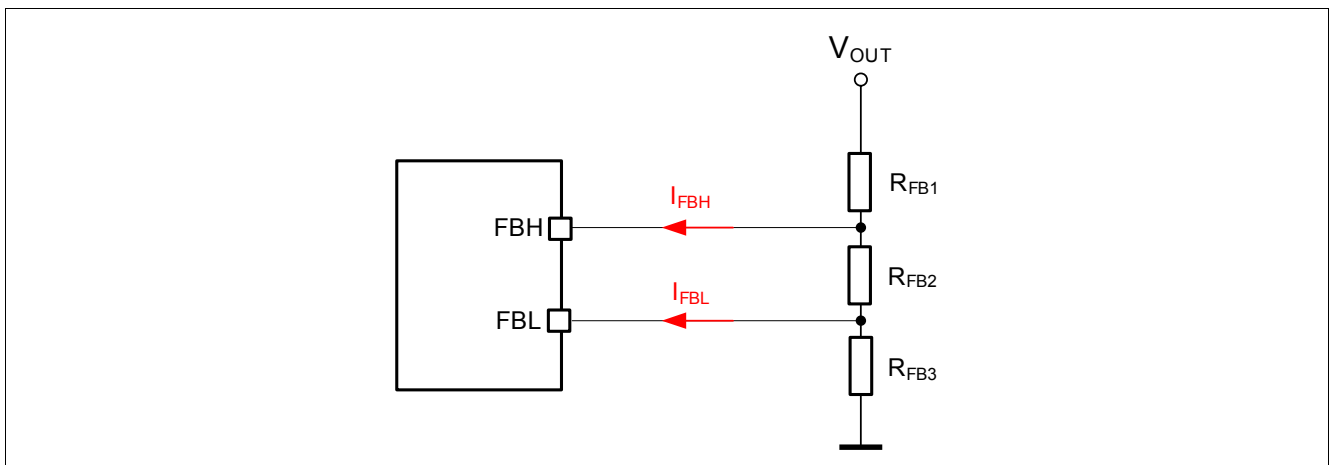


Figure 18 Programming Output Voltage (Constant Voltage Regulation)

Regulator Description

6.7 Electrical Characteristics

Table 6 EC Regulator

$V_{IN} = 8\text{ V to }36\text{ V}$, $T_J = -40^\circ\text{C to }+150^\circ\text{C}$, all voltages with respect to AGND (unless otherwise specified)

| Parameter | Symbol | Values | | | Unit | Note or Test Condition | Number |
|--|-----------------------|--------|------|-------|---------------|---|-----------|
| | | Min. | Typ. | Max. | | | |
| Regulator: | | | | | | | |
| $V_{(FBH-FBL)}$ threshold | $V_{(FBH-FBL)}$ | 145.5 | 150 | 154.5 | mV | $V_{SET} = 2\text{ V}$; | P_6.4.1 |
| $V_{(FBH-FBL)}$ threshold @ analog dimming 10% | $V_{(FBH-FBL)_10}$ | 10 | 15 | 20 | mV | $V_{SET} = 0.32\text{ V}$; | P_6.4.6 |
| FBH Bias current @ highside sensing setup | I_{FBH_HSS} | 65 | 110 | 155 | μA | ¹⁾ $V_{FBL} = 7\text{ V}$; $V_{FBH-FBL} = 150\text{ mV}$; | P_6.4.8 |
| FBL Bias current @ highside sensing setup | I_{FBL_HSS} | 17 | 30 | 43 | μA | ¹⁾ $V_{FBL} = 7\text{ V}$; $V_{FBH-FBL} = 150\text{ mV}$; | P_6.4.9 |
| FBH Bias current @ lowside sensing setup | I_{FBH_LSS} | -7.5 | -4 | -2.5 | μA | ¹⁾ $V_{FBL} = 0\text{ V}$; $V_{FBH-FBL} = 150\text{ mV}$; | P_6.4.39 |
| FBL Bias current @ lowside sensing setup | I_{FBL_LSS} | -45 | -30 | -20 | μA | ¹⁾ $V_{FBL} = 0\text{ V}$; $V_{FBH-FBL} = 150\text{ mV}$; | P_6.4.40 |
| FBH-FBL High Side sensing entry threshold | $V_{FBH_HSS_in_c}$ | - | 2 | - | V | ¹⁾ V_{FBH1} increasing; | P_6.9.1 |
| FBH-FBL High Side sensing exit threshold | $V_{FBH_HSS_d_ec}$ | - | 1.75 | - | V | ¹⁾ V_{FBH} decreasing; | P_6.9.2 |
| OUT Current sense Amplifier g_m | $IFBx_{gm}$ | - | 890 | - | μS | ¹⁾ | P_6.4.10 |
| Output Monitor Voltage | $V_{IOUTMON}$ | 1.33 | 1.4 | 1.47 | V | $V_{FBH-FBL} = 150\text{ mV}$; | P_6.4.11 |
| Maximum BOOST Duty Cycle | D_{BOOST_MAX} | 89 | 91 | 93 | % | ¹⁾ $f_{sw} = 300\text{ kHz}$; | P_6.4.12 |
| Input Current Sense threshold $V_{IIN1-IIN2}$ | $V_{IIN1-IIN2}$ | 46 | 50 | 54 | mV | - | P_6.4.13 |
| Input Current sense Amplifier g_m | I_{IN_gm} | - | 2.12 | - | mS | ¹⁾ | P_6.4.14 |
| Input current Monitor Voltage | V_{IINMON} | 0.95 | 1 | 1.05 | V | ¹⁾ $V_{IIN1-IIN2} = 50\text{ mV}$; $V_{IIN1} = V_{VIN(ON)}$ to 55 V; | P_6.4.15 |
| Switch Peak Over Current Threshold - BOOST | V_{SWCS_boost} | 40 | 50 | 60 | mV | ¹⁾ | P_10.8.15 |
| Switch Peak Over Current Threshold - BUCK | V_{SWCS_buck} | -60 | -50 | -40 | mV | ¹⁾ | P_10.8.16 |
| Soft Start | | | | | | | |
| Soft Start pull up current | $I_{Soft_Start_PU}$ | 22 | 26 | 32 | μA | $V_{Soft_Start} = 1\text{ V}$; | P_6.4.19 |
| Soft Start pull down current | $I_{Soft_Start_PD}$ | 2.2 | 2.6 | 3.2 | μA | $V_{Soft_Start} = 1\text{ V}$; | P_6.4.20 |