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Features

• All Functions and Channel Selections are Controlled by Serial Bus

RF Part

- All Oscillators and PLL Integrated
- IF Converter
- FM Demodulator
- RSSI

Low Frequency Part

- Asymmetrical Input of Microphone Amplifier
- Asymmetrical Output of Earpiece Amplifier
- Compander
- Power Supply Management
- Serial Bus

Application

- CT0 Standard
- Narrowband Voice and Data Transmitting/Receiving Systems

1. Description

The programmable single-chip multichannel cordless phone IC includes all necessary low frequency parts such as microphone- and earphone amplifier, compander, powersupply management as well as all RF parts such as IF converter, FM demodulator, RSSI, oscillators and PLL. Several gains and mutes in transmit and receive direction are controlled by the serial bus. The compander can be bypassed.





Single-chip Cordless Telephone IC

U3600BM

Rev. 4516D-CT0-10/05





Figure 1-1. Block Diagram



2. Pin Configuration

Figure 2-1. Pinning SSO44







Table 2-1.	Pin Descri	ption
Pin	Symbol	Function
1	PCLO	Phase comparator local oscillator
2	RFOGND	RF transmit output ground
3	RFO	RF transmit output
4	RFOVB	Power supply input of RF transmit output buffer
5	AGND	Analog ground for RF part
6	VBIAS	Decoupling capacitor of current reference
7	VRF	Supply voltage for RF part
8	MLF	Modulator loop filter
9	LFGND	Modulator loop filter ground
10	MODIN	Modulator input
11	VDD	Supply voltage output for peripherals and internal supply of digital part
12	VSS	Ground for LF analog and digital
13	D	Data input of serial bus
14	С	Clock input of serial bus
15	DACO	D/A and data comparator output
16	OPOUT	Operational amplifier output
17	OPIN	Operational amplifier input (inverting)
18	TXO	Output of limiter amplifier
19	LIMIN	Limiter input
20	COUT	Compressor output
21	CTC	Compressor time constant control analog output
22	COIN	Compressor input
23	MICO	Microphone amplifier output
24	MIC	Inverting input of microphone amplifier
25	DAIN	Data comparator input
26	RXO	Output of demodulator
27	RECO2	
28	RECO1	- Symmetrical output of receive ampliner
29	EXIN	Expander input
30	ETC	Expander time constant control analog output
31	IFIN2	Oursestrias Line at af IE annelifier
32	IFIN1	- Synmetrical input of in ampliner
33	MIX2IN	Input of Mixer2
34	MIX2GND	IF amplifier and Mixer2 ground
35	MIX2O	Mixer2 output
36	VAF	Supply voltage for AF/IF parts
37	ХСК	Crystal oscillator input 11.15 MHz
38	OSCGND	Oscillator ground
39	MIX1O	Output of Mixer1
40	MIX1IN1	Cummatrical input of Mixed
41	MIX1IN2	- Symmetrical input of Mixer i
42	GNDLO	Ground of LO
43	LO2	Tank elements for LO are connected to these nins
44	LO1	

3. System Description

Radio frequency IC for analog cordless telephone application in 26/50 MHz band (CTO standard). The IC performs full duplex communication. The transmitting and receiving frequency are depending on whether the IC is used in the handset or in the base station.

Frequency converter comprise an FM transmitter with switchable output power and first receiver mixer in the same unit. A two-wire bus interface can be used for the frequency control as well as for switching the transmitter power amplifier and the receiver. Fine frequency adjust of reference quartz oscillator is programmable.

The receive part is designed for a double conversion architecture. The incoming radio frequency signal will be filtered and amplified before reaching the first mixer. At this stage the RF signal will be converted down to the first intermediate frequency (10.7 MHz) by using a crystal oscillator (LO1).

The transmit part contains two PLL controlled VCOs. The frequency modulation is accomplished by super-posing the incoming audio signal on the PLL control voltage. Final frequency is a product of mixing VCO1 with first local oscillator of receiver part (VCO3). The FM modulated carrier is amplified by externals power amplifier before entering the output filter and the antenna connector.

3.1 Adjustments for VCO1 and VCO2

To be able to use a wide frequency range for the VCOs (i.e., VCO2 26.3 MHz to 49.9 MHz) the two internal VCOs (VCO1 and VCO2, i.e., the VCOs of the transmit part) have a rough adjust and a fine adjust to increase the frequency range given by the phase comparator.

The rough adjusts for these VCOs are correlated with the country setting. For every country there are two sets of VCO rough adjust settings, one for the base and one for the handset. See tables at channels frequencies and dividers.

To compensate the variation in production there is a fine adjust for each of the VCOs. The fine adjusts of the internal VCOs could be set manually (for test purposes) or set by the automatic mode. Theoretically the sign of the changing (increase/ decrease when the voltage of the phase comparator is to high) is selectable, but we need value 1 () in all cases.

Setting VCO1 (VCO2) under normal conditions:

EAFA1 (EAFA2) = 1, automatic fine adjust VCO1(VCO2) enabled SAFA1 (SAFA2) = 1, sign of auto fine adjustment of VCO1 (VCO2) = 1.

3.2 Adjustment for VCO3

In order to increase the adjustment range of VCO3 with fixed external tank elements and/or for "band switching", especially for US frequencies, VCO3 has programmable capacitors inside. These capacitors can be added by serial bus (FA3 [4:0]) between LO1 and LO2. There are 31 steps available, every step adding a capacitor of 0.5 pF.





3.3 Speed-up of the Loop Filter of PLL1 ("Modulator PLL")

To have a fast locking time for the modulator loop there is a precharge and a speed-up mode for the external loop filter.

During receive mode (VCO3 enabled, VCO1 disabled) the modulator loop filter is precharged to about half of the internally regulated 2.5V charge-pump voltage.

During the first 30 ms after enabling VCO1 the modulator phase comparator is in speed-up mode. In this mode the current of the pase comparator which charges the loop filter is much larger than in normal mode. Additionally to the automatically switched 30 ms speed-up mode, the speed-up can be activated for any time by setting the bit SU1.

3.4 Speed-up of the Loop Filter of PLL3 ("1st. LO.")

Similiar to PLL1, there is also a possibility to increase the locking speed of PLL3. This can be done by setting the bit SU3. Having done this, the charge pump at the output of the phase comparator has a bigger current capability and therefore charges the external capacitors faster.

3.5 Adjustment of the Modulator Gain

To fulfil the different requirements of the different countries three conversion gains of the modulator are selectable by the bits GMOD [1:0] (R6: D2, D3).

Country settings see tables at channel frequencies and dividers. Ranges see electrical characteristics at RF transmitter.

3.6 Modulator PLL

The fractional divider has been chosen to increase the reference frequency of the modulator PLL.

557.5 kHz =
$$f_{Mod} / \left(P_1 + \frac{Q_1}{223} \right)$$

 P_1 : integer part of the fractional divider (M = 1) Q_1 : fractional part of the fractional divider (M = 1)

$$\mathsf{Q}_{1} = 223 \times \left(\frac{\mathsf{f}_{\mathsf{Mod}}}{557.5 \,\mathsf{kHz}} - \mathsf{P}_{1}\right)$$

$$223 = \frac{557.5 \text{ kHz}}{2.5 \text{ kHz}}$$

The frequency step 2.5 kHz is a fraction of the reference frequency 557.5 kHz. In fact, the fractional divider divides Q_1 times by $(P_1 + 1)$ and $(223 - Q_1)$ times by P_1 during 223 cycles.

$$\frac{Q_1 \times (P_1 + 1) + (223 - Q_1)P_1}{223} = P_1 + \frac{Q_1}{223}$$

For each comparison cycle ($f_{Ref1} = 557.5 \text{ kHz}$), the accumulator content is incremented by the Q_1 value and the divider divides by the P_1 value. When the accumulator value reaches or exceeds 223, the divider divides by the value ($P_1 + 1$). Then, the accumulator holds the excess value (accumulator value - 223). After 223 cycles, the correct division is executed.

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3.7 Serial Bus Interface

The circuit is remoted by an external microcontroller through the serial bus.

The data is a 12-bit word:

A0 - A3: address of the destination register (0 to 15)

D7 - D0: contents of register

The data line must be stable when the clock is high and data must be serially shifted.

After 12 clock periods, the transfer to the destination register is (internally) generated by a low to high transition of the data line when the clock is high.

Figure 3-1. Serial Bus















Figure 3-4. Serial Bus Timing Diagram



3.8 Content of Internal Registers

The registers have the following structure

D7	D6 D5	D4	D3	D2	D1	D0
----	-------	----	----	----	----	----

R0: Reference for D/A converter

MUXDA	DA6	DA5	DA4	DA3	DA2	DA1	DA0

MUXDA: D/A multiplexing VBAT/RSSI

DA(0:6): Reference voltage D/A

R1: Gain of earpeace amplifier and demodulator

GEA4	GEA3	GEA2	GEA1	GEA0	GDEM	free	free
------	------	------	------	------	------	------	------

GEA[0:4]: Gain of earpeace amplifier; "0" is LSB, "4" is MSB GDEM: Demodulator gain (1 = low gain)

R2: Switches and mutes for receive and data reception

DATRX BEXP EEA ERXO ERX1 ERXHF MRX ERX	2
--	---

DATRX:	Switch data comparator output to "DACO"-pin
BEXP:	Bypass expander
EEA:	Enable earpiece amplifier
ERXO:	Enable RXO output driver
ERX1:	Enable RX low frequency part 1
ERXHF:	Enable Mixer2 and IF-amplifier
MRX:	Mute RX low frequency path (expander) keeping circuit enabled
ERX2:	Enable RX low frequency part 2 (expander)

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U3600BM

R3: Switches and mutes for transmit and power managemant

PDVDD	RBAT	free	free	free	free	MTX	ETX
-------	------	------	------	------	------	-----	-----

PDVDD: Enable pull-down transistor in power-down mode

RBAT: Battery detection high/low range

MTX: Mute TX low frequency path (compressor) keeping circuit enabled

ETX: Enable TX low frequency part

R4: free (not used, for future extensions)

free free	free	free	free	free	free	free
-----------	------	------	------	------	------	------

R5: Gain VCO2

(
free	free	KV23	KV22	KV21	M12	free	free

KV2[1:3]: Gain of VCO2

M12: Double phase comparator frequency of PLL2

R6: Miscellaneus settings in synthesizer part

ETXO M1CP FRMT IMIXI GMOD1 GMOD0 SU1 (TM)

ETXO: Enable HF-transmit output

M1CP: Changes 1 dB compression point and current consumption of Mixer1 ("0" -> high, "1" -> low)

FRMT: Output frequency range of MixerT

IMIXI: Invert inputs of phase comparator in PLL2

GMOD[0:1]: Modulation gain of VCO1

SU1: Speed-up phase comparator for PLL1

(TM): Enable the internal test mode. It is mandatory that TM is kept to "0"! (if not 0, the circuit will not work as expected or described here in this paper)

R7: PLL1 setting

DR1I[0:1]: Additional divider reference frequency PLL1

RA1[0:1]: Rough adjustment VCO1

DV1I[0:3]: Divider setting PLL1 integer part; "0" is LSB, "3" is MSB

R8: Divider PLL1 fractional part

DV1F7 DV1F6 DV1F5 DV1F4 DV1F3 DV1F2 DV1F1 DV1F0

DV1F[0:7]: Divider setting PLL1 fractional part; "0" is LSB, "7" is MSB





R9: Divider PLL3 LSBs

DV3I7	DV3I6	DV3I5	DV3I4	DV3I3	DV312	DV3I1	DV3I0
-------	-------	-------	-------	-------	-------	-------	-------

R10: Divider PLL3 MSBs and MSB of VCO3 fine adjustment

FA34	DV3I14	DV3I13	DV3I12	DV3I11	DV3I10	DV319	DV3I8
------	--------	--------	--------	--------	--------	-------	-------

FA34: Fine adjustment VCO3 (frequency reduction) MSB DV1I[0:14]: Divider setting PLL3 integer part; "0" is LSB, "14" is MSB

R11: Setting PLL2 and VCO3

FA33	FA32	FA31	FA30	AMIX2	AMIX1	RA21	RA20
------	------	------	------	-------	-------	------	------

FA3[0:4]: Fine adjustment of VCO3 (frequency reduction); "0" is LSB, "4" is MSB

AMIX[1:2]: Lengthening antibacklash signal PLL2

RA2[1:0]: Rough adjustment VCO2

R12: Divider for country setting, fine adjustment oscillator

	FAOS2	FAOS1	FAOS0	D31	D30	D20	D11	D10
--	-------	-------	-------	-----	-----	-----	-----	-----

FAOS[0:2]: Fine adjustment of crystal oscillator (frequency reduction);

"0" is LSB, "2" is MSB

D3[0:1]: Setting divider D3 D20: Setting divider D2

D20: Setting divider D2 D1[0:1]: Setting divider D1

R13: VCO1 enable and fine adjustment

EVCO1 SAFA1 EAFA1 FA14 FA13 FA12 FA11 FA10	10
--	----

EVCO1: Enable VCO1

SAFA1: Sign for automatic fine adjustment of VCO1

EAFA1: Enable automatic fine adjustment of VCO1

FA1(0:4): Manual fine adjustment of VCO1 (frequency reduction); "0" is LSB, "4" is MSB

R14: VCO2 enable and fine adjustment

EVCO2 SAFA2 EAFA2 FA24 FA23 FA22 FA21 FA20	I
--	---

EVCO2: Enable VCO2 and MixerT

SAFA2: Sign for automatic fine adjustment of VCO2

EAFA2: Enable automatic fine adjustment of VCO2

FA2(0:4): Manual fine adjustment of VCO2 (frtequency reduction); "0" is LSB, "4" is MSB R15: VCO3 enable, speed-up and referencq frequency, crystal oscillator enable

EVCO3	EOSC	SU3	E25K	E12K5	E10K	E6K25	E5K
EVCO3.	Enable V(CO3 and M	ivor1				
EOSC:	Enable cr	ystal oscilla	ator (11.15	MHz)			
SU3:	Speed-up	phase con	nparator for	PLL3			
E25K:	Selection	phase com	parator fre	quency for	PLL3: f _{Ref3}	= 25 kHz	
E12K5:	Selection	phase com	parator fre	quency for	PLL3: f _{Ref3}	= 12.5 kHz	
E10K:	Selection	phase com	parator fre	quency for	PLL3: f _{Ref3}	= 10 kHz	
E6K25:	Selection	phase com	parator fre	quency for	PLL3: f _{Ref3}	= 6.25 kHz	
E5K:	Selection	phase com	parator fre	quency for	PLL3: f _{Ref3}	= 5 kHz	
E5K, E6K2	25, E10K, E	15K5, E25I	K = 0:				
	Selection	phase com	parator fre	quency for	PLL3: f _{Ref3}	= 2.5 kHz	

4. Absolute Maximum Ratings

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Parameters	Symbol	Value	Unit
Supply voltage	V_{Batt}, V_{DD}	5.5	V
Junction temperature	Tj	+125	°C
Ambient temperature	T _{amb}	-25 to +75	°C
Storage temperature	T _{stg}	-50 to +125	°C
Power dissipation $T_{amb} = 60^{\circ}C$	P _{tot}	0.9	W

5. Thermal Resistance

Parameters	Symbol	Value	Unit
Junction ambient SSO44	R _{thJA}	70	K/W





6. Electrical Characteristics

 T_{amb} = +25°C, VRF = VAF = RFOVB = 3.6V, all bits set to "0", unless otherwise specified. Test circuit, see Figure 8-1 on page 18. Crystal specifications, see table "Crystal Specifications".

Parameters	Test Conditions	Symbol	Min.	Тур.	Max.	Unit
Power Supply				1		
Operating voltage range			3.1	3.6	5.2	V
Current Consumption	1			1		
Operating current in inactive mode (low voltage)	VRF = VAF = RFOVB = 2.9V VDD = 0V		30	65	85	μΑ
Operating current in standby mode	VRF = VAF = RFOVB = 3.6V		30	100	350	μΑ
Operating current in RX mode "waiting for RSSI"	ERXHF = EVCO3 = EOSC = 1			7.5	10.4	mA
Operating current in RX mode "receiving data"	ERXHF = EVCO3 = EOSC = ERX1 = ERXO = 1			8.5	11.5	mA
Operating current in conversation mode: all blocks enabled	ERXHF = EVCO3 = EOSC = ERX1 = ERXO = ERX2 = EEA = EVCO2 = ETXO = 1 no load at RFO pin 3			20	29	mA
Charge Pump of LL1					1	1
Charge pump output voltage	Output high		2.38	2.5	2.63	V
Precharge voltage at the loop filter	SB127 = 1, SB119 = 0		1.15	1.4	1.65	V
Charge pump output current	VMLF = 1.25V, output low		190		400	μA
in speed-up mode	VMLF = 1.25V, output high		-400		-190	μA
	VMLF = 1.25V, output low		4.3	6.2	8	μA
Charge pump output current	VMLF = 1.25V, output high		-8	-6.2	-4.3	μA
Charge pump leakage current	VMLF = 1.25V, output tristate		-150		+150	nA
Charge Pump of PLL3						
Charge pump output voltage	Output high		2.38	2.5	2.63	V
Charge pump output current	VPCLO = 1.25V, output low		220		420	μA
in speed-up mode	VPCLO = 1.25V, output high		-420		-220	μA
	VPCLO = 1.25V, output low		80		160	μA
Charge pump output current	VPCLO = 1.25V, output high		-160		-80	μA
Charge pump leakage current	VPCLO = 1.25V, output tristate		-50		+50	nA
Receiver Input Mixer (Mixer1)	, EVCO3 = EOSC = 1					
Input frequency range			20		50	MHz
Output frequency				10.7		MHz
Input resistance	MIX1IN1/MIX1IN2 to GND			3.0		kΩ
Input capacitance	MIX1IN1/MIX1IN2 to GND			3.5		pF
Output impedance	MIX10		210	330	390	Ω
Voltage gain	MIX1IN1/2 -> MIX1O "Loaded" (330 Ω with serial capacitance) "Unloaded"			11.5 17.5		dB dB
Input noise voltage				9		nV Hz ^{-1/2}

Electrical Characteristics (Continued) 6.

 T_{amb} = +25°C, VRF = VAF = RFOVB = 3.6V, all bits set to "0", unless otherwise specified. Test circuit, see Figure 8-1 on page 18. Crystal specifications, see table "Crystal Specifications".

Parameters	Test Conditions	Symbol	Min.	Тур.	Max.	Unit
Input 1-dB compression point	"Loaded" (330Ω with serial capacitance) M1CP=0 M1CP=1 "unloaded" M1CP=1			140 40 100		mV mV mV
Third order input intercept point	"Loaded" (330Ω with seial capacitance) M1CP=0			430		mV
IF Mixer (Mixer2), EOSC = ER	XHF = 1; Input Frequency: 10.7 MHz					
Input resistance	MIX2IN to GND		2.0	3.0	4.0	kΩ
Input capacitance	MIX2IN to GND		2.5	3	3.5	pF
Output impedance	MIX2O		1200	1500	1800	Ω
Voltage gain	MIX2IN -> MIX2O "Loaded" (1500 Ω with serial capacitance)		13	15	17	dB
Input 1-dB compression point	"Loaded" (1500 Ω with serial capacitance)		32			mV
Third order input intercept point	"Loaded" (1500 Ω with serial capcitance)		80			mV
IF Amplifier and Demodulator	, ERXHF=1, ERX1=1, ERXO=1; Input Signal:	450 kHz, 50	0 μV, FM-	modulatio	n Frequer	ncy = 1 kHz
Recovered audio at RXO, demodulator gain	GDEM=0 GDEM=1			180 90		mV/kHz mV/kHz
AM rejection ratio	30% AM, 2.5 kHz FM			35		dB
Expander, ERX2 = 1; 470 nF f	rom ETC to GND (VSS)			1		1
Gain reference level = G.R.L. (gain = 0 dB)			70	80	90	mVrms
Gain versus input signal level ("gain tracking")	VEXIN = 10 dB less than G.R.L. VEXIN = 20 dB less than G.R.L. VEXIN = 30 dB less than G.R.L.		-11 -21 -35	-10 -20 -30	-9 -19 -25	dB dB dB
Attack time	VEXIN = step 25 mV -> 50 mV measure time after step, when output voltage has 0.75 times of final value			16		ms
Release time	VEXIN = step 50 mV -> 25 mV measure time after step, when output voltage has 1.5 times of final value			16		ms
Input resistance			9.5		15	kΩ
Earpiece Amplifier, EEA = 1, E	ERX2 = 1, BEXP = 1; Apply Input Voltage to I	EXIN; Measu	re Differe	entially at	RECO1/2	
Minimum gain	GEA[4:0]=0		0	1	2	dB
Medium gain	GEA[4:0]=16		16	17	18	dB
Maximum gain	GEA[4:0]=31		31	32	33	dB
Gain adjust step			0.8	1	1.2	dB
Output voltage swing	Maximum gain; 1 k Ω load; increase input voltage until distortion $\approx 5\%$		4.8	5		Vpp
Input resistance			7.3		12.5	kΩ





6. Electrical Characteristics (Continued)

Γ _{amb} = +25°C, VRF = VAF = RFO Γest circuit, see Figure 8-1 on pa	VB = 3.6V, all bits set to "0", unless otherwise s ge 18. Crystal specifications, see table "Crysta	specified. I Specificatio	ns".			
Parameters	Test Conditions	Symbol	Min.	Тур.	Max.	Unit
IF Amplifier: RSSI	·		-			
Input frequency	ERXHF=1			450		kHz
Input resistance			1.6	2.0	2.5	kΩ
RSSI sensitivity	$\label{eq:VIF} VIF = 0 \ \mu V$ starting from 0 increase RSSI-level until mean of sampled signal at DACO is ≥ 0.5 . RSSI-level = ION0 $\ VIF = 25.4 \ \mu V, \ f = 450 \ \text{kHz}$ increase RSSI level again until mean of sampled signal at DACO is ≥ 0.5 . RSSI-level = ION1 RSSI-sensitivity = ION1-ION0			1		
RSSI input voltage dynamic range				65		dB
RSSI level number of programmable steps (see folowing table "RSSI Level Programming (Typical Values)				127		dB
RSSI level step size in the logarithmic region			0.35	0.46	0.6	dB

Table 6-1. RSSI Level Programming (Typical Values)

Input Voltage VIF (μV)	RSSI Level (Decimal)
0	5
25.4	8
42.4	14
424	54
4240	97
42400	111

7. Electrical Characteristics

 T_{amb} = +25°C, VRF = VAF = RFOVB = 3.6V, all bits set to "0", unless otherwise specified. Test circuit, see Figure 8-1 on page 18.

Parameters	Test Conditions	Symbol	Min.	Тур.	Max.	Unit
Data Comparator, ERX1 = DA	TRX = 1	·		·		·
Hysteresis				50		mV
Threshold voltage				1.5		V
Input impedance	DAIN			100		kΩ
Output high voltage	DACO, without load (CMOS-output -> full swing)			3.5		V
Output low voltage	DACO, without load (CMOS-output -> full swing)			0.1		V
Output impedance	DACO			6		kΩ
Battery Switch						•
"Off" threshold	Decrease VBAT until internal switch between VBAT and VDD becomes high ohmic ("off")		2.85	2.95	3.1	v
"On" threshold	Increase VBAT until internal switch between VBAT and VDD becomes low ohmic ("on")		3.1	3.2	3.35	v
Hysteresis	Difference between on and off threshold			250		mV
"Off"-leakage current					10	μA
Switch "On"-resistance					50	Ω
Battery Management, MUXD	A = 1					1
Maximum bat low	DA[6:0] = 127, RBAT = 1		3.7	3.95	4.1	V
Minimum bat low over switch	DA[6:0] = 27, RBAT = 1		3.05	3.2	3.35	V
Maximum bat high	DA[6:0] = 127, RBAT = 0		4.75	5.05	5.25	V
Minimum bat high	DA[6:0] = 0, RBAT = 0		3.83	4.1	4.27	V
Adjust step			3.5	7.5	11.5	mV
Maximum - Minimum			852.5	952.5	1052.5	mV
Microphone Amplifier, ETX=1	ĺ	·				
Open loop gain				80		dB
Gain bandwidth product				3		MHz
Input noise voltage, BW = 300 Hz to 3.4 kHz, psophometrically weighted				0.8	2	μVrmsp
Compressor, ETX = 1; 470 nF	from CTC to GND (VSS)					
Gain reference level = G.R.L. (gain = 0 dB)			298	316	340	mVrms
Gain versus input signal level ("gain tracking")	$\label{eq:VCOIN} \begin{array}{l} VCOIN = 20 \ dB \ less \ than \ G.R.L. \\ VCOIN = 40 \ dB \ less \ than \ G.R.L. \\ VCOIN = 50 \ dB \ less \ than \ G.R.L. \\ VCOIN = 60 \ dB \ less \ than \ G.R.L. \end{array}$		9 19 22	10 20 25 30	11 21 28	dB
Attack time	VCOIN = step 31.6 mV -> 126 mV, (-30 dBV -> -18 dBV) measure time after step, when output voltage has 1.5 times of final value			3.5		ms





7. Electrical Characteristics (Continued)

 $T_{amb} = +25^{\circ}C$, VRF = VAF = RFOVB = 3.6V, all bits set to "0", unless otherwise specified. Test circuit, see Figure 8-1 on page 18.

Parameters	Test Conditions	Symbol	Min.	Тур.	Max.	Unit
Release time	VCOIN = step 126 mV -> 31.6 mV (-18 dBV -> -30 dBV) measure time after step, when output voltage has 0.75 times of final value			14.4		ms
Input resistance			14	19.5	26	kΩ
Splatter Amplifier, ETX = 1						
Open loop gain				90		dB
Gain bandwidth product				150		kHz
Maximum output voltage swing			2.4			Vpp
Limiter Amplifier, ETX = 1, T _j	= 25°C					
Gain for signals below limitation	LIMIN -> TXO, 20 mV _{RMS} applied to LIMIN (AC coupled)			26		dB
Distortion for signals below limitation	LIMIN -> TXO, 20 mV _{RMS} applied to LIMIN (AC coupled)				2	%
Maximum output voltage swing (above limitation, clipping)			1.8	2.1	2.35	V _{pp}
Input resistance at LIMIN			15	20	25	kΩ
Note: The gain and maximu ture dependancy of M circuitry.	m output voltage swing of the limiter amplifie ODIN ("tx conversion gain" of RF transmit pa	r changes w urt), fundam	vith tempera entally deter	ture to com mined by th	pensate the the the the the the the the the t	tempera- of the
MODIN input impedance	$01 = EVC02 = EVC03 = E03C = 1, 1_j = 23$		70	100	130	kO
BEO output impedance	Load - 200 a		230	300	300	NS2
REO output voltage level	EVAC = 0 incload		250	300	0.3	52 V
Highest operating frequency	USA Base Channel 9 (US1b9)			49.99 00	0.5	MHz
	For the complete programming see "Channel Frequencies, Dividers and Country Settings" on page 20"					
	USA1: GMOD[1:0] = 00; fMod = ~7.6 MHz			5.2		kHz/V
TX conversion gain MODIN - RFO	USA2: GMOD[1:0] = 01; fMod = ~5.7 MHz			5.2		kHz/V
	France: GMOD[1:0] = 01; fMod = 4.3 MHz GMOD[1:0] = 00; fMod = 4.3 MHz			3.8 2.7		kHz/V kHz/V
	Spain/Netherlands: GMOD[1:0] = 10; fMod = 1.8 MHz			7.9		kHz/V
Demodulated distortion THD MODIN - RFO	Modulation frequency:1 kHzUS: $\Delta F = 4.0$ kHzFrance: $\Delta F = 2.5$ kHz			1.5	5	%

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7. Electrical Characteristics (Continued)

 T_{amb} = +25°C, VRF = VAF = RFOVB = 3.6V, all bits set to "0", unless otherwise specified. Test circuit, see Figure 8-1 on page 18.

Parameters	Test Conditions	Symbol	Min.	Тур.	Max.	Unit			
Note: The tx conversion gain of the RF transmitter is somehow dependent on temperature. This is determined by the fundamental principle of this circuitry. Means have been taken inside the limiter amplifier, being in the signal path before MODIN, which are able to completely compensate this temperature behavior.									
Logical Part									
Inputs: C, D Low voltage input High voltage input		Vil Vih	$0.8 \times V_D$		$0.2 imes V_{DD}$				
Input leakage current (0 < VI < VDD)		li	-1		+5	μΑ			
Input leakage current Pin XCK (0 < VI < VDD)			-5		+5	μΑ			
Serial bus (Figure 8-2) Data set-up time Data hold time Clock low time Clock high time Hold time before transfer condition Data low pulse on transfer		tsud thd tcl tch teon teh	0.1 0 2 0.1 0.2			µs µs µs µs µs			
condition Data high pulse on transfer condition		teoff	0.2			μs			

8. Fine Adjustment of the Oscillator Frequency

To set the frequency of the oscillator exact to 11.15 MHz, the frequency is adjustable in 8 steps, by adding 3 different internal capacities the frequency could be reduced.

Parameters	Test Conditions/Pins	Min.	Тур.	Max.	Unit
Oscillator frequency without reduction	FAOS (0:2) = 0		11.15 +∆		MHz
Changing of oscillator frequency with FOSC reduction	FAOS2 FAOS1 FAOS0 0 0 1 0 1 0 1 0 0 1 0 1		140 280 560 700		Hz





Figure 8-1. Test Circuit



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Figure 8-2.

Application Circuit



9. Channel Frequencies, Dividers and Country Settings

To meet all requirements of various countries – France (F), Spain (E), Netherlands (NL), USA, Portugal (P), Taiwan, New Zealand and Korea – and modes – base (b), handset (h) – several bits have to be set which do not change for the different channels. These settings are called country settings.

- The country-setting bits contain:
- Rough adjustments for 2 VCOs
- Setting three integer divider in the mixer PLL and modulator PLL
- · Conversion gain adjustment of mixer PLL
- Modulator gain
- Setting of the pulling direction of PLL2 (value dependent, if TX frequency is higher or lower than LO frequency)
- Demodulator gain

Name Register	Function	Notes	Number of Positions
RA1[1:0]	Rough adjust VCO1	00: is the highest frequency	3
RA2[1:0]	Rough adjust VCO2	00: is the highest frequency	4
D1[1:0]	Integer divider D1	Division by 2, 4, 6, 8	4
D20	Integer divider D2	Division by 6, 8	2
M12	Integer divider M12	Doubles reference frequency of PLL2 when set to "1"	2
D3[1:0]	Integer divider D3	Division by 1, 2, 4	3
KV[3:1]	Conversion gain VCO2		6
GMOD[1:0]	Modulator gain	00: gain minimal	3
ΙΜΙΧΙ	Reverse inputs of PC of PLL	0: if fVCO2 lower than fVCO3	2
DR1[1:0]	Additional divider M for reference frequency f _{Ref1}	"0" means no reduction, >0 only necessary in E, NL, Portugal	4
FRMT	Frequency range Mixer T	0: output frequency < 5 MHz	2
GDEM	Demodulator gain	0: high gain 1: low gain	2

Note: Setting the fractional dividers:

For N, $\ensuremath{Q_{M}}\xspace$, send the binary equivalent of the numbers given below.

For P_M (integer part of modulator PLL), send the D2 complement (16 – P_M)

i.e., Fb1 ($P_M = 7$, $Q_M = 159 \Rightarrow$ integer: send 16 - $P_M = 9$, fractional: send 159)

10. Tables for Programming of the Dividers (Refer to Block Diagram)

D11 (bit)	D10 (bit)	Decimally	D1 (Block Diagram),if M12 = 0	D1 (Block Diagram),if M12 = 1
0	0	0	2	1
0	1	1	8	4
1	0	2	6	3
1	1	3	4	2

Table 10-1. Divider D1 for PLL2

Table 10-2. Divider D2 between PLL1 and PLL2

D20 (bit)	Decimally	D2 (Block Diagram),if M12 = 0	D2 (Block Diagram),if M12 = 1
0	0	6	3
0	1	8	4

Table 10-3. Divider D3 for PLL1

D31 (bit)	D30 (bit)	Decimally	D3 (Block Diagram)
0	0	0	1
0	1	1	2
1	0	2	6
1	1	3	4

10.1 Divider M for Reference Frequency of PLL1

There are several countries like Spain, the Netherlands and Portugal with relatively low modulator frequencies fMod. In case of modulation there will be a big maximum time shift between pulses coming from fractional divider and pulses coming from reference frequency divider. As a consequence the phase comparator enters an undesired operation mode. To avoid entering this operation mode the reference frequency f_{Ref1} has to be reduced by a factor M. Simultaneously, keeping f_{Mod} constant, the factors of fractional dividers have to be changed as well.

The connection between the additional reference frequency divider M and the factors P_M and Q_M of fractional divider is given below. The subscript M denotes which value of M refers to the factors P_M and Q_M of fractional divider. The formulas take into account that the numerator of the fraction $Q_M/223$ must not exceed 223.

 $P_{M} = P_{1} \times M$ + integer (Q × M/223)

 Q_{M} = $Q_{1} \times$ M - 223 \times integer (Q_{1} \times M/223)





10.2 France Base

Table 10-4.Country Setting

Name	RA1[1:0]	RA2[1:0]	D1[1:0]	D20	D3[1:0]	KV2[3:1]	GMOD[1:0]	IMIXI	DR1I[1:0]	FRMT	GDEM
Setting	00	11	11	1	01	100	01 ⁽¹⁾	0	00	0	0
Value	max	min	D1 = 4	D2 = 8	D3 = 2			supra	M = 1	low	high gain

Note: Alternatively, GMOD[1:0] could be set to "00". This reduces the TX conversion gain (MODIN → RFO) from about 3.8 kHz/V to about 2.7 kHz/V, a value, which should be still sufficient for a maximum Δf of -2.5 kHz that is useful in the French case.

Table 10-5. Channel Frequencies and 1st LO Divider, $f_{Ref3} = 6.25$ kHz

Channel Number	TX Channel (MHz)	Rx Channel Frequency (MHz)	f _{LO} = 1/2 f _{VCO3} (MHz)	DV3I[14:0] = N
1	26.3125	41.3125	30.6125	4898
2	26.3250	41.3250	30.6250	4900
3	26.3375	41.3375	30.6375	4902
4	26.3500	41.3500	30.6500	4904
5	26.3625	41.3625	30.6625	4906
6	26.3750	41.3750	30.6750	4908
7	26.3875	41.3875	30.6875	4910
8	26.400	41.4000	30.7000	4912
9	26.4125	41.4125	30.7125	4914
10	26.4250	41.4250	30.7250	4916
11	26.4375	41.4375	30.7375	4918
12	26.4500	41.4500	30.7500	4920
13	26.4625	41.4625	30.7625	4922
14	26.4750	41.4750	30.7750	4924
15	26.4875	41.4875	30.7875	4926

10.2.1 France Modulation Loop Frequency and Divider

 $f_{Mod} = 4.3 \text{ MHz}, P_M = 7, Q_M = 159, M = 1$

10.3 France Hand

Table 10-6.Country Setting

Name	RA1[1:0]	RA2[1:0]	D1[1:0]	D20	D3[1:0]	KV2[3:1]	GMOD[1:0]	IMIXI	DR1I[1:0]	FRMT	GDEM
Setting	00	01	11	1	01	101	01 ⁽¹⁾	1	00	0	0
Value	max		D1 = 4	D2 = 8	D3 = 2			infra	M = 1	low	high gain

Note: Alternatively, GMOD[1:0] could be set to "00". This reduces the TX conversion gain (MODIN -> RFO) from about 3.8 kHz/V to about 2.7 kHz/V, a value, which should be still sufficient for a maximum ∆f of -2.5 kHz that is useful in the French case.

Table 10-7. Channel Frequencies and 1st LO Divider, $f_{Ref3} = 6.25$ kHz

Channel Number	TX Channel Frequency (MHz)	RX Channel Frequency (MHz)	f _{LO} = 1/2 f _{VCO3} (MHz)	DV3I[14:0] = N
1	41.3125	26.3125	37.0125	5922
2	41.3250	26.3250	37.0250	5924
3	41.3375	26.3375	37.0375	5926
4	41.3500	26.3500	37.0500	5928
5	41.3625	26.3625	37.0625	5930
6	41.3750	26.3750	37.0750	5932
7	41.3875	26.3875	37.0875	5934
8	41.4000	26.4000	37.1000	5936
9	41.4125	26.4125	37.1125	5938
10	41.4250	26.4250	37.1250	5940
11	41.4375	26.4375	37.1375	5942
12	41.4500	26.4500	37.1500	5944
13	41.4625	26.4625	37.1625	5946
14	41.4750	26.4750	37.1750	5948
15	41.4875	26.4875	37.1875	5950

10.3.1 France Modulation Loop Frequency and Divider

 $f_{Mod} = 4.3 \text{ MHz}, P_M = 7, Q_M = 159, M = 1$





10.4 Spain Base

Table 10-8. Country Setting

Name	RA1[1:0]	RA2[1:0]	D1[1:0]	D20	D3[1:0]	KV2[3:1]	GMOD[1:0]	IMIXI	DR1I[1:0]	FRMT	GDEM
Setting	10	10	00	1	11	001	10	1	11	1	1
Value			D1 = 2	D2 = 8	D3 = 4			infra	M = 4	high	low gain

Table 10-9. Channel Frequencies and 1st LO Divider, $f_{Ref3} = 6.25 \text{ kHz}$

Channel Number	TX Channel Frequency (MHz)	RX Channel Frequency (MHz)	f _{LO} = 1/2 f _{VCO3} (MHz)	DV3I[14:0] = N
1	31.025	39.925	29.225	4676
2	31.050	39.950	29.250	4680
3	31.075	39.975	29.275	4684
4	31.100	40.000	29.300	4688
5	31.125	40.025	29.325	4692
6	31.150	40.050	29.350	4696
7	31.175	40.075	29.375	4700
8	31.200	40.100	29.400	4704
9	31.250	40.150	29.450	4712
10	31.275	40.175	29.475	4716
11	31.300	40.200	29.500	4720
12	31.325	40.225	29.525	4724

10.4.1 Spain Modulation Loop Frequency and Divider

 $f_{Ref1} = 557.5 \text{ kHz}/4, f_{Mod} = 1.8 \text{ MHz}/4, P_M = 12, Q_M = 204, M = 4$

10.5 Spain Hand

Table 10-10. Country Setting

Name	RA1[1:0]	RA2[1:0]	D1[1:0]	D20	D3[1:0]	KV2[3:1]	GMOD[1:0]	IMIXI	DR1I[1:0]	FRMT	GDEM
Setting	10	01	00	1	11	100	10	0	11	1	1
Value		high	D1 = 2	D2 = 8	D3 = 4		high	supra	M = 4	high	low gain

Table 10-11. Channel Frequencies and 1st LO Divider, $\rm f_{Ref3}$ = 6.25 kHz

Channel Number	TX Channel Frequency (MHz)	RX Channel Frequency (MHz)	$f_{LO} = 1/2 f_{VCO3}$ (MHz)	DV3I[14:0] = N
1	39.925	31.025	41.725	6676
2	39.950	31.050	41.750	6680
3	39.975	31.075	41.775	6684
4	40.000	31.100	41.800	6688
5	40.025	31.125	41.825	6692
6	40.050	31.150	41.850	6696
7	40.075	31.175	41.875	6700
8	40.100	31.200	41.900	6704
9	40.150	31.250	41.950	6712
10	40.175	31.275	41.975	6716
11	40.200	31.300	42.000	6720
12	40.225	31.325	42.025	6724

10.5.1 Spain Modulation Loop Frequency and Divider

 $f_{Ref1} = 557.5 \text{ kHz}/4, f_{Mod} = 1.8 \text{ MHz}/4, P_M = 12, Q_M = 204, M = 4$

